



# DIÁRIO OFICIAL DO ESTADO DE SÃO PAULO

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## PORTARIA Nº 080/25, DE 16 DE JUNHO DE 2025

Processo SEI nº 139.00064959/2024-57

Portaria PR/DER-080/2025

Homologa a Norma Técnica - NT-DE-COO-001- REV-B - conforme especifica. (2.1)

O Presidente do Departamento de Estradas de Rodagem do Estado de São Paulo, em conformidade com os incisos I, III e IX do artigo 33 do Decreto nº 69.322, de 22 de janeiro de 2025, resolve:

Artigo 1º - Fica homologada, de conformidade com o disposto na Portaria SUP/DER-035-01/06/2011, a Norma Técnica de Avaliação de Segurança para a passagem de guindastes de 7 (sete) eixos e 84 (oitenta e quatro) toneladas para 8 (oito) eixos e 96 (noventa e seis) toneladas em Obras de Arte Especiais (OAEs), conforme descrição abaixo:

NT-DE-COO-001- REV-B.

Artigo 2º - A Norma Técnica a que se refere o artigo anterior encontra-se no anexo parte integrante desta portaria

Artigo 3º- Esta portaria entra em vigor na data de sua publicação, ficando revogada a Portaria PR/DER-033/2025.



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## NOTA TÉCNICA

TÍTULO

**AVALIAÇÃO DE SEGURANÇA PARA A PASSAGEM DE GUINDASTES AUTOPROPELIDOS DE 7 E 8 EIXOS (12TF/EIXO) EM OBRAS DE ARTE ESPECIAIS**

ÓRGÃO

**DIRETORIA DE ENGENHARIA**

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DOCUMENTOS DE REFERÊNCIA

DOCUMENTOS RESULTANTES

OBSERVAÇÕES

REVISÃO	DATA	RESP. TÉCNICO	VERIFICAÇÃO	LIBERAÇÃO	APROVAÇÃO
A	Set/2025	José Carlos De M. R. Alves			



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### 1. OBJETIVO

O presente estudo tem como objetivo comparar os esforços gerados pela passagem de um guindaste de 8 eixos e 96 toneladas, calculado com os critérios atuais do trem-tipo TB-45, com os esforços de projeto calculados com os trem-tipos TB-24 e TB-36 em OAEs – Obras de Arte Especial, isto com o intuito de analisar e verificar quais pontes são capazes de suportar a passagem do guindaste.

O TB-24 começou a ser utilizado em 1943 e durou até 1960 (NB6-43), o TB-36 a partir de 1960 até 1984 (NB6-60) e o TB-45 a partir de 1984 até os dias atuais (NBR 7188/24).



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### 2. METODOLOGIA

Foram elaborados 90 modelos para obras calculadas com TB-36 e 24 modelos para o TB-24.

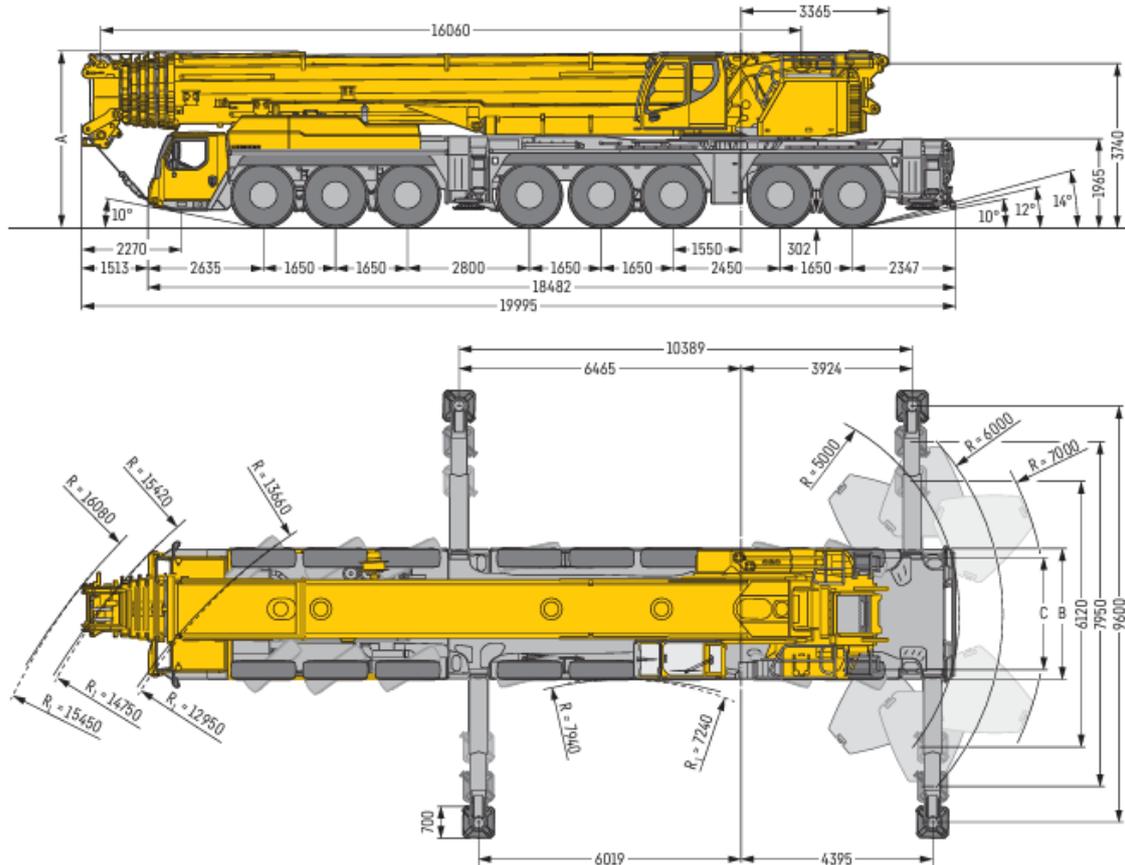
As larguras dos tabuleiros para os modelos TB-36, variam de acordo com os PP's do DER, e assumem valores de 11,20; 12,60; 14,10; 16,10; 16,90 e 19,60 metros, com os comprimentos de 20, 25, 30, 35 e 40 metros. Para cada tabuleiro, três casos foram estudados: cargas permanentes, cargas acidentais TB-36 e cargas acidentais do guindaste.

Já para os tabuleiros do TB-24, as larguras da época eram praticamente padronizadas, por isso foram estudadas larguras de 8,30; 10,00 e 10,30 metros, com os comprimentos de 20, 25, 30 e 35 metros. Para cada tabuleiro, estudamos dois casos: cargas acidentais TB-24 e cargas acidentais de guindaste.



### NOTA TÉCNICA

## 3. DESCRIÇÃO DO GUINDASTE



**Maße** • Dimensions • Encombrement • Dimensioni • Dimensiones • Размеры mm

	A	A	B	C
385/95 R 25 (14.00 R 25)	4000	3850	3000	2610
445/95 R 25 (16.00 R 25)	4000	3900	3000	2550
525/80 R 25 (20.5 R 25)	4000	3900	3100	2570

\* **abgesenkt** - lowered - abaissé - abbassato - suspensión abajo - шасси осажено

As medidas das imagens acima foram utilizadas para o cálculo do estudo.

O primeiro passo foi realizar a homogeneização do guindaste, o seus eixos precisam ser aliviados proporcionalmente pela área de influência do eixo com a carga de multidão de 0,50 tf/m<sup>2</sup>.



## NOTA TÉCNICA

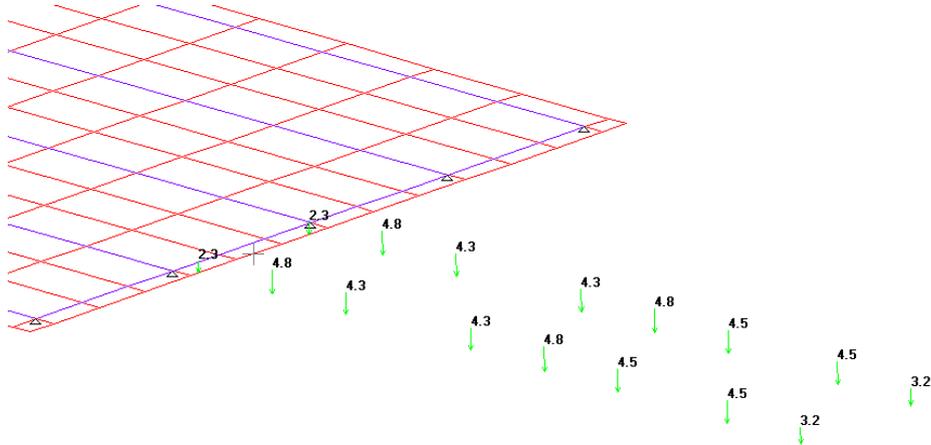
Segue abaixo a tabela utilizada para o cálculo da homogenização:

EIXOS	DISTÂNCIAS (m)	DIST. INFL (m)	LARG (m)	ÁREA DE INFL. (m <sup>2</sup> )	MULTIDÃO (tf/m <sup>2</sup> )	ALÍVIO EIXO (tf)	CARGA EIXO (tf)	COM ALÍVIO (tf)	RODA COM ALÍVIO (tf)
0	4,15	-	-	-	-	-	-	-	-
1	1,65	4,97	3,00	14,92	0,50	7,46	12,00	4,54	2,27
2	1,65	1,65	3,00	4,95	0,50	2,48	12,00	9,53	4,76
3	2,80	2,23	3,00	6,68	0,50	3,34	12,00	8,66	4,33
4	1,65	2,23	3,00	6,68	0,50	3,34	12,00	8,66	4,33
5	1,65	1,65	3,00	4,95	0,50	2,48	12,00	9,53	4,76
6	2,40	2,03	3,00	6,09	0,50	3,05	12,00	8,96	4,48
7	1,65	2,03	3,00	6,09	0,50	3,05	12,00	8,96	4,48
8	2,85	3,67	3,00	11,02	0,50	5,51	12,00	6,49	3,25

- **Eixos:** Listagem da quantidade de eixos.
- **Distâncias (m):** Informa a distância que há de um eixo para o outro.
- **Distância de influência (m):** Representa a distância entre os pontos de apoio do guindaste.
- **Largura (m):** A largura sobre a qual a carga está sendo aplicada.
- **Área de influência (m<sup>2</sup>):** É o produto da distância de influência pela largura.
- **Multidão (tf/m<sup>2</sup>):** Representa a carga distribuída por metro quadrado.
- **Alívio eixo (tf):** É o total de carga que está sendo aliviada pelo guindaste sobre o eixo específico.
- **Carga eixo (tf):** Representa a carga total teórica que seria suportada pelo eixo sem considerar qualquer alívio. Para todos os eixos é constante, aqui indicado como 12,00 tfeladas.
- **Com alívio (tf):** É a carga real no eixo após o alívio ser aplicado.
- **Roda com alívio (tf):** O guindaste tem duas rodas por eixo, então a carga é dividida igualmente entre as duas rodas.



## NOTA TÉCNICA



### LTM1500-C-HOAlpu

CONC -2.27 C 0.00 1.305  
CONC -2.27 C 0.00 -1.305  
CONC -4.76 C 1.65 1.305  
CONC -4.76 C 1.65 -1.305  
CONC -4.33 C 3.30 1.305  
CONC -4.33 C 3.30 -1.305  
CONC -4.33 C 6.10 1.305  
CONC -4.33 C 6.10 -1.305  
CONC -4.76 C 7.75 1.305  
CONC -4.76 C 7.75 -1.305  
CONC -4.48 C 9.40 1.305  
CONC -4.48 C 9.40 -1.305  
CONC -4.48 C 11.85 1.305  
CONC -4.48 C 11.85 -1.305  
CONC -3.25 C 13.50 1.305  
CONC -3.25 C 13.50 -1.305



## NOTA TÉCNICA

### 4. DESENVOLVIMENTO: TB-36

#### 4.1. Introdução

A partir dos Projetos Padrão (PPs) do DER, foram desenvolvidos os 90 modelos estruturais listados abaixo, permitindo a obtenção dos momentos de inércia reais das vigas longarinas.

tabuleiro 11,20 - 20,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 11,20 - 20,00 m - permanentes
tabuleiro 11,20 - 20,00 m - TB-36
tabuleiro 11,20 - 25,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 11,20 - 25,00 m - permanentes
tabuleiro 11,20 - 25,00 m - TB-36
tabuleiro 11,20 - 30,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 11,20 - 30,00 m - permanentes
tabuleiro 11,20 - 30,00 m - TB-36
tabuleiro 11,20 - 35,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 11,20 - 35,00 m - permanentes
tabuleiro 11,20 - 35,00 m - TB-36
tabuleiro 11,20 - 40,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 11,20 - 40,00 m - permanentes
tabuleiro 11,20 - 40,00 m - TB-36

tabuleiro 12,60 - 20,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 12,60 - 20,00 m - permanentes
tabuleiro 12,60 - 20,00 m - TB-36
tabuleiro 12,60 - 25,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 12,60 - 25,00 m - permanentes
tabuleiro 12,60 - 25,00 m - TB-36
tabuleiro 12,60 - 30,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 12,60 - 30,00 m - permanentes
tabuleiro 12,60 - 30,00 m - TB-36
tabuleiro 12,60 - 35,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 12,60 - 35,00 m - permanentes
tabuleiro 12,60 - 35,00 m - TB-36
tabuleiro 12,60 - 40,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 12,60 - 40,00 m - permanentes
tabuleiro 12,60 - 40,00 m - TB-36

tabuleiro 16,10 - 20,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 16,10 - 20,00 m - permanentes
tabuleiro 16,10 - 20,00 m - TB-36
tabuleiro 16,10 - 25,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 16,10 - 25,00 m - permanentes
tabuleiro 16,10 - 25,00 m - TB-36
tabuleiro 16,10 - 30,00 m - Leibherr LTM 1500 HOMO A.INFL.
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tabuleiro 16,10 - 40,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 16,10 - 40,00 m - permanentes
tabuleiro 16,10 - 40,00 m - TB-36

tabuleiro 14,10 - 20,00 m - Leibherr LTM 1500 HOMO A.INFL.
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tabuleiro 14,10 - 40,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 14,10 - 40,00 m - permanentes
tabuleiro 14,10 - 40,00 m - TB-36

tabuleiro 16,90 - 20,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 16,90 - 20,00 m - permanentes
tabuleiro 16,90 - 20,00 m - TB-36
tabuleiro 16,90 - 25,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 16,90 - 25,00 m - permanentes
tabuleiro 16,90 - 25,00 m - TB-36
tabuleiro 16,90 - 30,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 16,90 - 30,00 m - permanentes
tabuleiro 16,90 - 30,00 m - TB-36
tabuleiro 16,90 - 35,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 16,90 - 35,00 m - permanentes
tabuleiro 16,90 - 35,00 m - TB-36
tabuleiro 16,90 - 40,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 16,90 - 40,00 m - permanentes
tabuleiro 16,90 - 40,00 m - TB-36

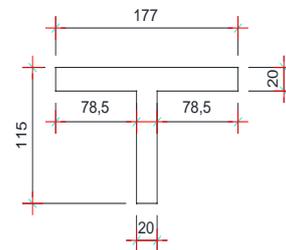
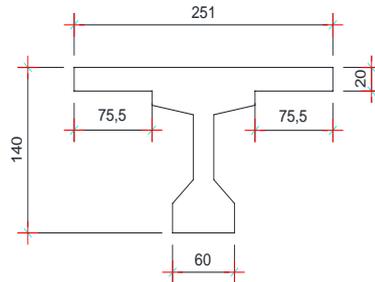
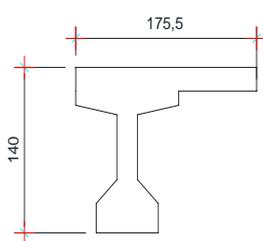
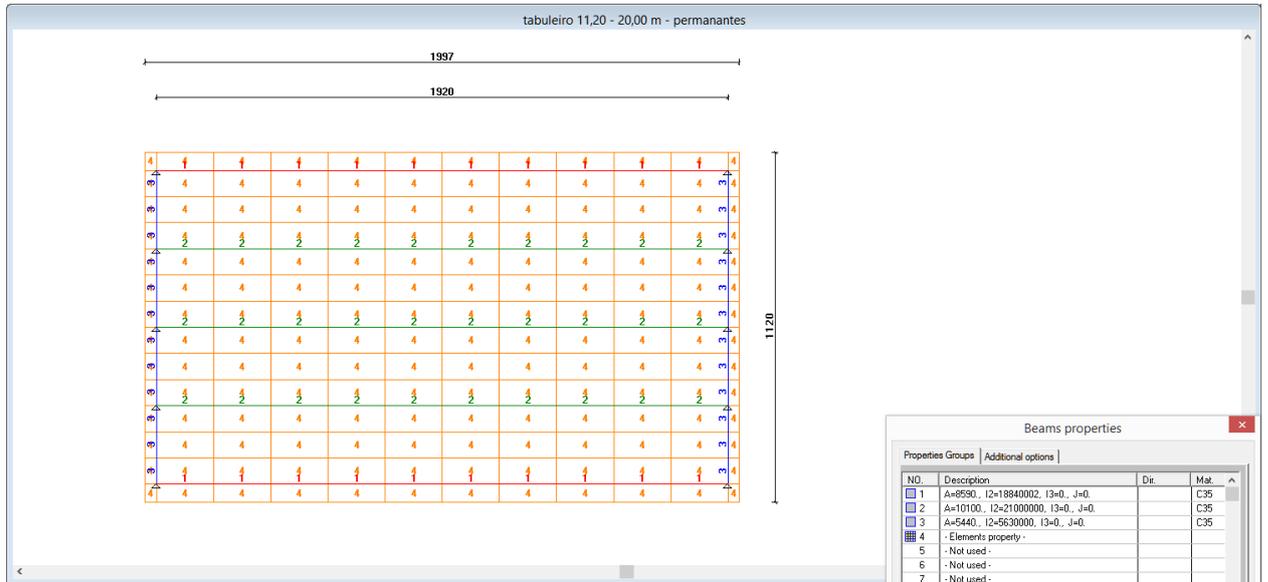
tabuleiro 19,60 - 20,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 19,60 - 20,00 m - permanentes
tabuleiro 19,60 - 20,00 m - TB-36
tabuleiro 19,60 - 25,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 19,60 - 25,00 m - permanentes
tabuleiro 19,60 - 25,00 m - TB-36
tabuleiro 19,60 - 30,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 19,60 - 30,00 m - permanentes
tabuleiro 19,60 - 30,00 m - TB-36
tabuleiro 19,60 - 35,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 19,60 - 35,00 m - permanentes
tabuleiro 19,60 - 35,00 m - TB-36
tabuleiro 19,60 - 40,00 m - Leibherr LTM 1500 HOMO A.INFL.
tabuleiro 19,60 - 40,00 m - permanentes
tabuleiro 19,60 - 40,00 m - TB-36



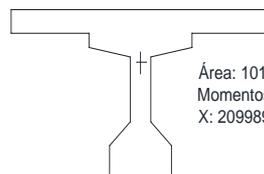
## NOTA TÉCNICA

### 4.2. Momento de inércia e geometria

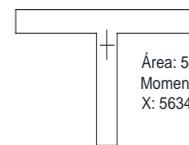
#### 4.2.1. Tabuleiro 11,20 m



Área: 8590.00 cm<sup>2</sup> = 0,8590 m<sup>2</sup>  
Momentos de inércia:  
X: 18839843.27 cm<sup>4</sup> = 0,1884 m<sup>4</sup>



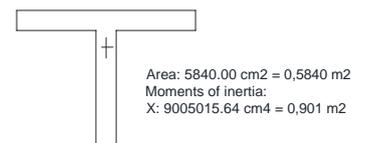
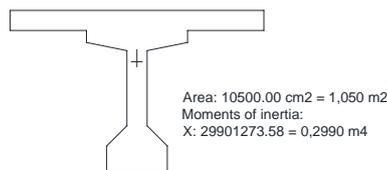
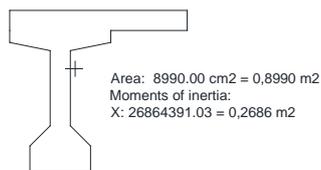
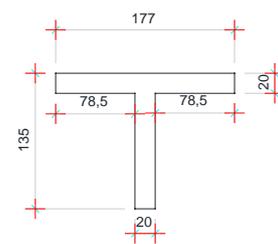
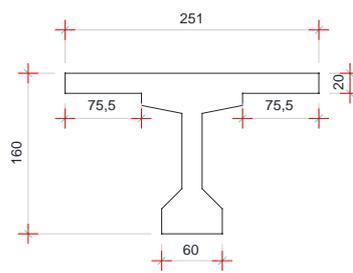
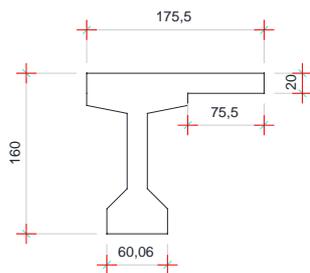
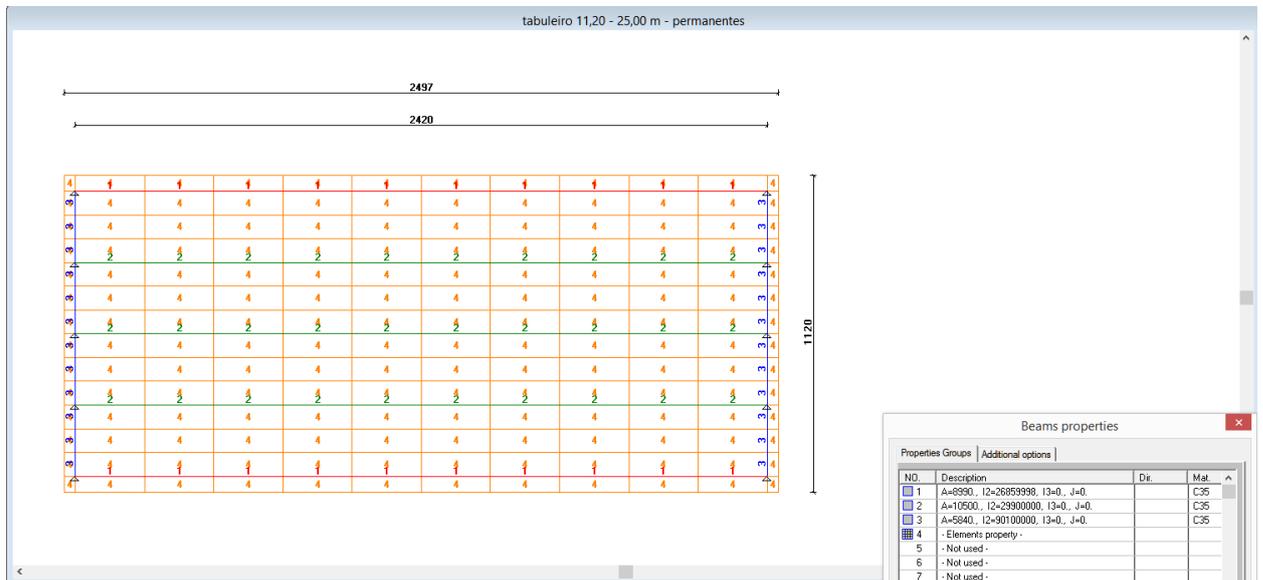
Área: 10100.00 cm<sup>2</sup> = 1,0100 m<sup>2</sup>  
Momentos de inércia:  
X: 20998985.43 cm<sup>4</sup> = 0,2100 m<sup>4</sup>



Área: 5440.00 cm<sup>2</sup> = 0,5440 m<sup>2</sup>  
Momentos de inércia:  
X: 5634796.15 cm<sup>4</sup> = 0,0563 m<sup>4</sup>

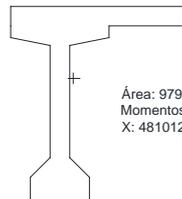
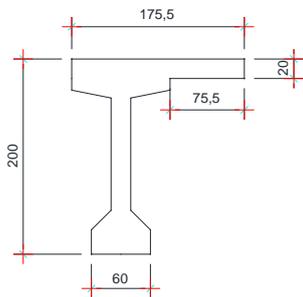
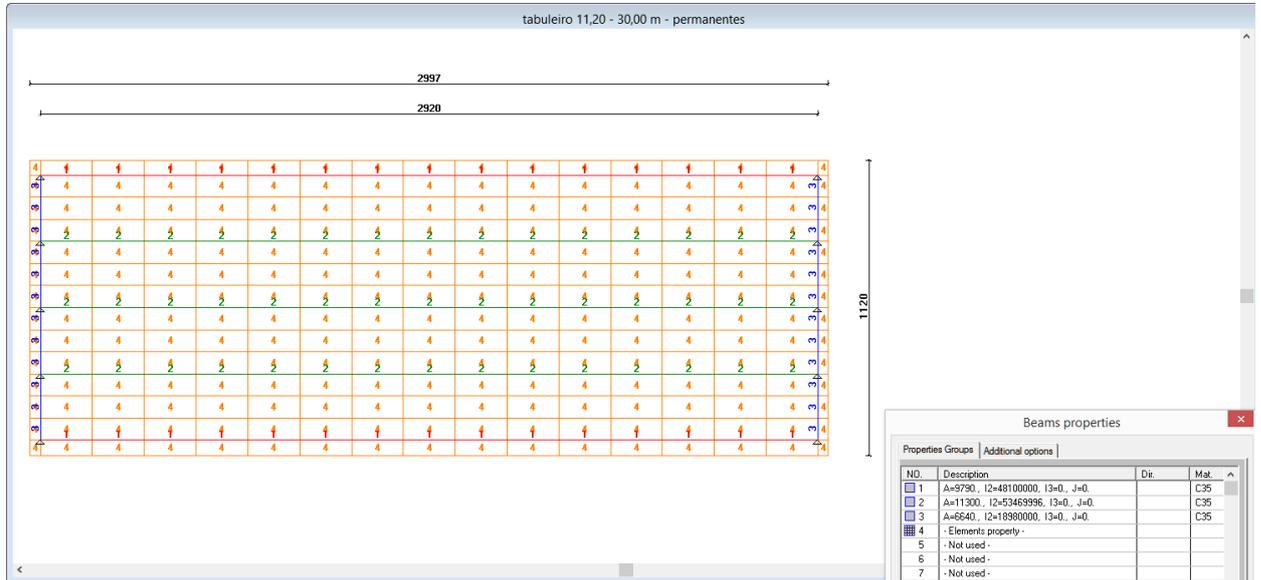


### NOTA TÉCNICA

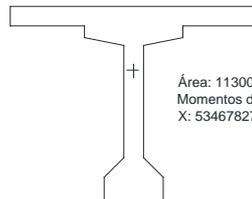
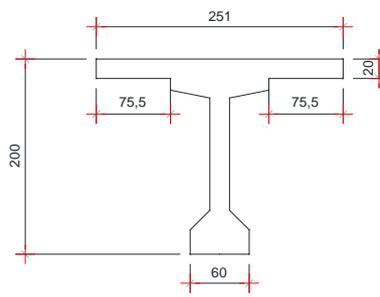




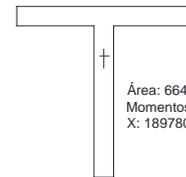
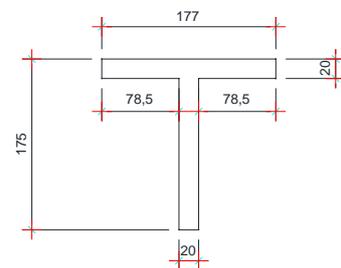
### NOTA TÉCNICA



Área: 9790.00 cm<sup>2</sup> = 0,9790 m<sup>2</sup>  
Momentos de inércia:  
X: 48101241.87 cm<sup>4</sup> = 0,4810 m<sup>4</sup>



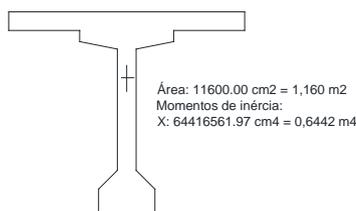
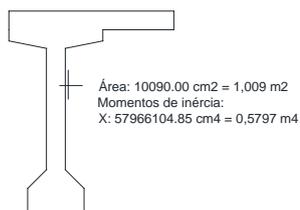
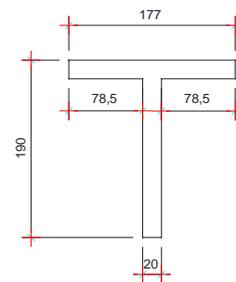
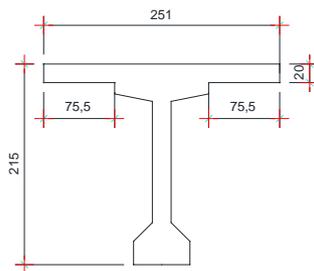
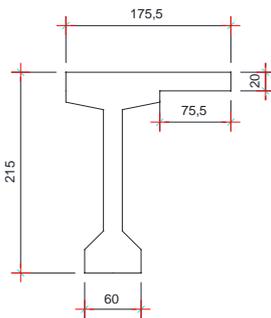
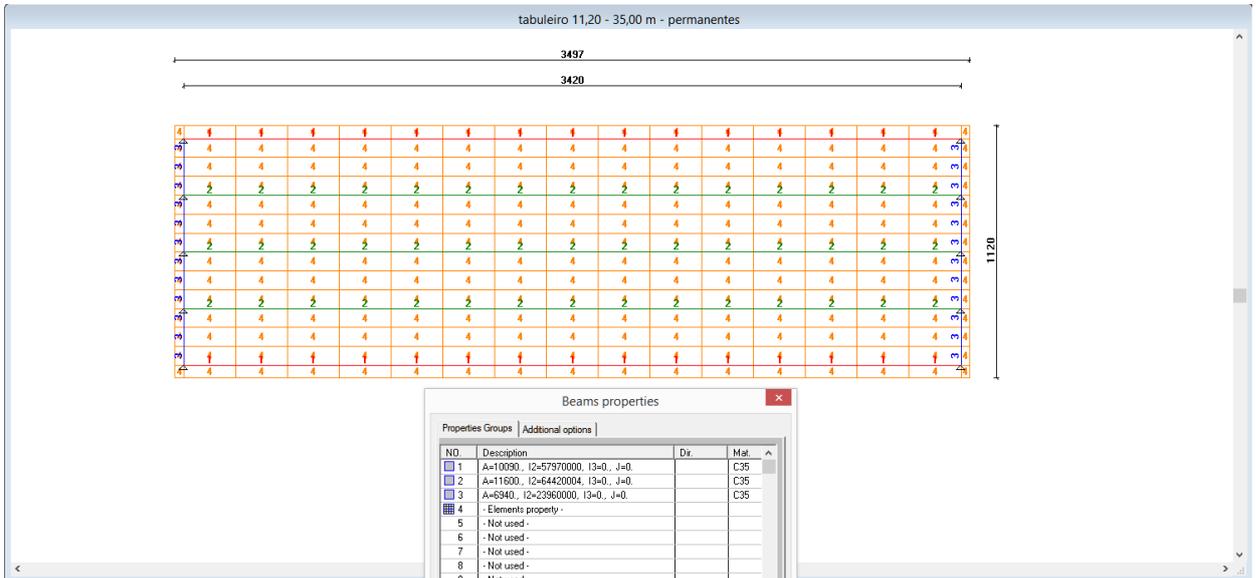
Área: 11300.00 cm<sup>2</sup> = 1,130 m<sup>2</sup>  
Momentos de inércia:  
X: 53467827.90 cm<sup>4</sup> = 0,5347 m<sup>4</sup>



Área: 6640.00 cm<sup>2</sup> = 0,6640 m<sup>2</sup>  
Momentos de inércia:  
X: 18978025.73 cm<sup>4</sup> = 0,1898 m<sup>4</sup>

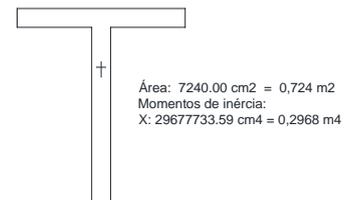
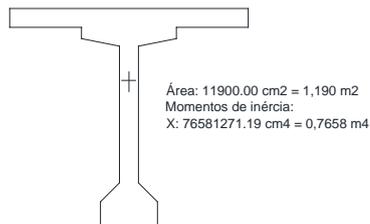
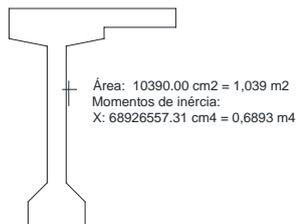
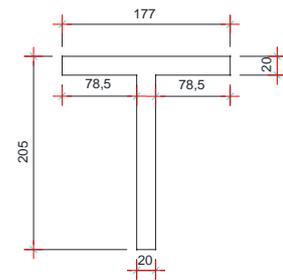
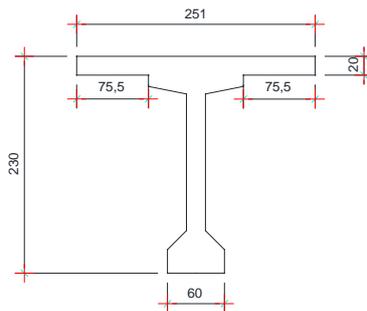
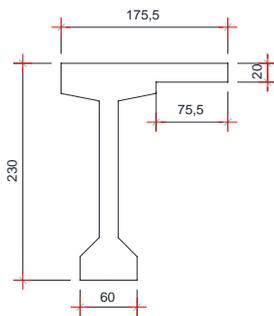
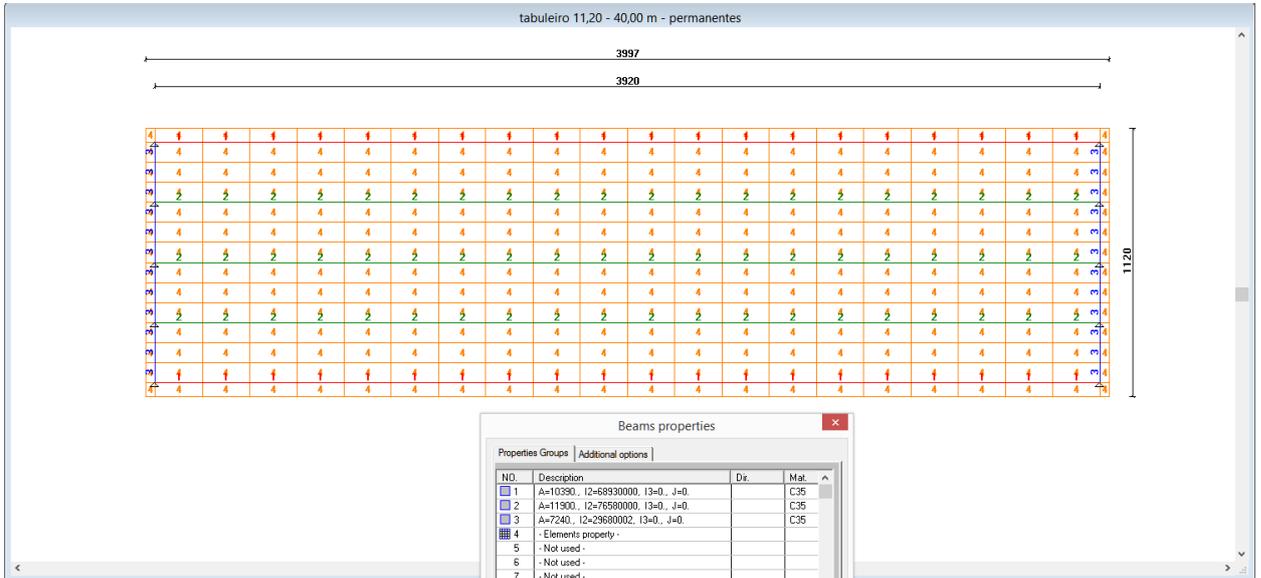


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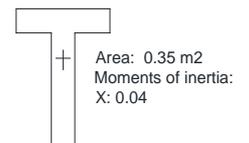
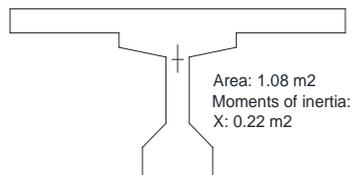
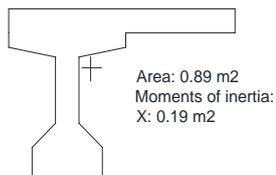
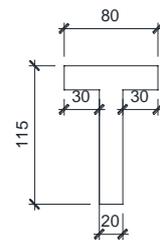
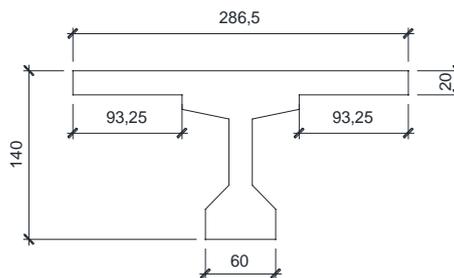
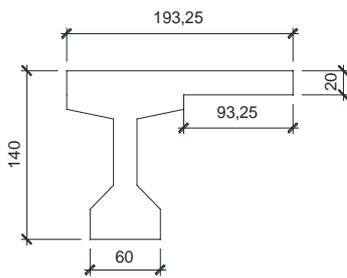
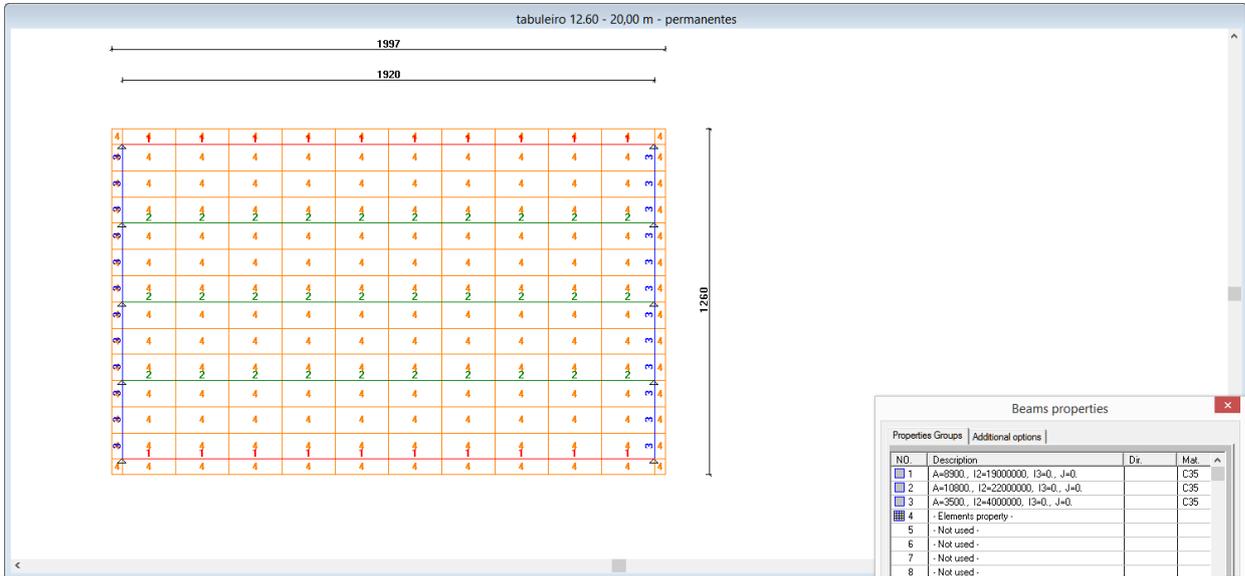
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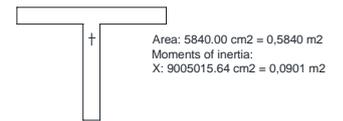
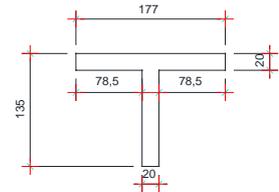
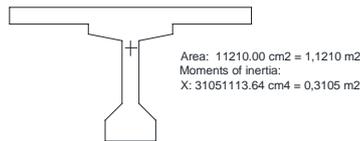
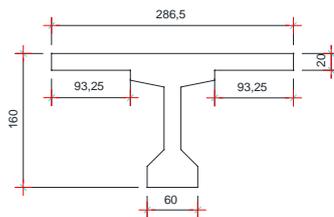
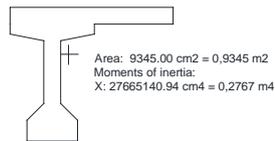
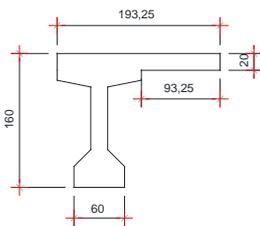
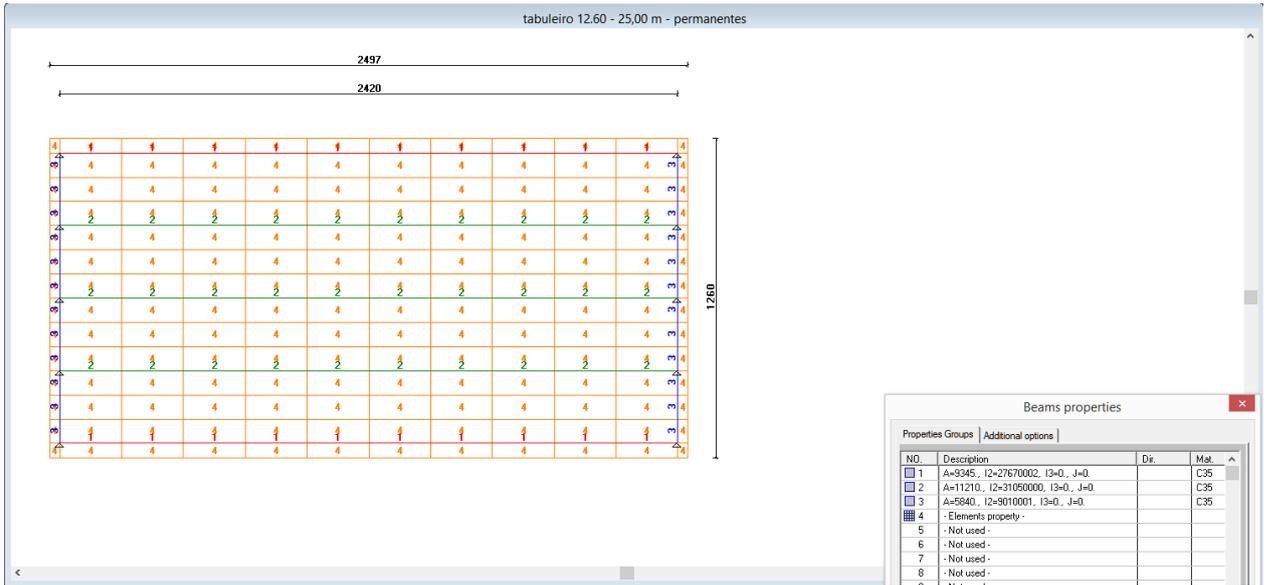
### NOTA TÉCNICA

#### 4.2.2. Tabuleiro 12,60 m



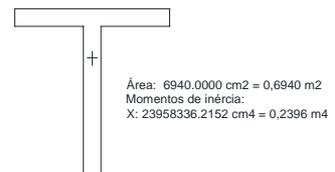
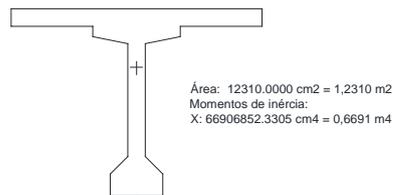
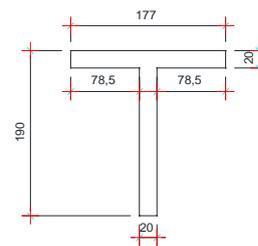
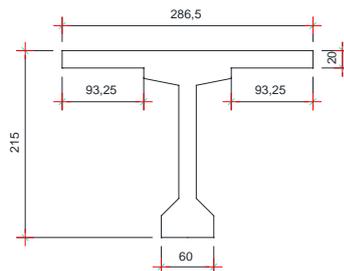
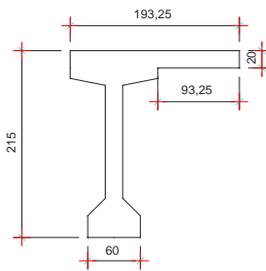
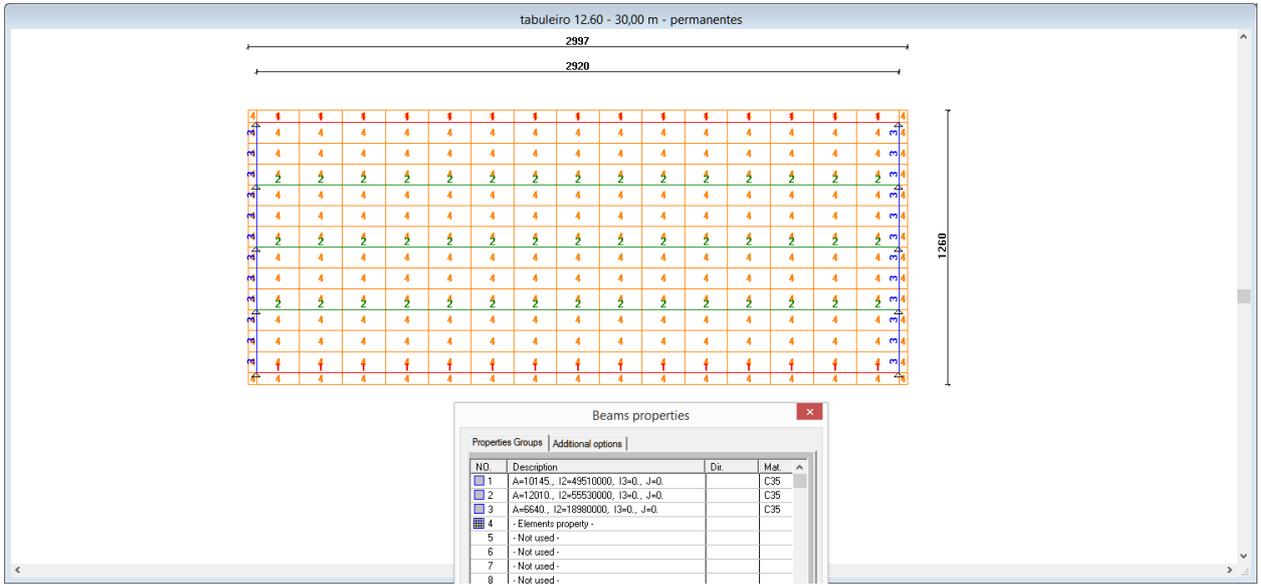


### NOTA TÉCNICA



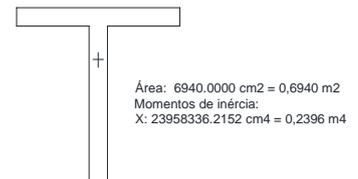
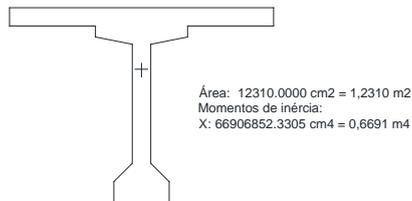
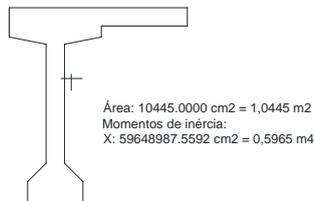
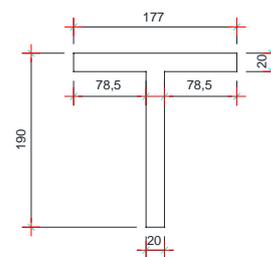
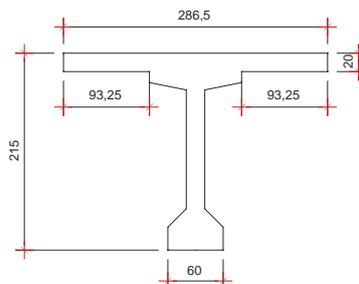
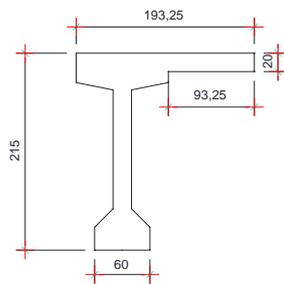
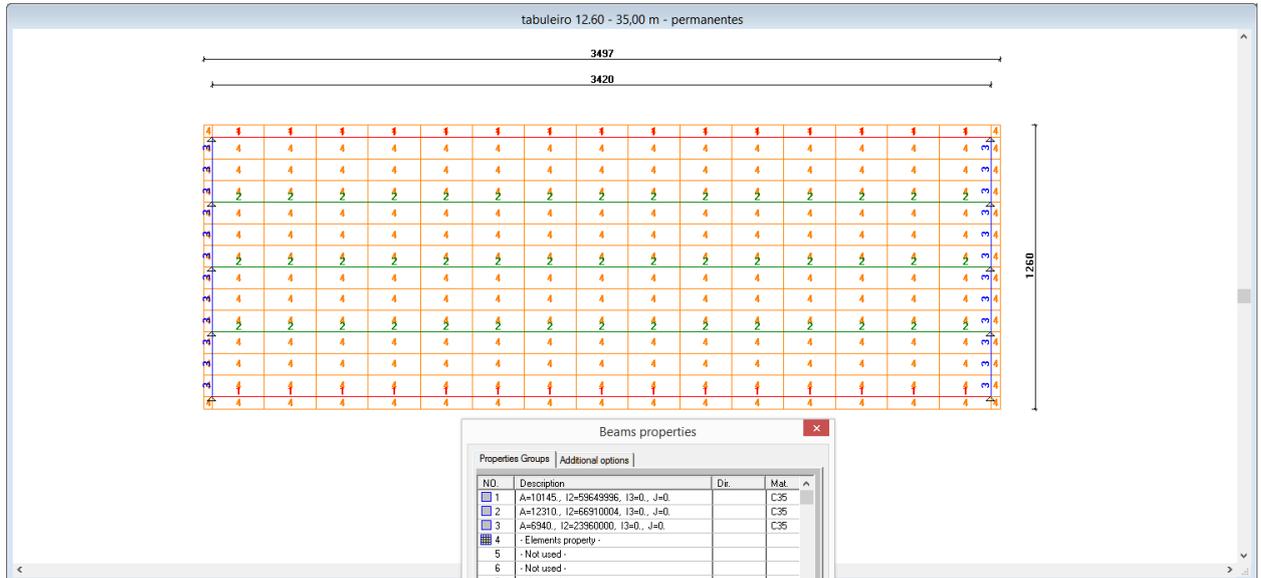


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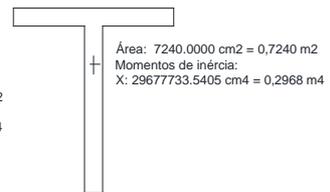
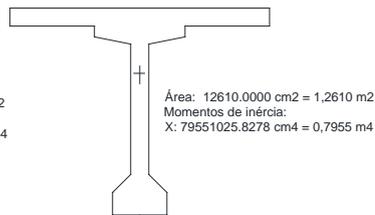
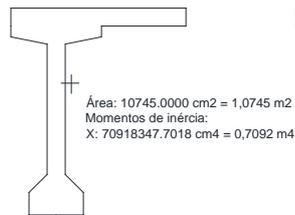
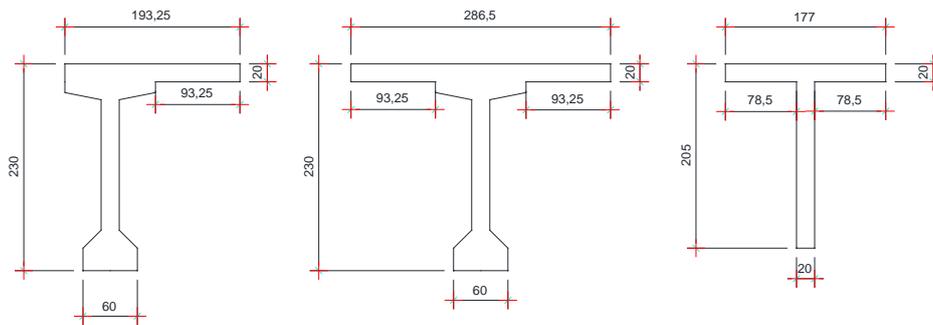
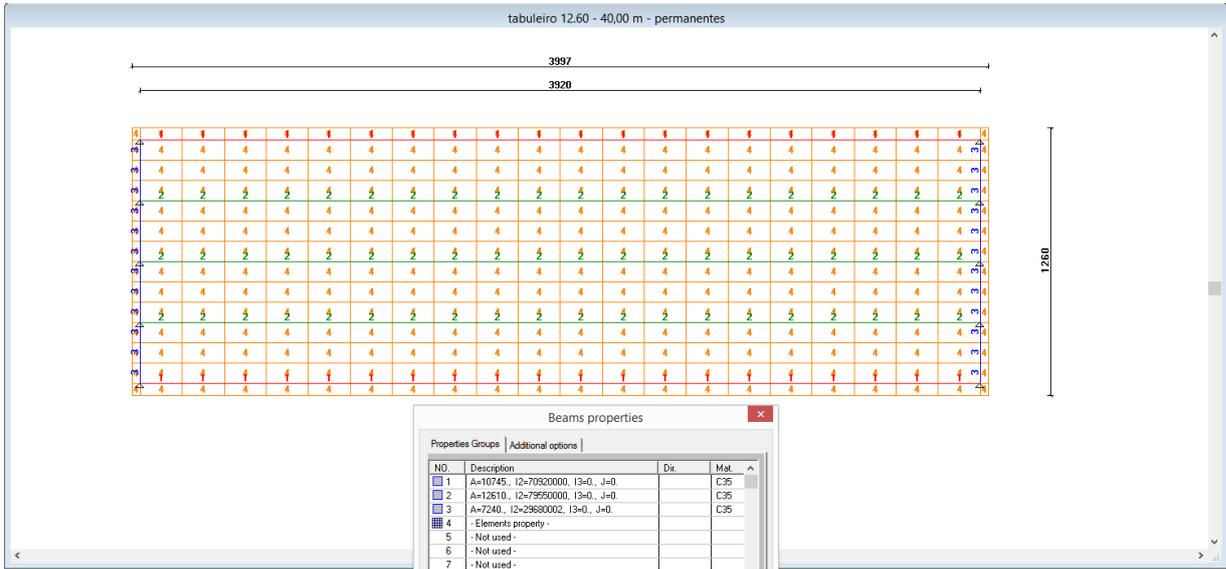


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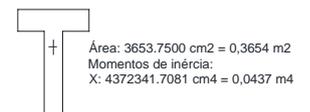
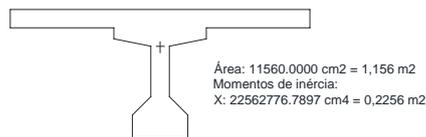
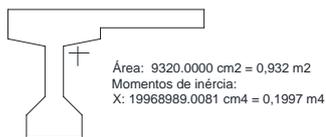
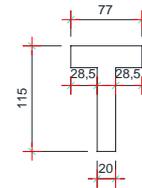
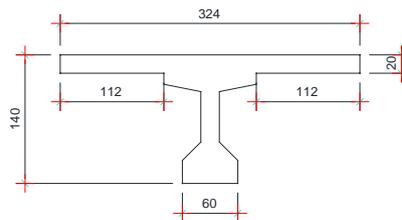
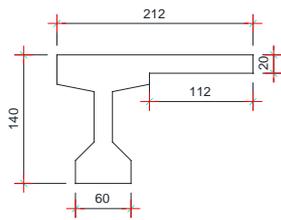
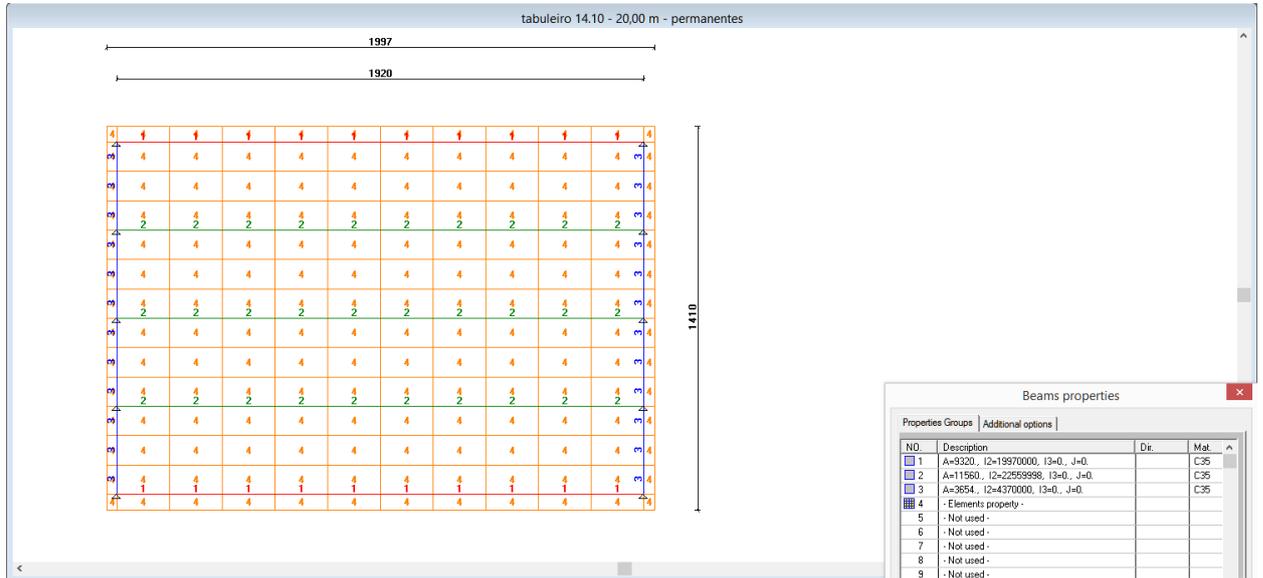
### NOTA TÉCNICA





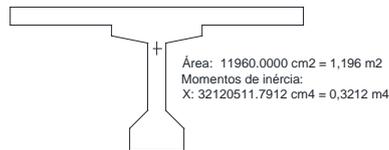
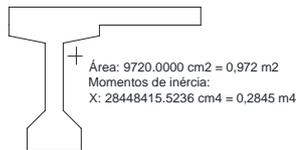
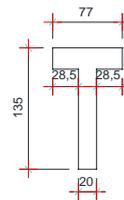
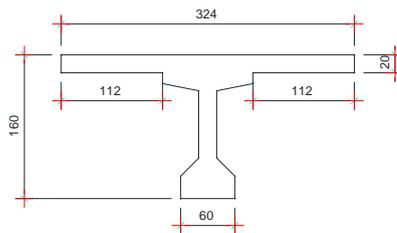
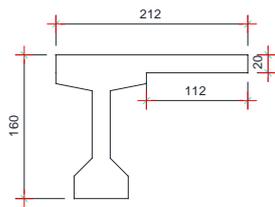
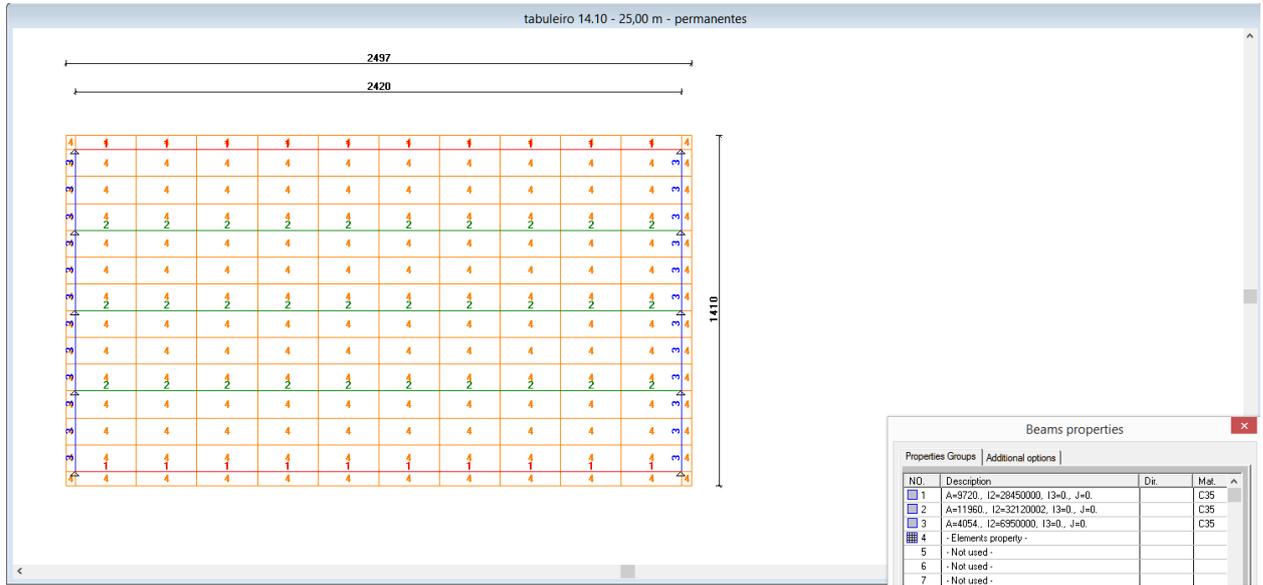
### NOTA TÉCNICA

#### 4.2.3. Tabuleiro 14,10 m



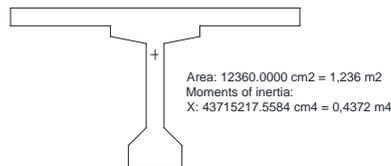
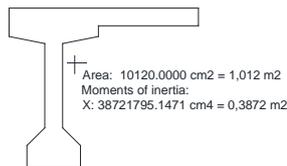
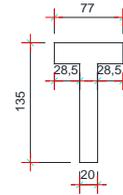
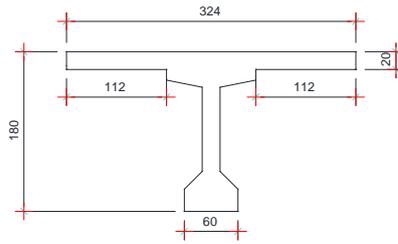
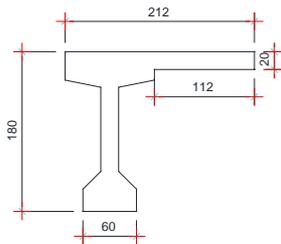
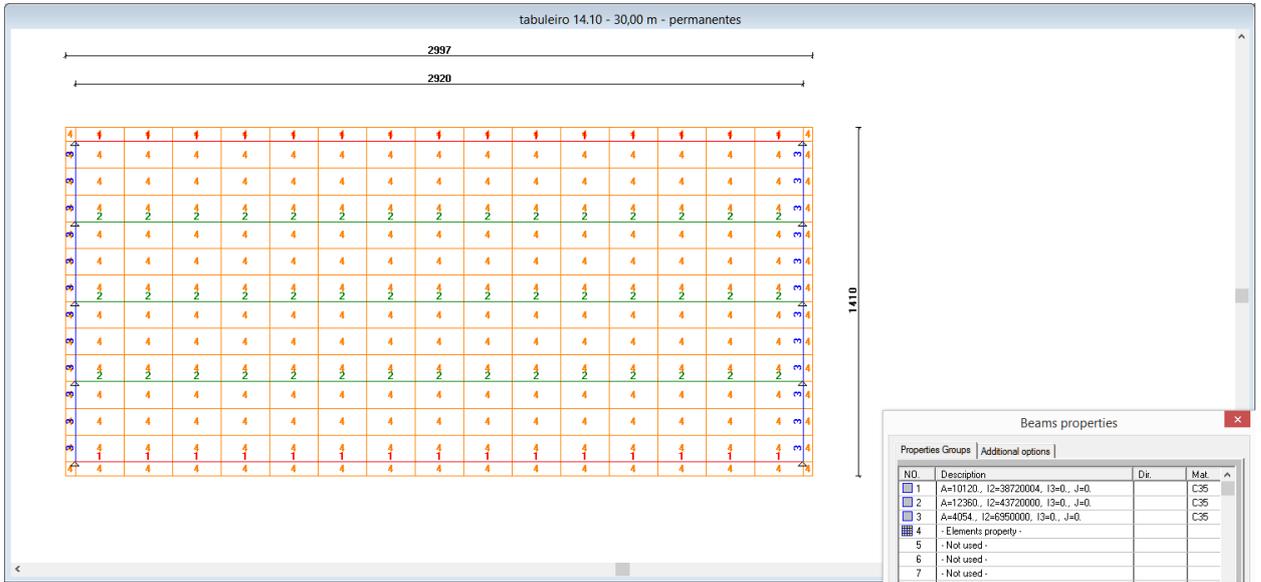


### NOTA TÉCNICA



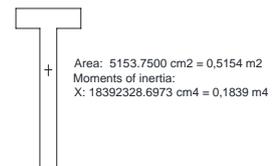
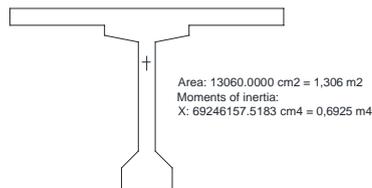
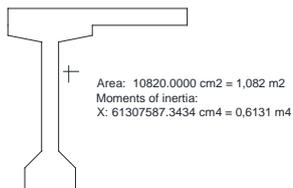
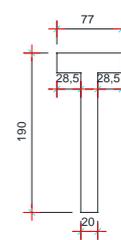
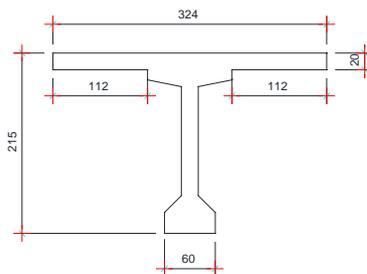
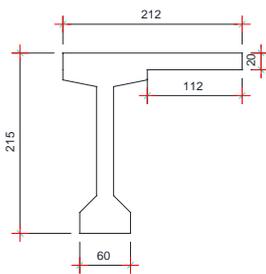
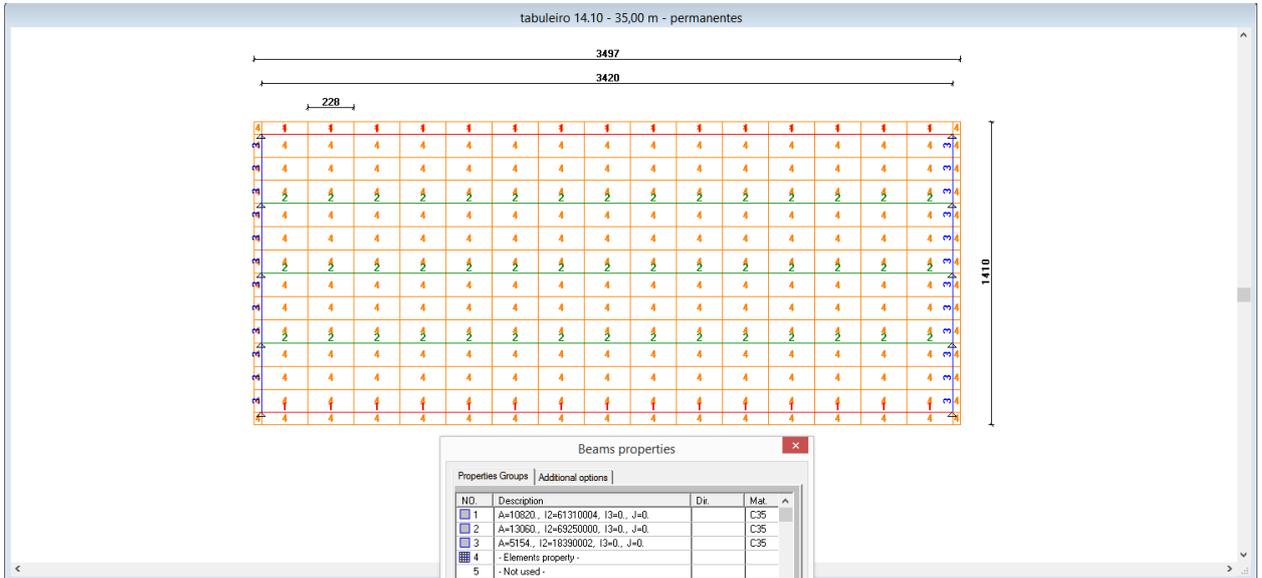


### NOTA TÉCNICA



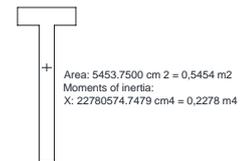
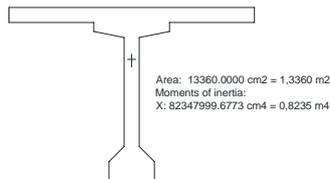
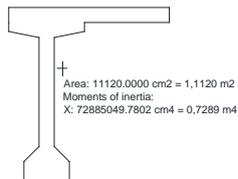
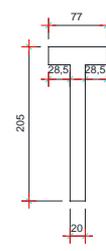
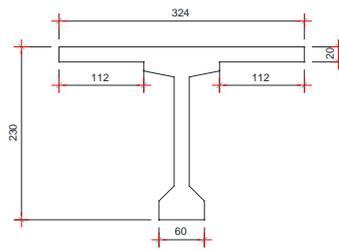
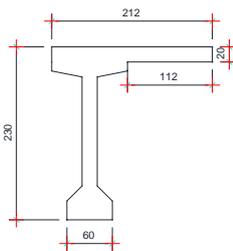
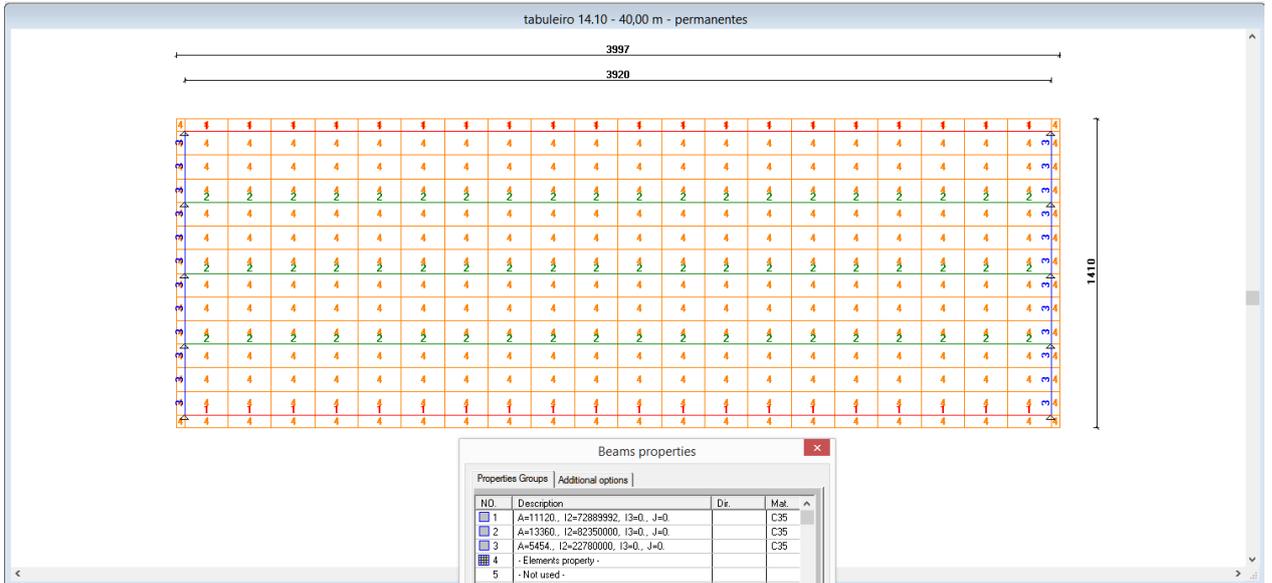


### NOTA TÉCNICA





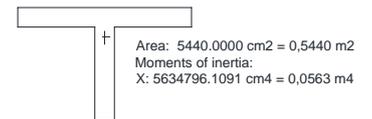
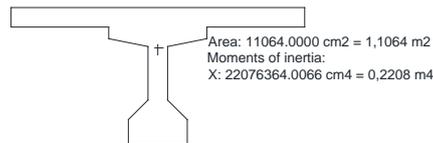
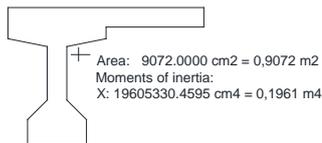
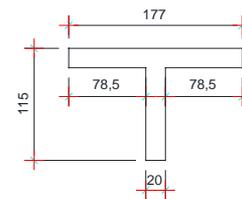
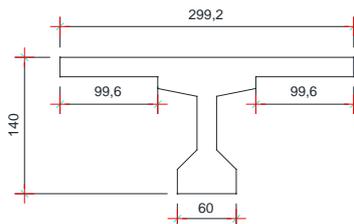
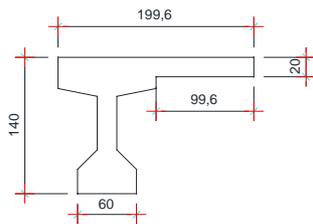
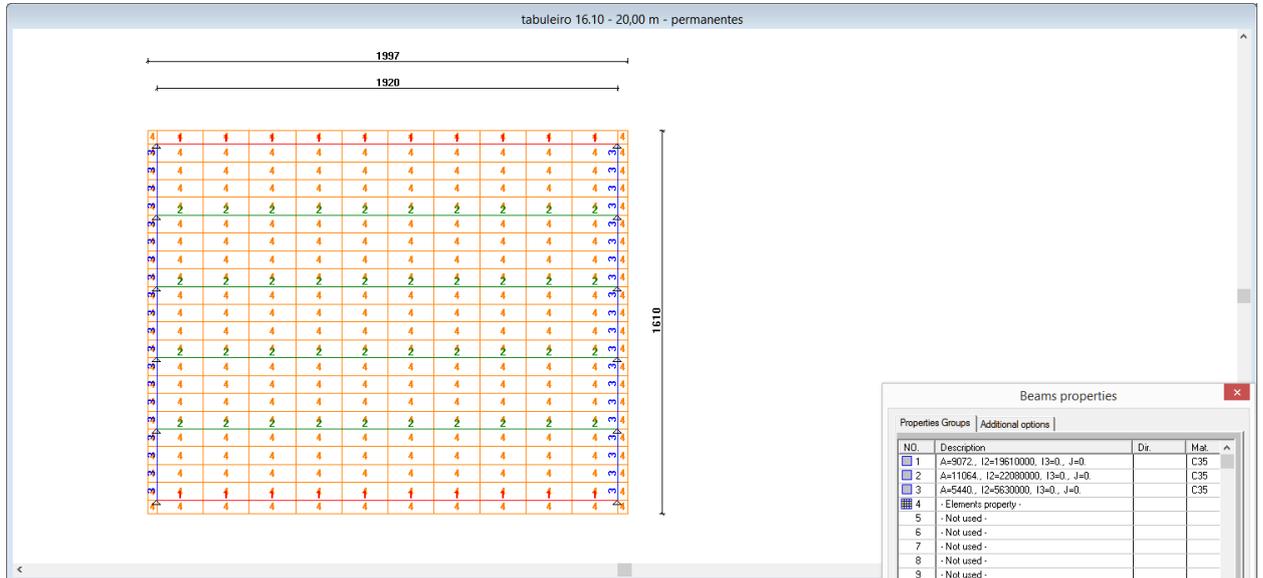
### NOTA TÉCNICA





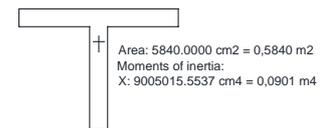
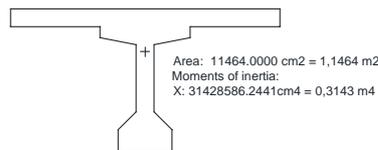
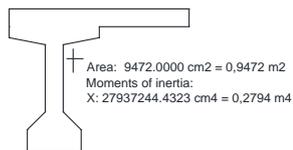
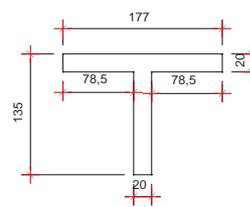
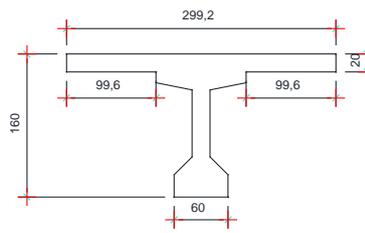
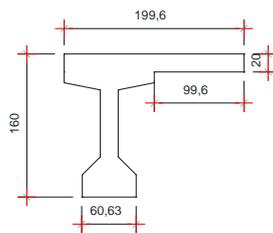
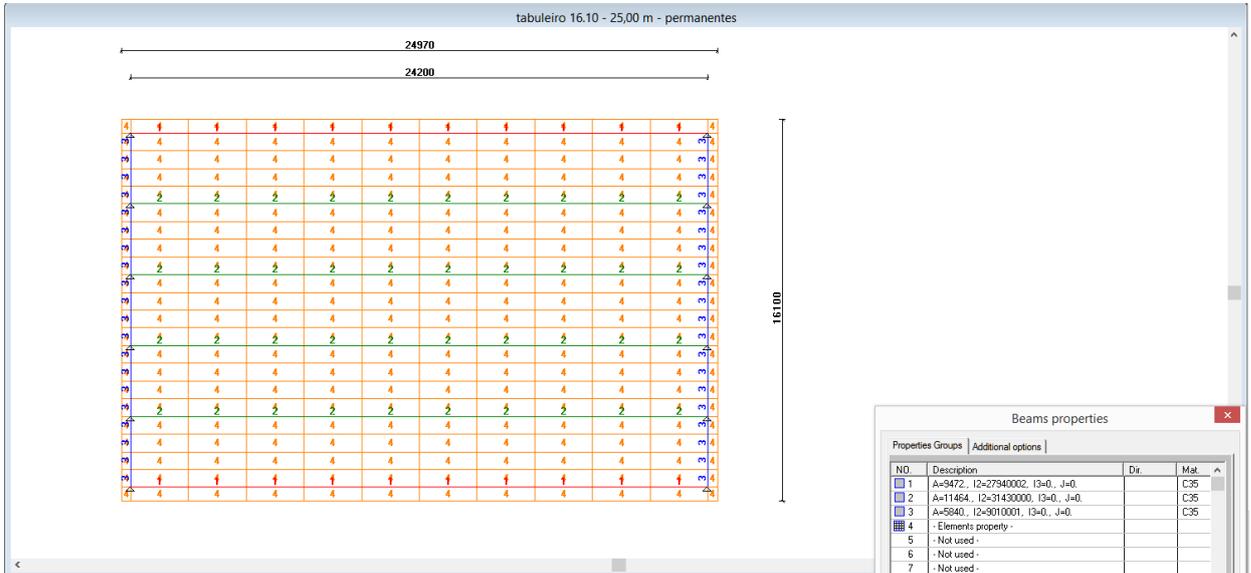
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#### 4.2.4. Tabuleiro 16,10 m



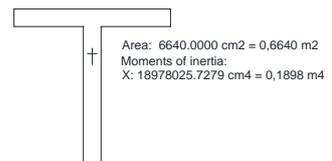
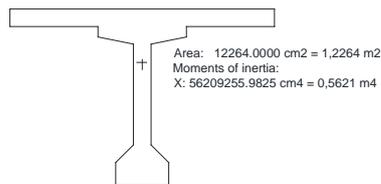
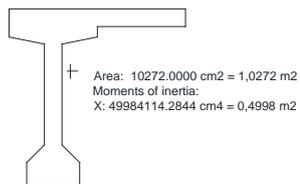
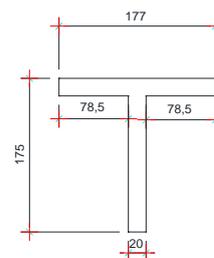
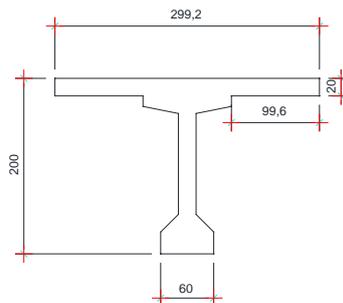
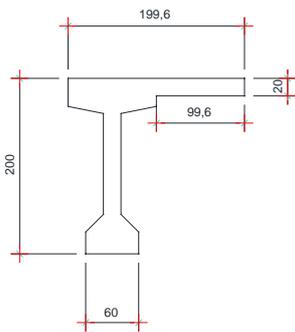
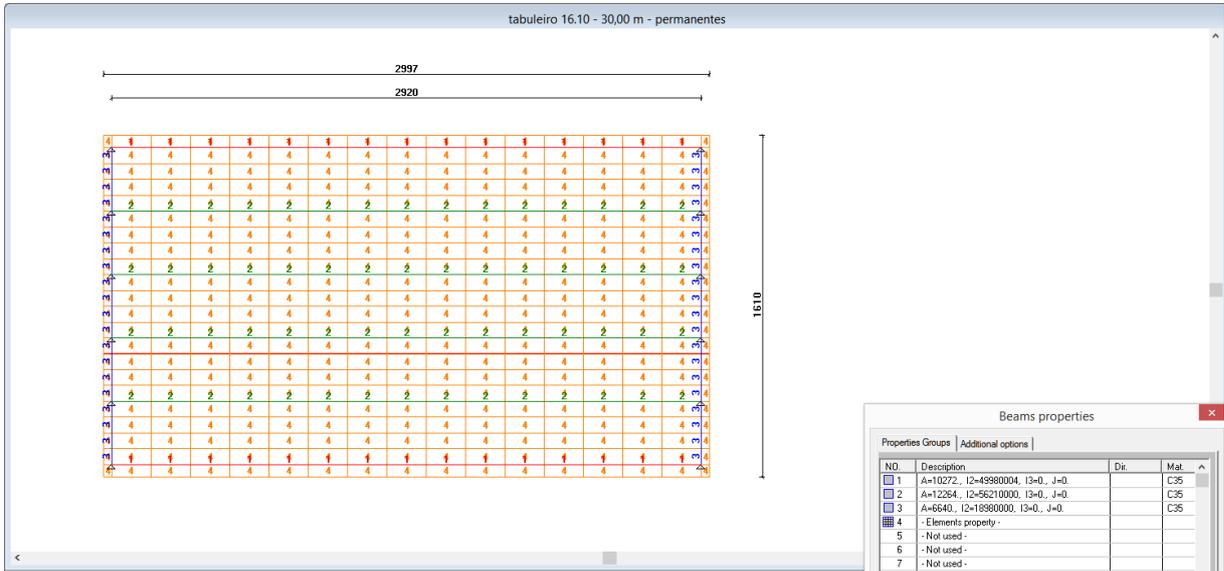


### NOTA TÉCNICA



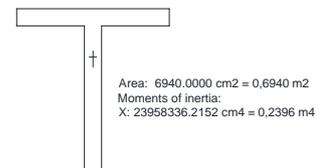
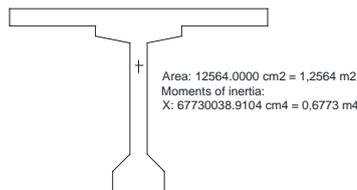
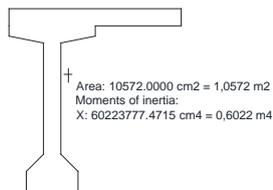
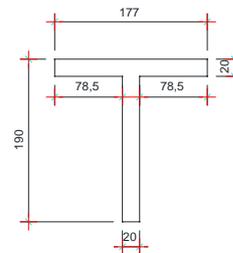
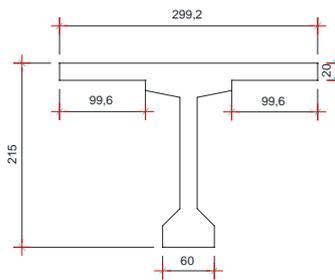
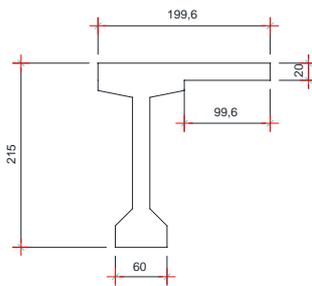
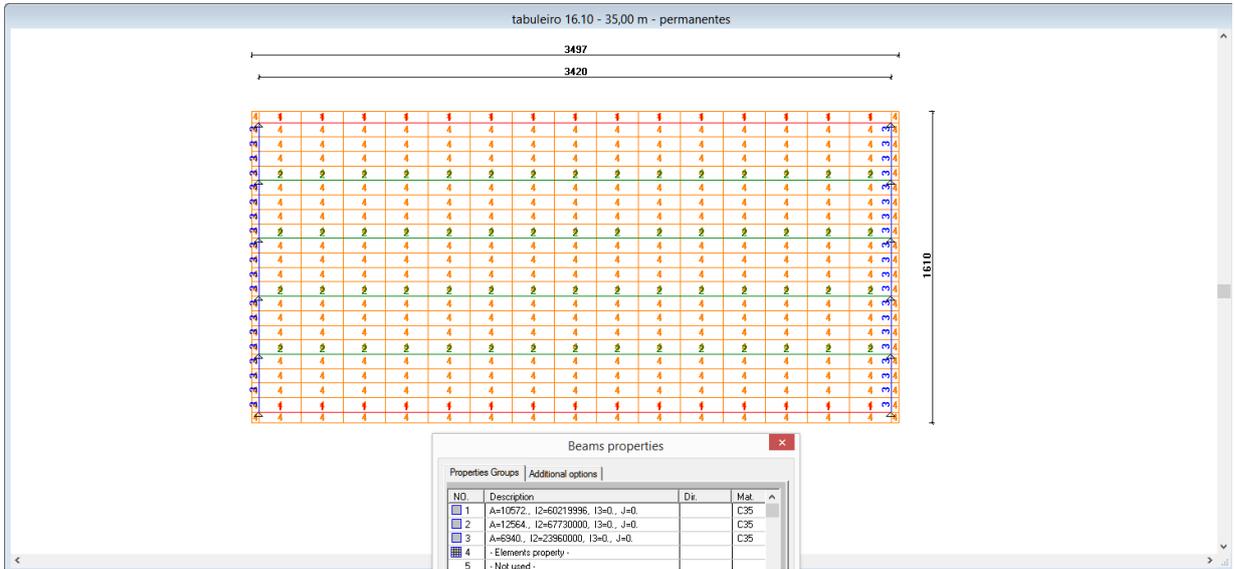


### NOTA TÉCNICA



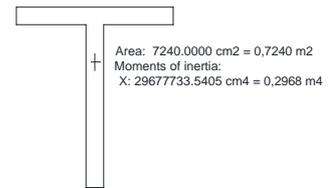
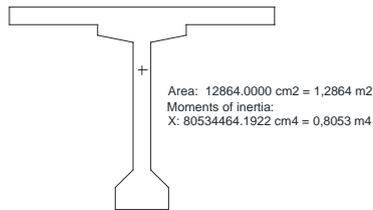
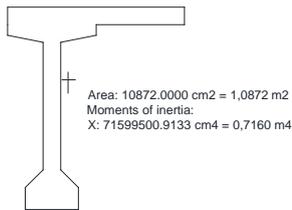
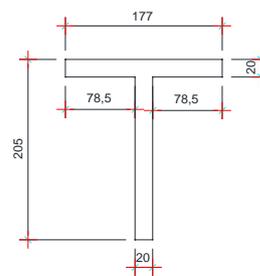
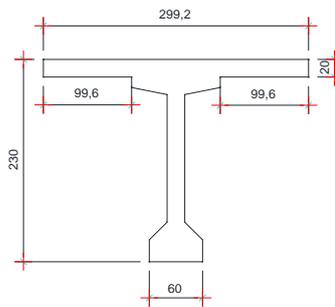
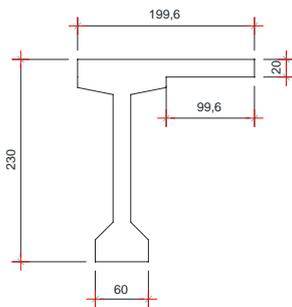
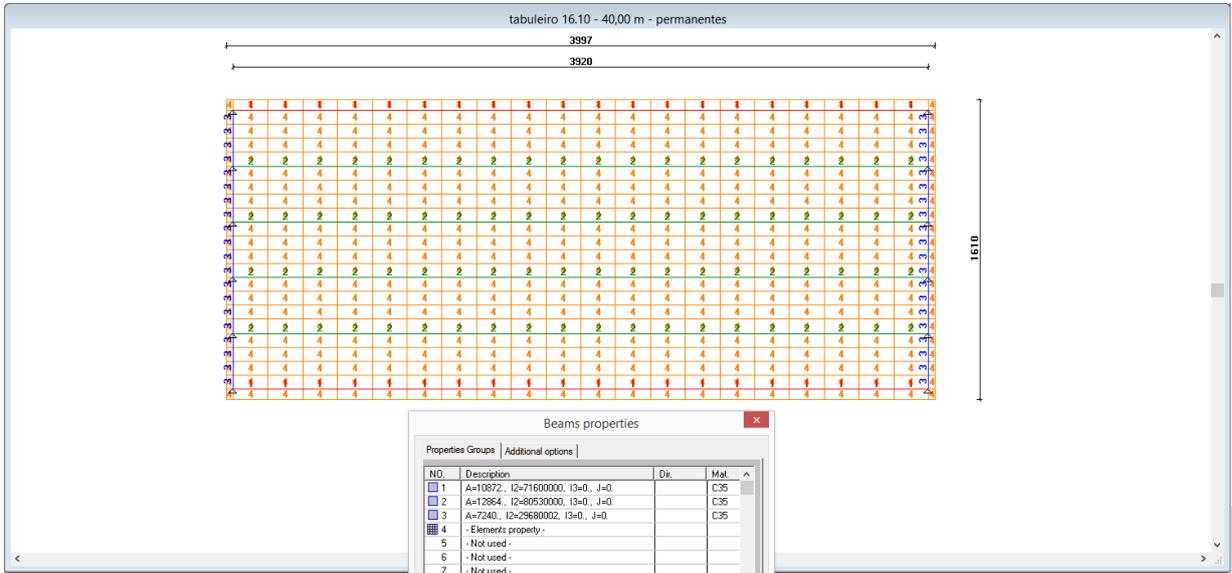


### NOTA TÉCNICA





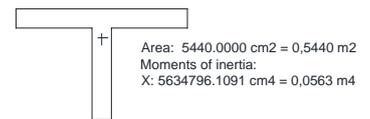
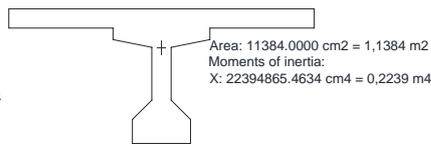
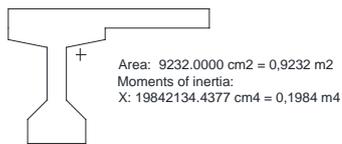
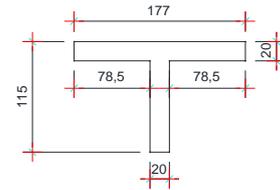
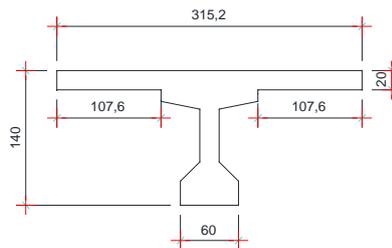
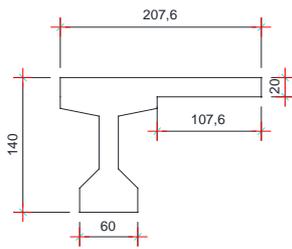
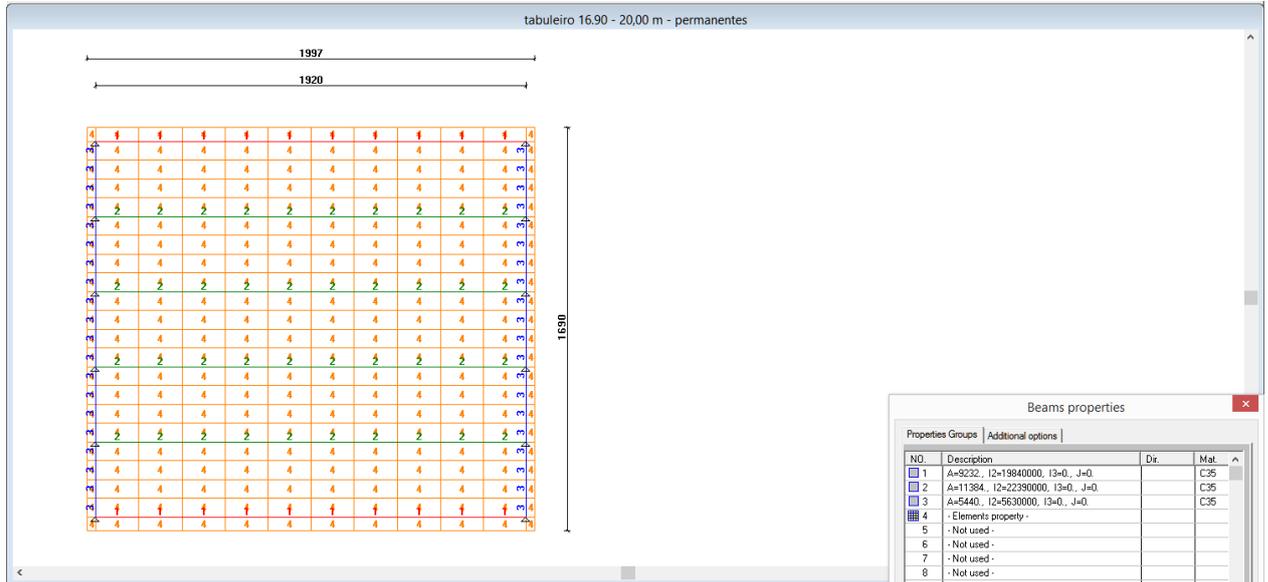
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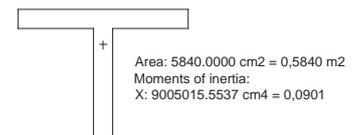
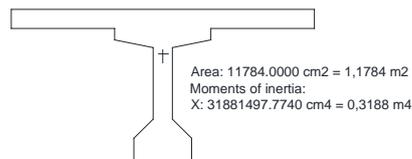
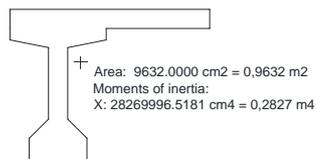
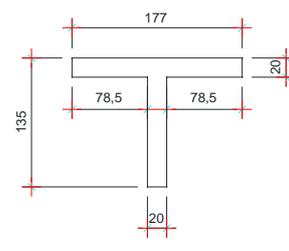
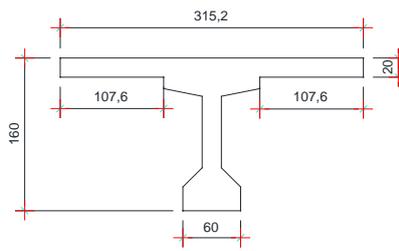
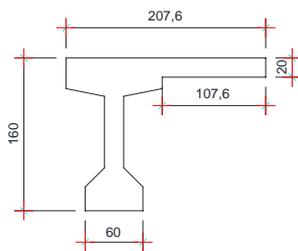
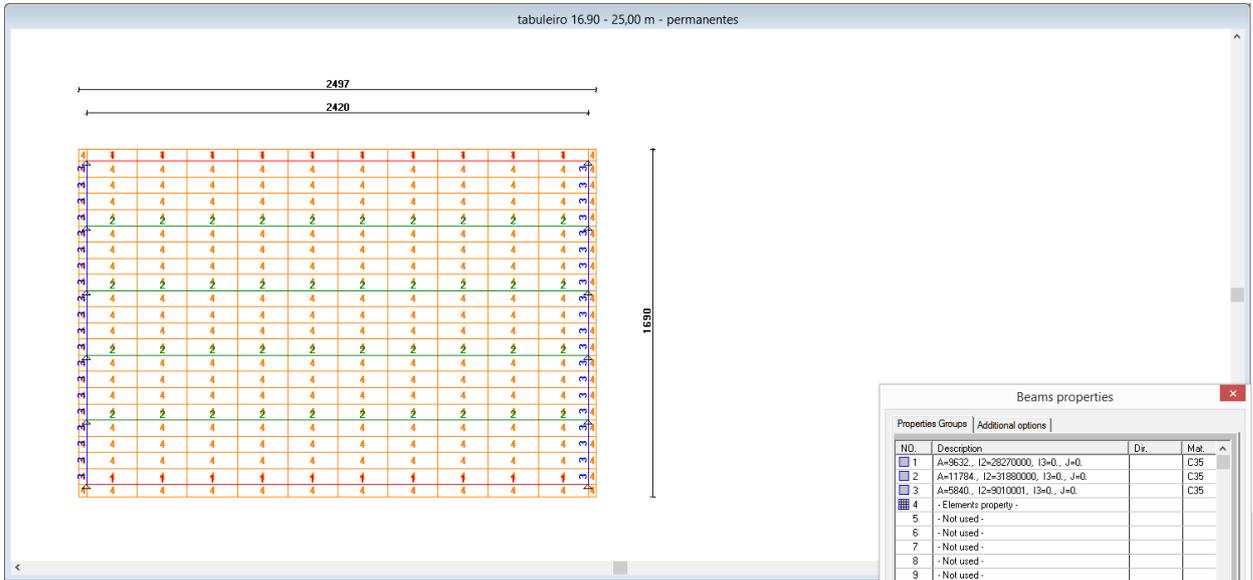
### NOTA TÉCNICA

#### 4.2.5. Tabuleiro 16,90 m



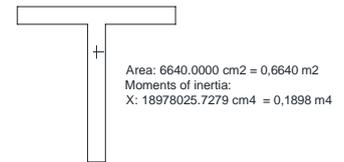
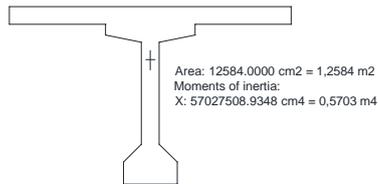
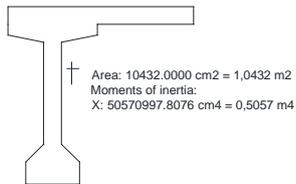
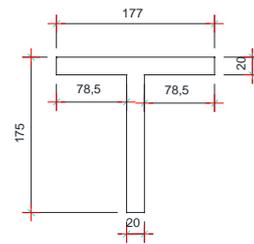
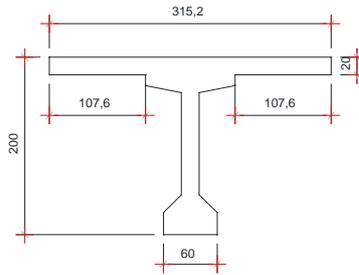
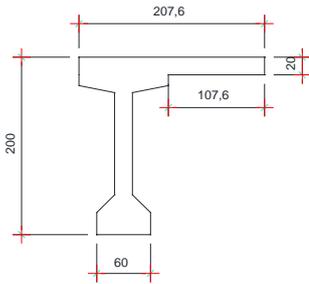
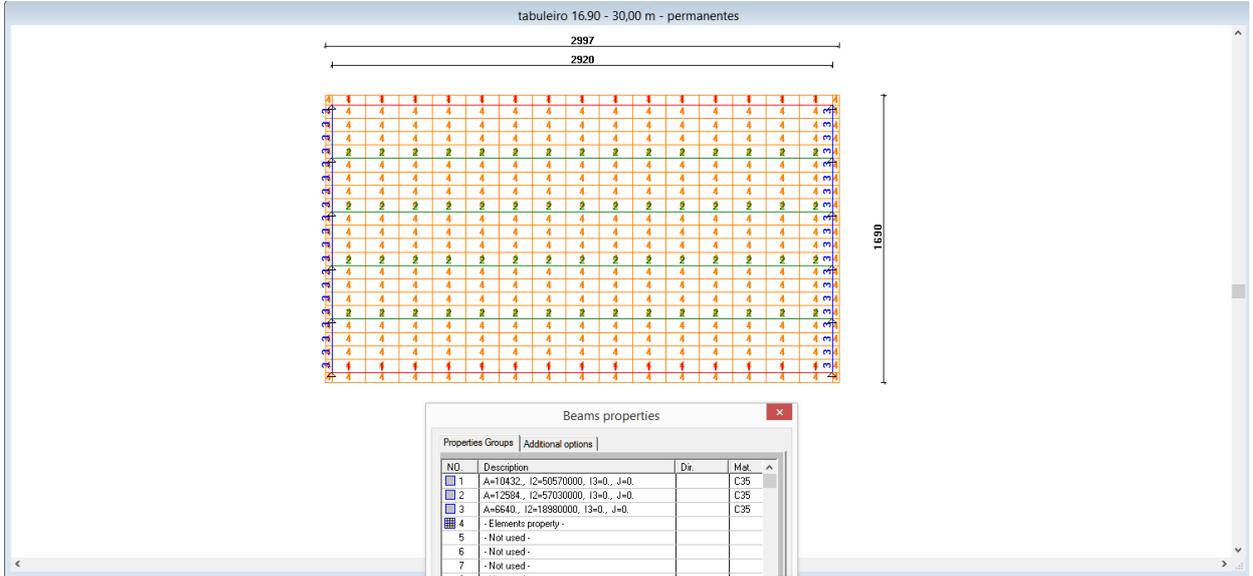


### NOTA TÉCNICA



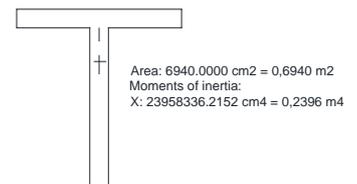
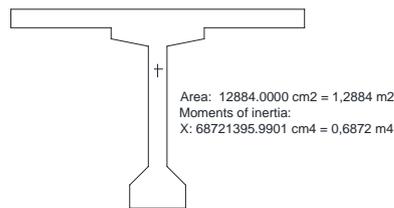
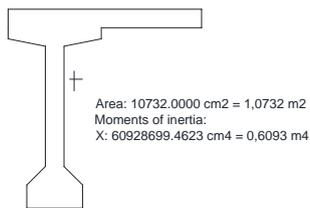
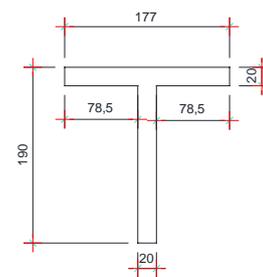
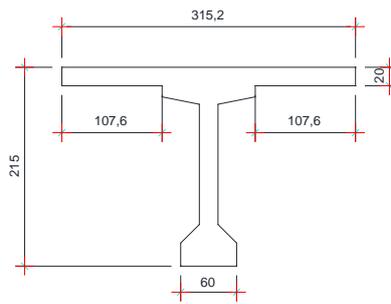
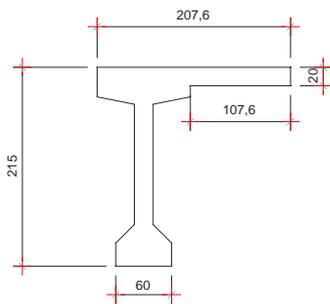
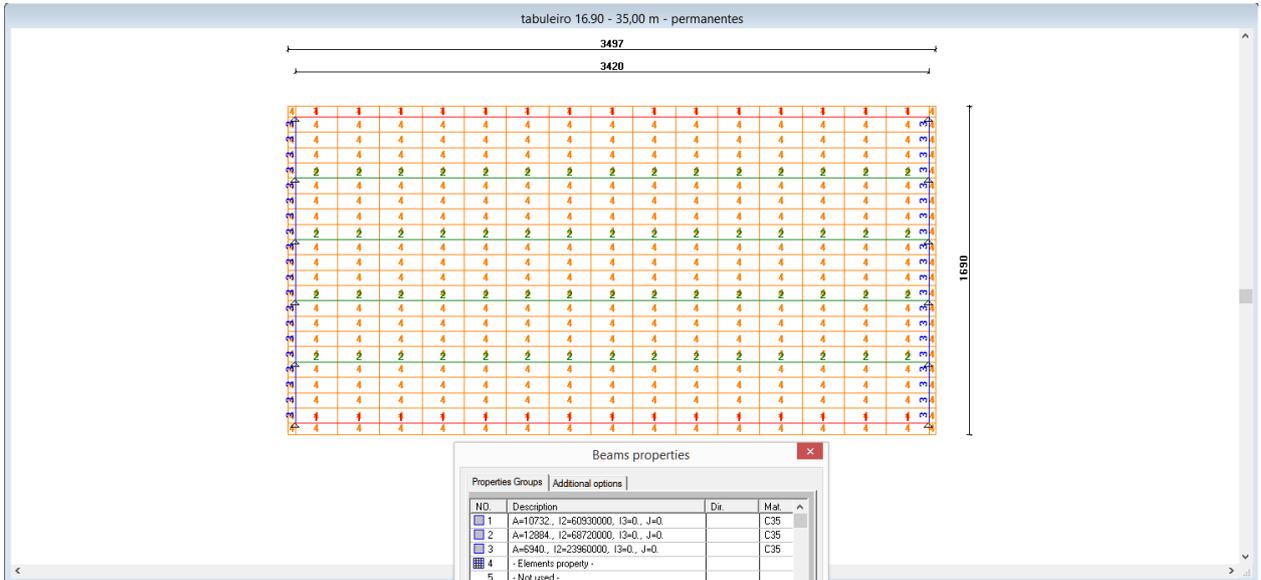


### NOTA TÉCNICA



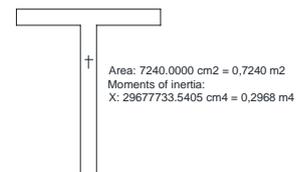
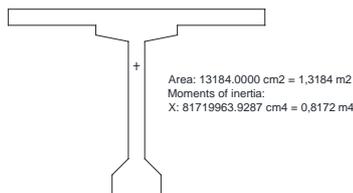
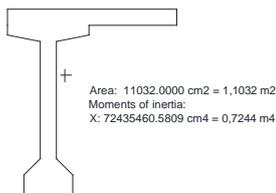
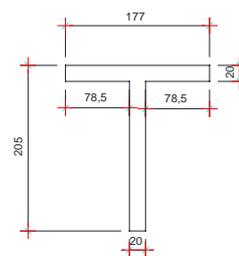
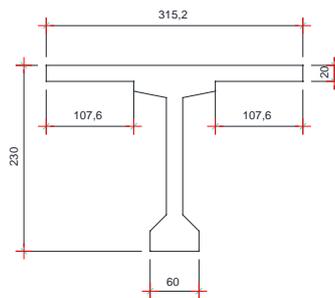
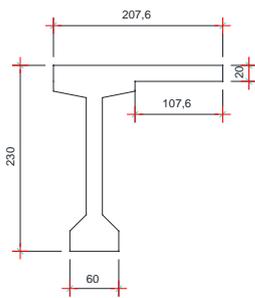
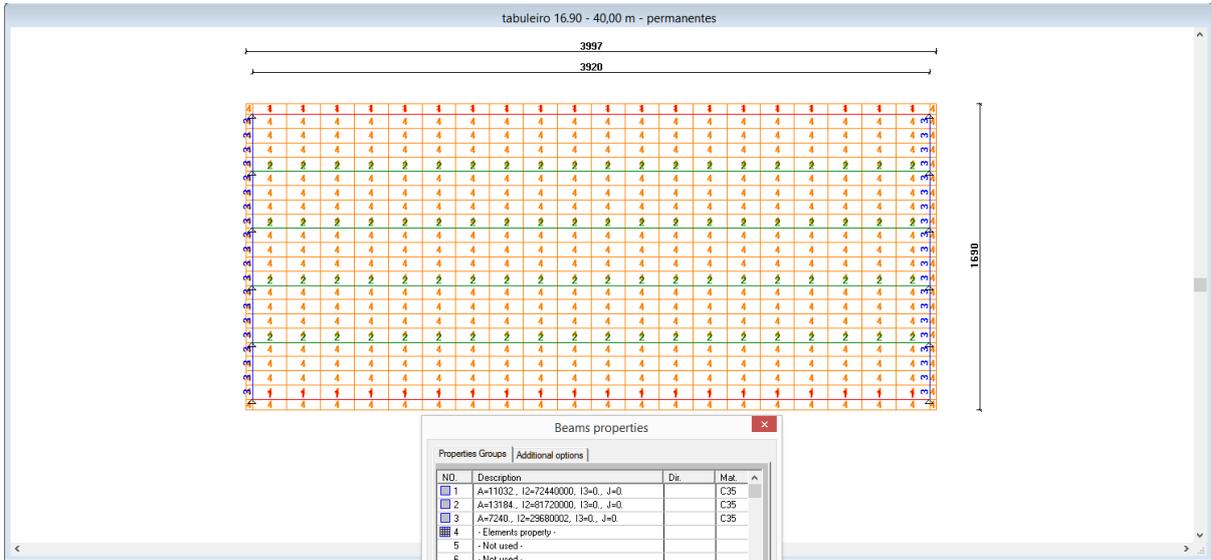


### NOTA TÉCNICA





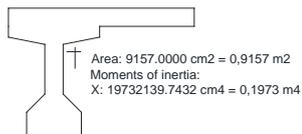
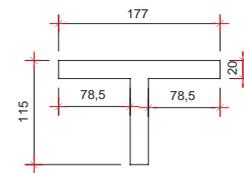
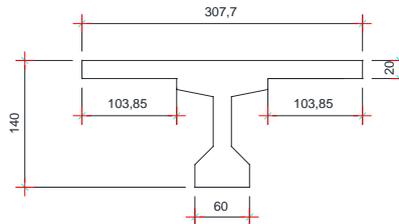
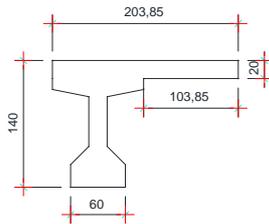
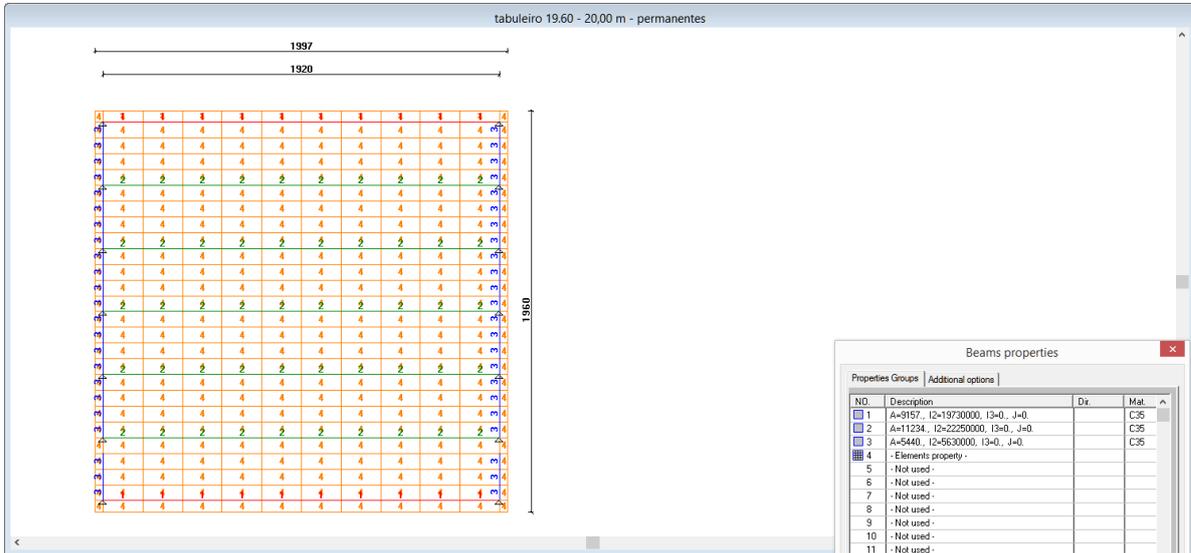
### NOTA TÉCNICA





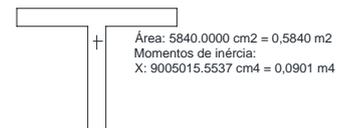
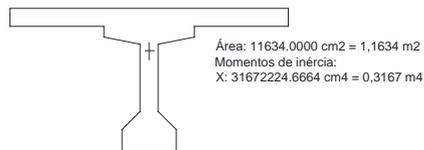
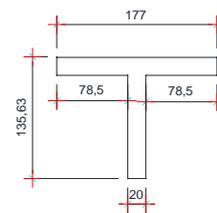
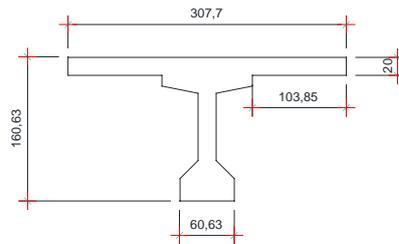
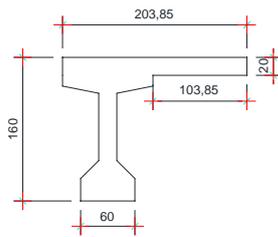
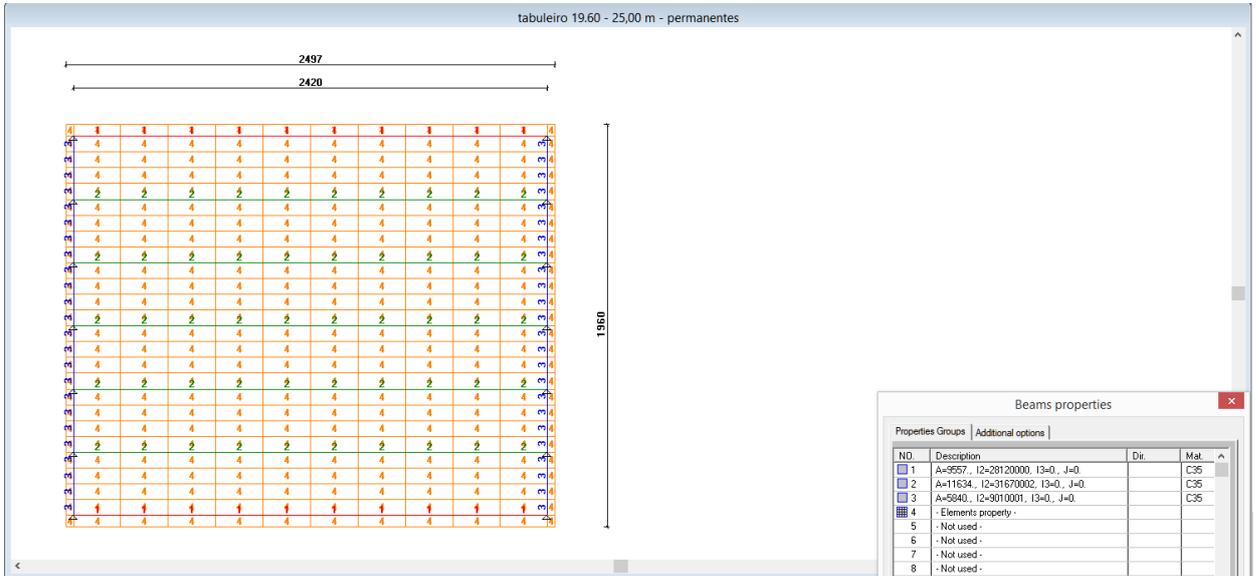
### NOTA TÉCNICA

#### 4.2.6. Tabuleiro 19,60 m



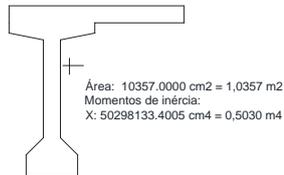
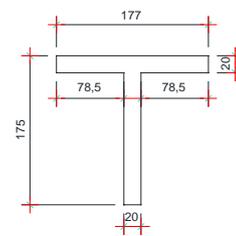
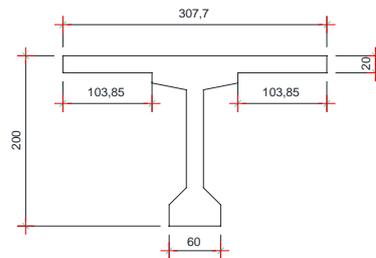
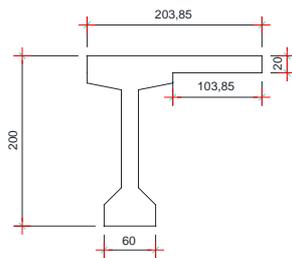
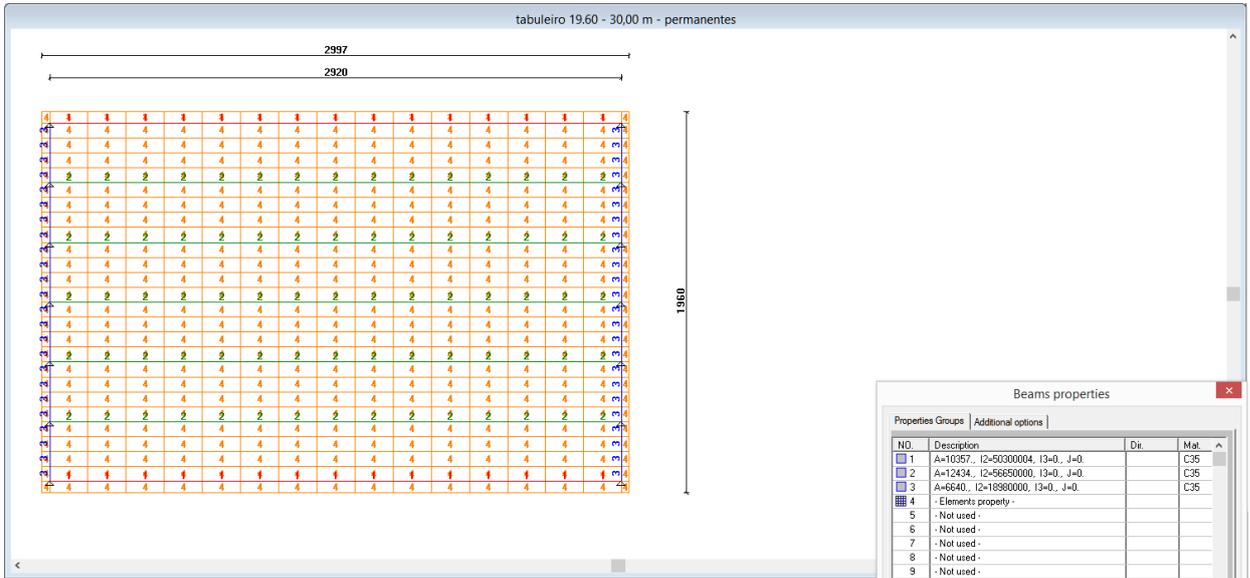


### NOTA TÉCNICA



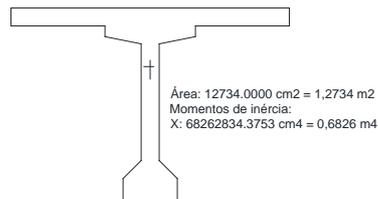
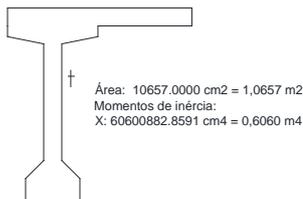
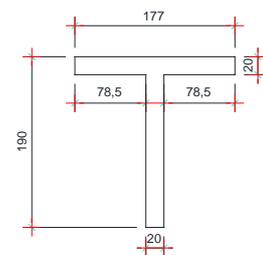
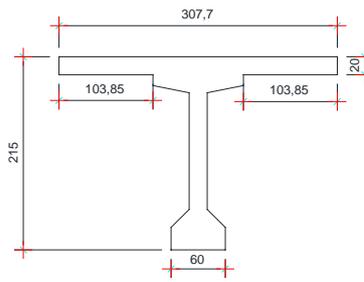
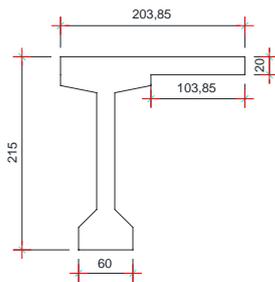
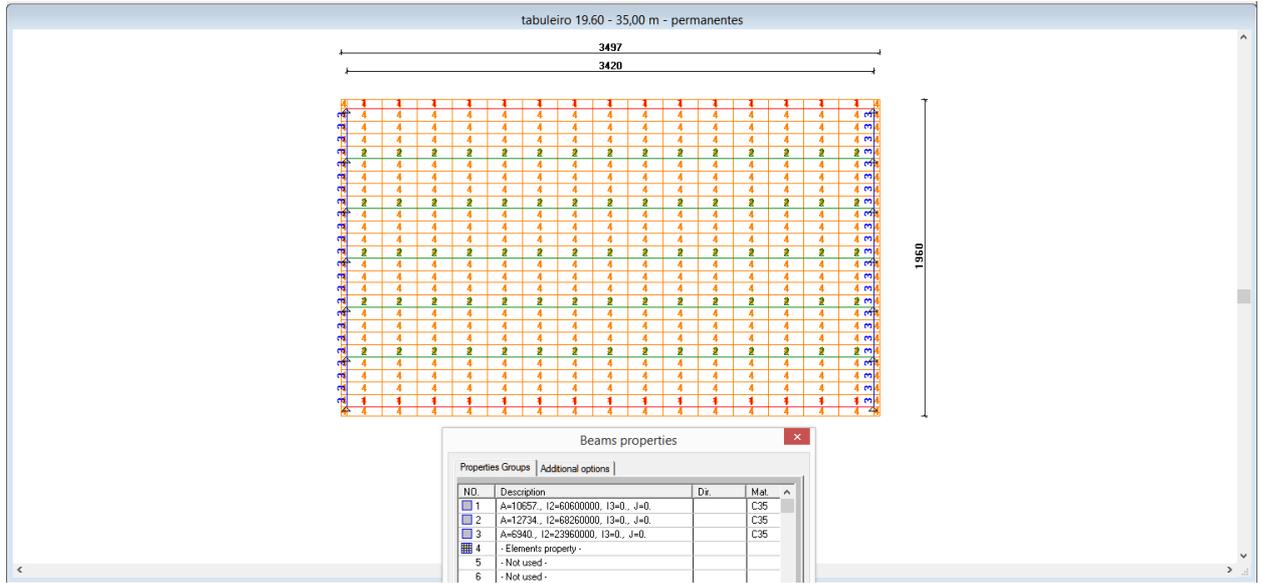


### NOTA TÉCNICA



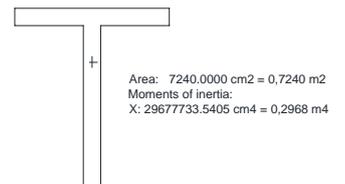
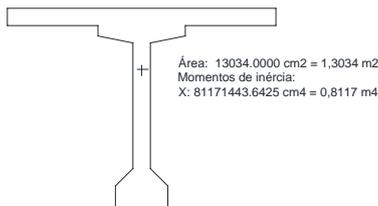
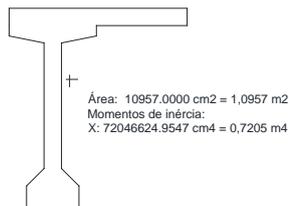
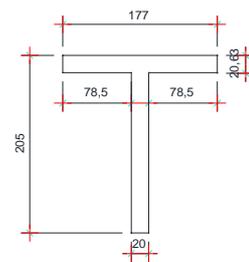
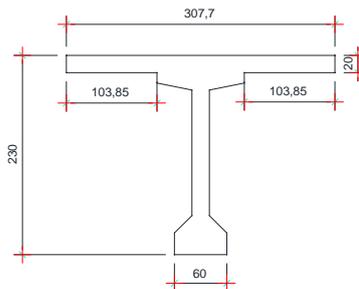
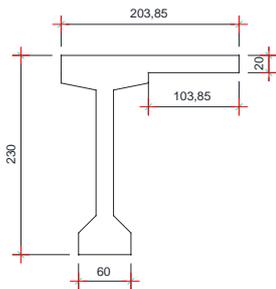
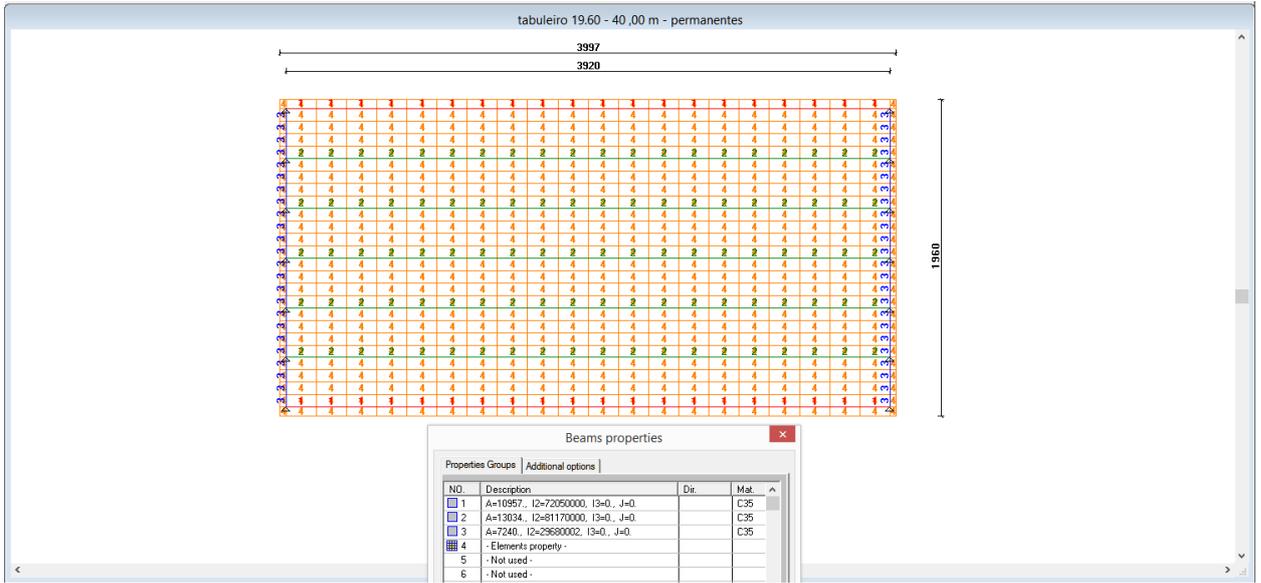


### NOTA TÉCNICA





### NOTA TÉCNICA





## NOTA TÉCNICA

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### 4.3. Cargas permanentes

O peso próprio considerado para o pavimento e a recapa é de:

$$g_{\text{peso próprio}} = (2,40 \times 0,10) + 0,20 = 0,44 \text{ tf/m}^2$$

Foi adotada uma espessura de pavimento de 10 cm.

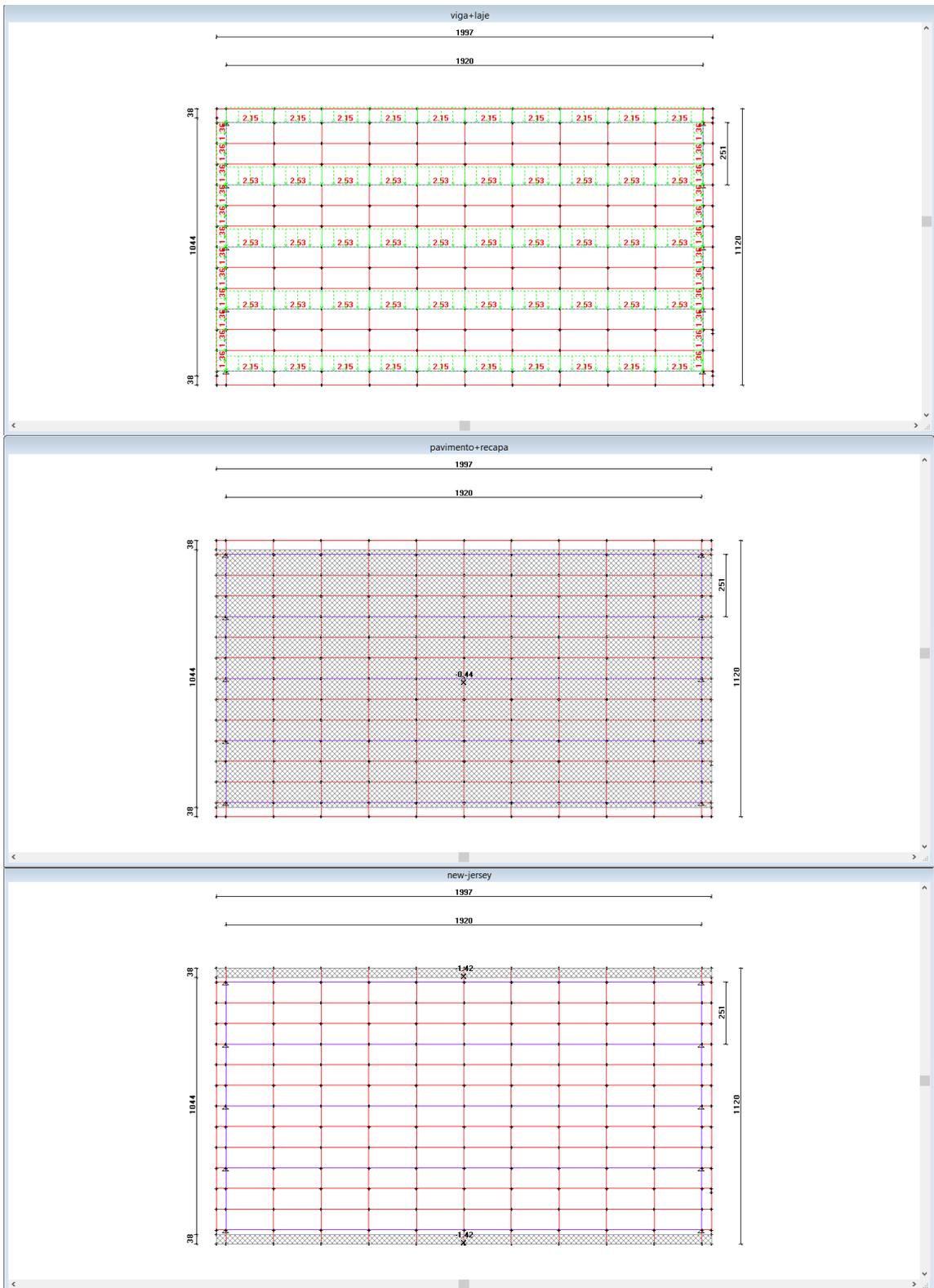
Para o New Jersey, realizamos o cálculo da área da defesa com a placa, que resultou em 0,2158 m<sup>2</sup> e multiplicamos pelo peso próprio do concreto armado, que é igual a 2,5 tf/m<sup>2</sup>. Por fim, distribuimos o resultado em 0,38 metros e obtivemos uma pressão de 1,42 tf/m<sup>2</sup>.

$$g_{\text{new jersey}} = \frac{0,2158 \times 2,50}{0,38} = 1,42 \text{ tf/m}^2$$



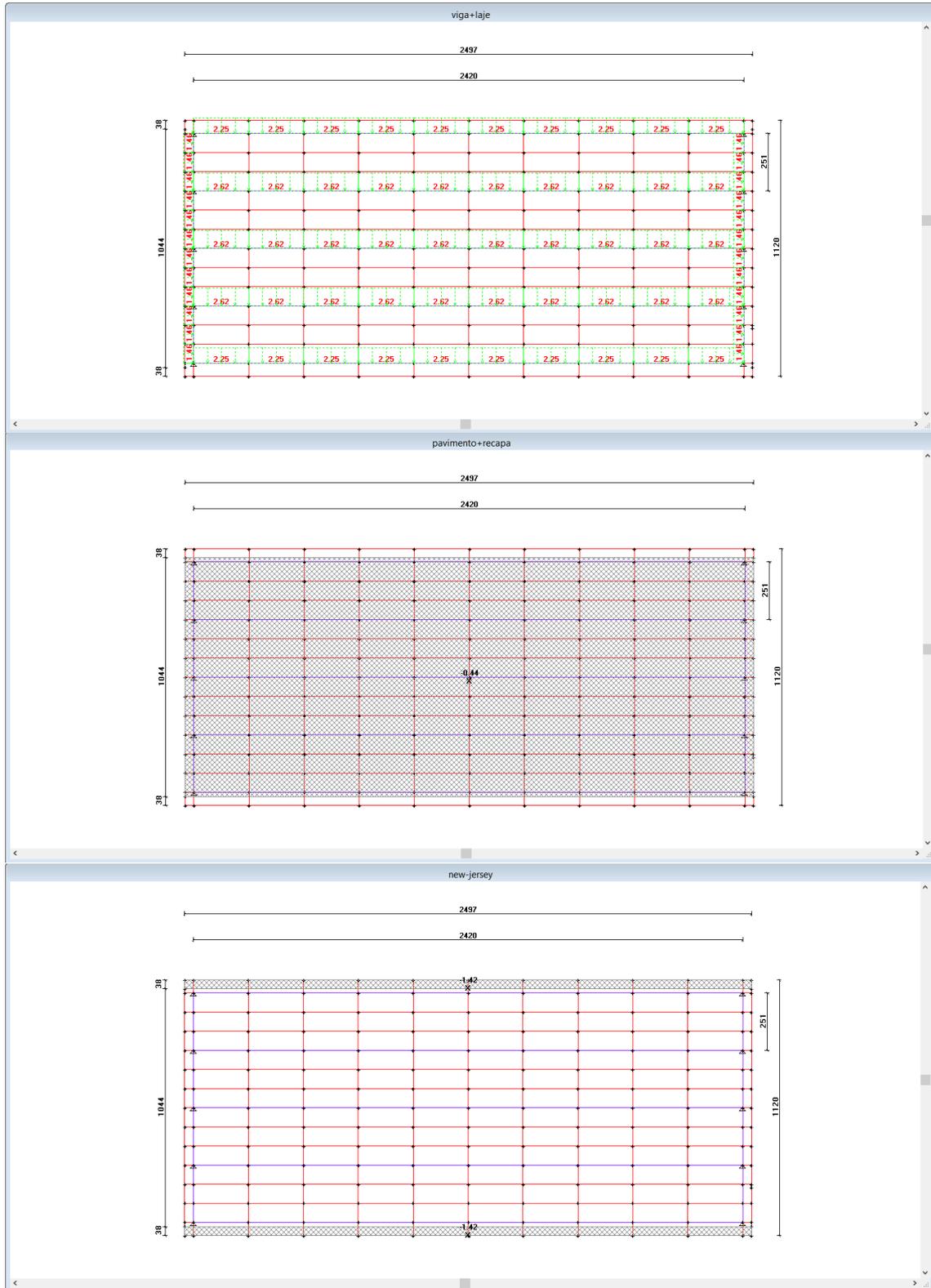
### NOTA TÉCNICA

#### 4.3.1. Tabuleiro 11,20 m



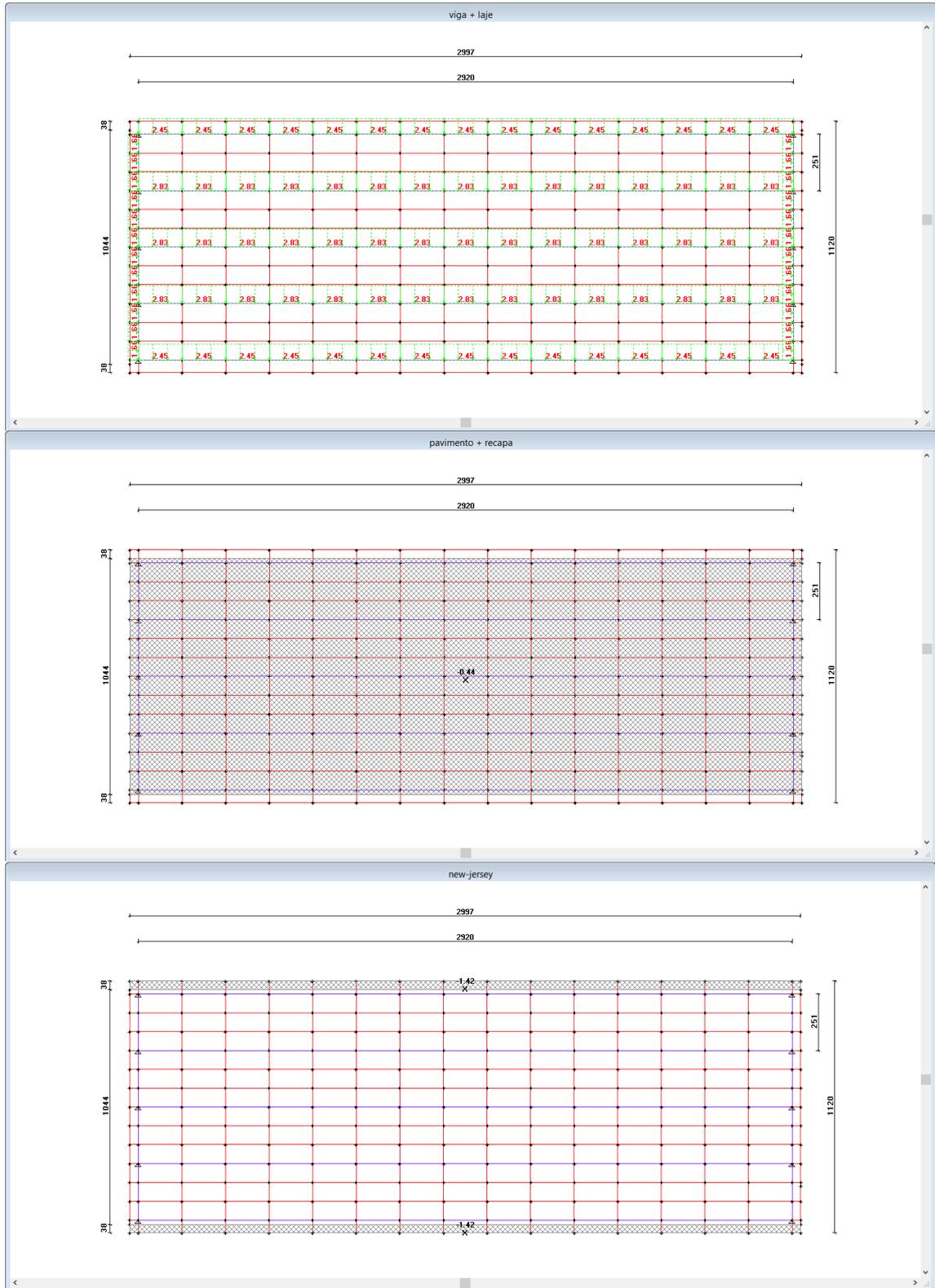


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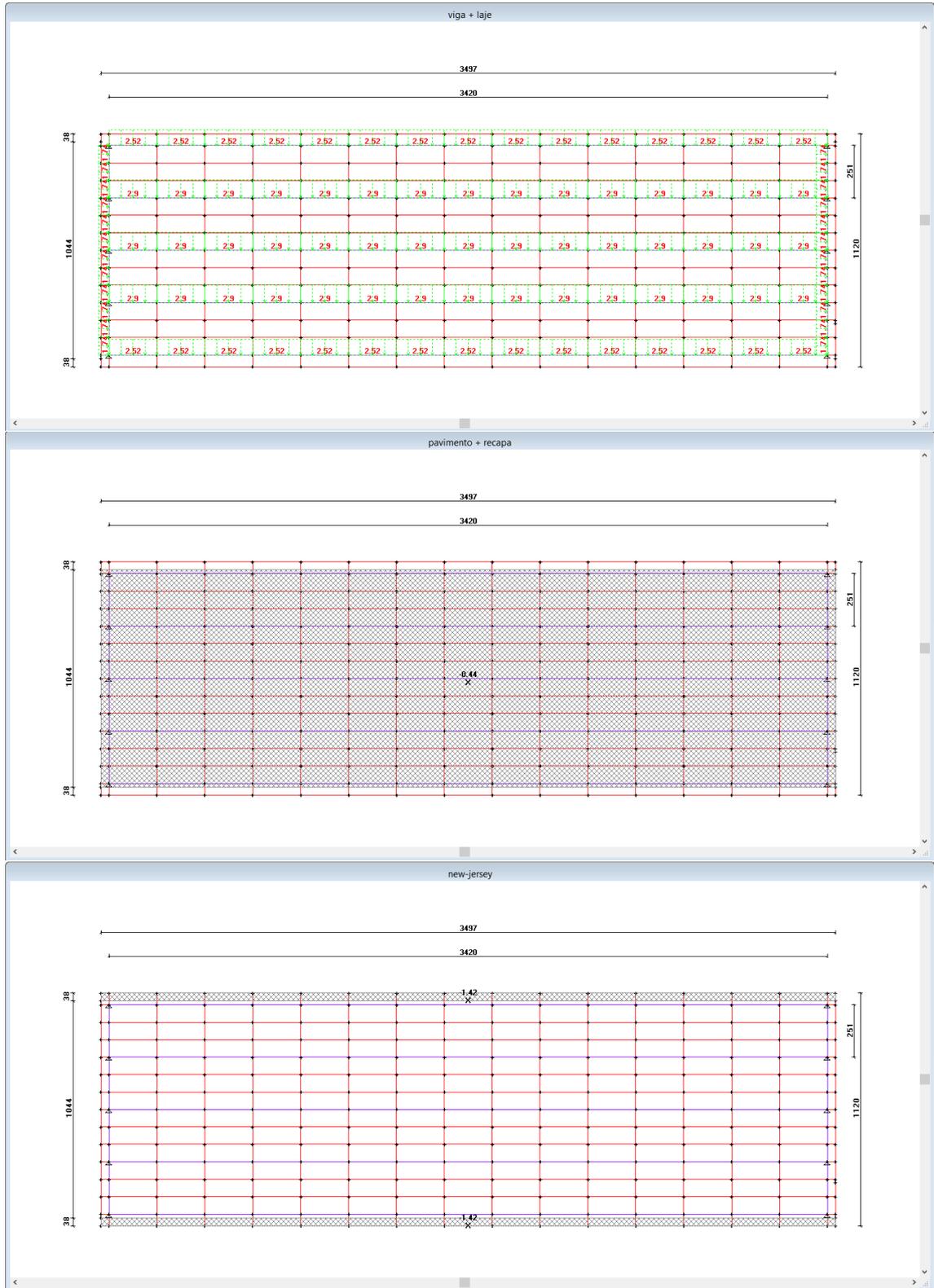


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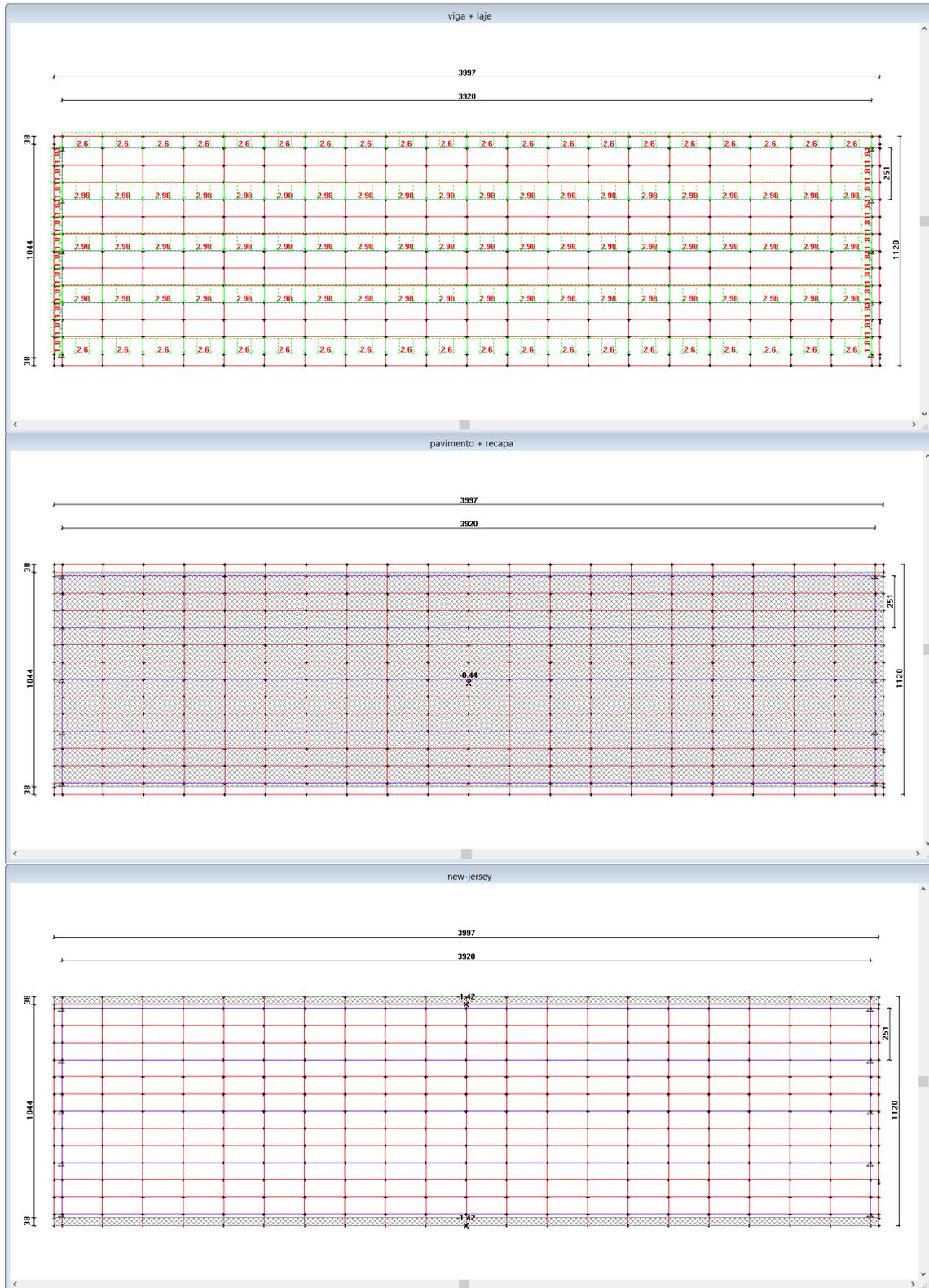


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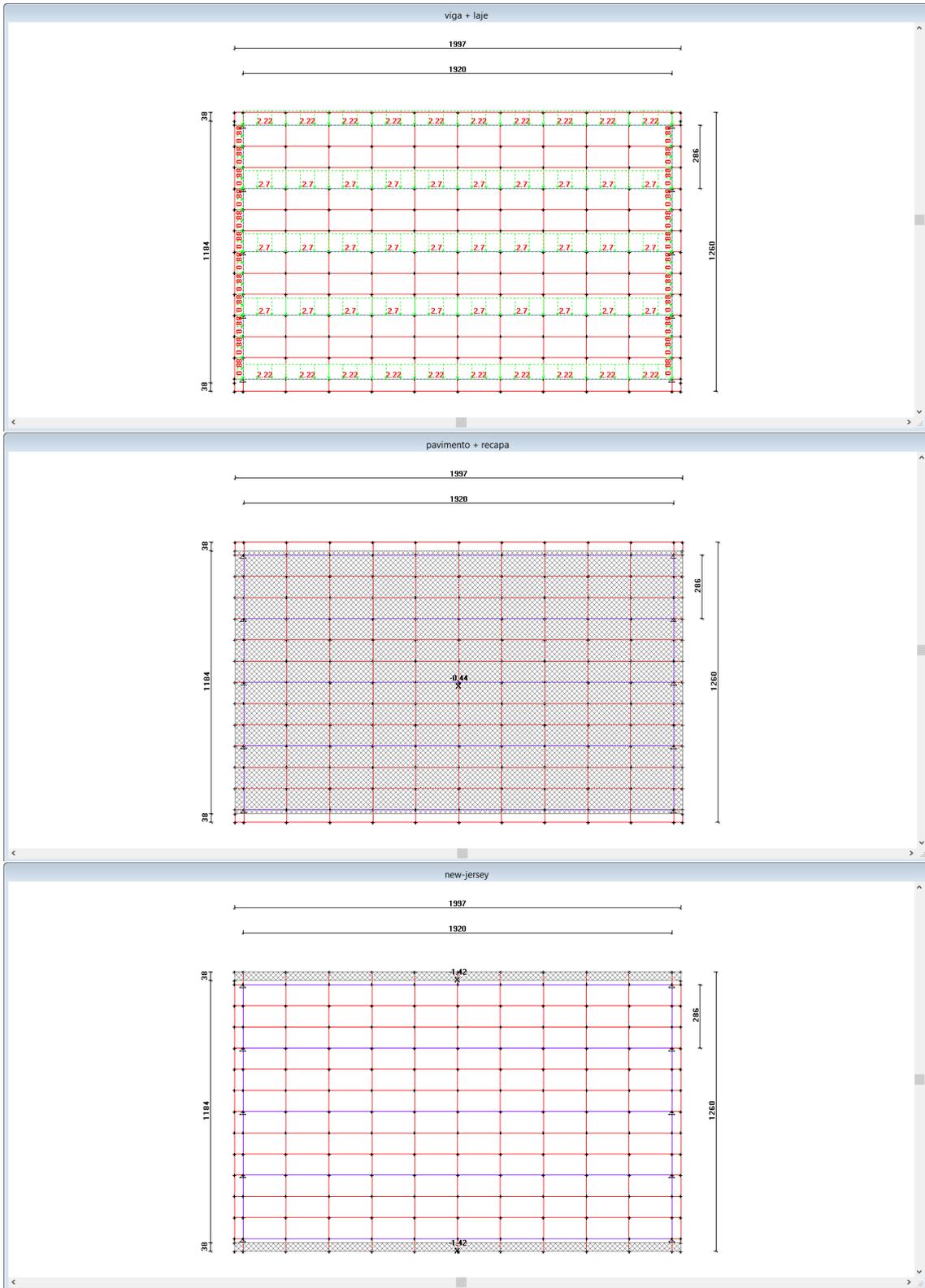
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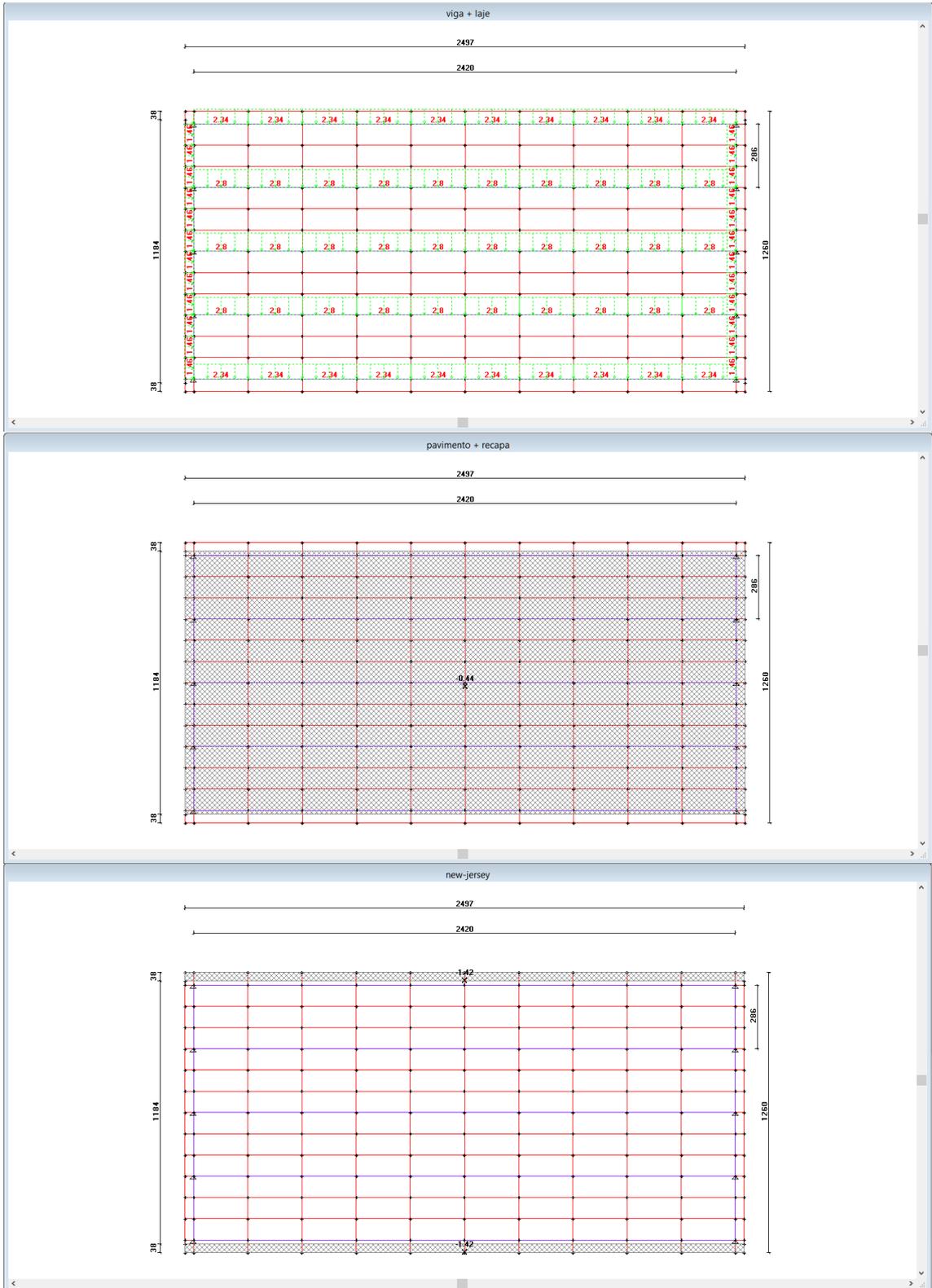
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#### 4.3.2. Tabuleiro 12,60 m



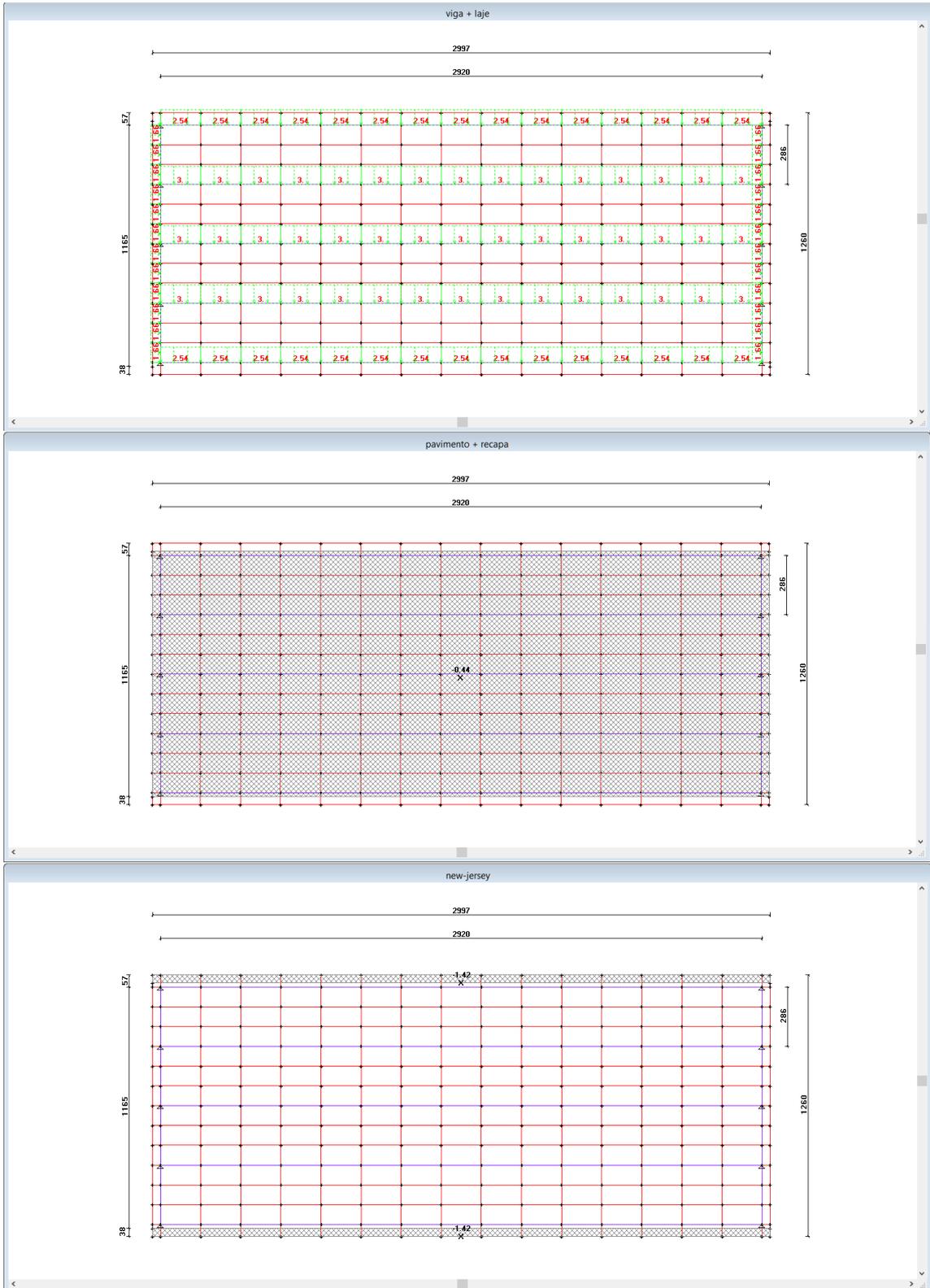


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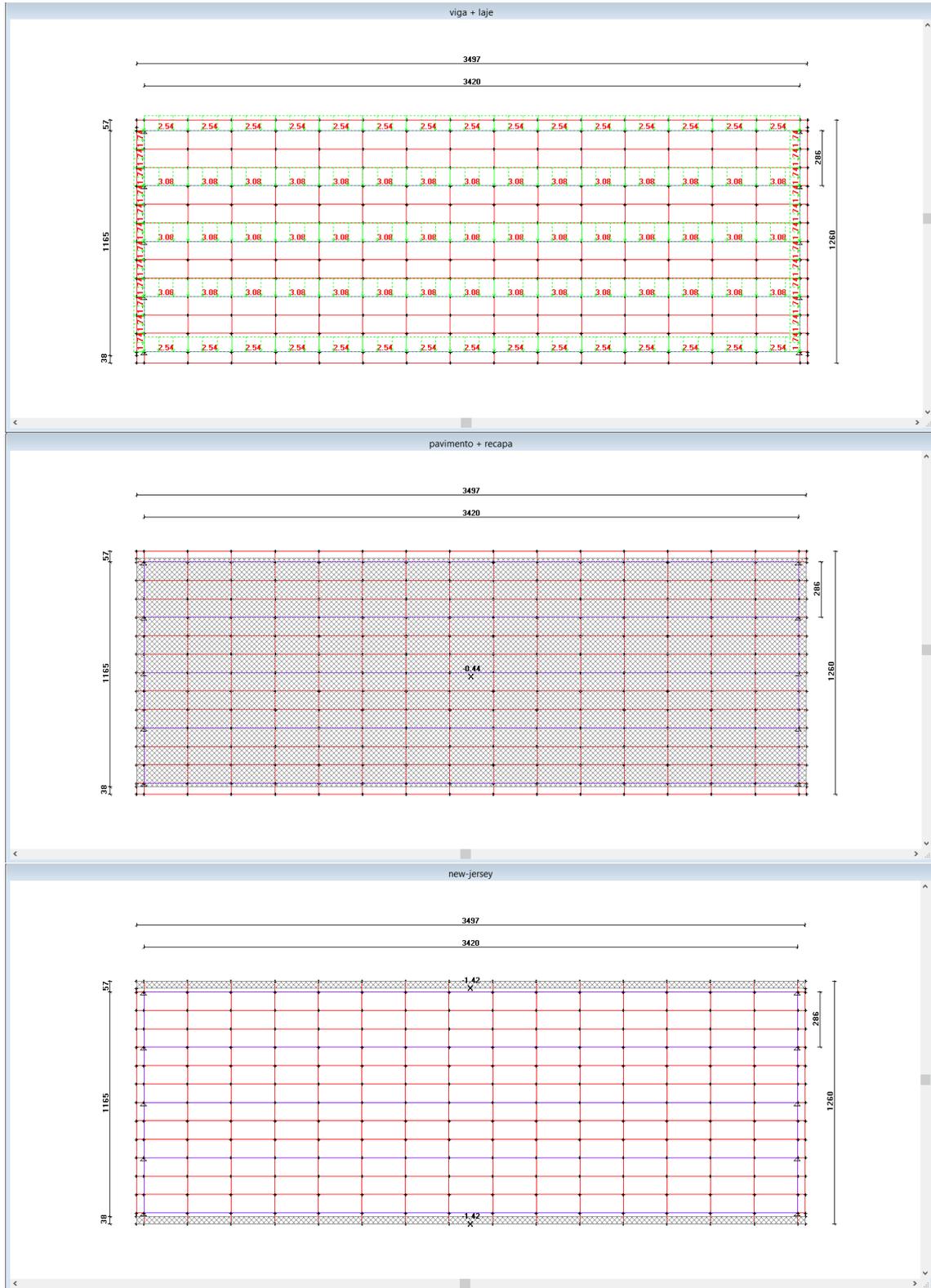


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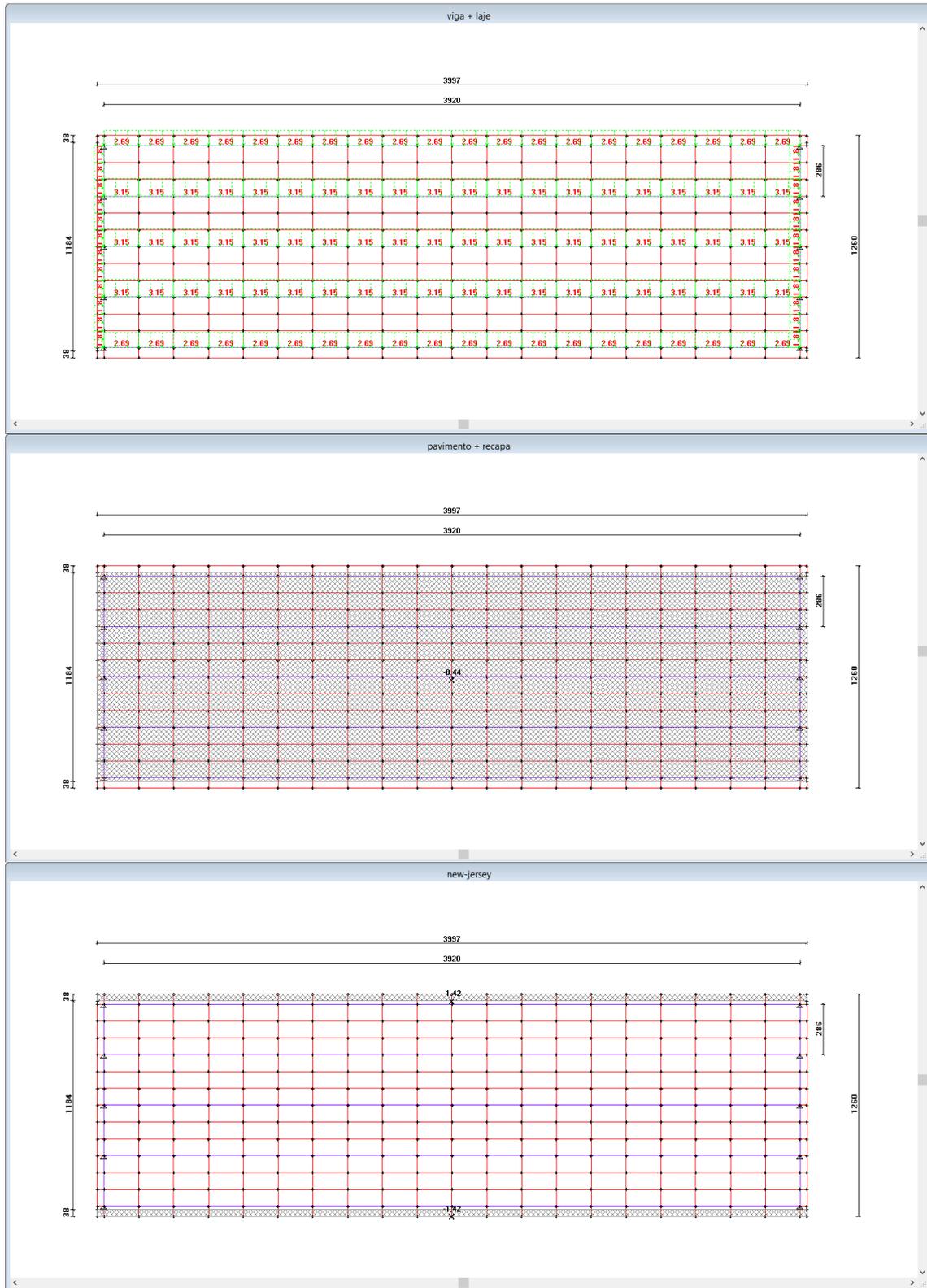


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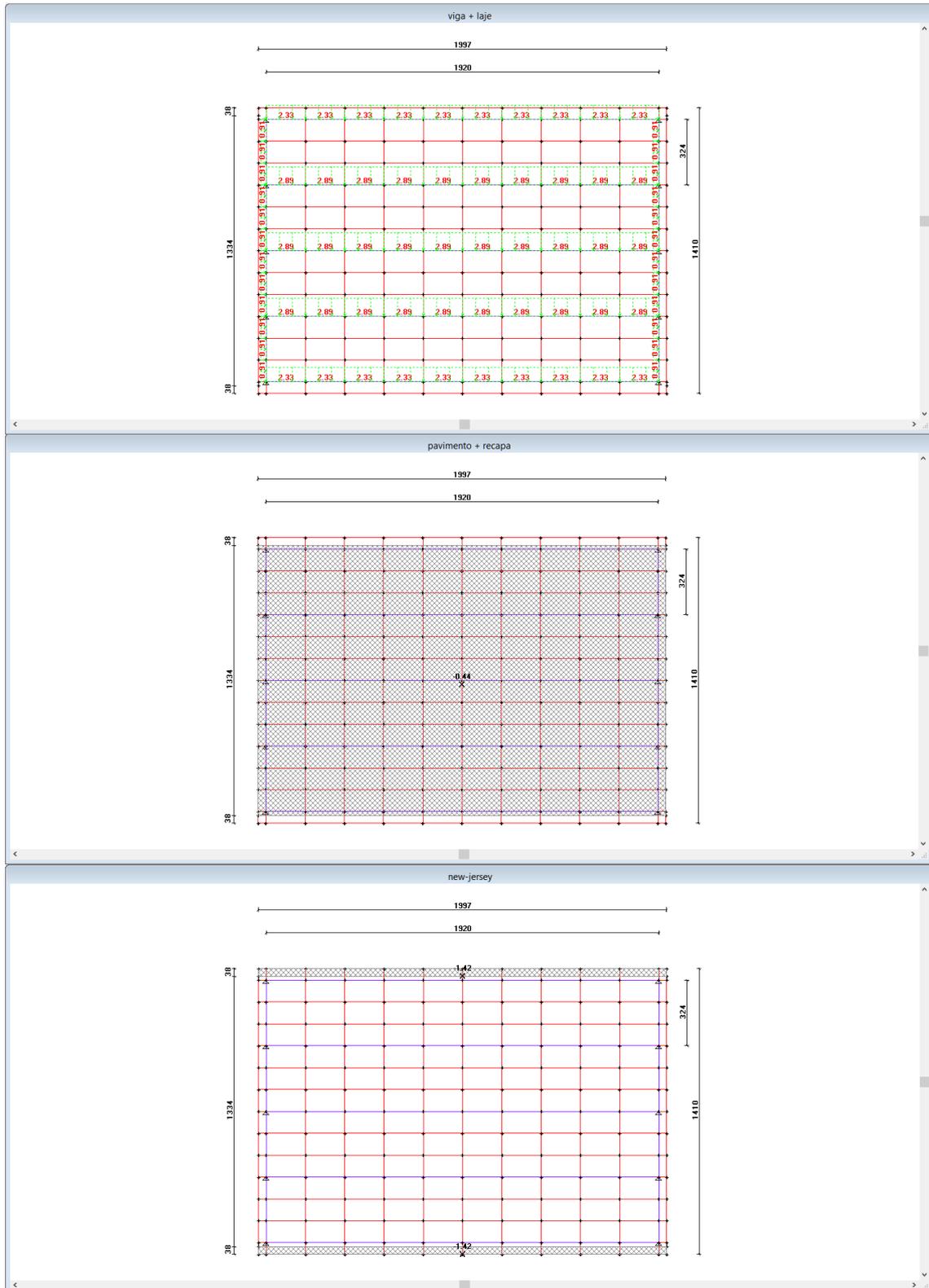
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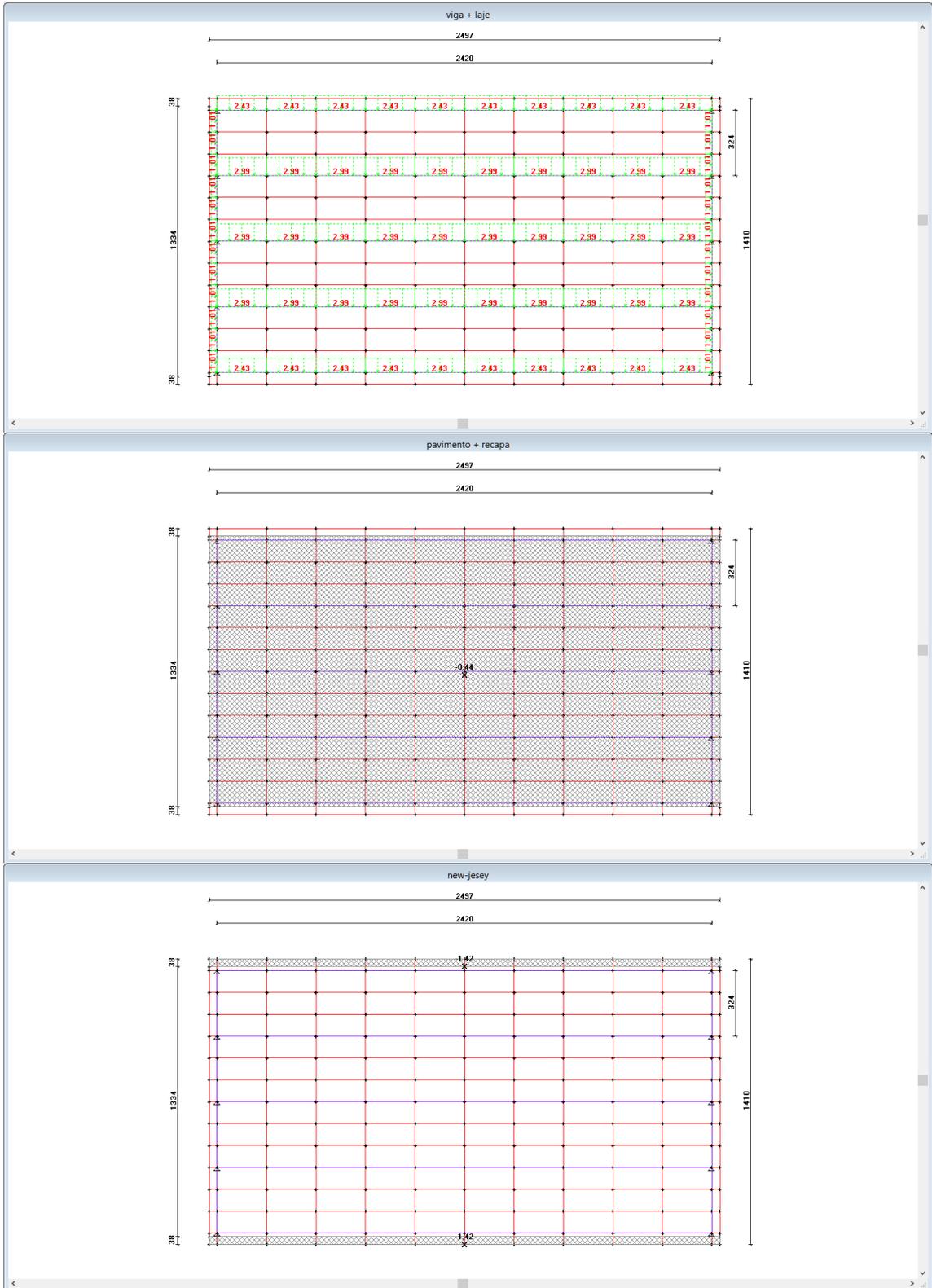
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#### 4.3.3. Tabuleiro 14,10 m



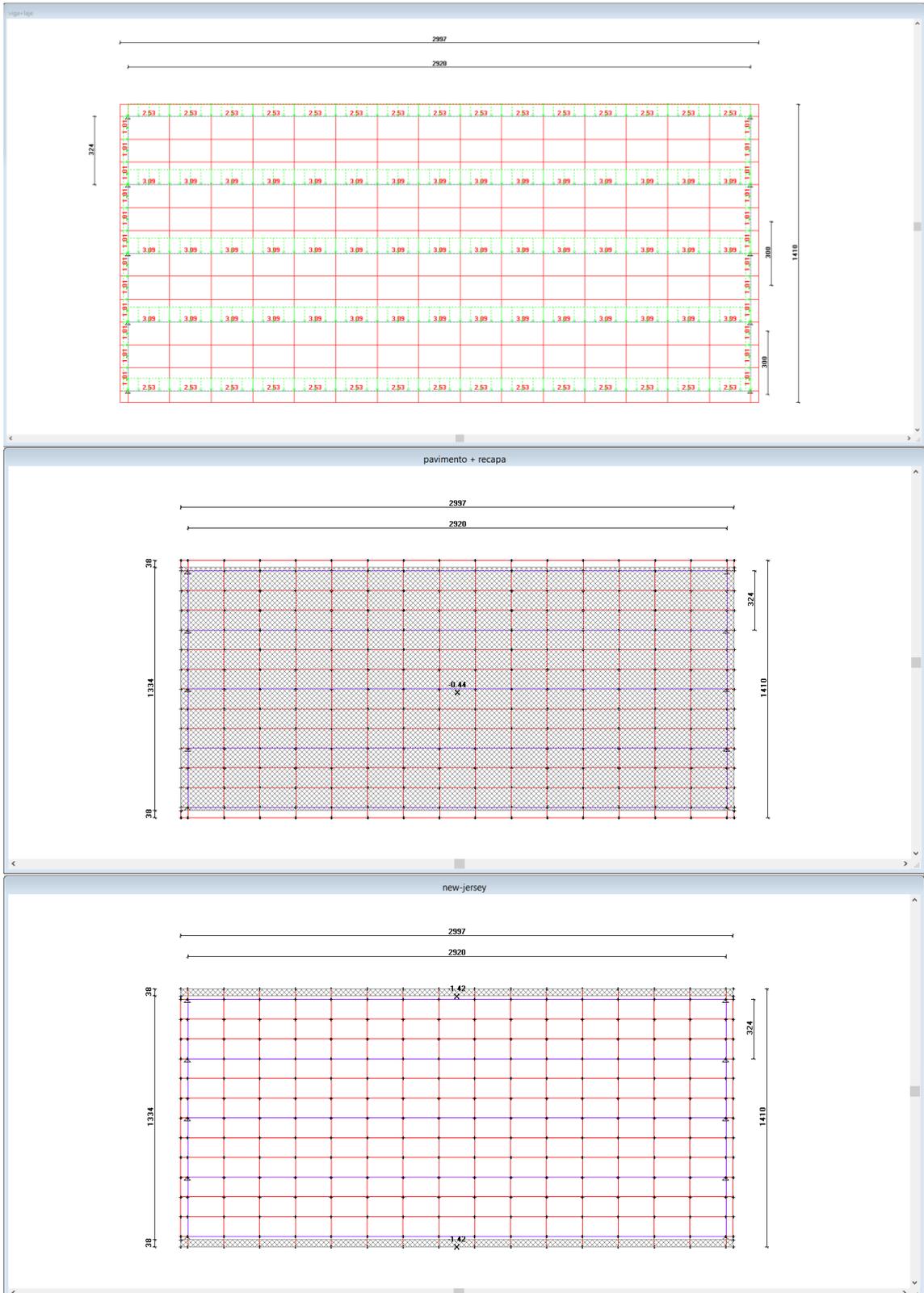


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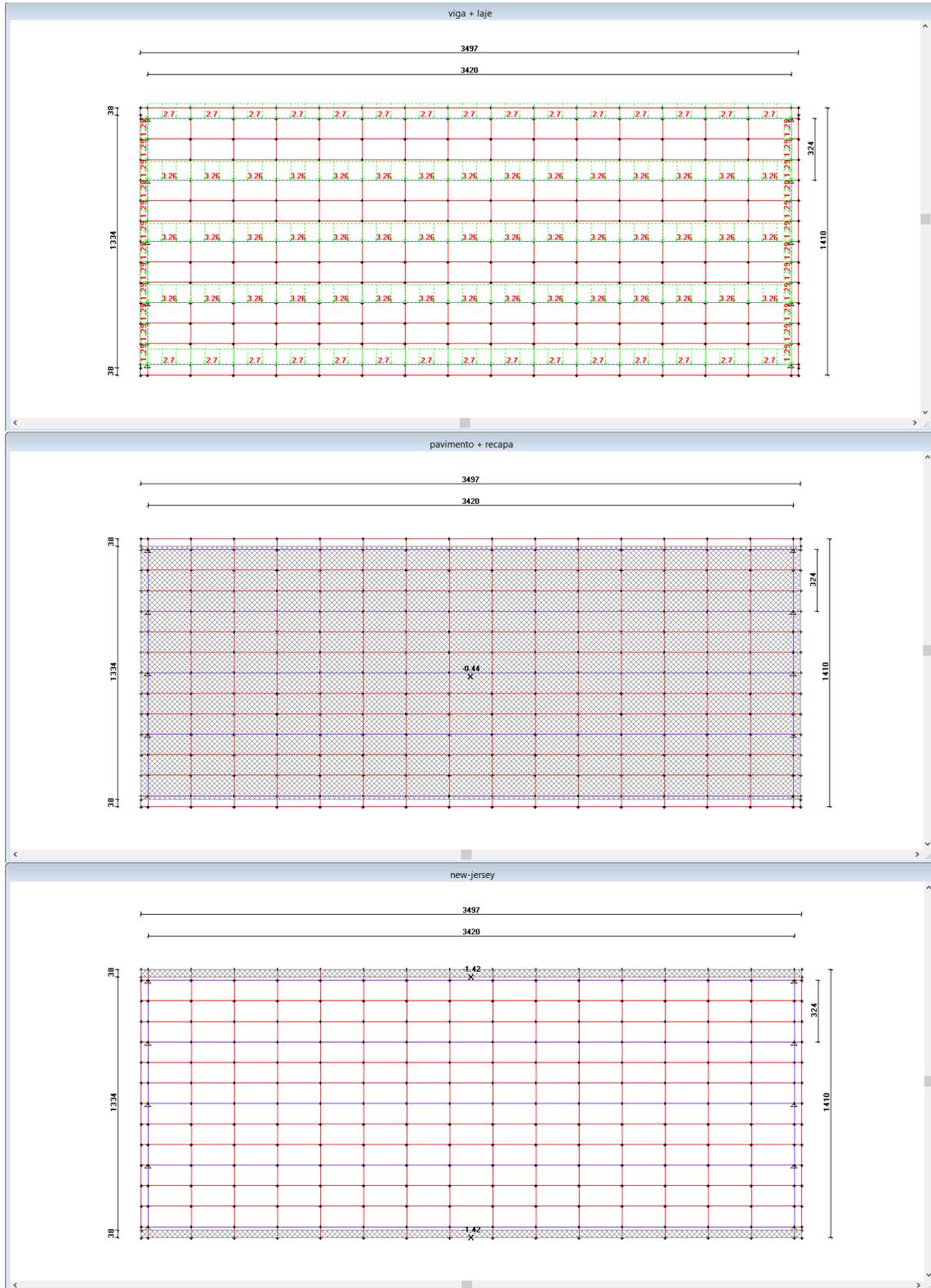


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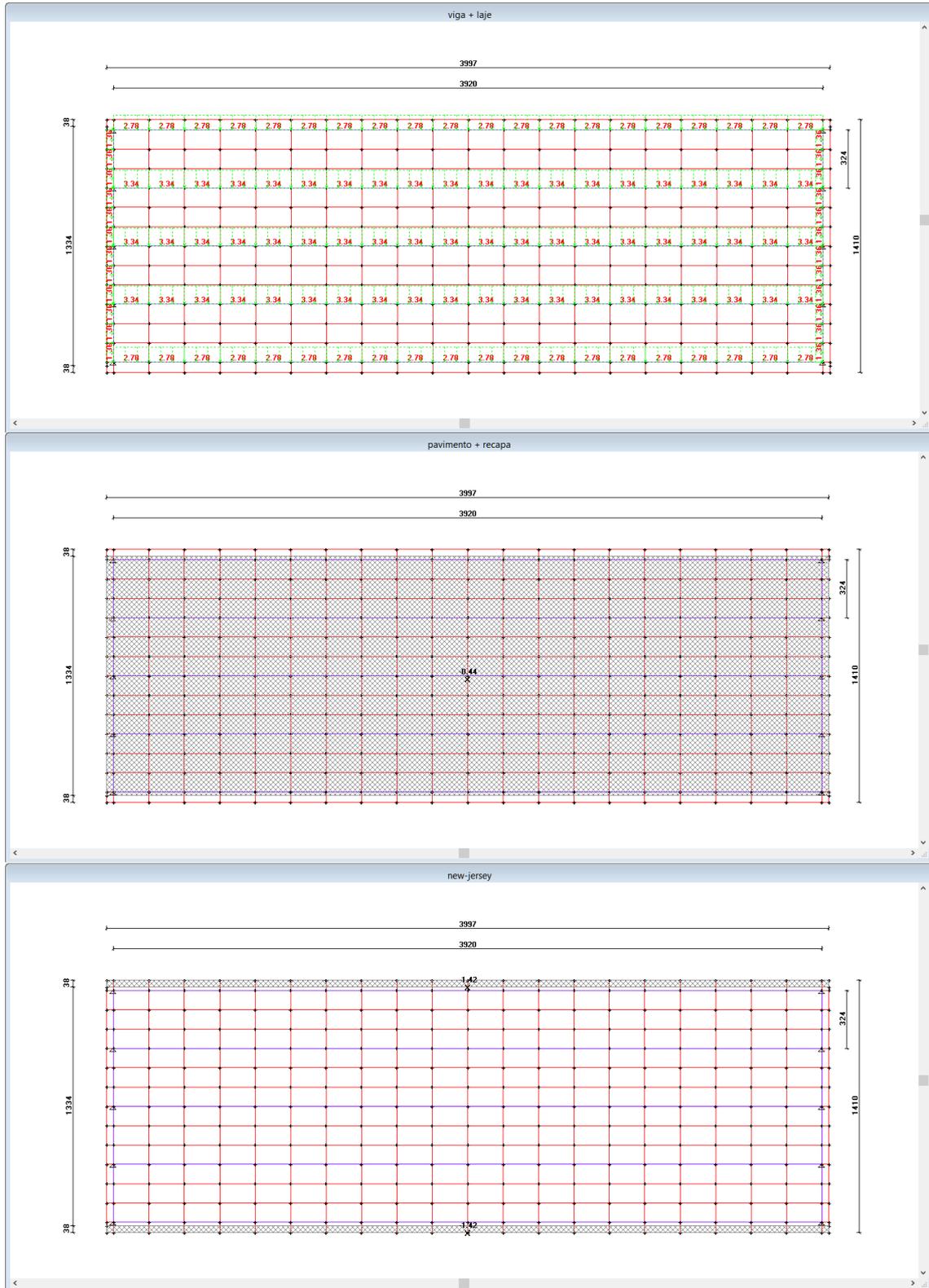


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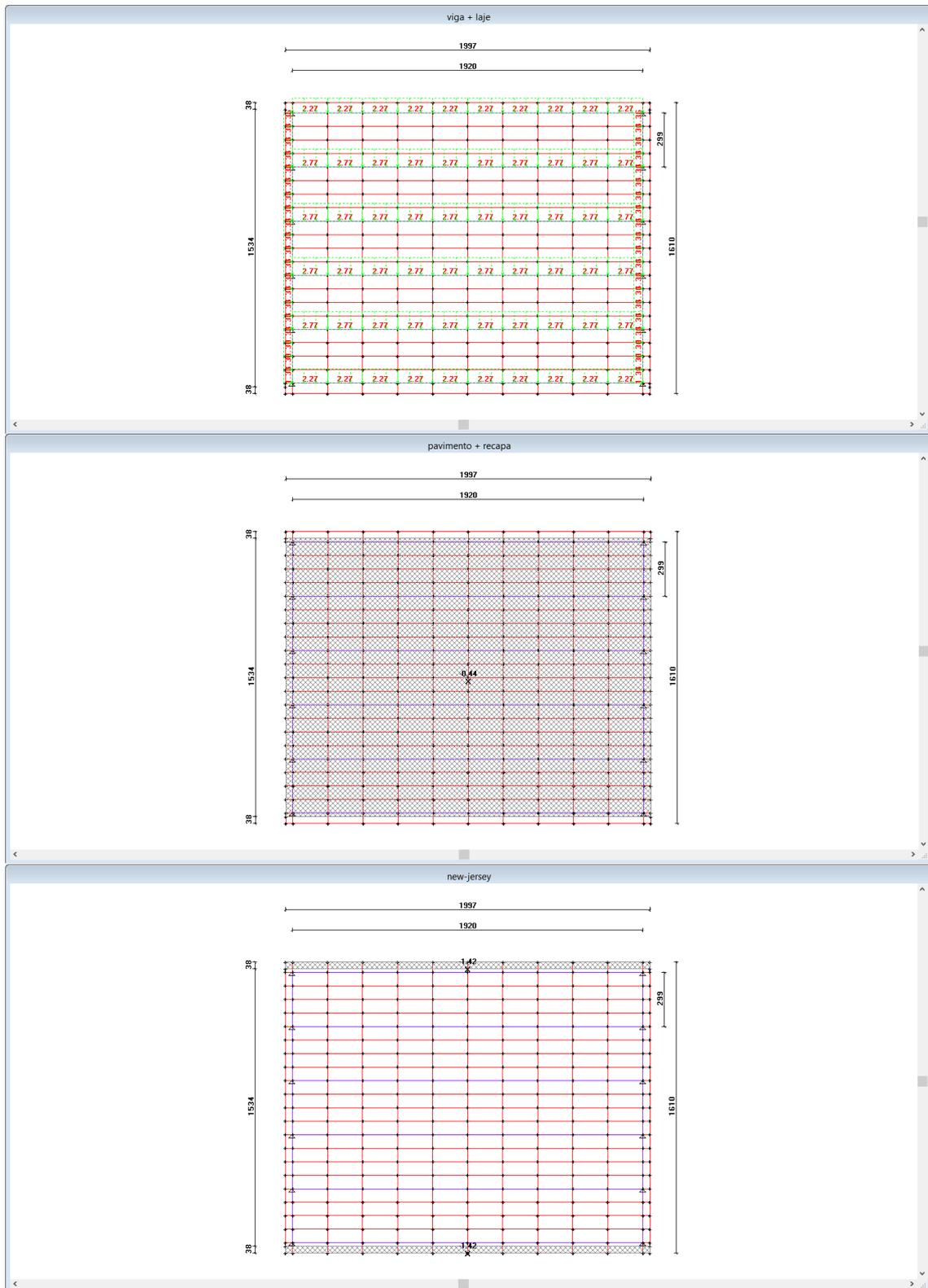
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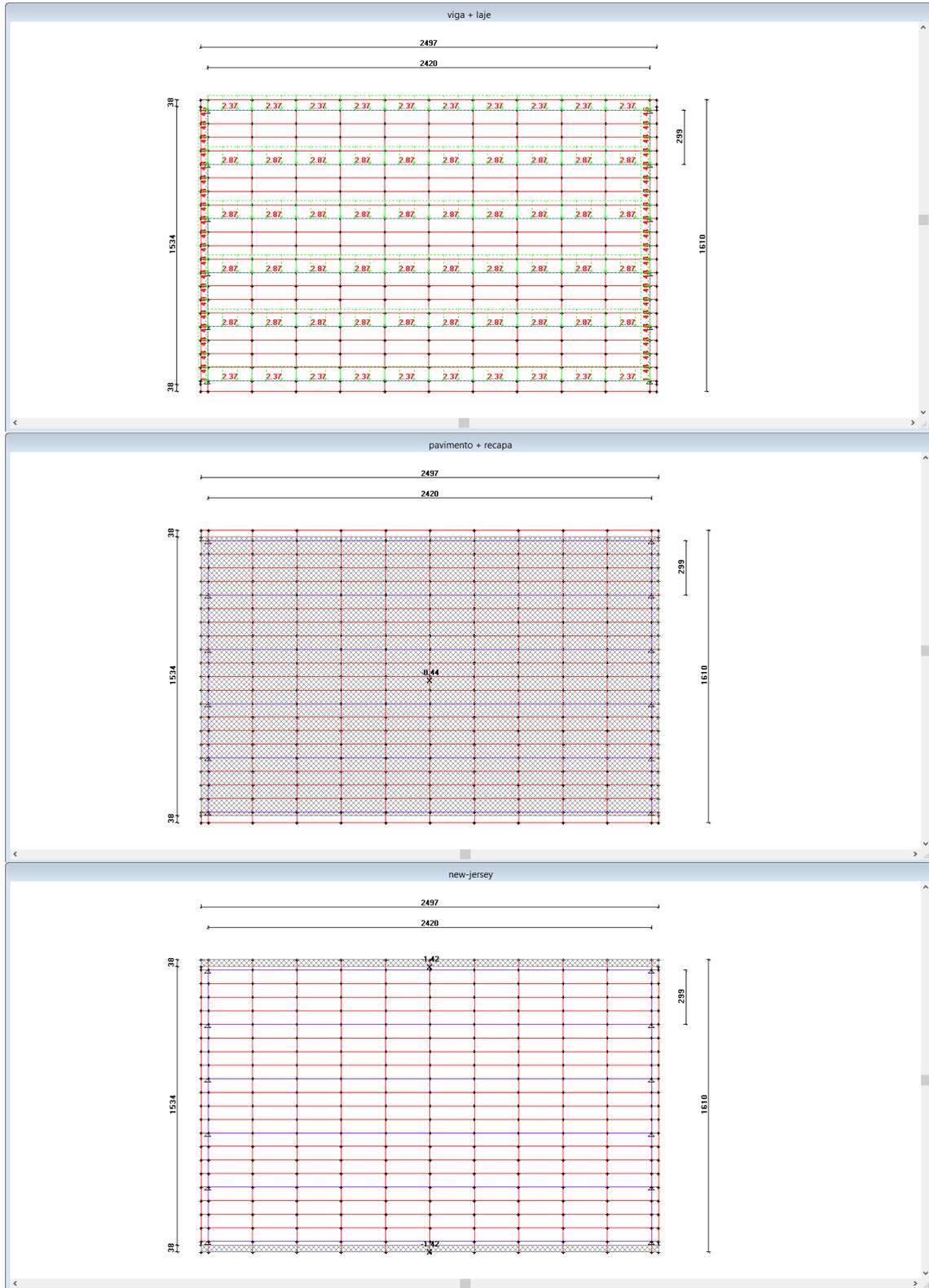
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#### 4.3.4. Tabuleiro 16,10 m



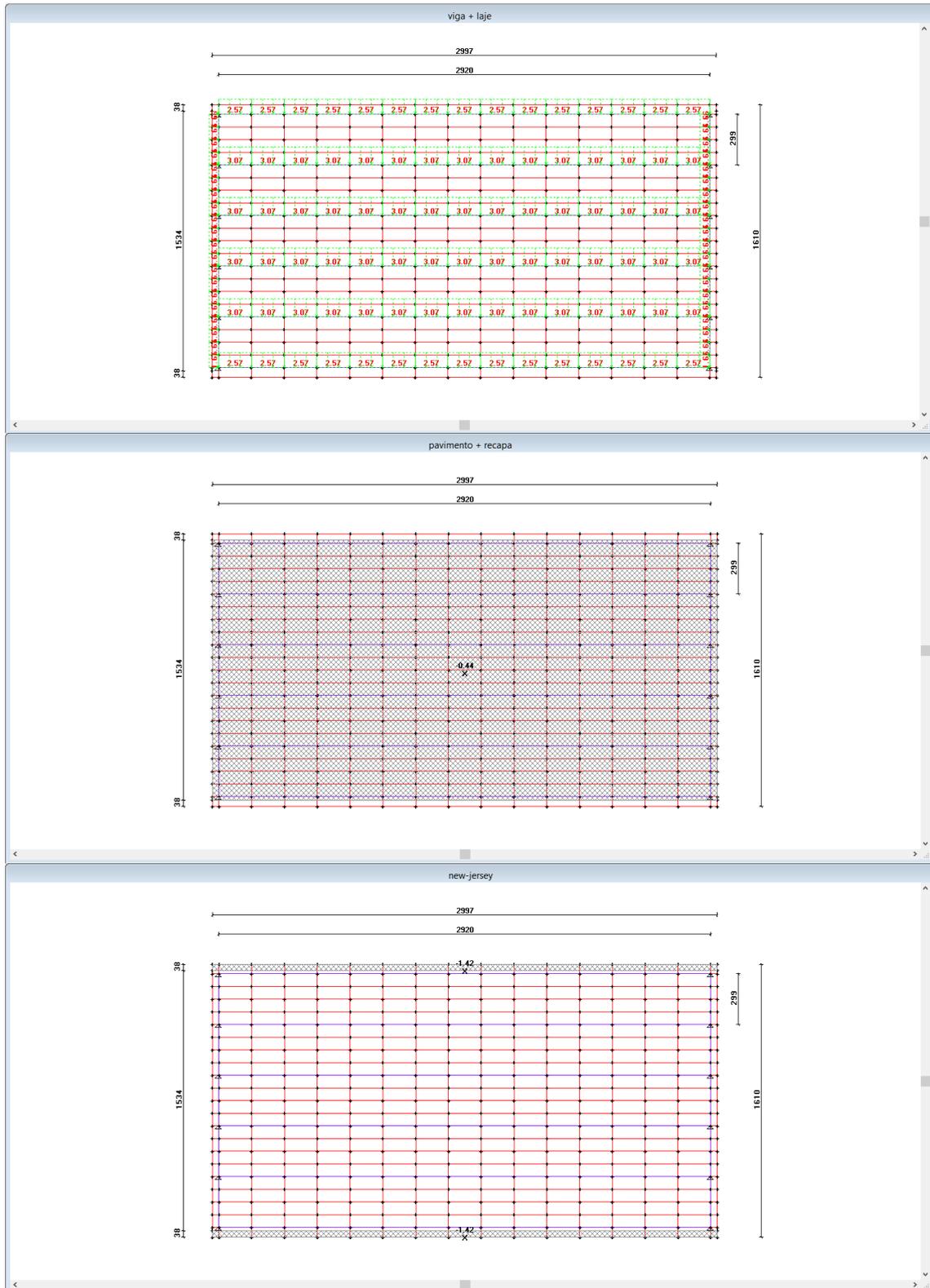


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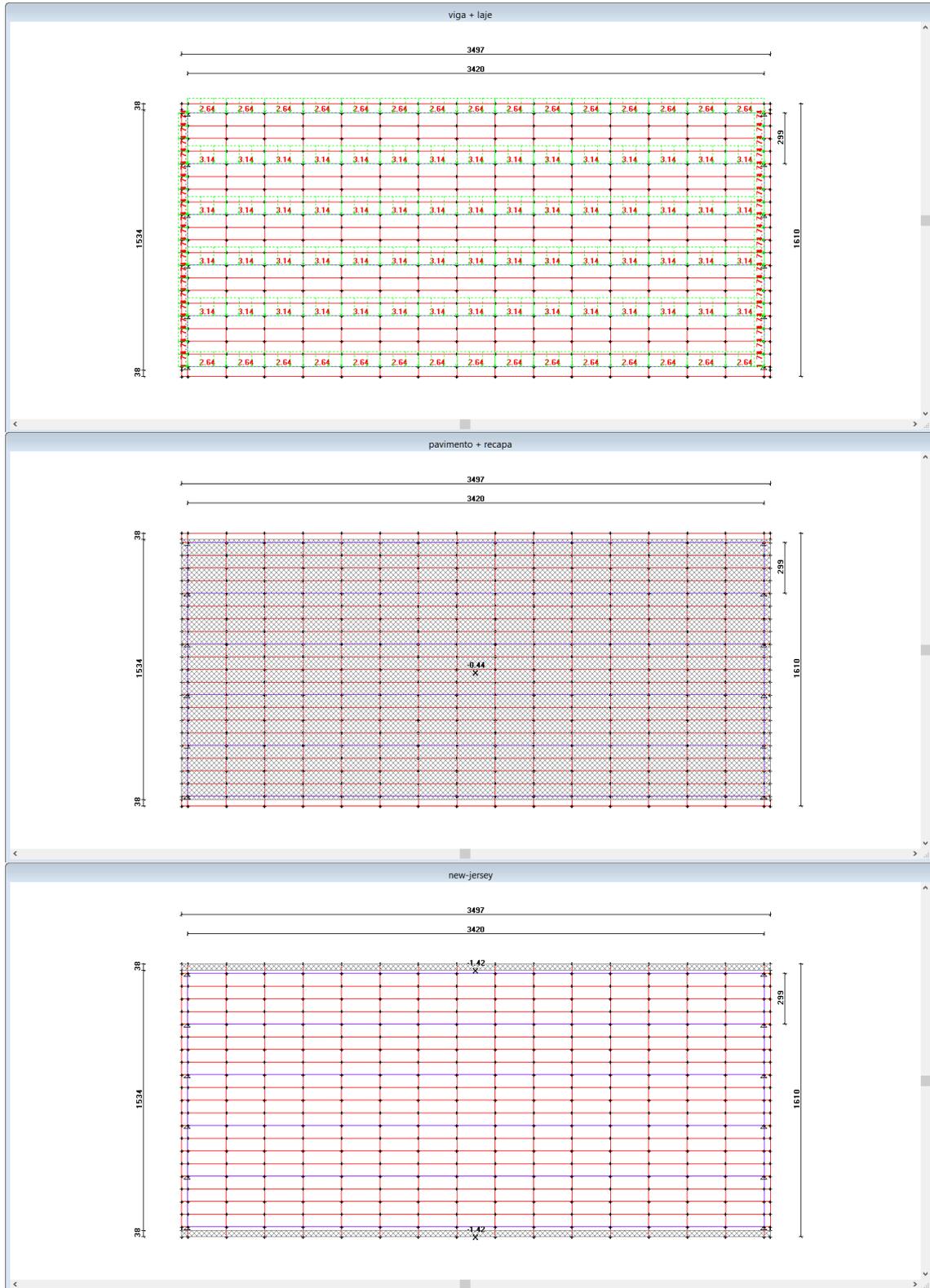


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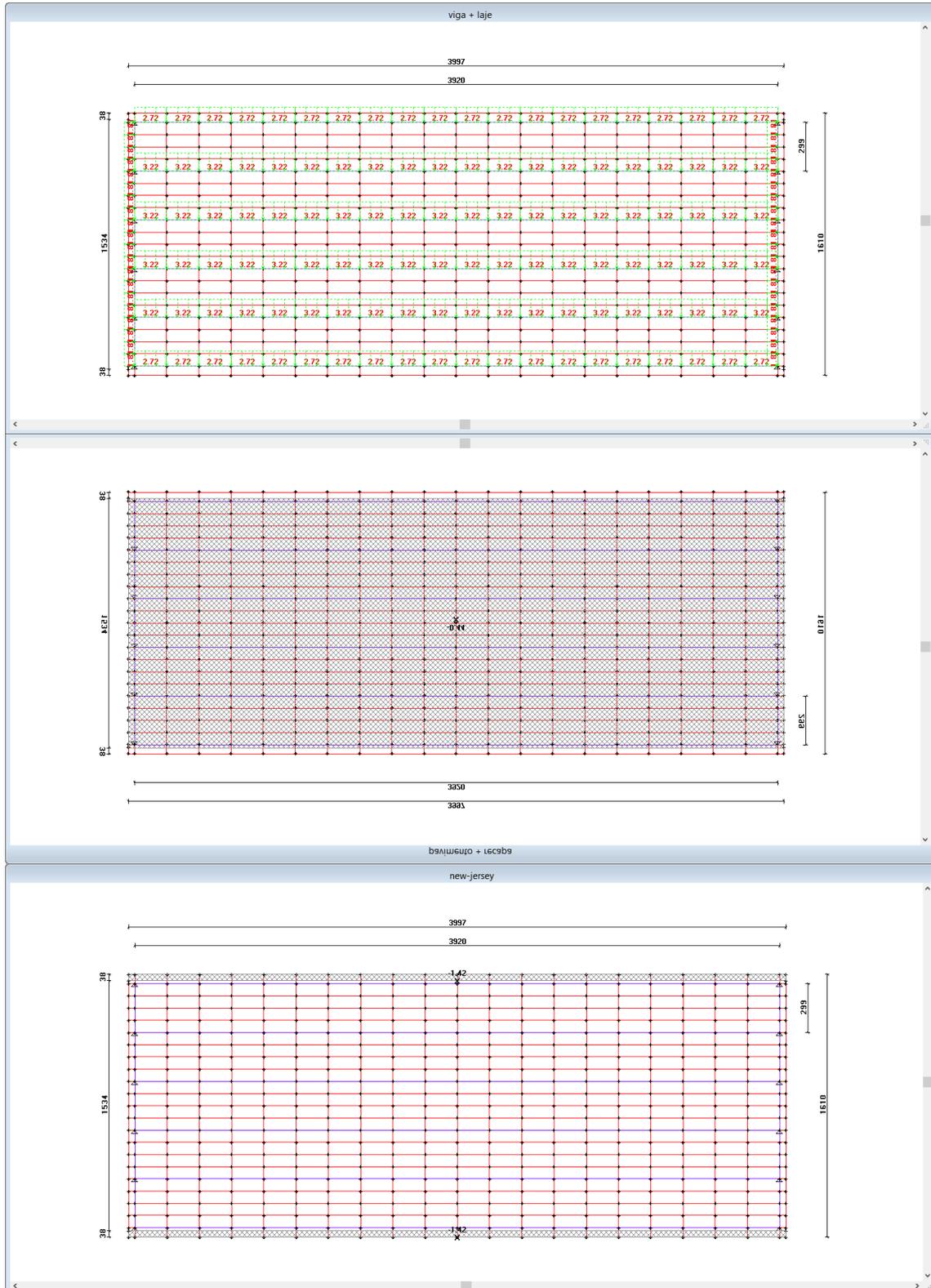


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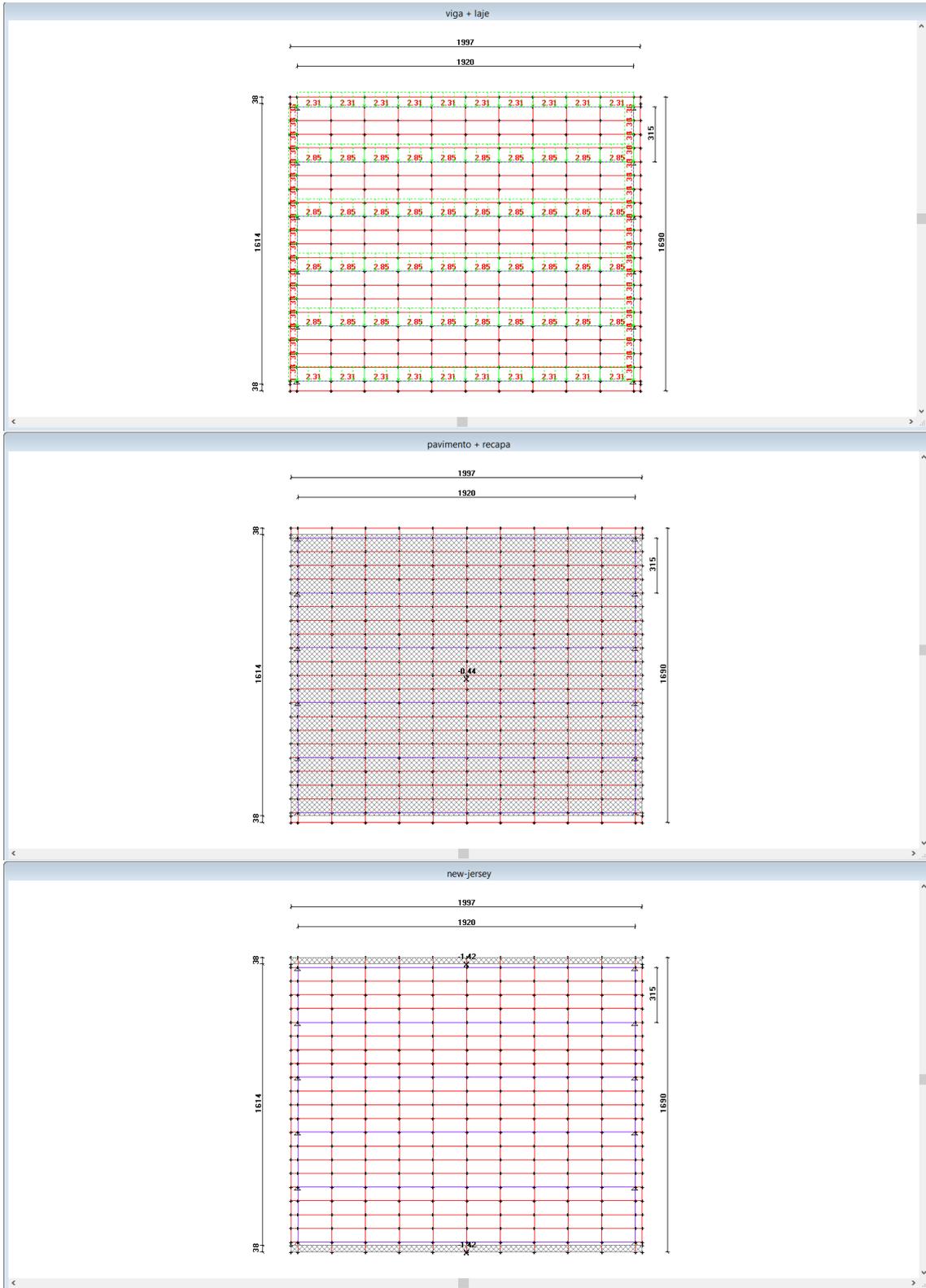
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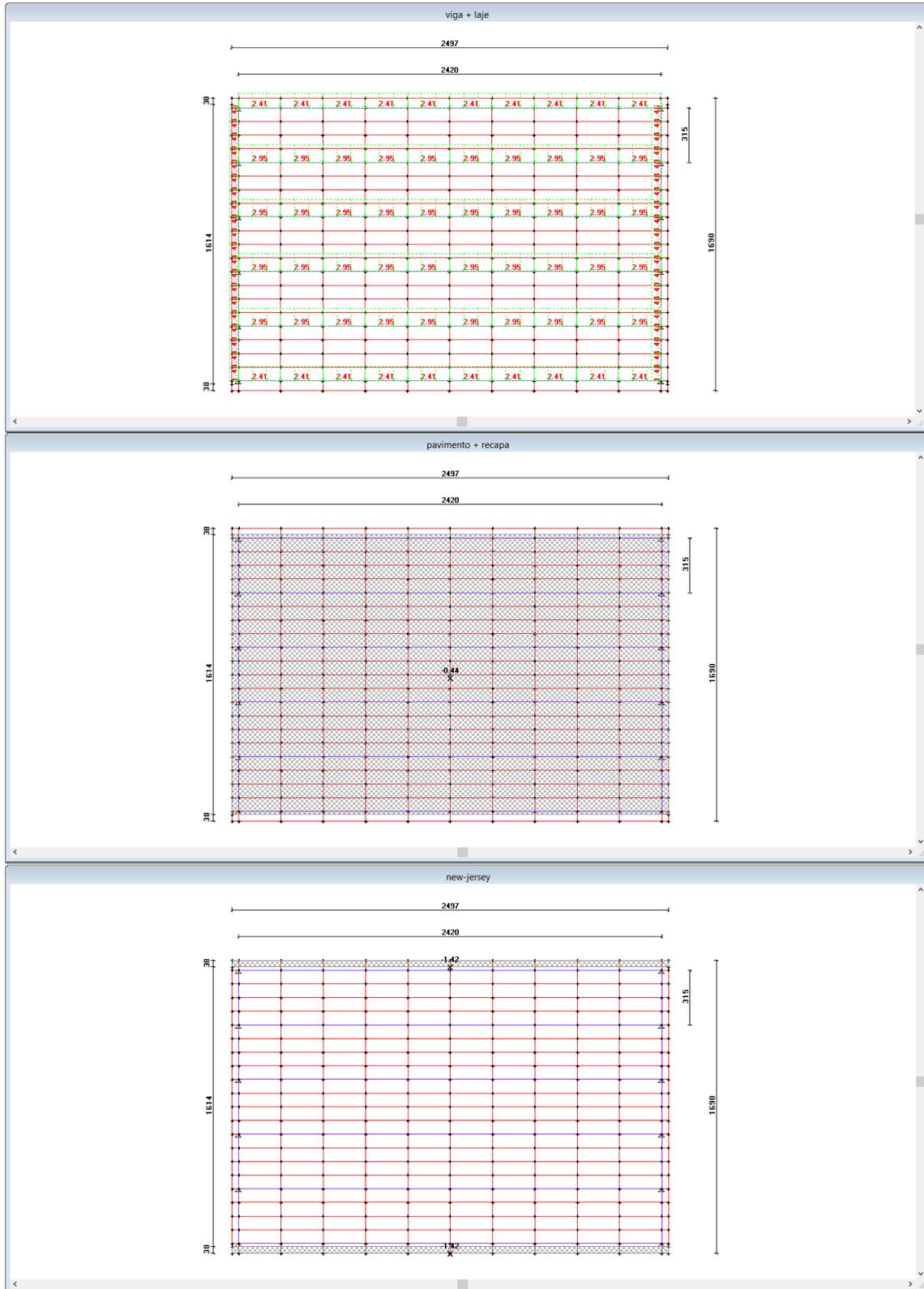
### NOTA TÉCNICA

#### 4.3.5. Tabuleiro 16,90 m



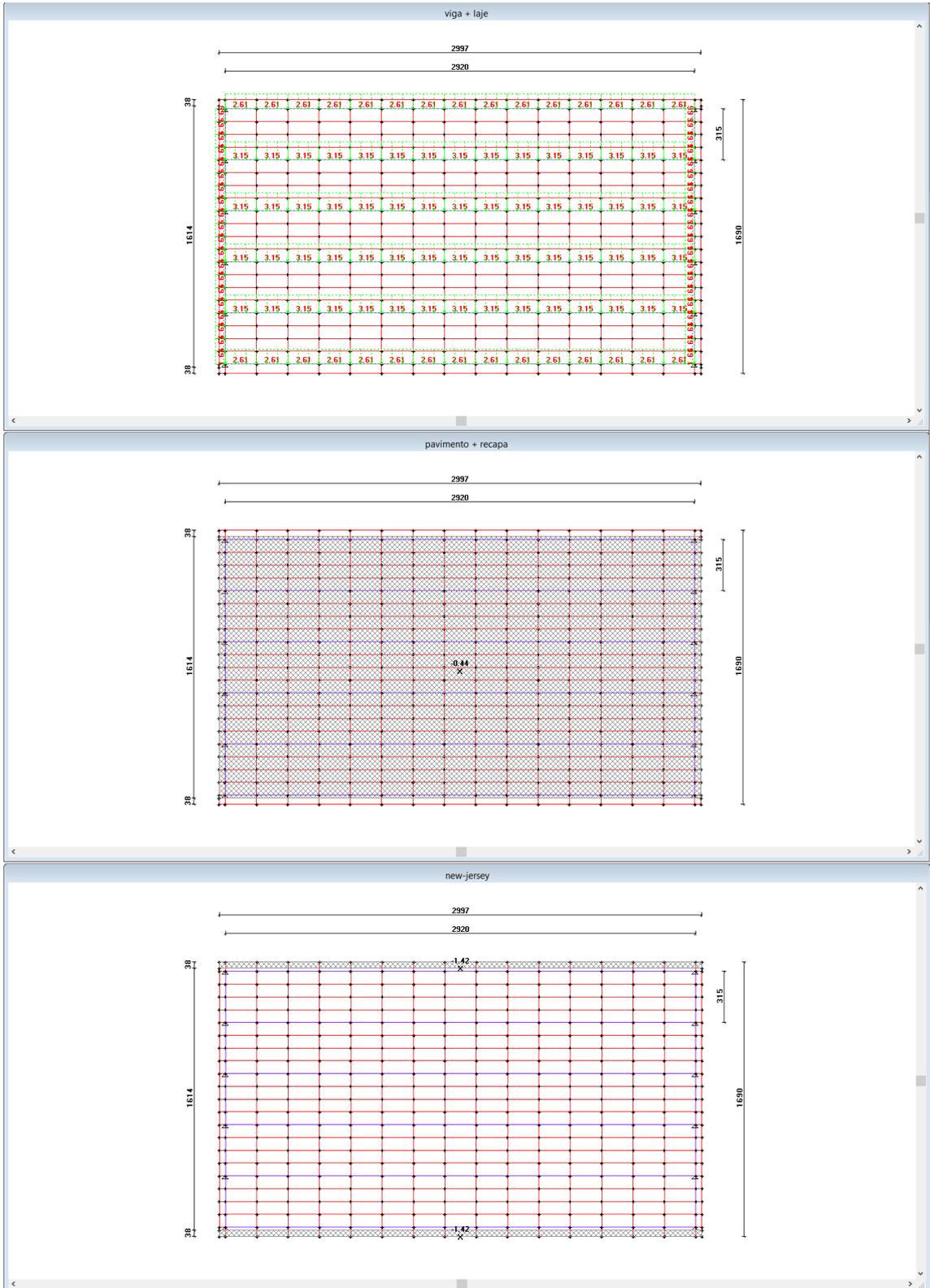


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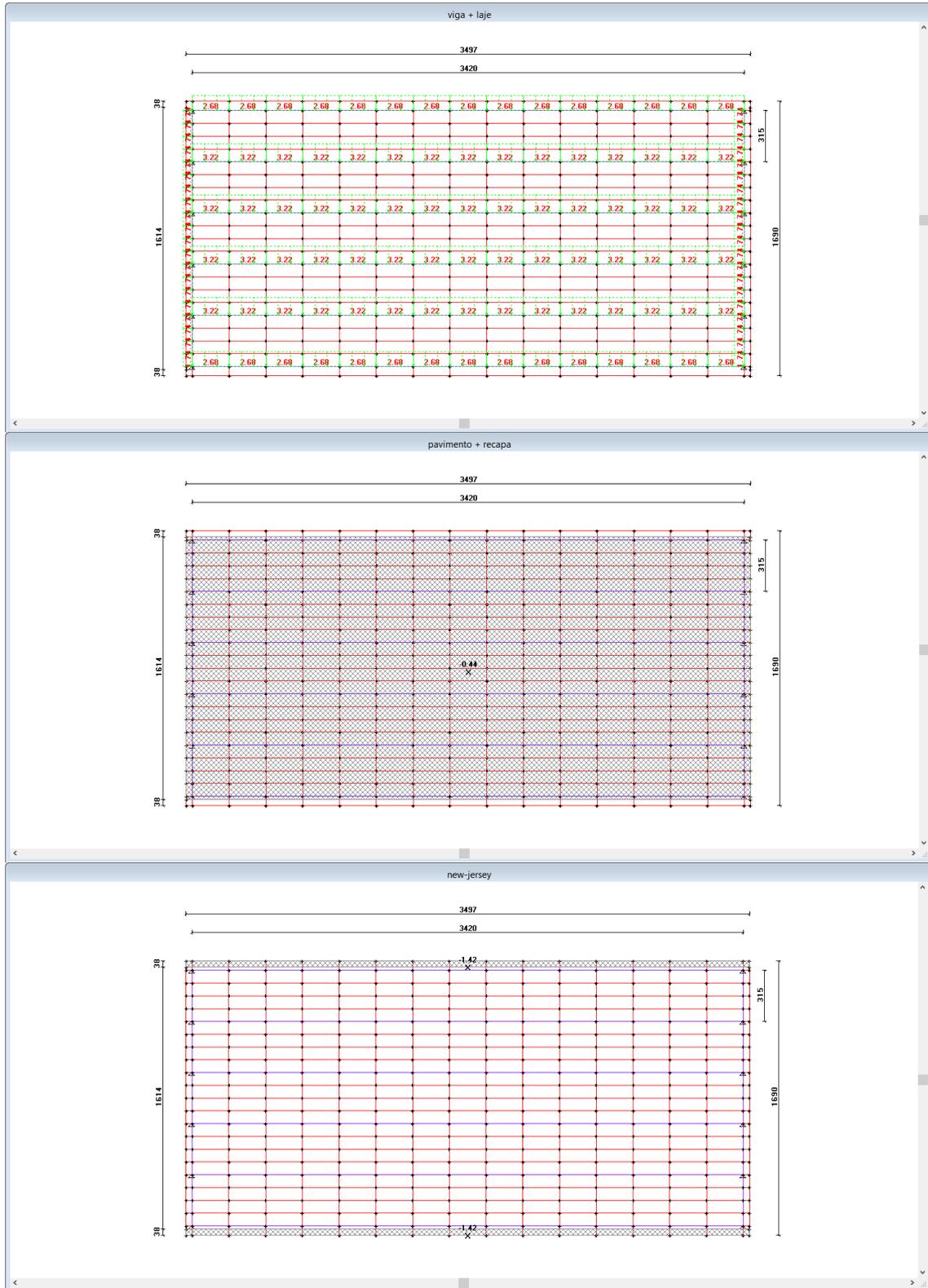


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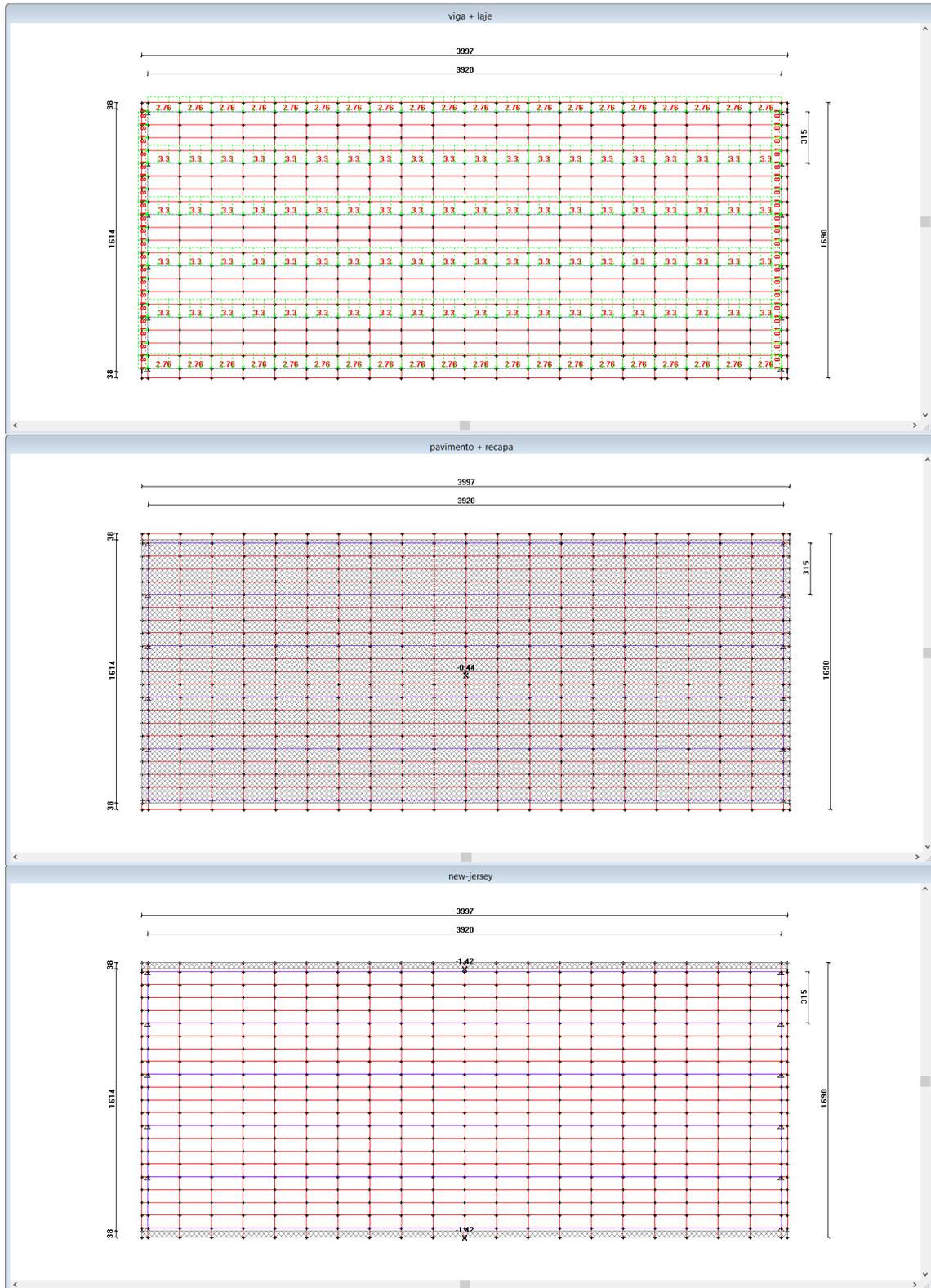


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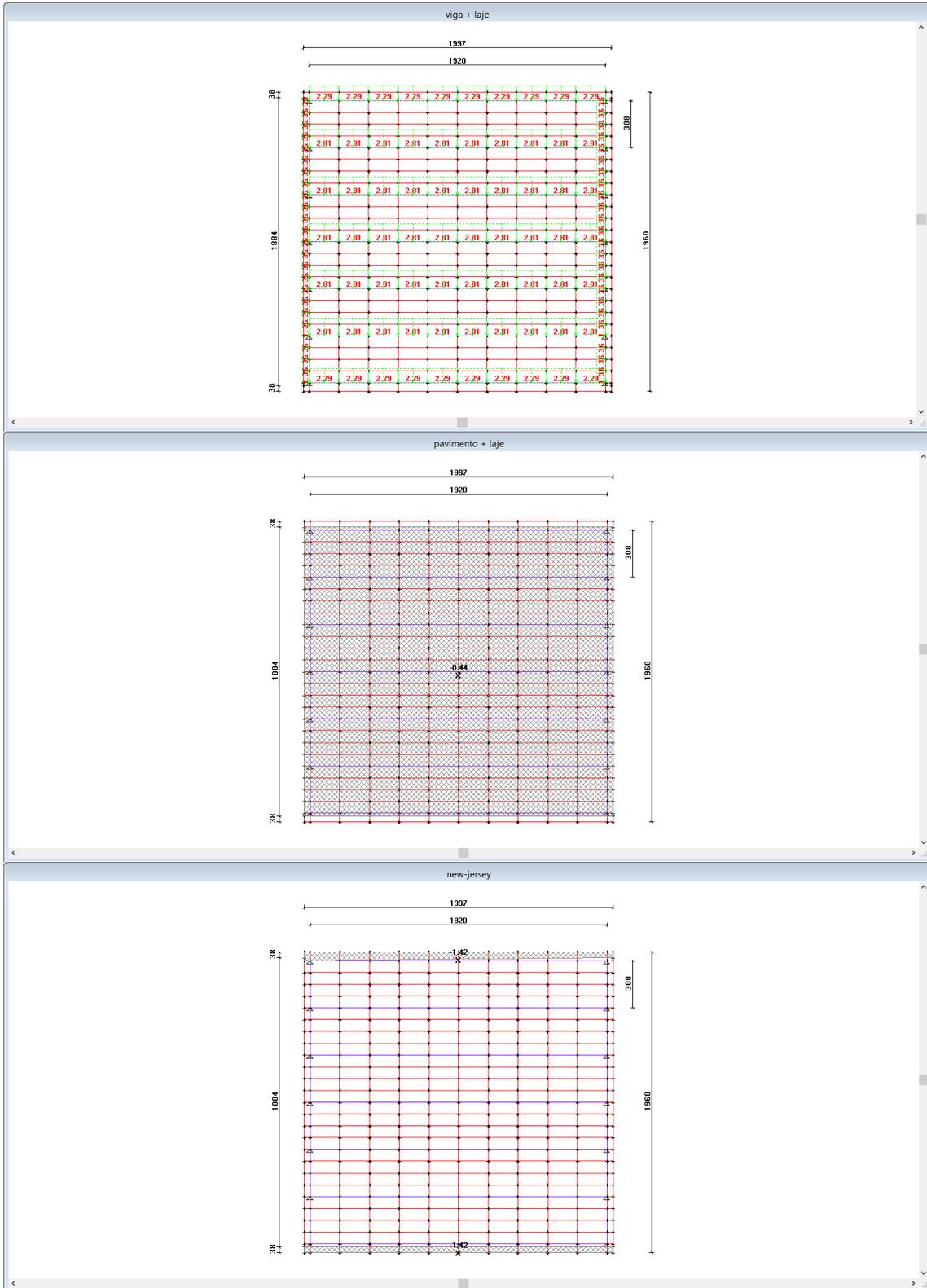
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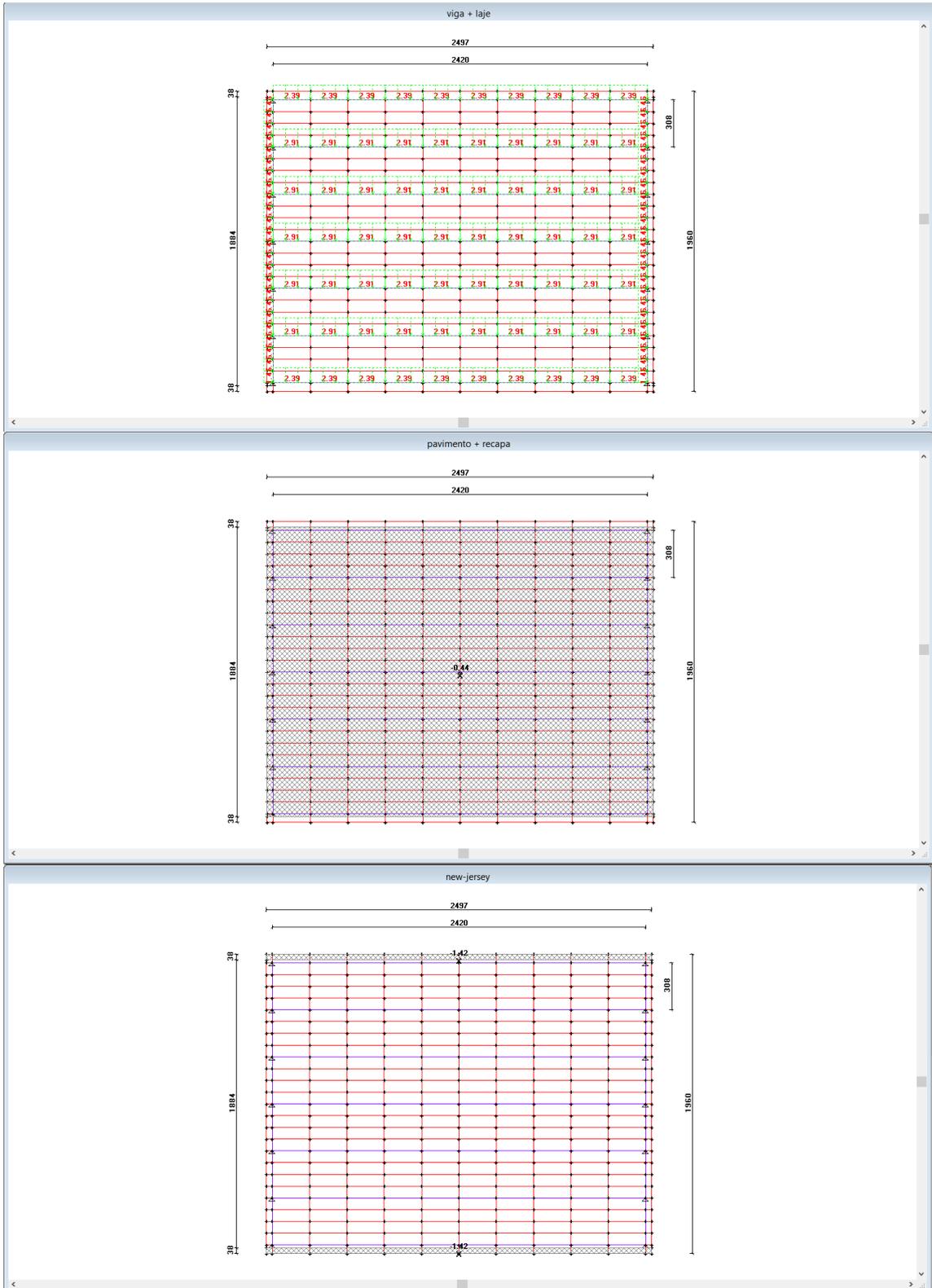
### NOTA TÉCNICA

#### 4.3.6. Tabuleiro 19,60 m



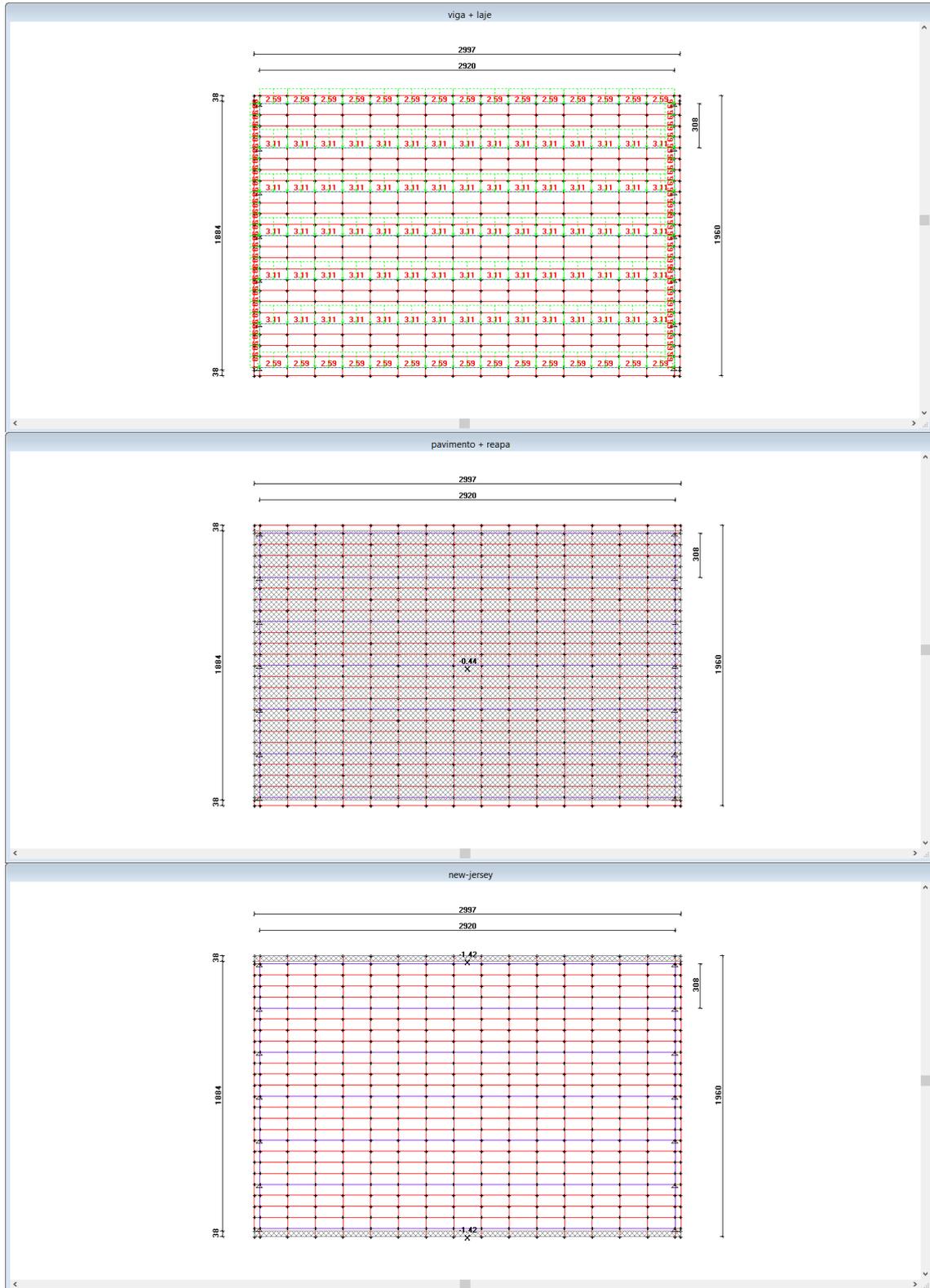


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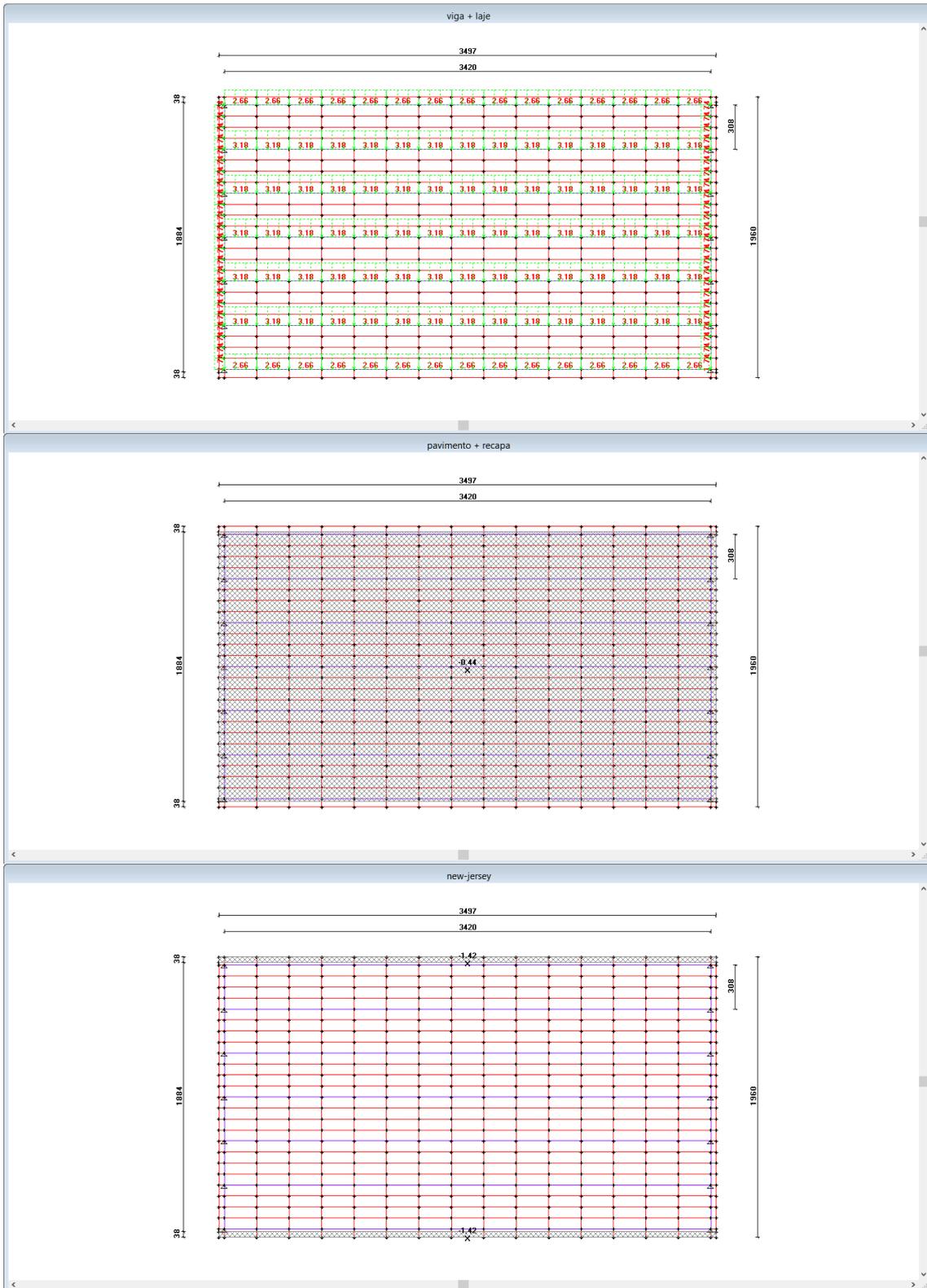


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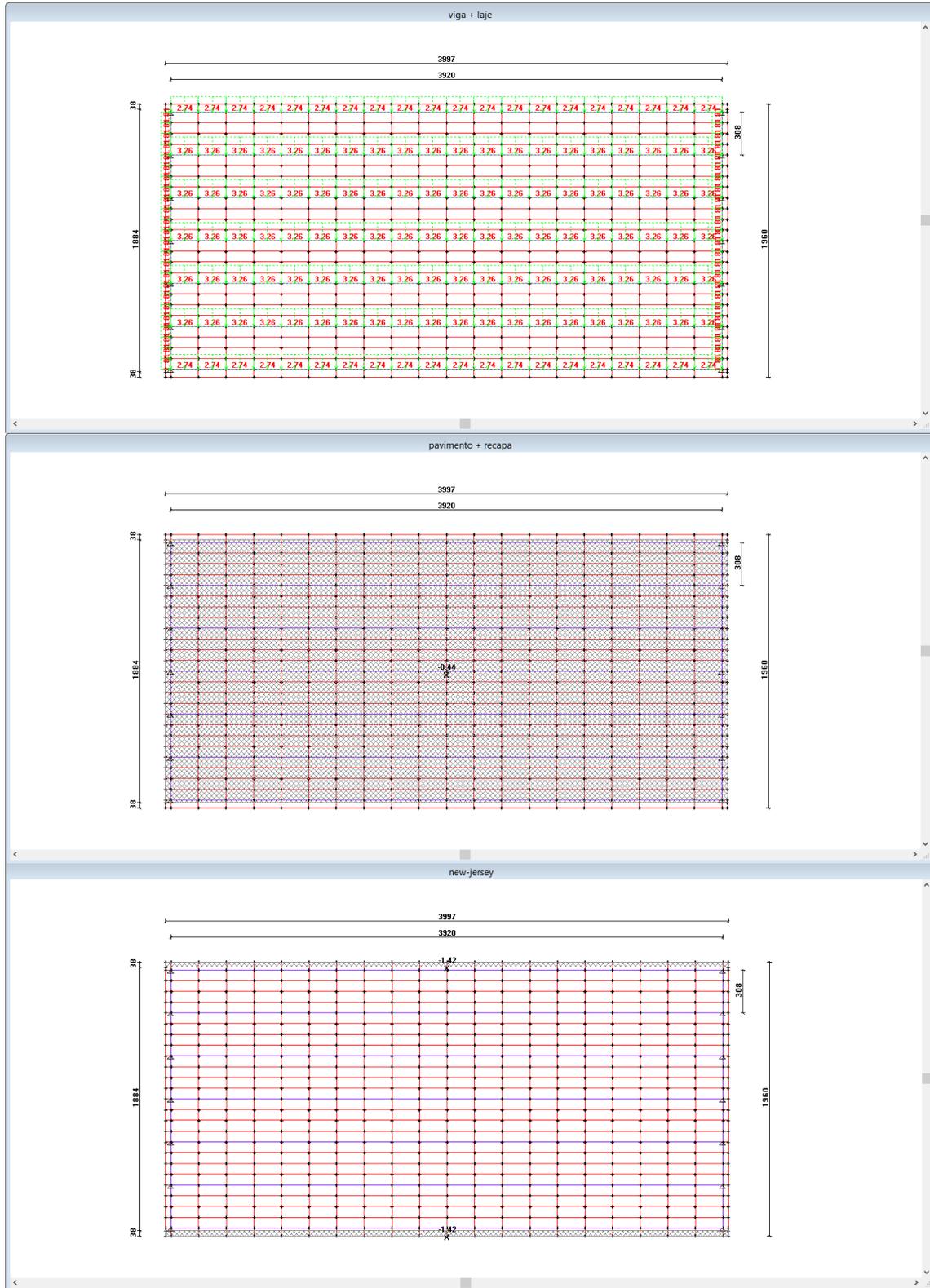


### NOTA TÉCNICA





### NOTA TÉCNICA





## NOTA TÉCNICA

### 4.4. Cargas acidentais – TB-36

Para multidão, inserimos os valores no STRAP multiplicados pelo CIV – Coeficiente de Impacto Vertical:

$$20 \text{ m} \rightarrow \varphi = 1,40 - (0,007 \times 20) = 1,26$$

$$25 \text{ m} \rightarrow \varphi = 1,40 - (0,007 \times 25) = 1,23$$

$$30 \text{ m} \rightarrow \varphi = 1,40 - (0,007 \times 30) = 1,19$$

$$35 \text{ m} \rightarrow \varphi = 1,40 - (0,007 \times 35) = 1,16$$

$$40 \text{ m} \rightarrow \varphi = 1,40 - (0,007 \times 40) = 1,12$$

Adotando a multidão de norma de 0,30 e 0,50 tf/m, a multiplicação resulta em:

$$20 \text{ m} \rightarrow 1,26 \times 0,30 = 0,38 \text{ tf/m}$$

$$1,26 \times 0,50 = 0,63 \text{ tf/m}$$

$$25 \text{ m} \rightarrow 1,23 \times 0,30 = 0,37 \text{ tf/m}$$

$$1,23 \times 0,50 = 0,62 \text{ tf/m}$$

$$30 \text{ m} \rightarrow 1,19 \times 0,30 = 0,36 \text{ tf/m}$$

$$1,19 \times 0,50 = 0,60 \text{ tf/m}$$

$$35 \text{ m} \rightarrow 1,16 \times 0,30 = 0,35 \text{ tf/m}$$

$$1,16 \times 0,50 = 0,58 \text{ tf/m}$$

$$40 \text{ m} \rightarrow 1,12 \times 0,30 = 0,34 \text{ tf/m}$$

$$1,12 \times 0,50 = 0,56 \text{ tf/m}$$

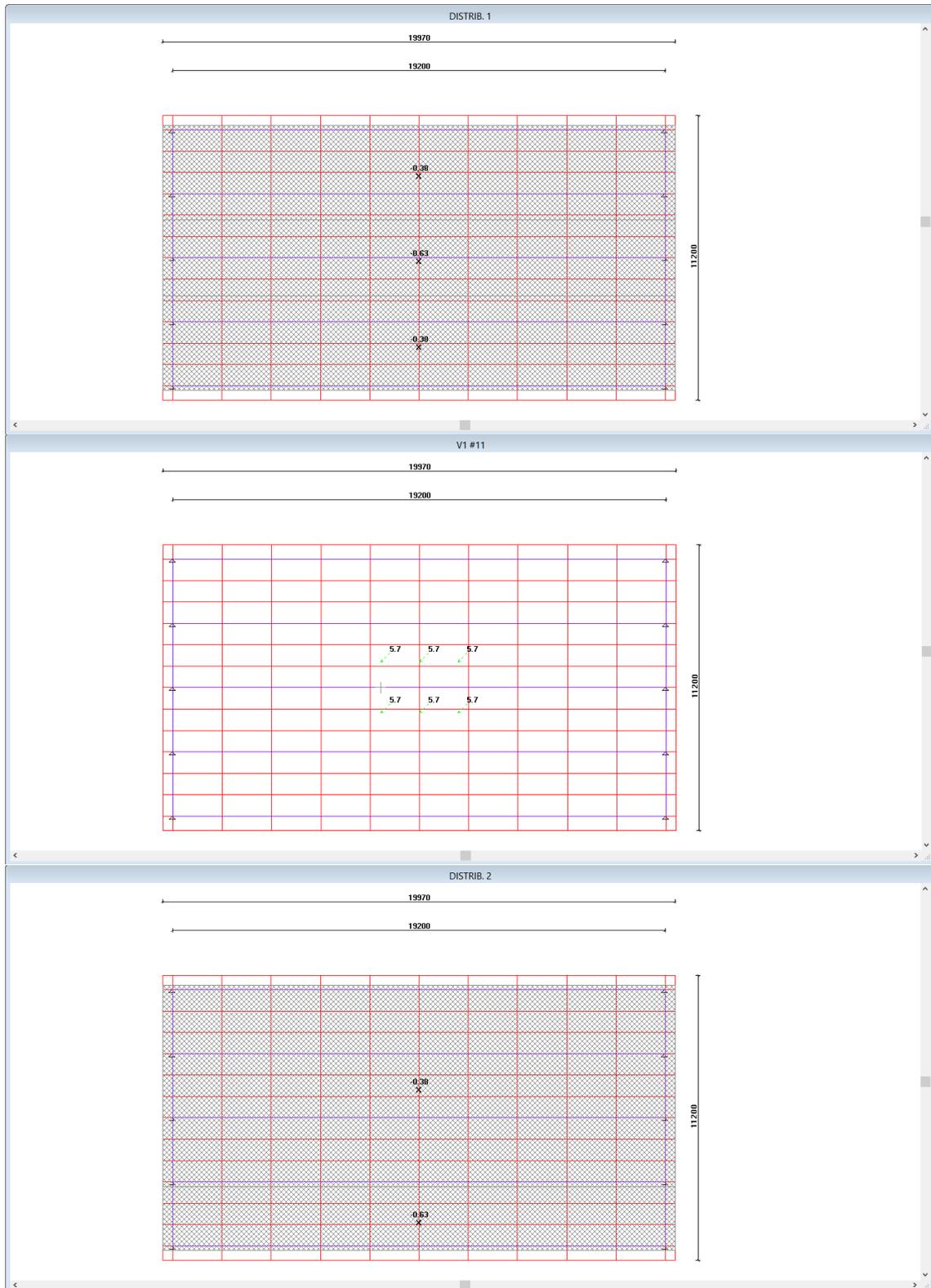
O veículo TB-36 foi homogeneizado com um coeficiente de 0,945, o que resultou em:

$$6 \times 0,945 = 5,67 \text{ tf por roda do veículo}$$



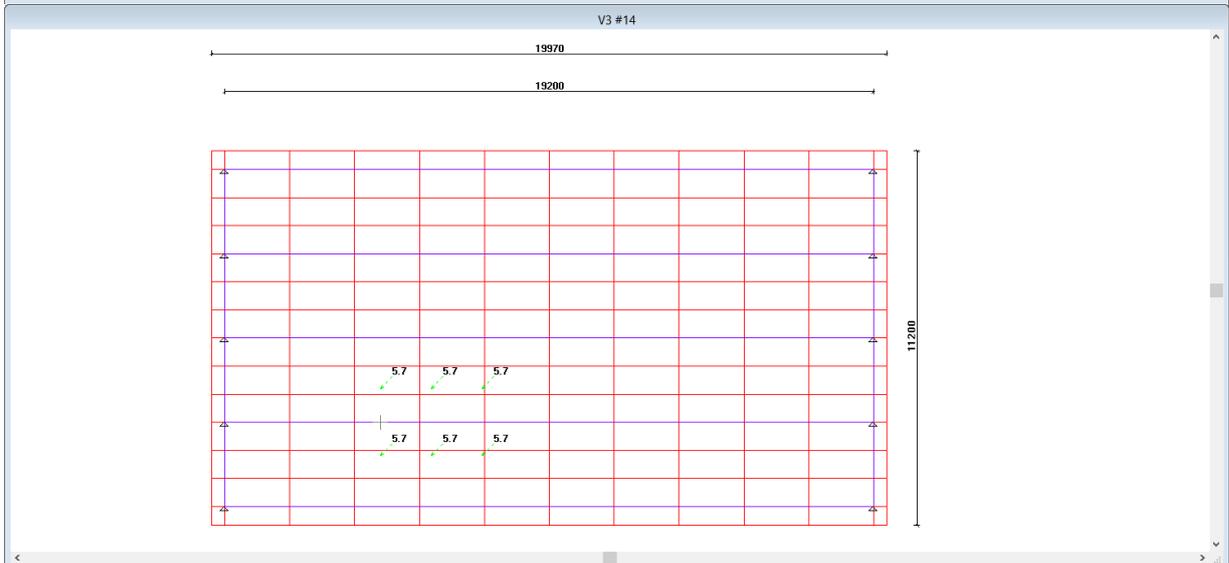
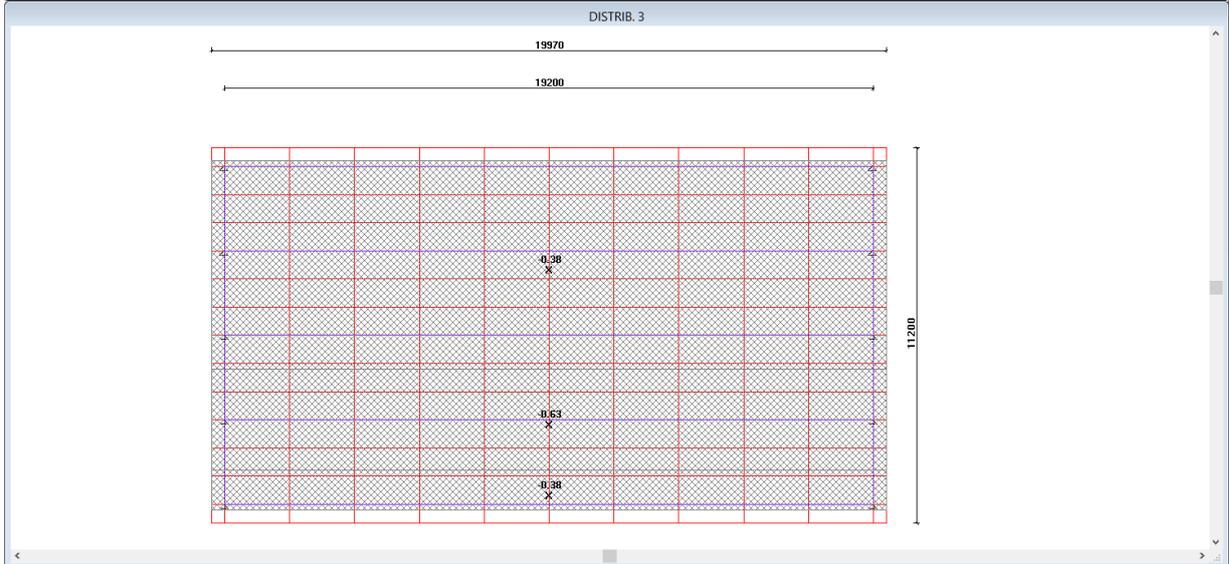
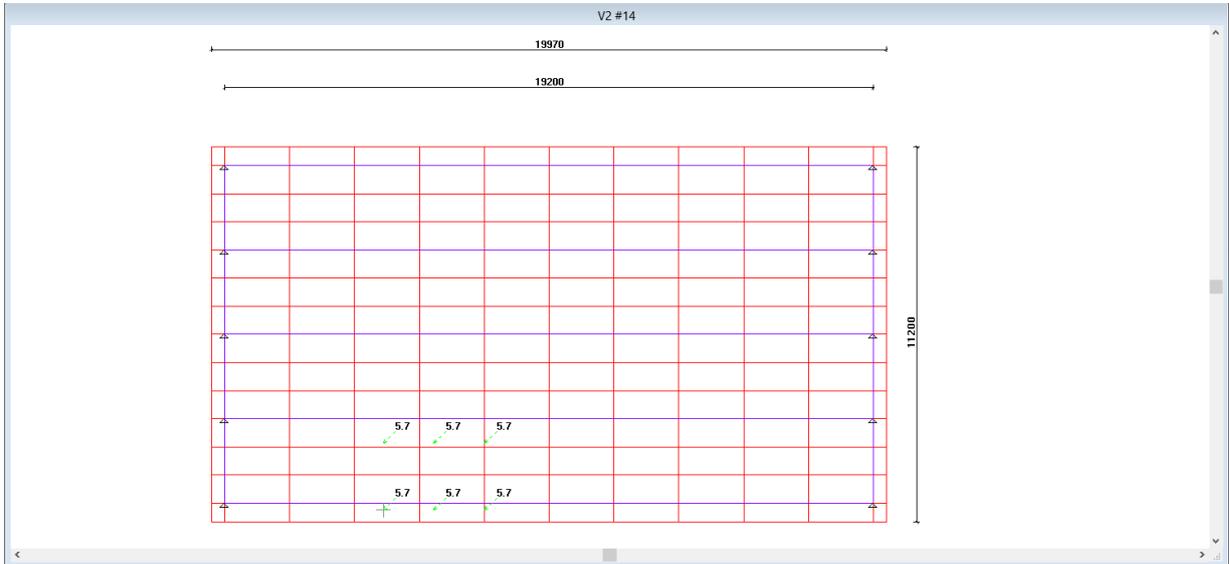
### NOTA TÉCNICA

#### 4.4.1. Tabuleiro 11,20 m



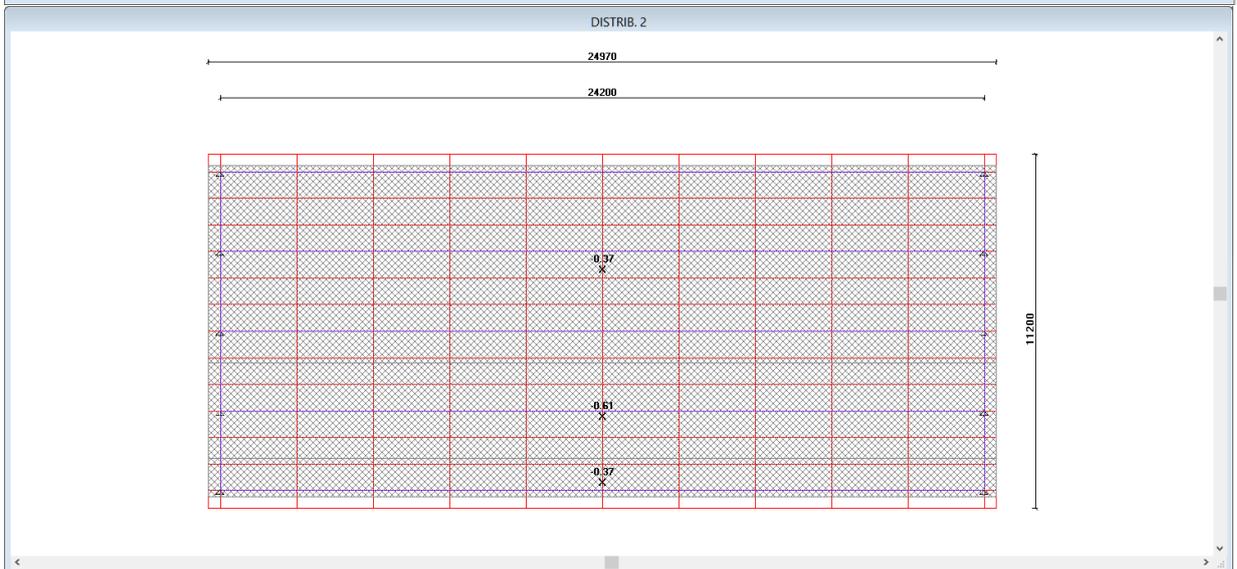
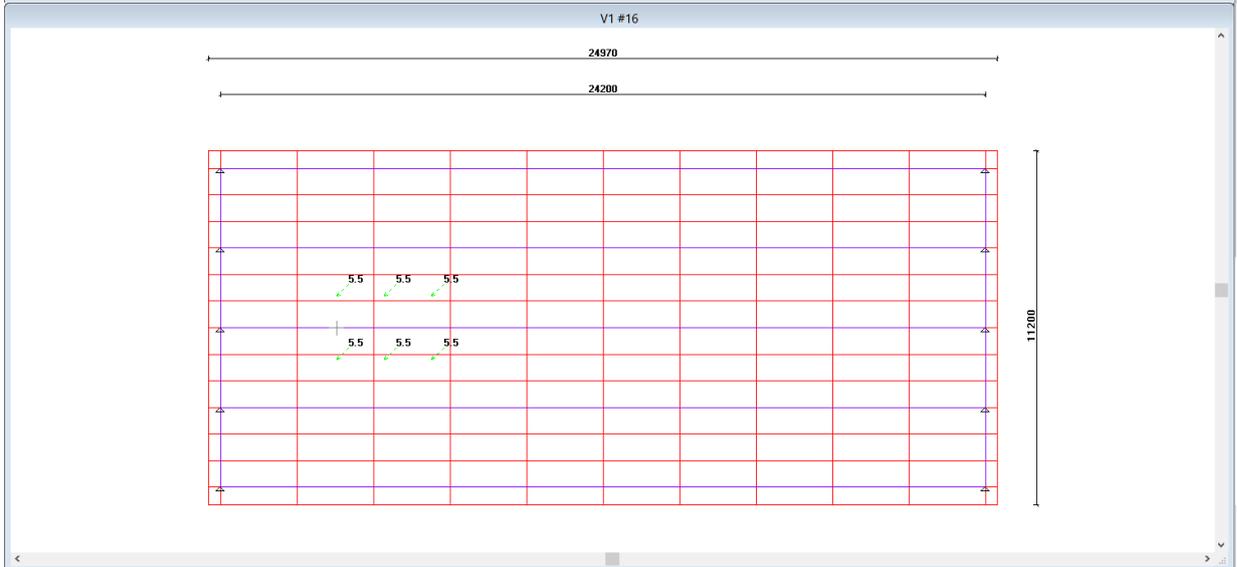
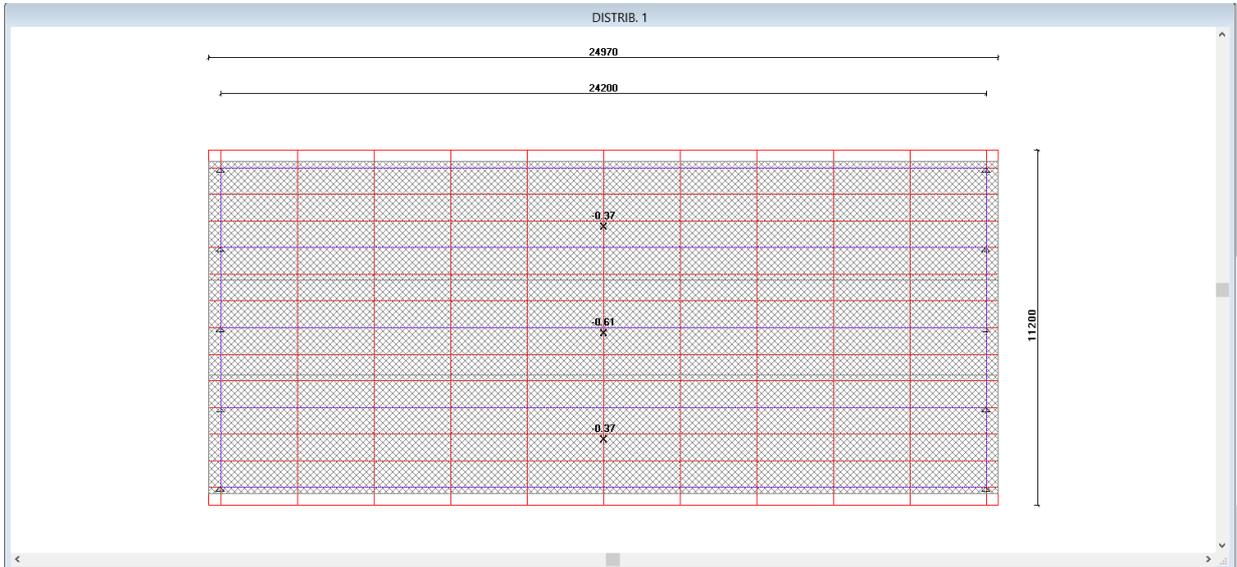


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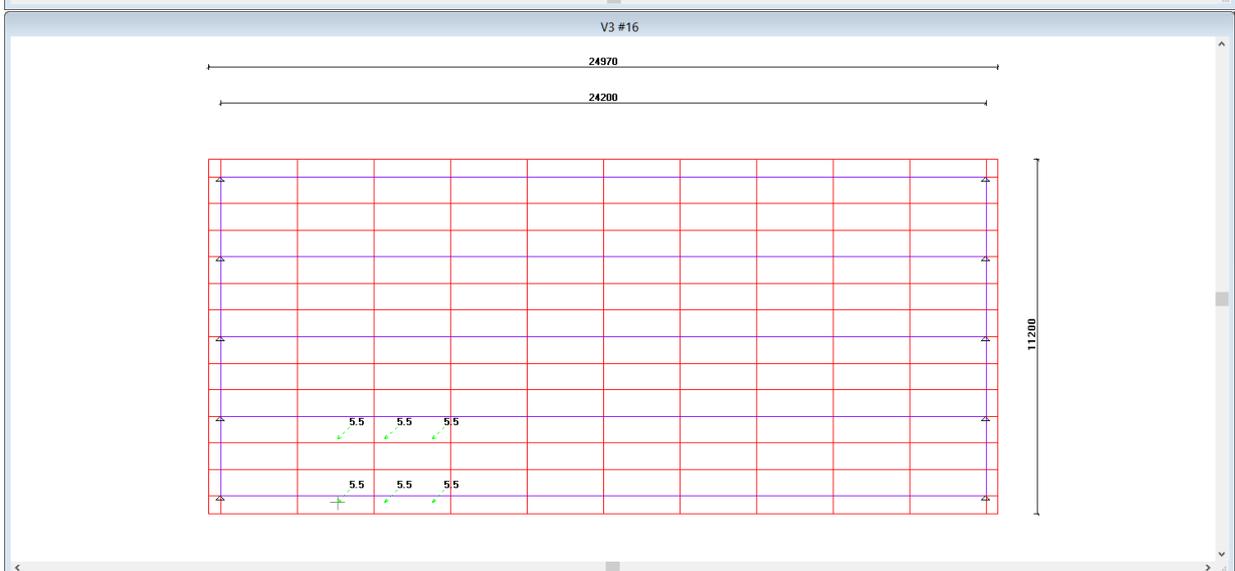
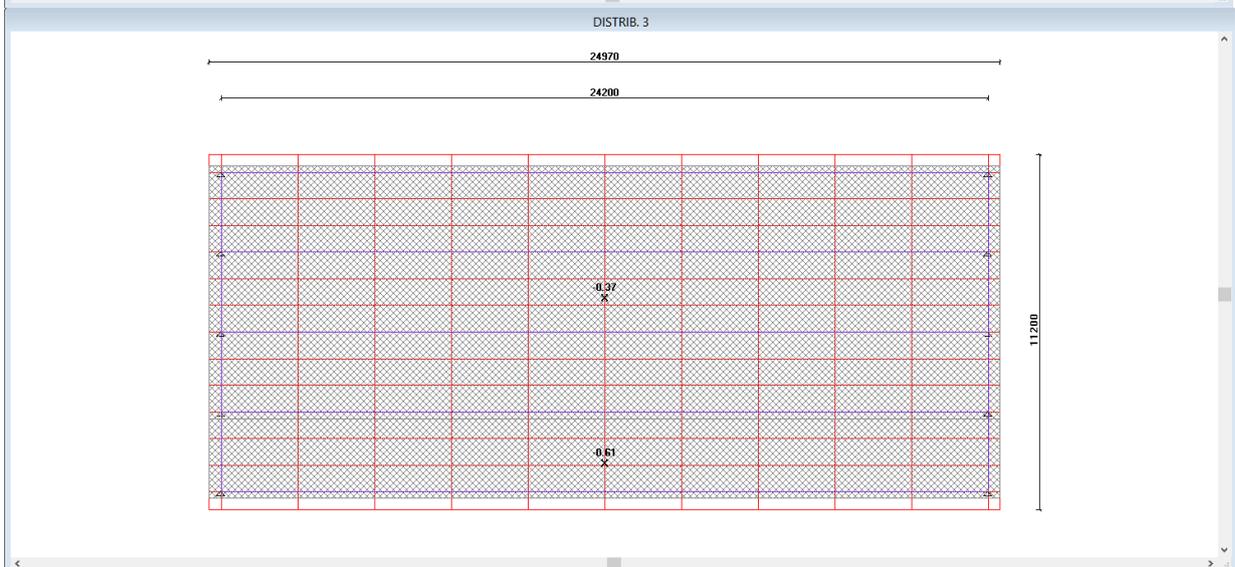
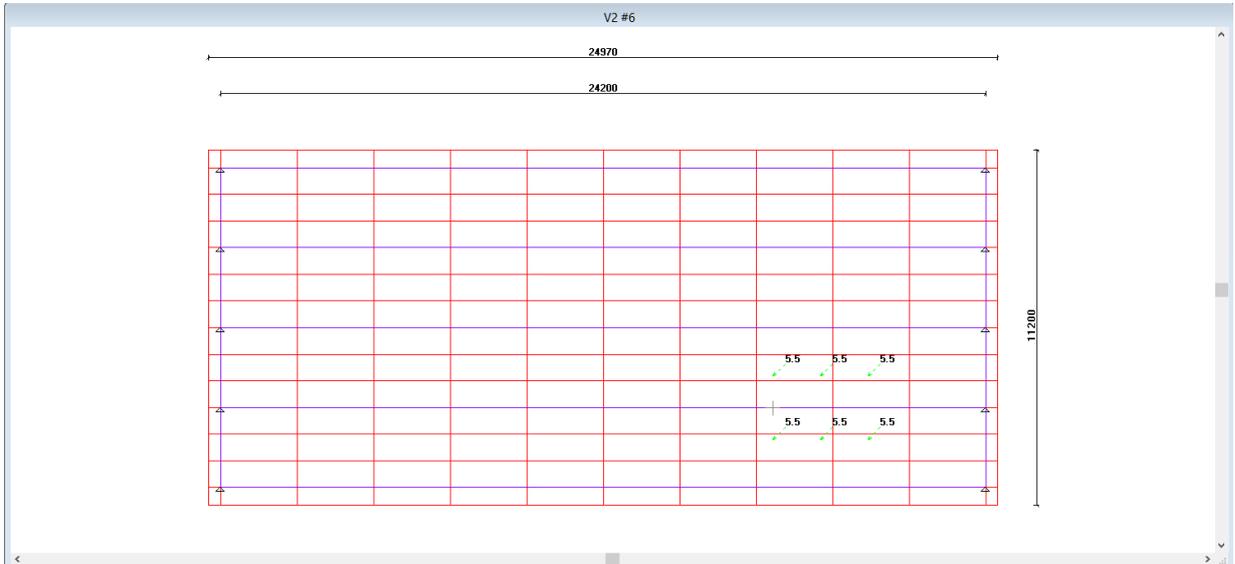


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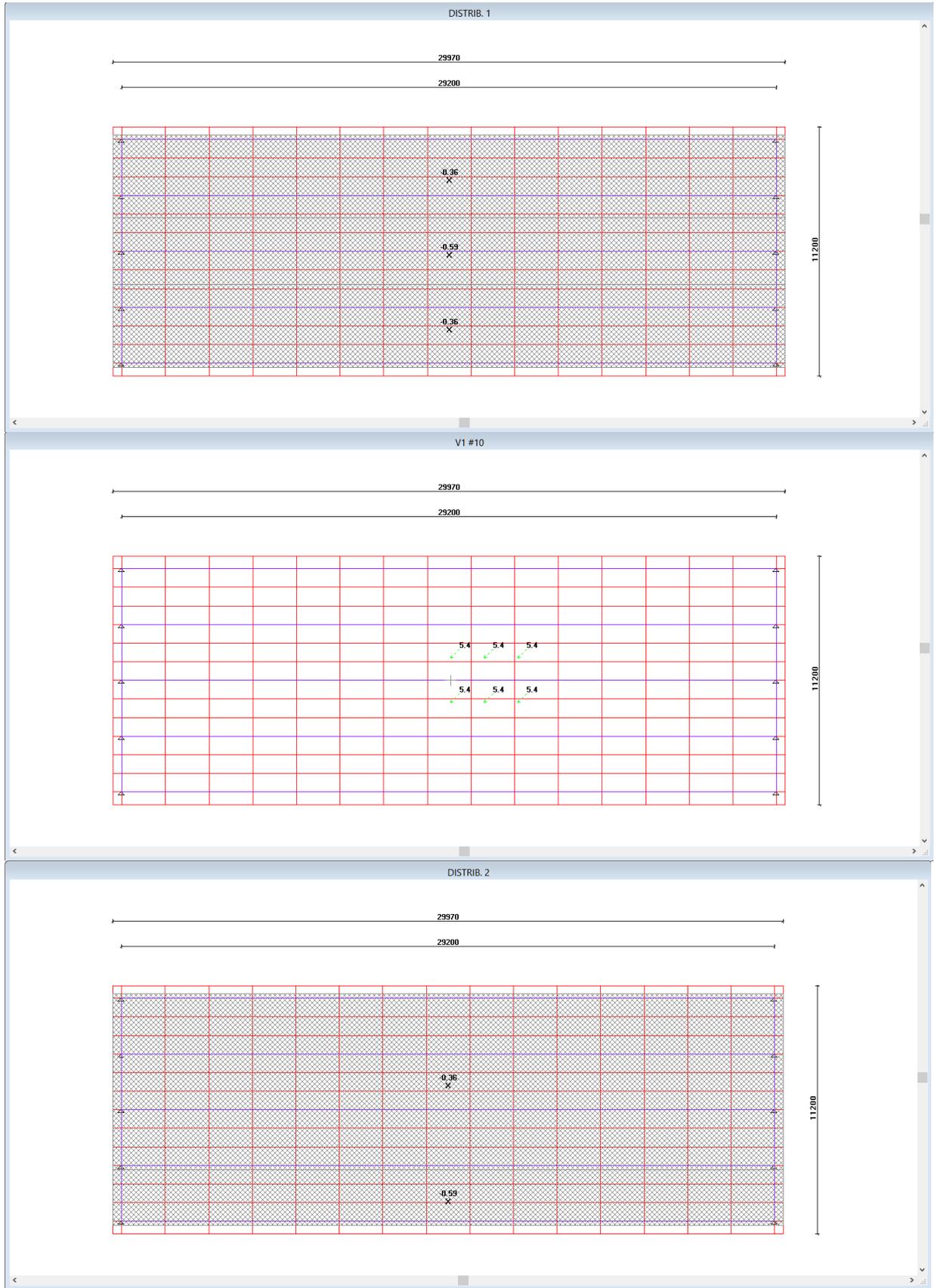


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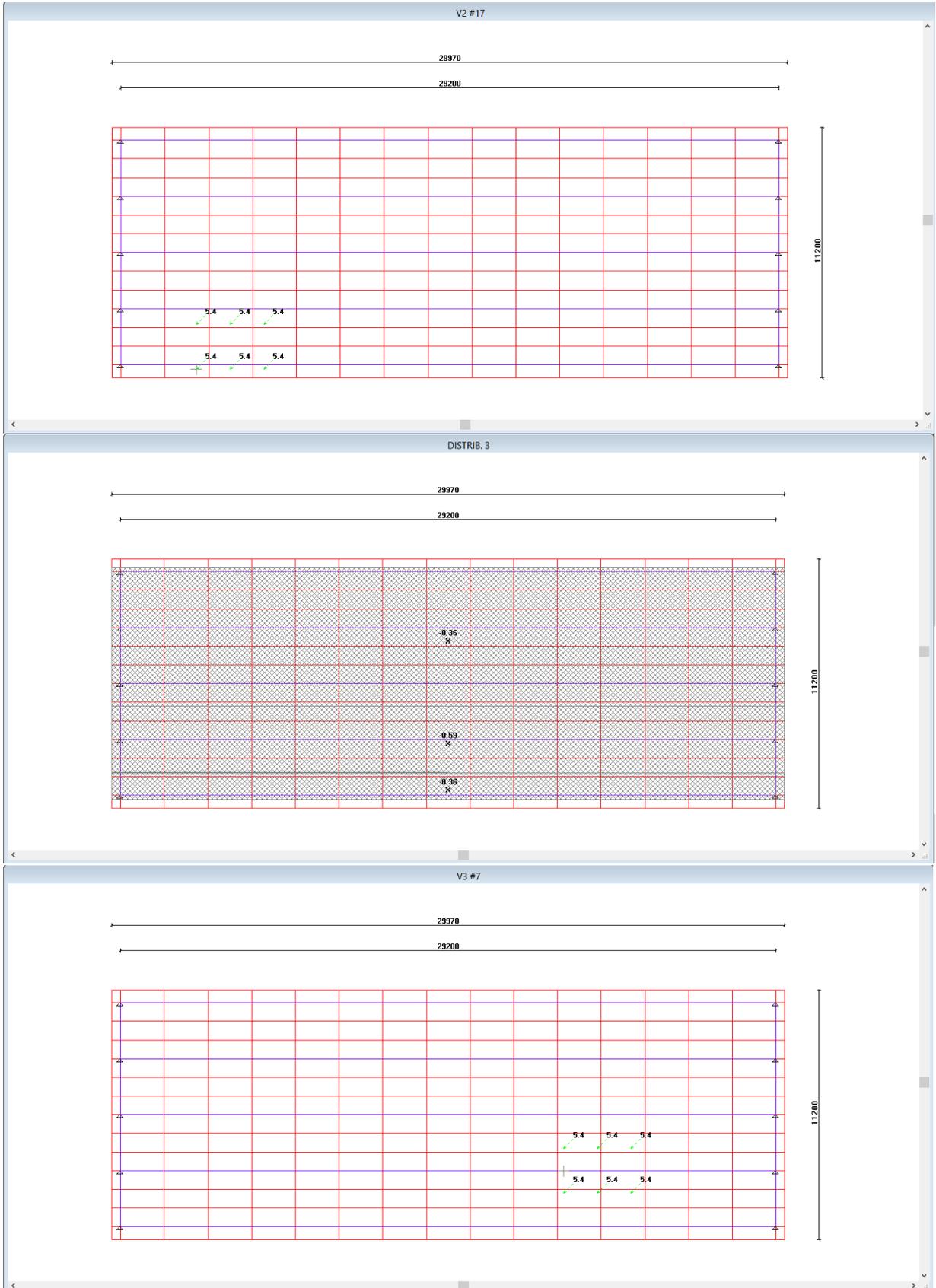


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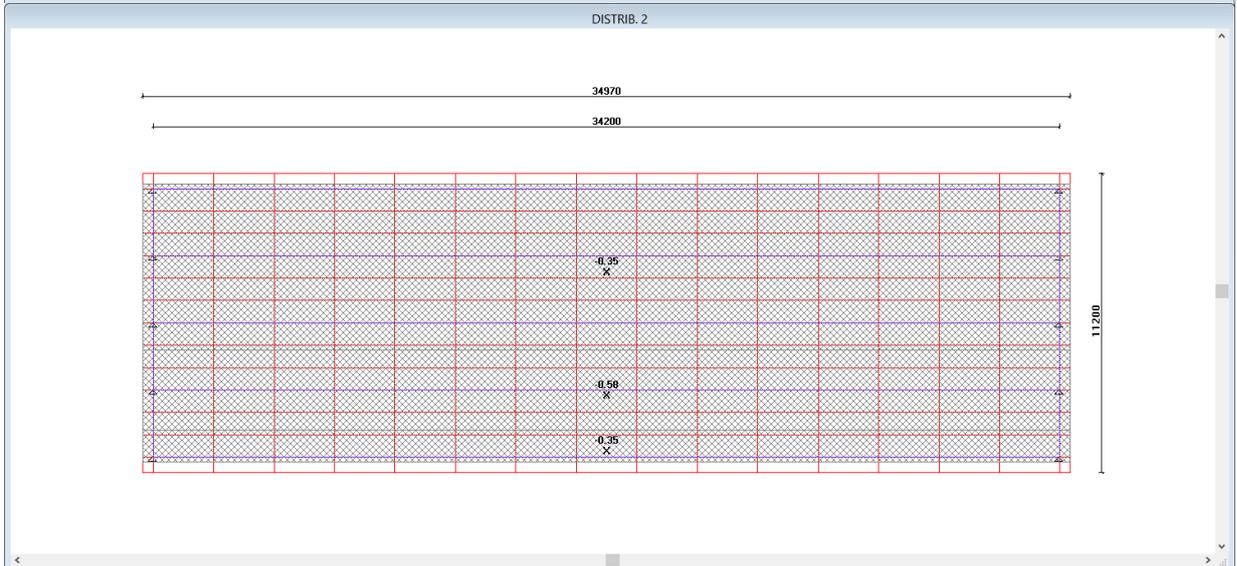
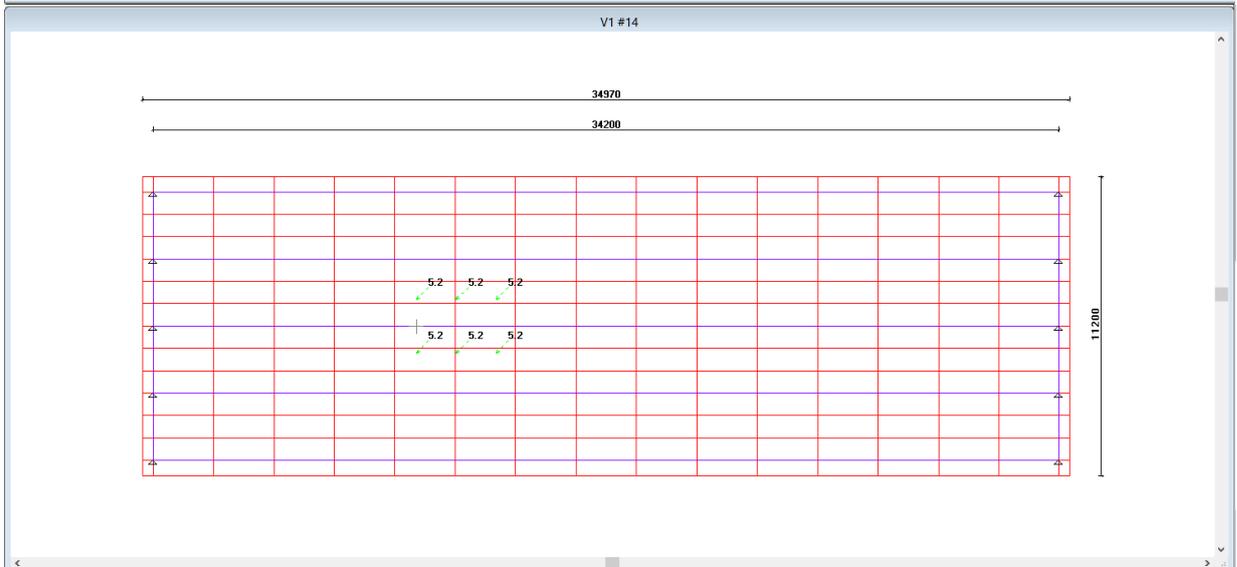
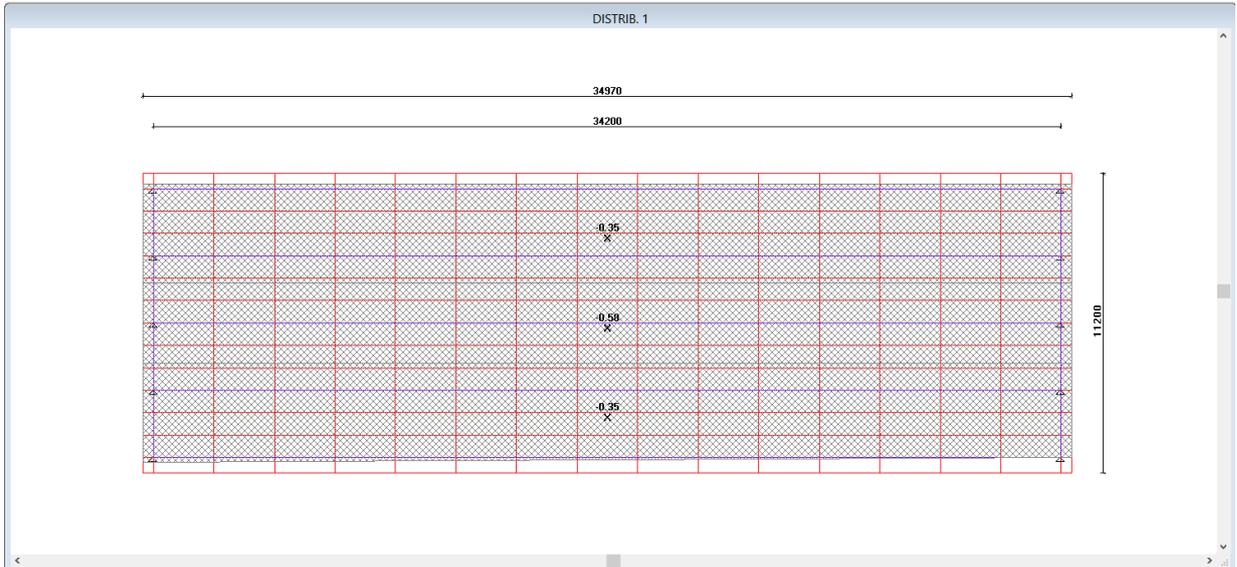


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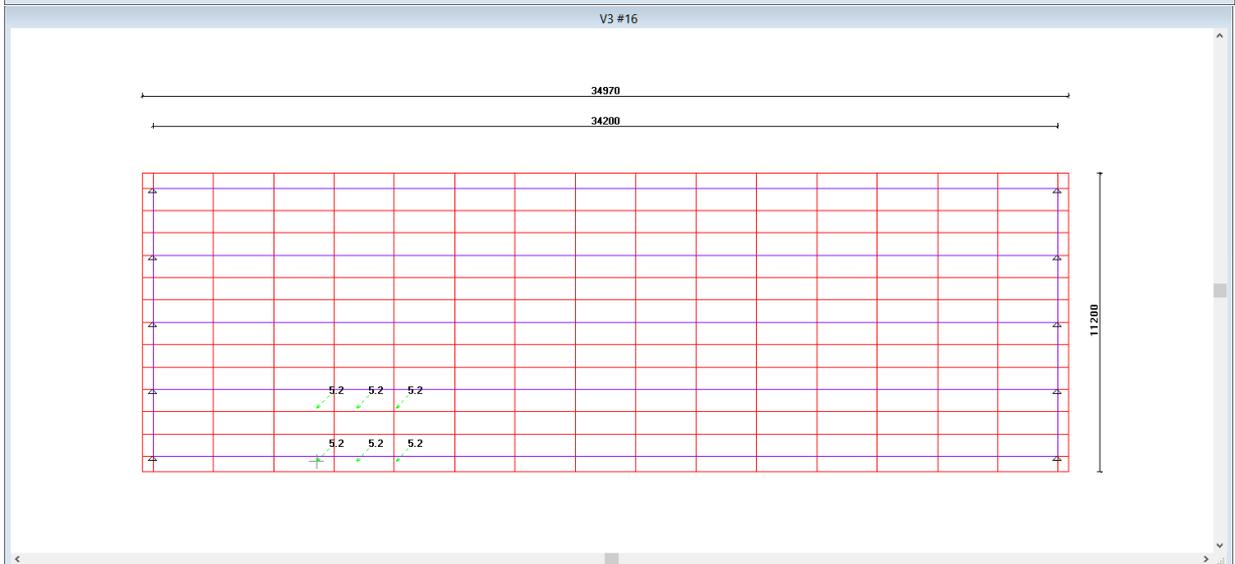
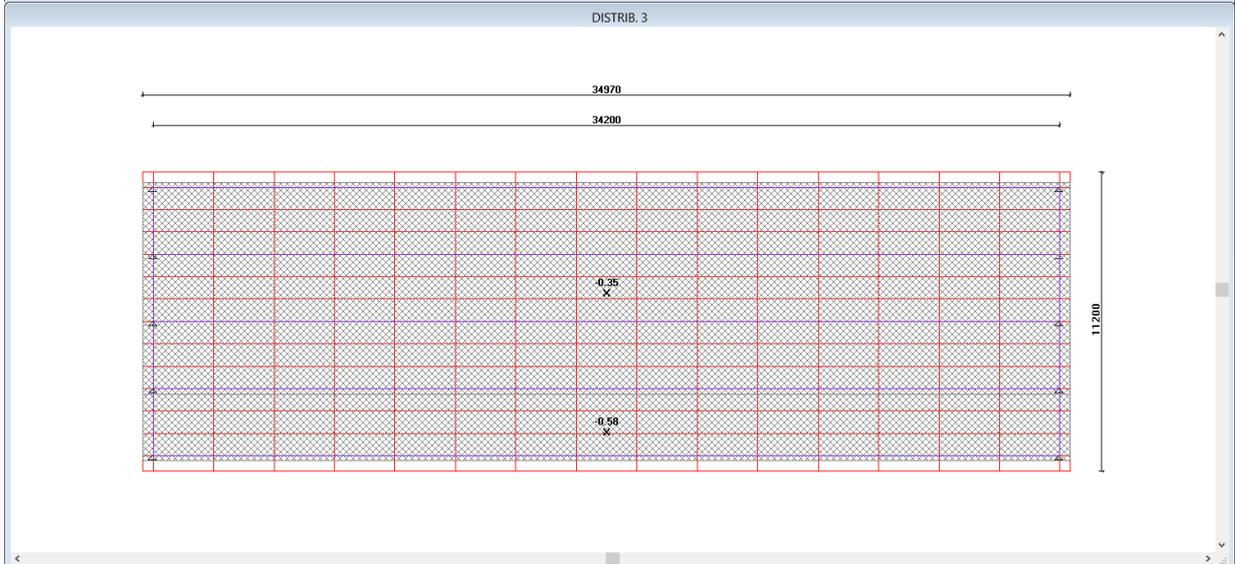
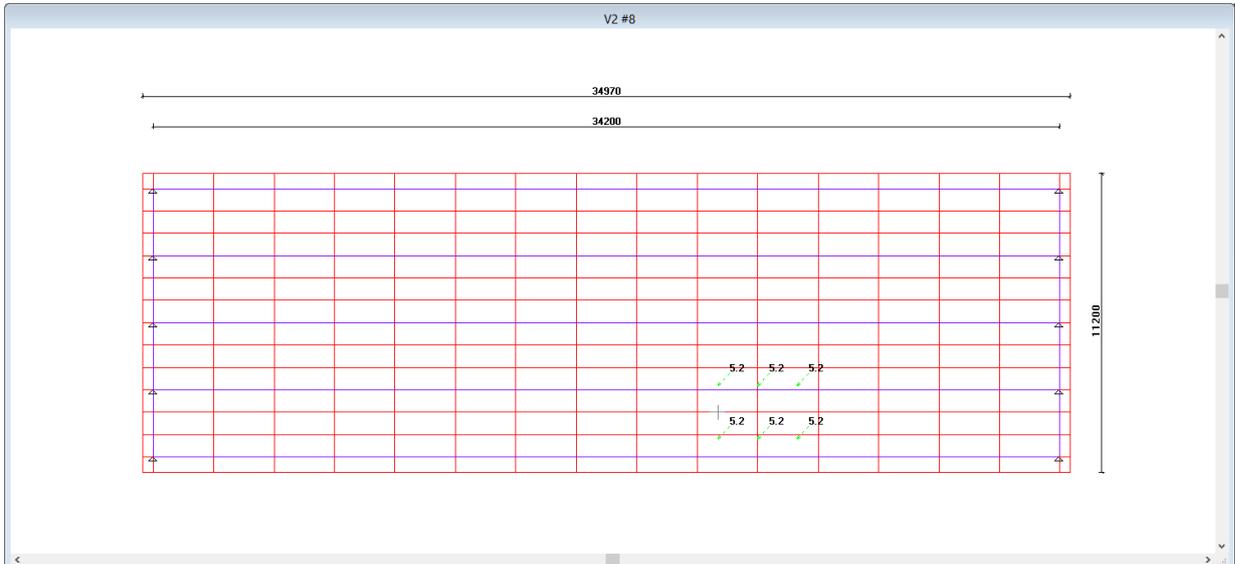


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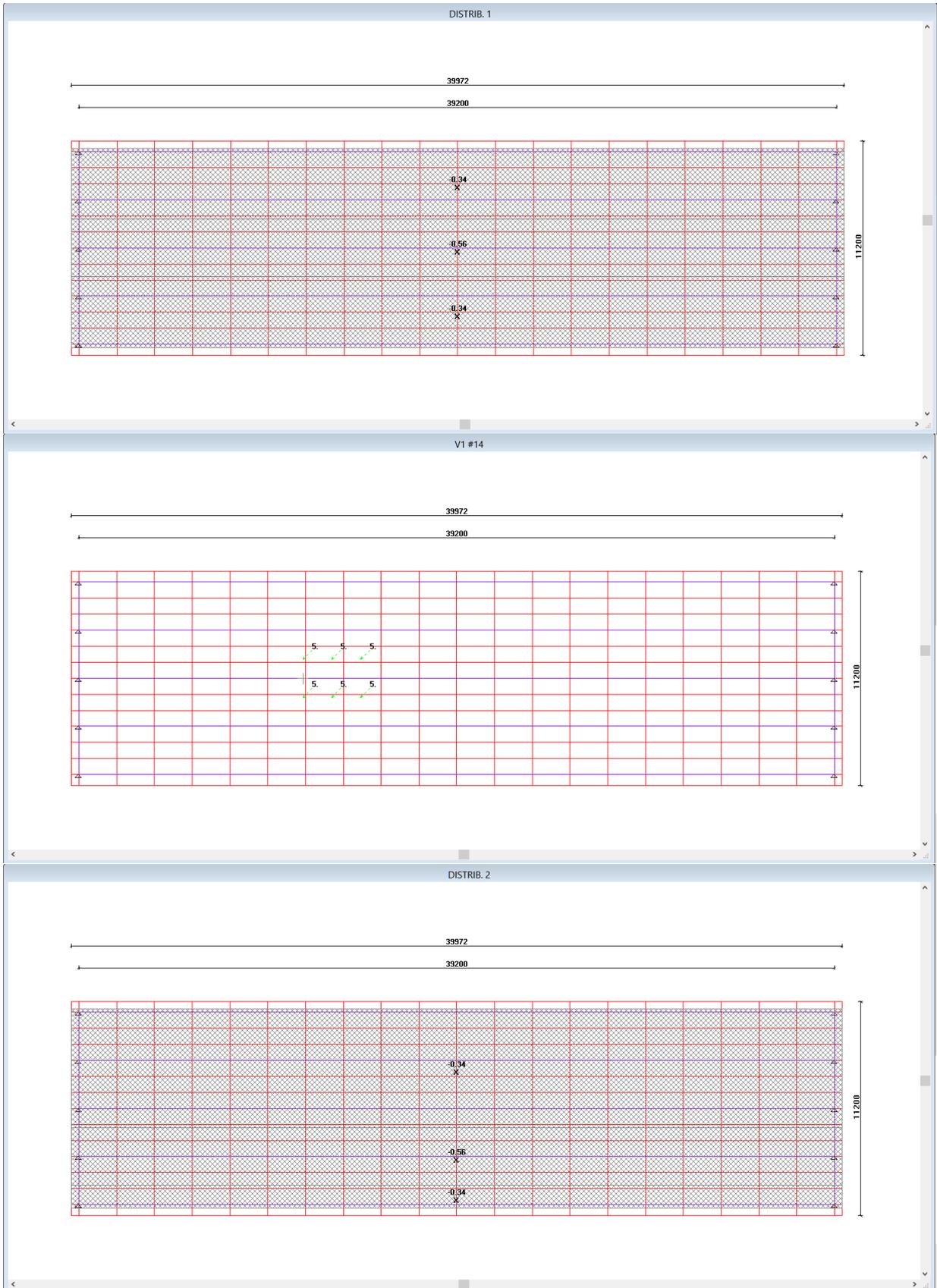


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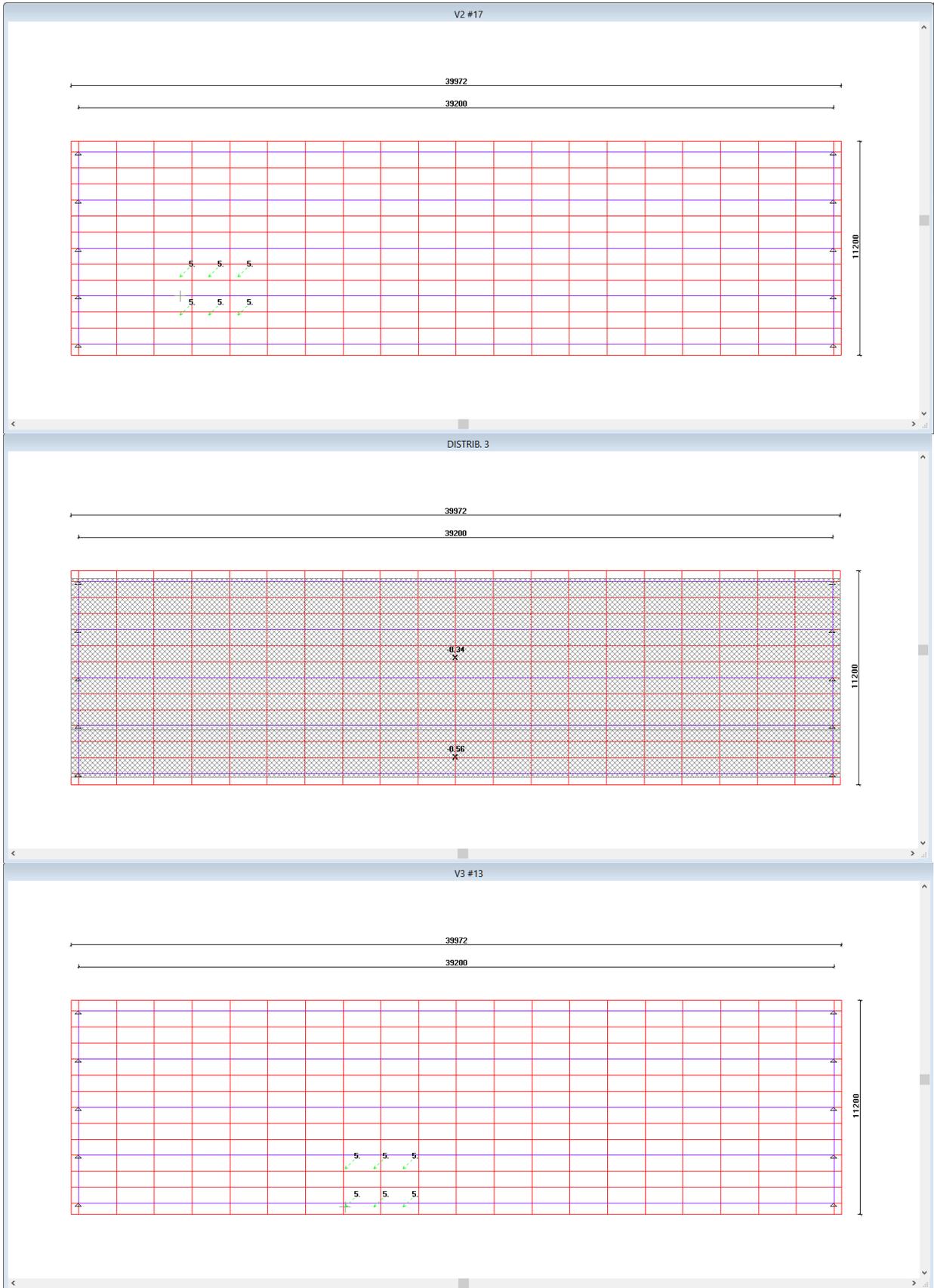


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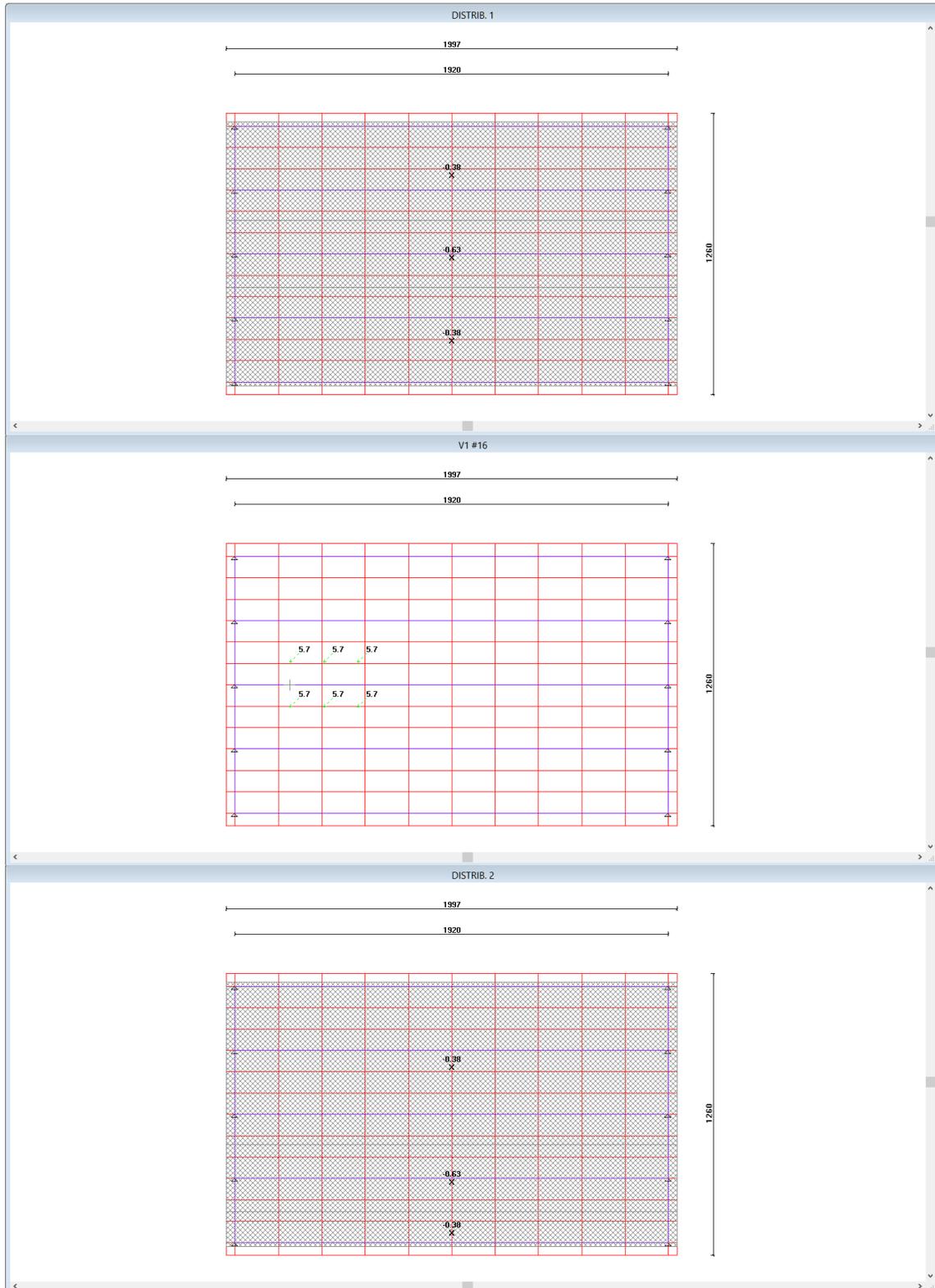
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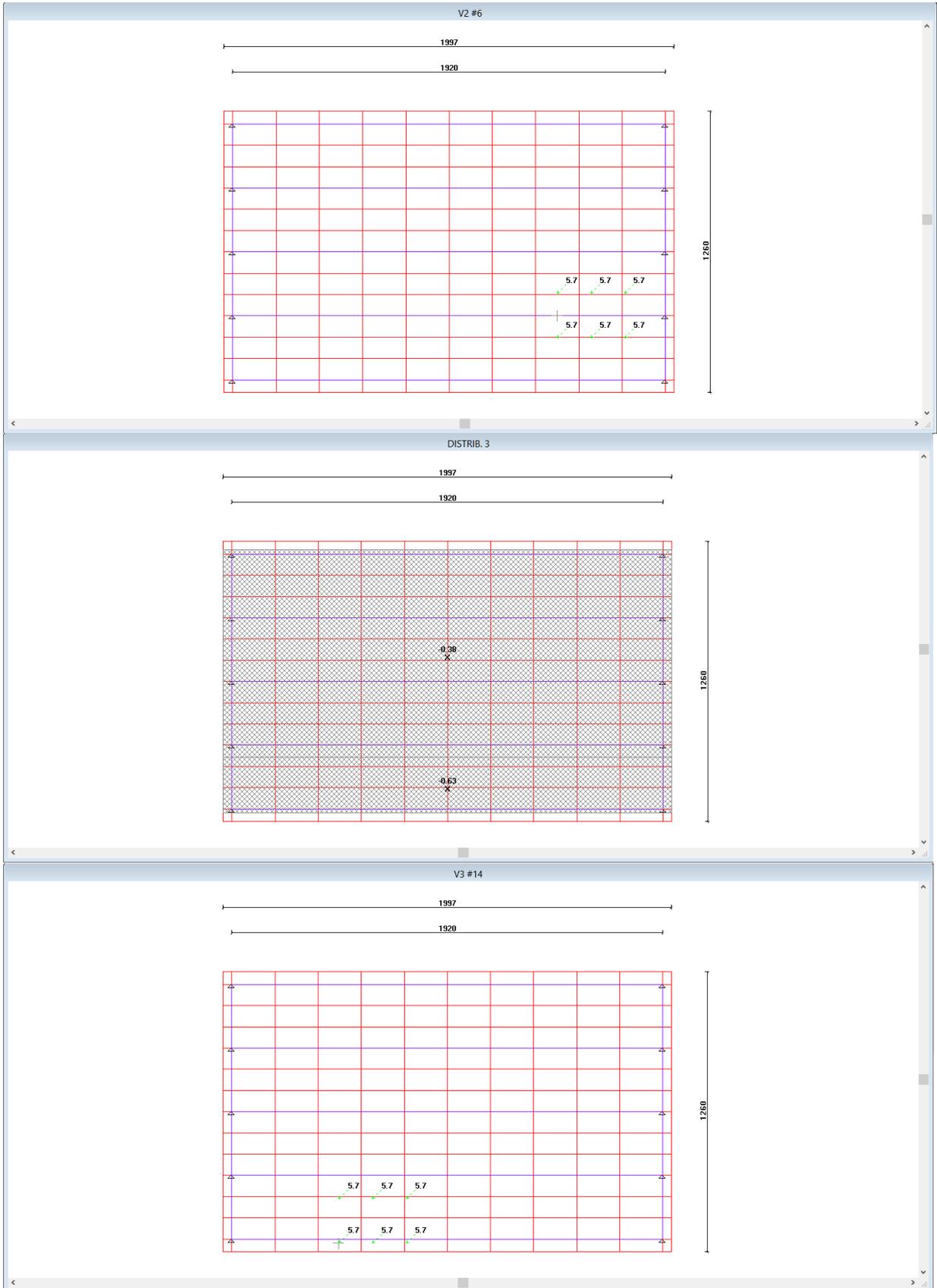
### NOTA TÉCNICA

#### 4.4.2. Tabuleiro 12,60 m



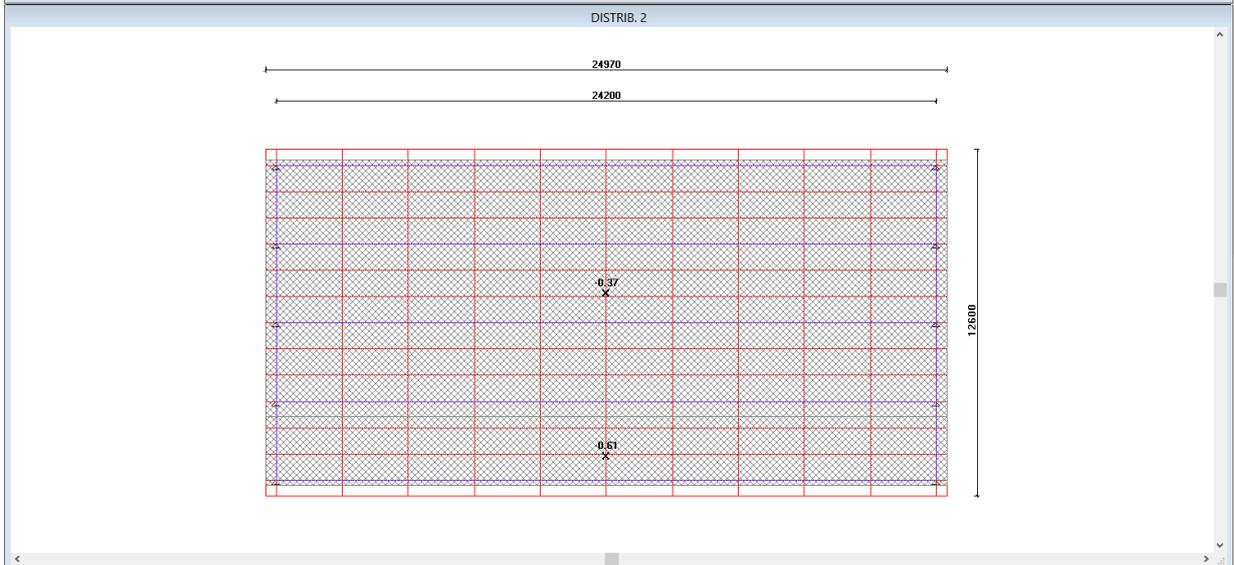
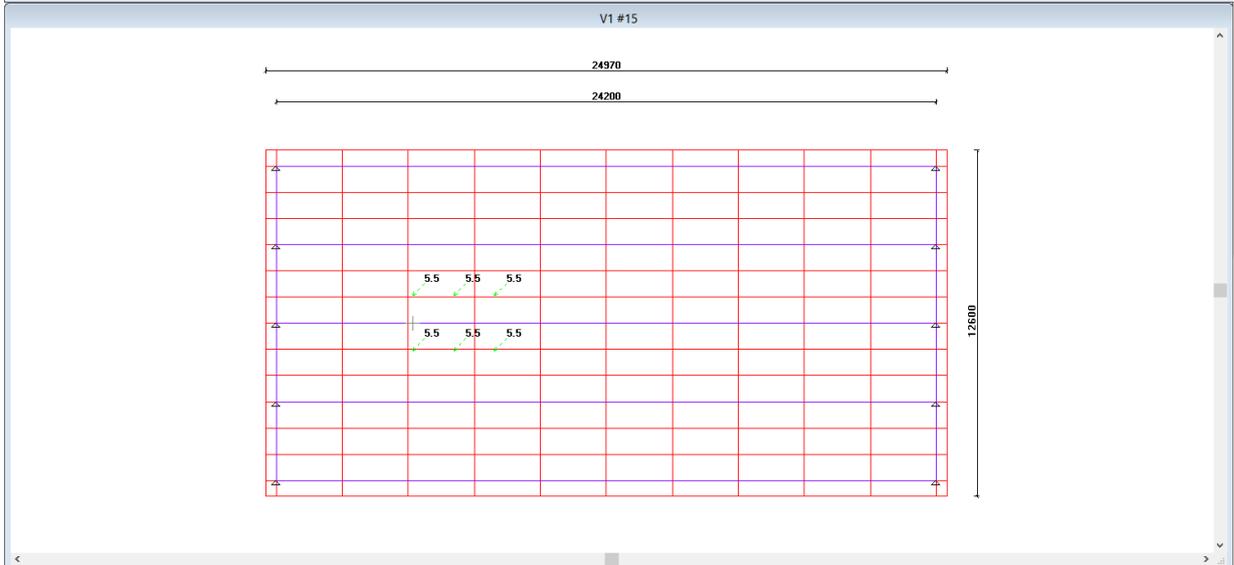
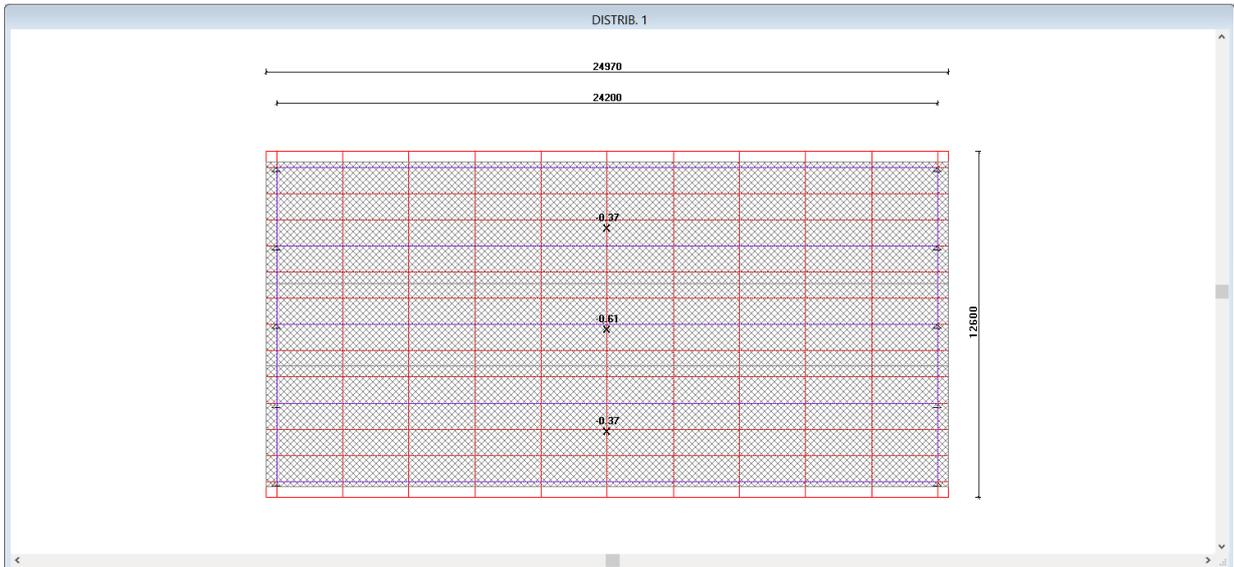


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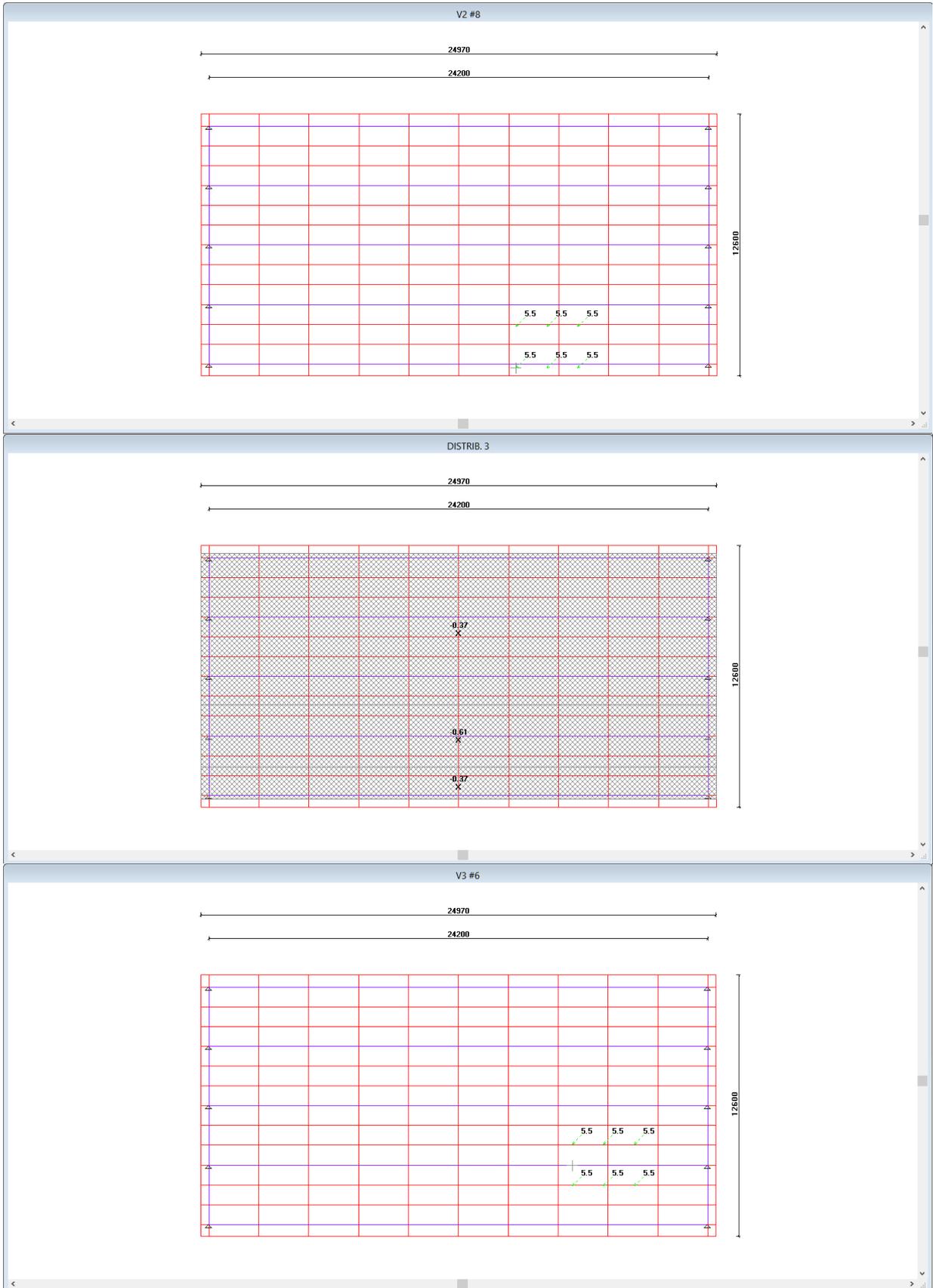


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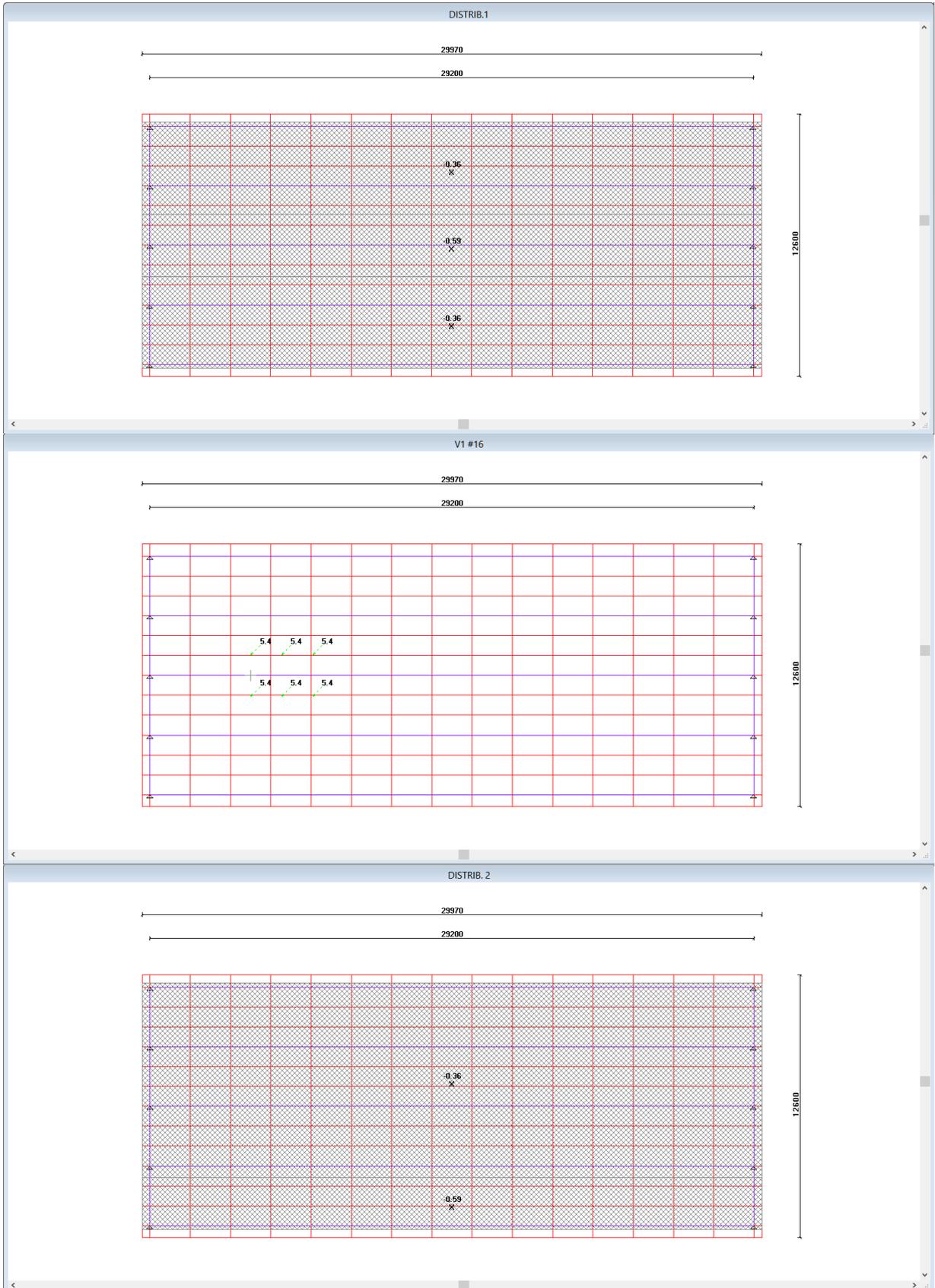


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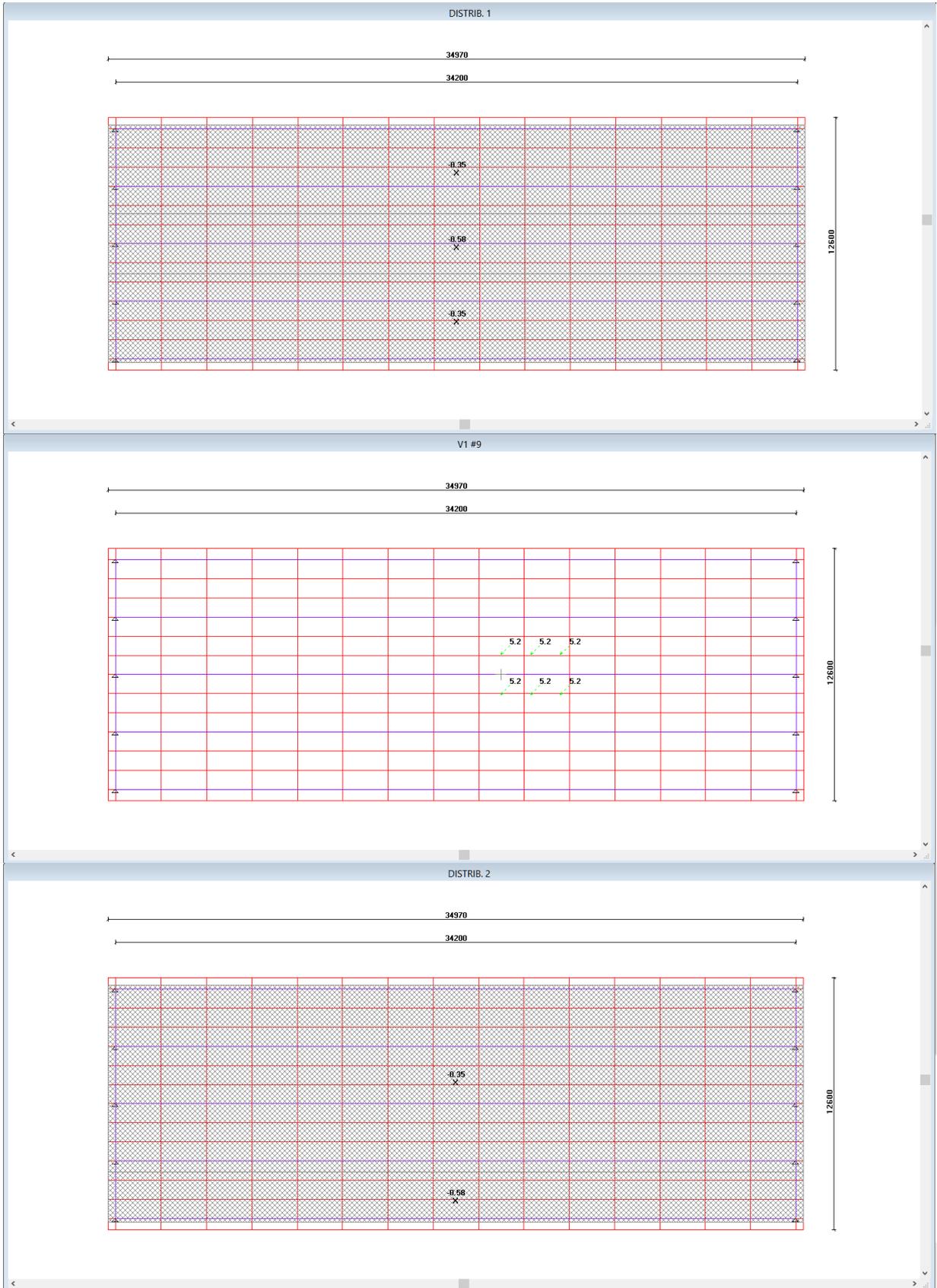


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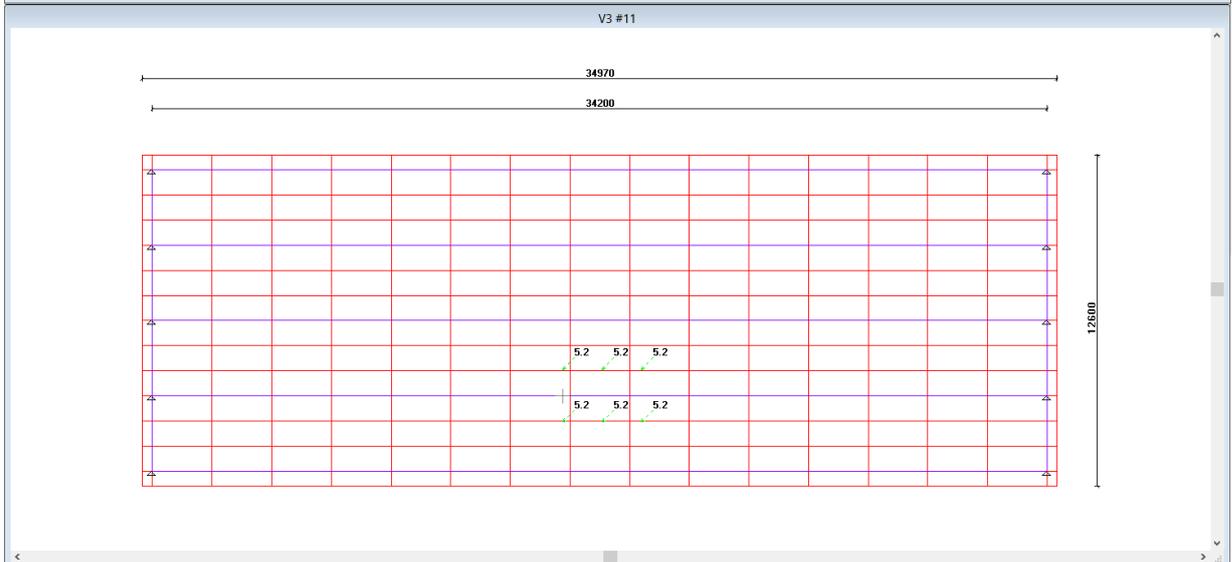
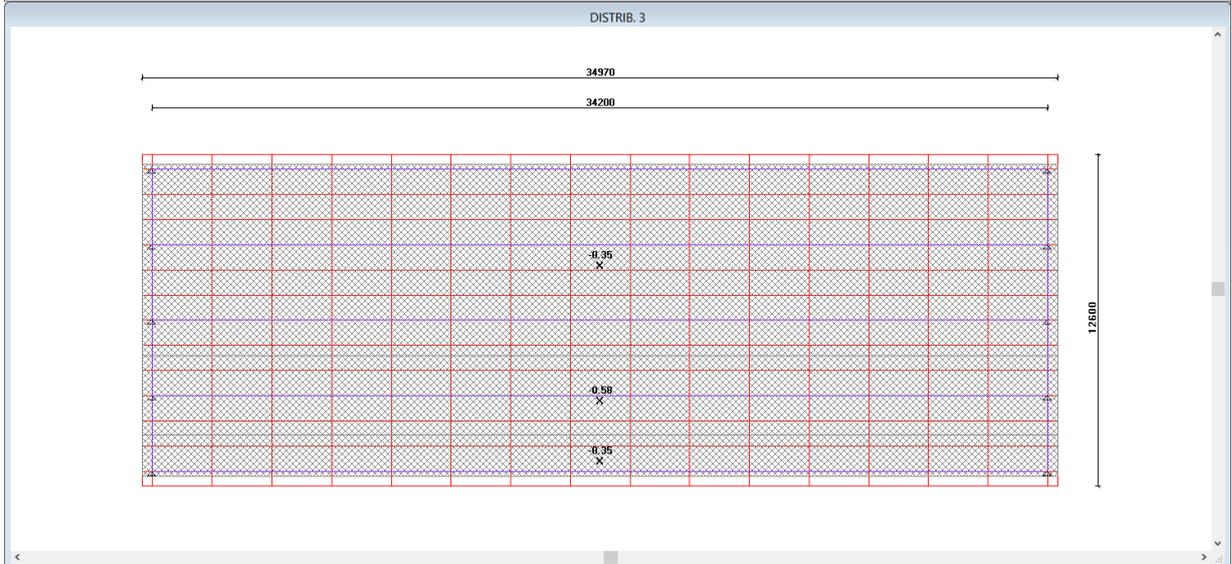


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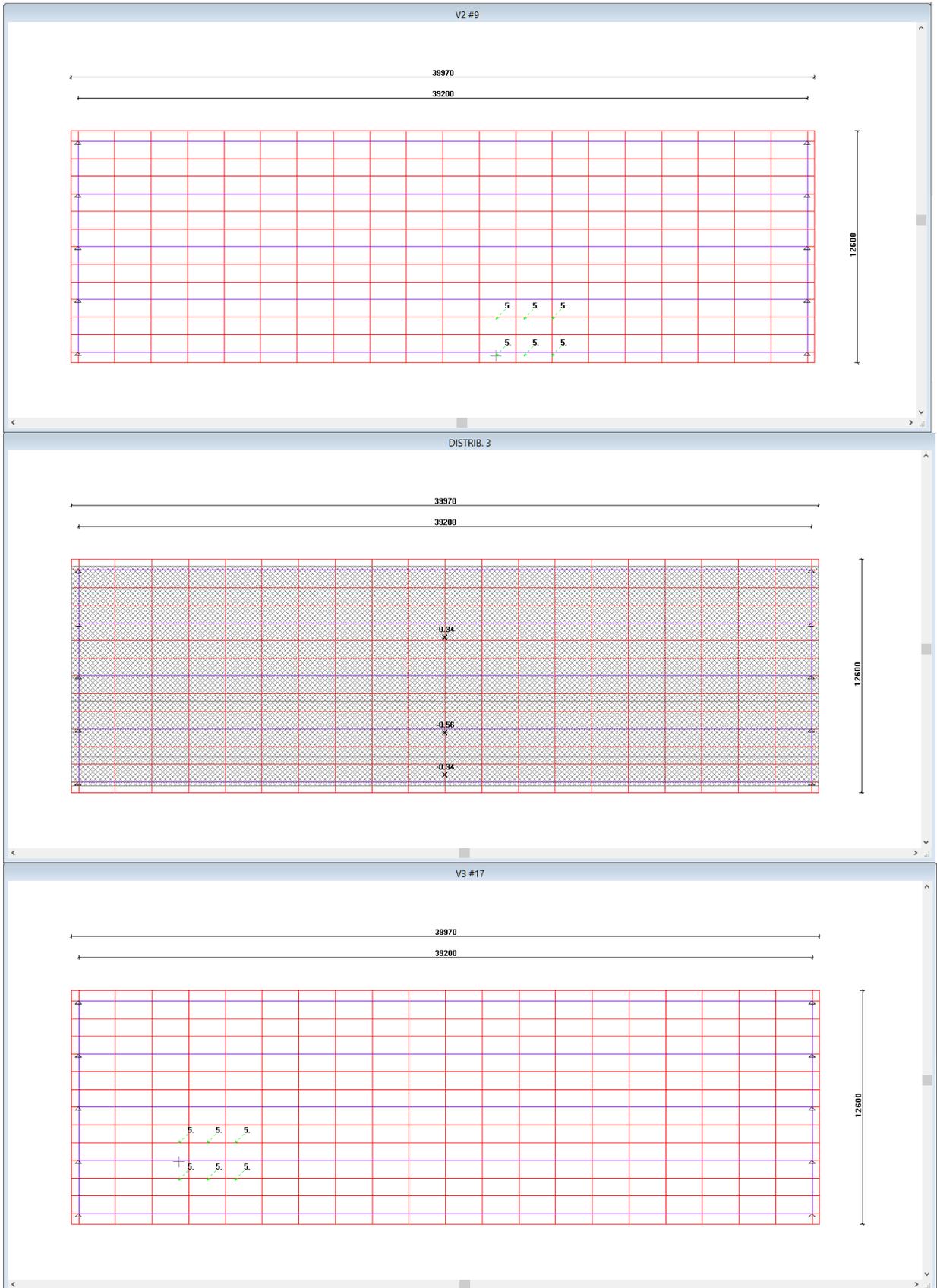


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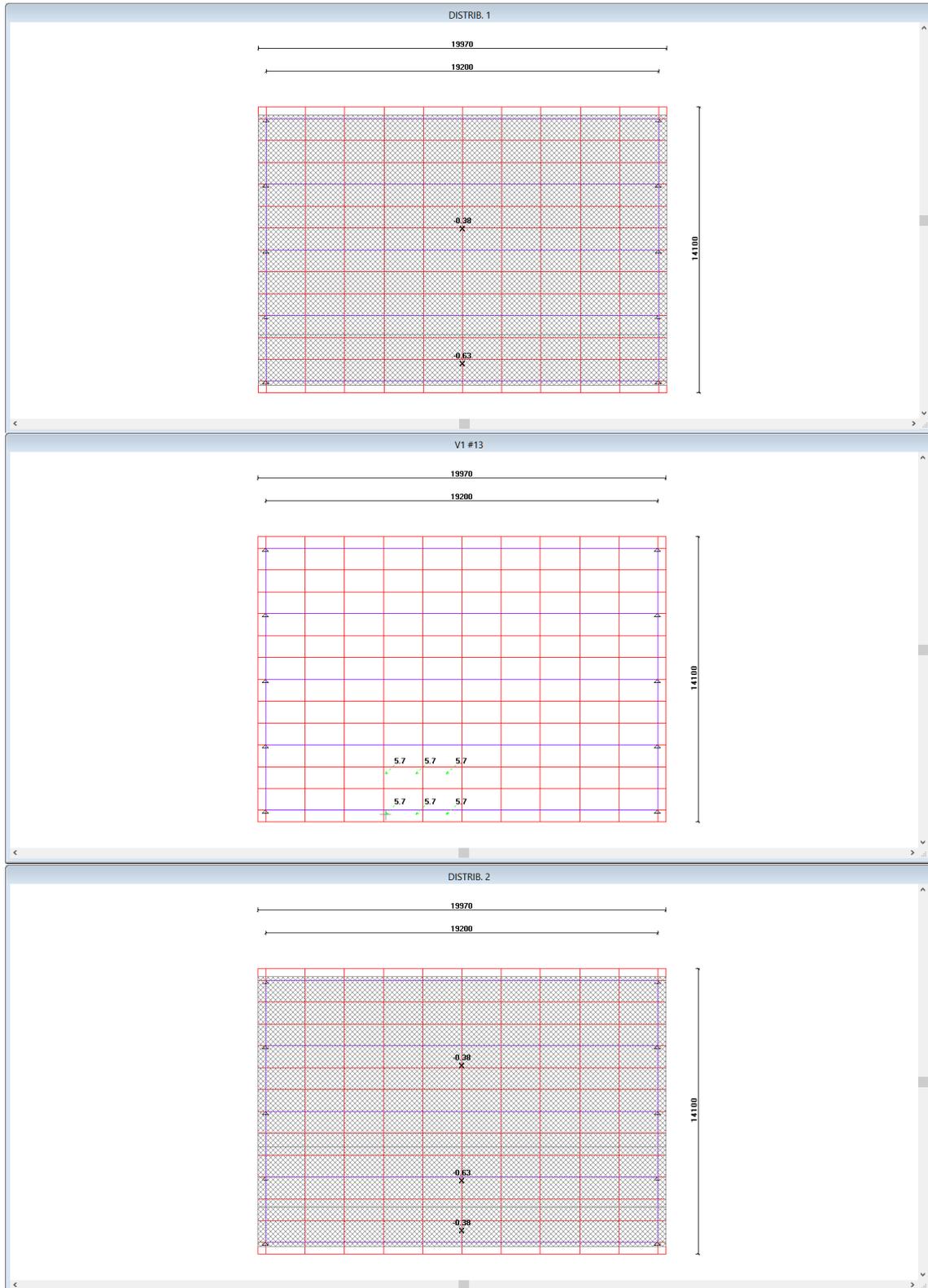
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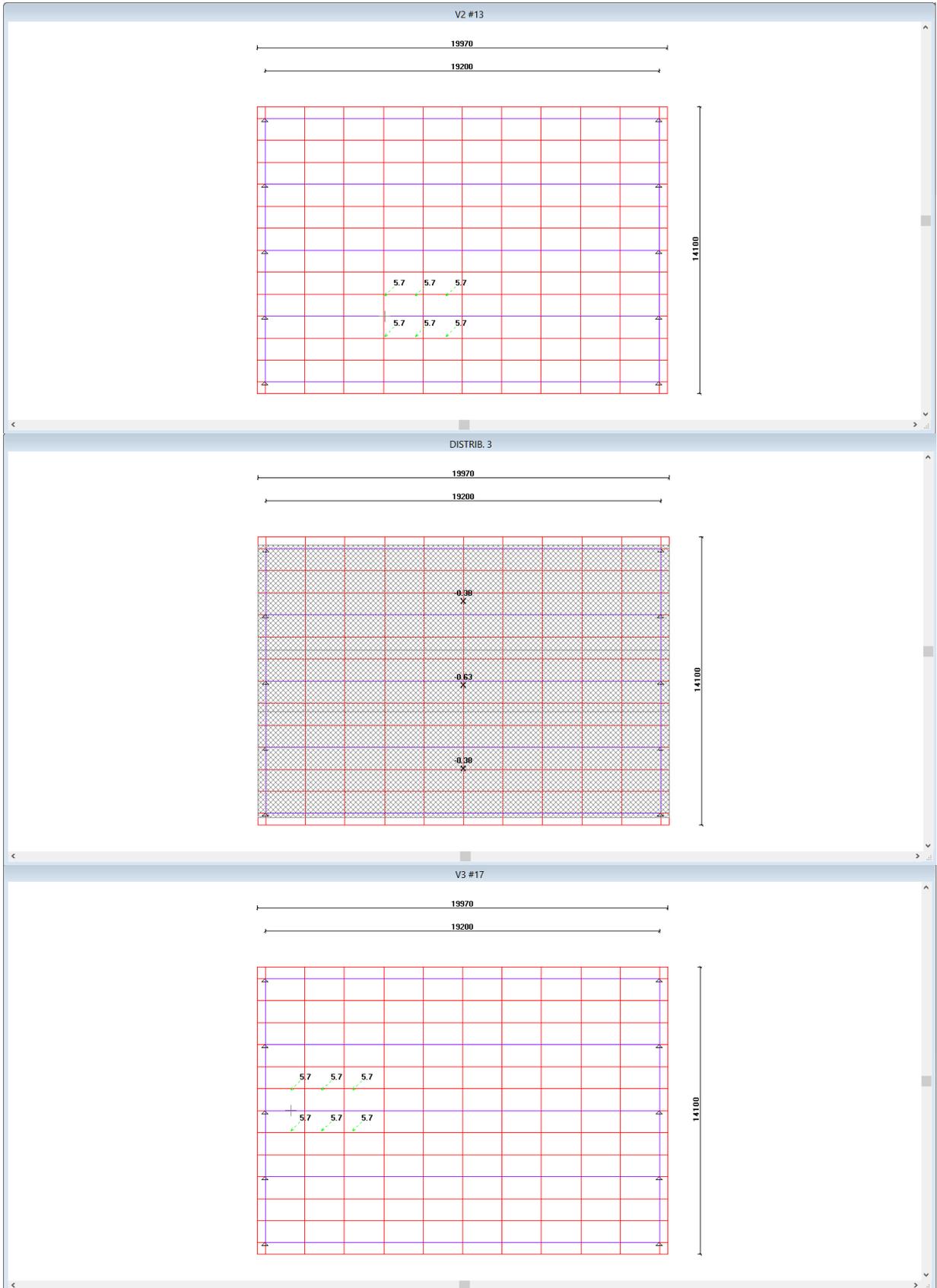
### NOTA TÉCNICA

#### 4.4.3. Tabuleiro 14,10 m





### NOTA TÉCNICA



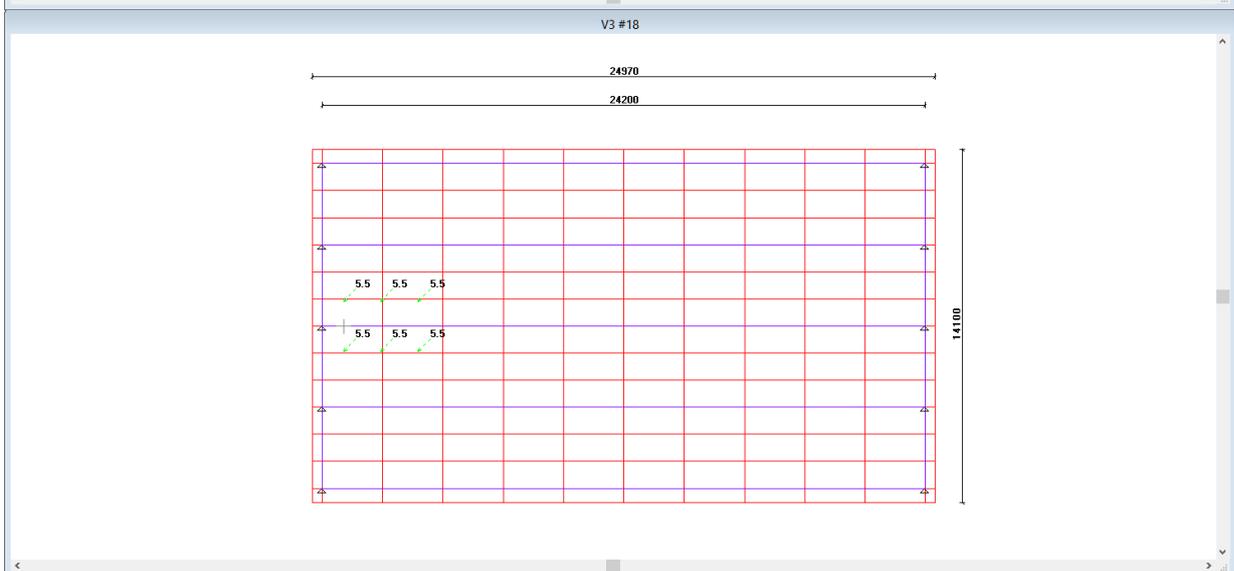
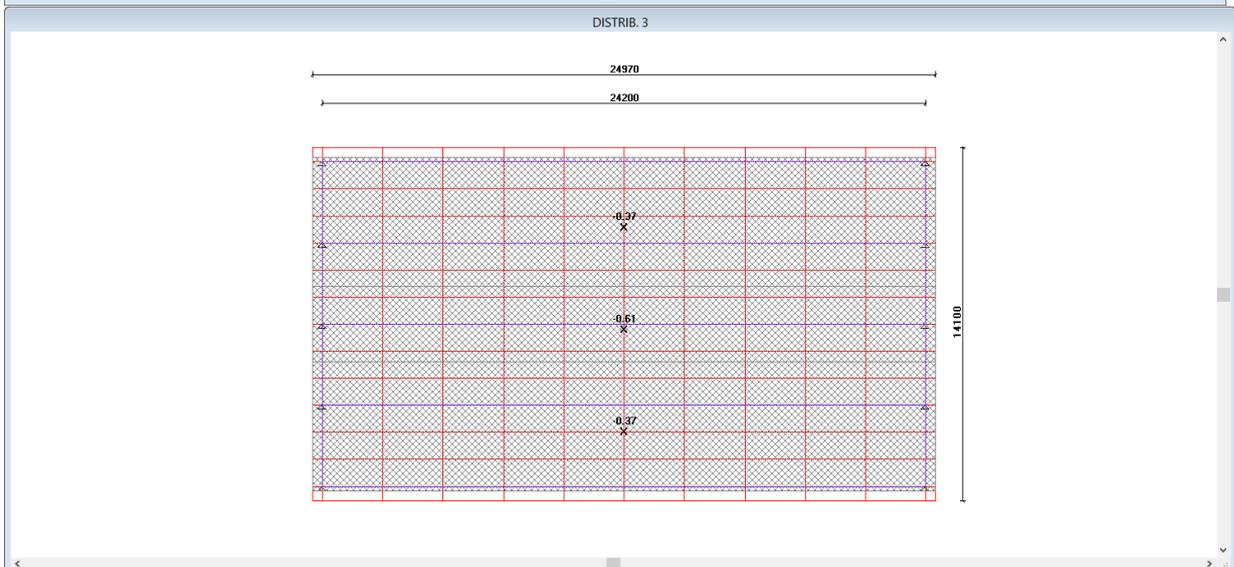
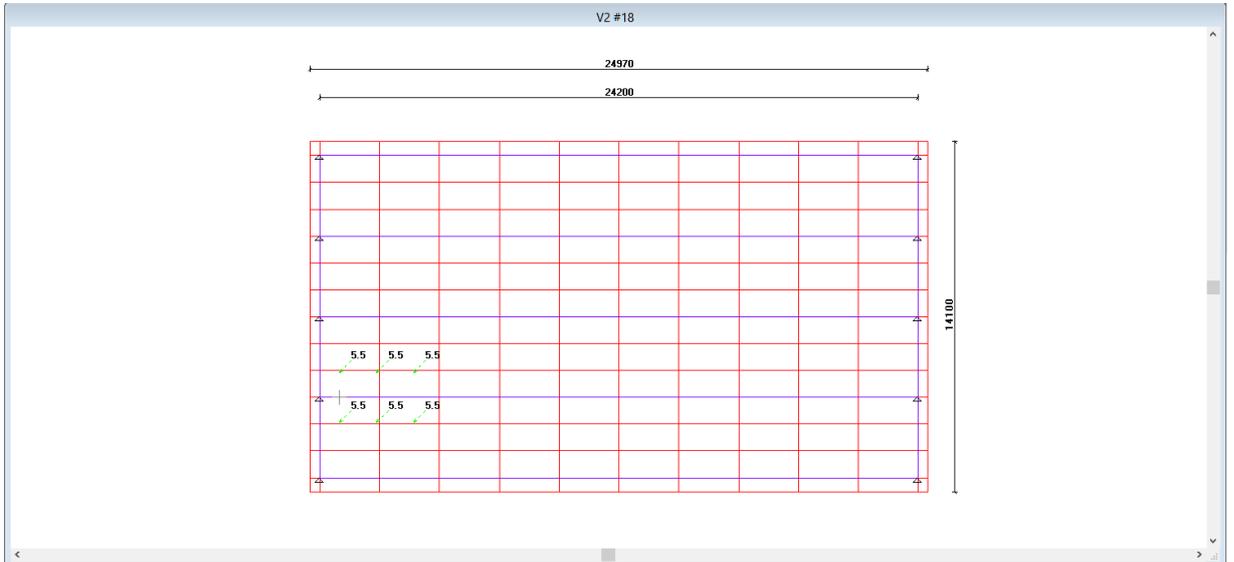


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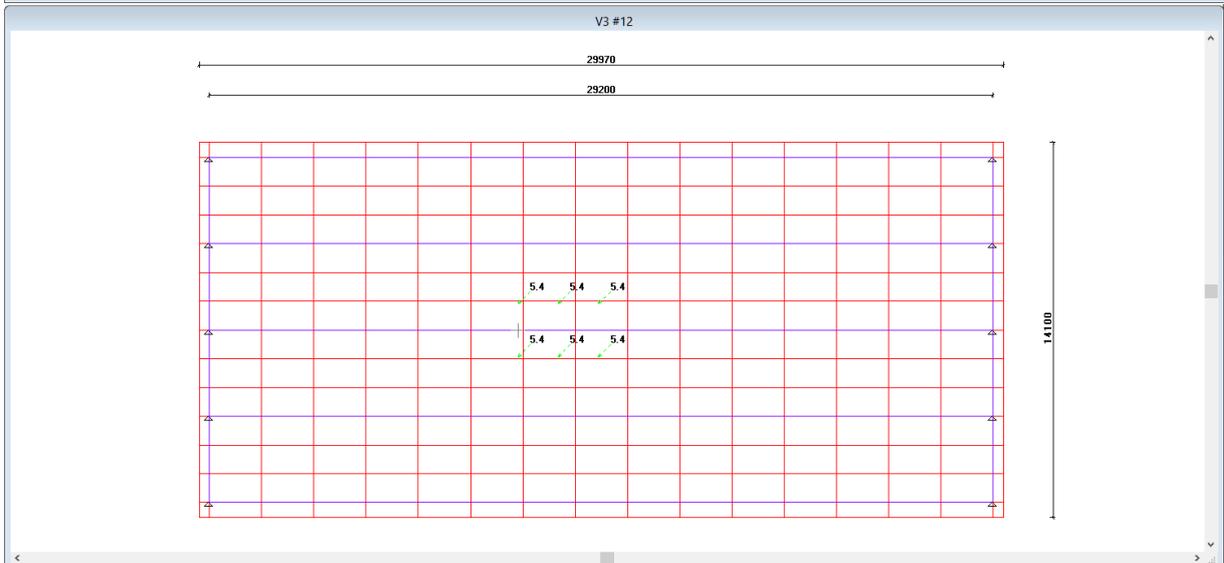
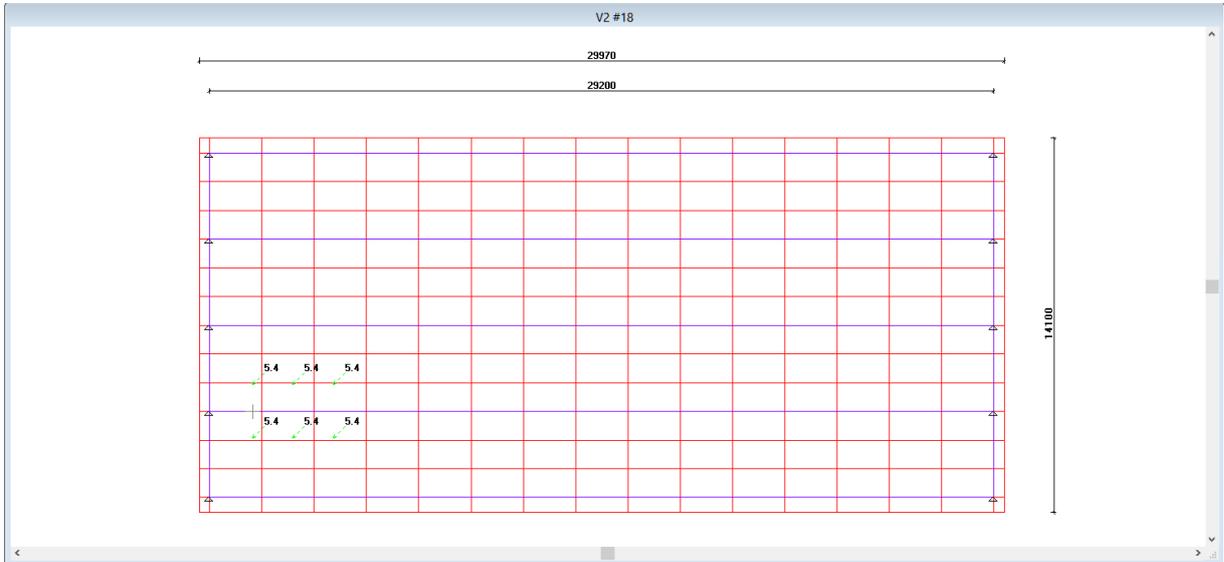


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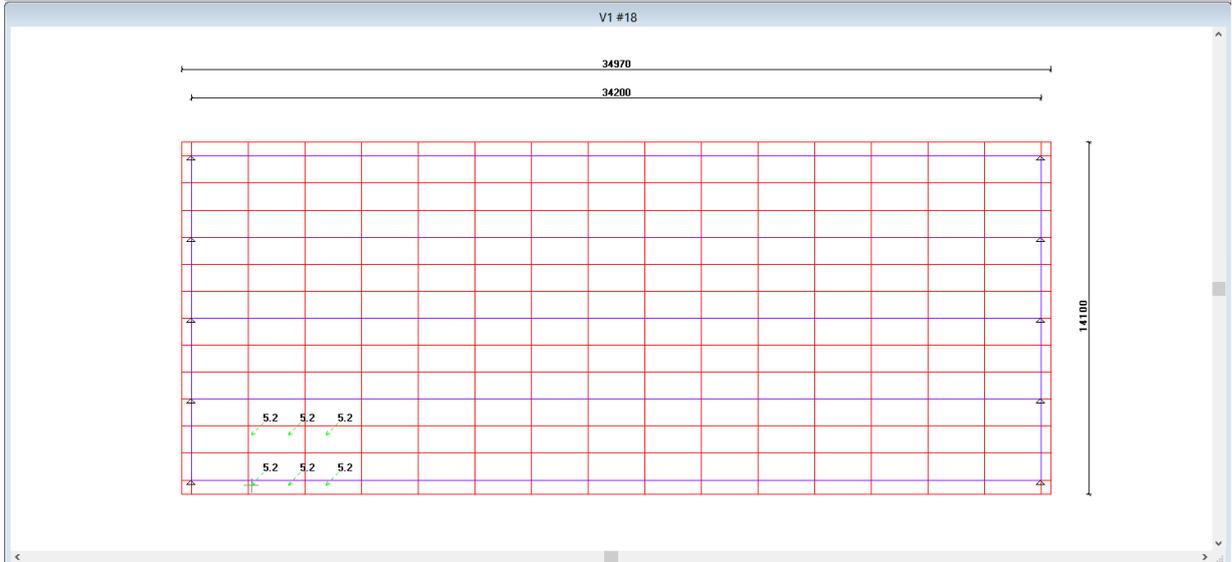
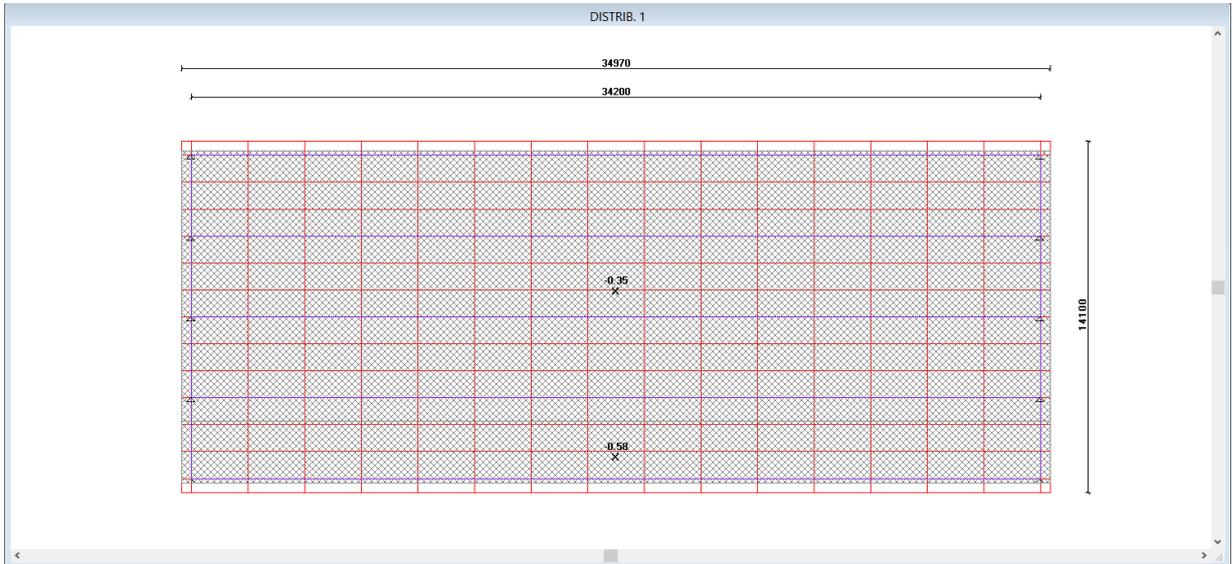


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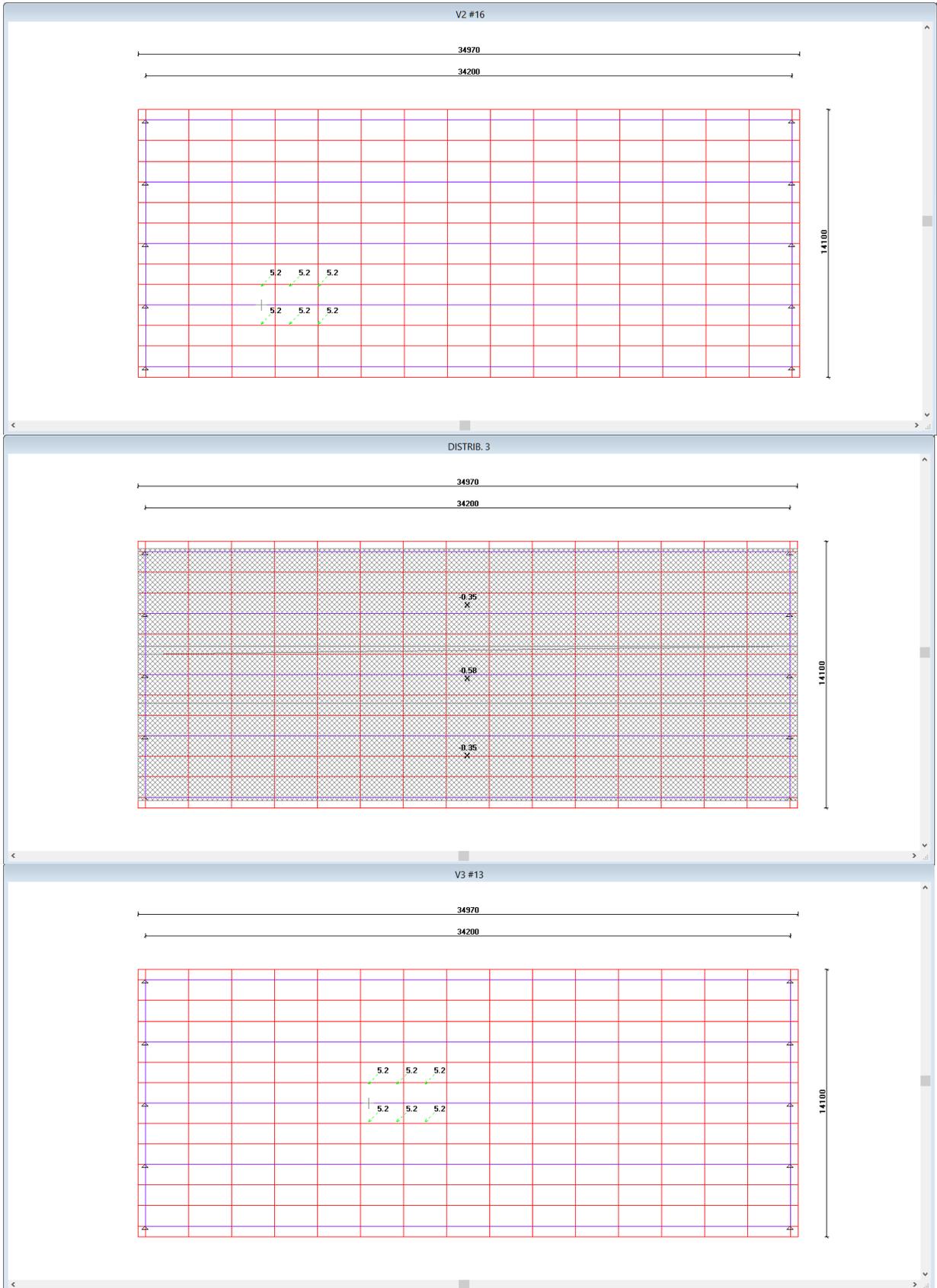


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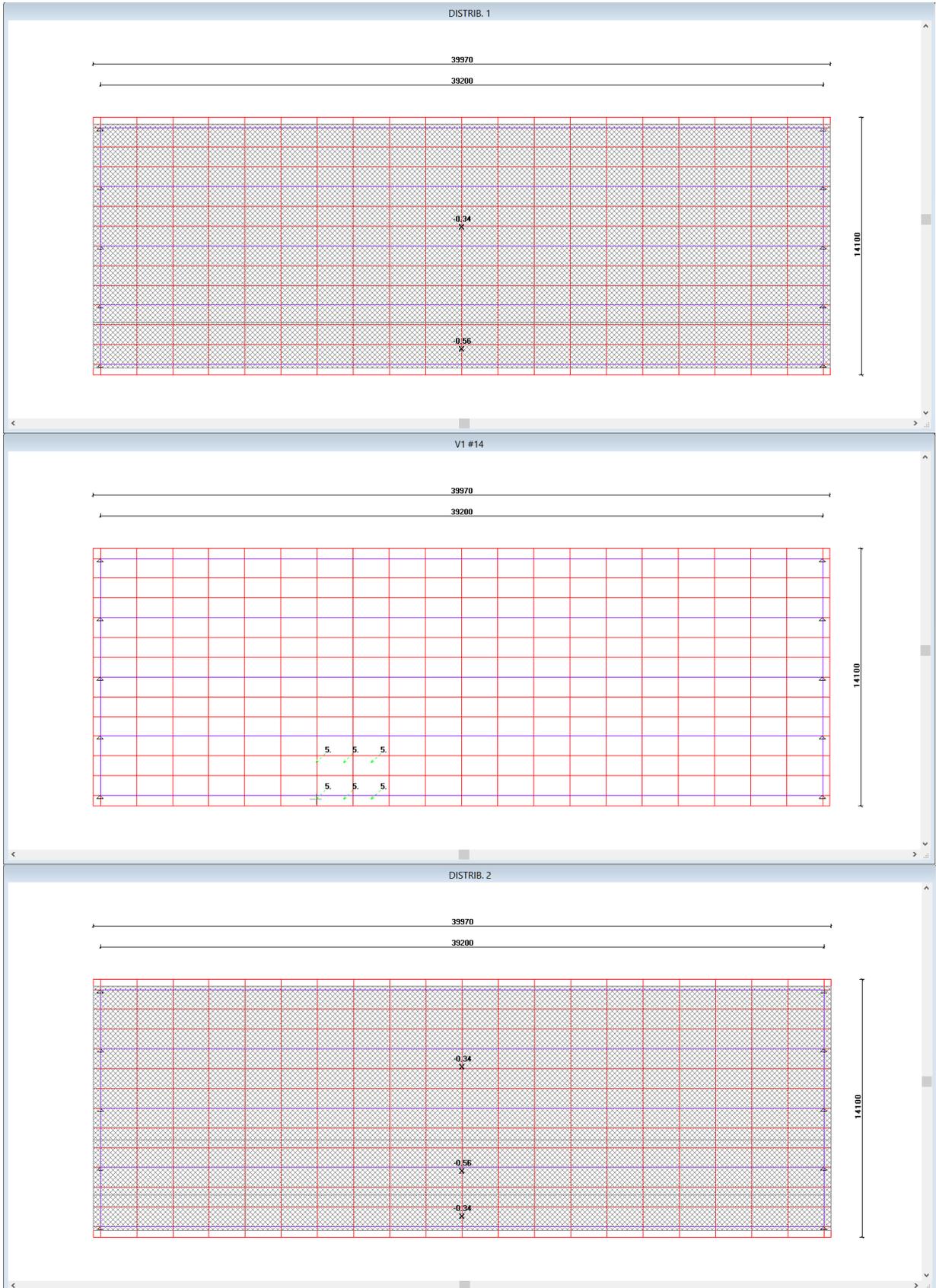


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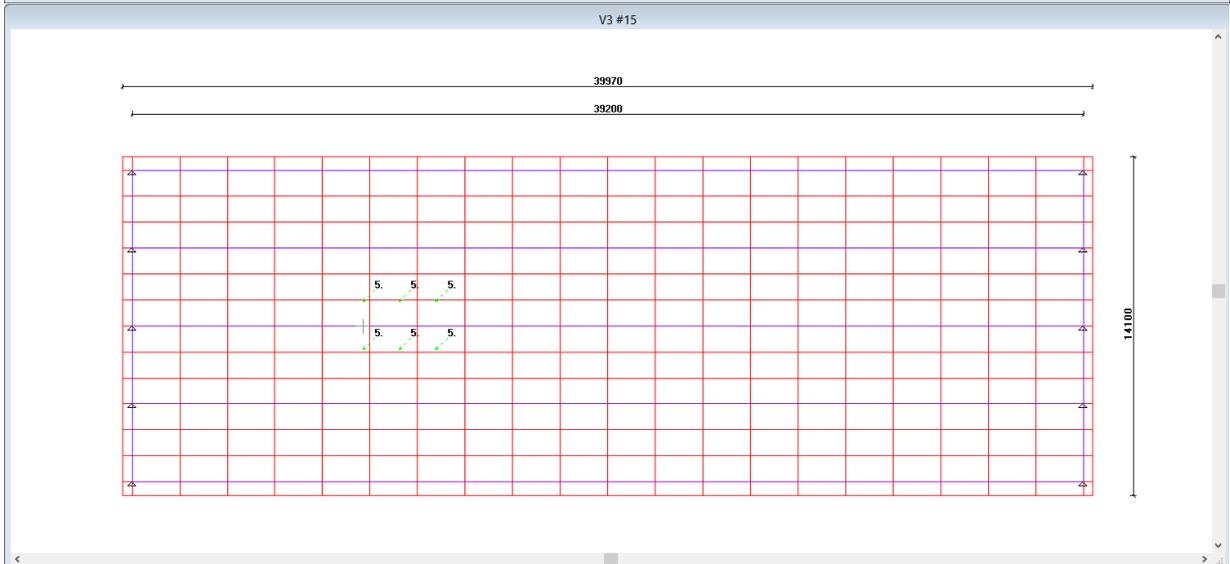
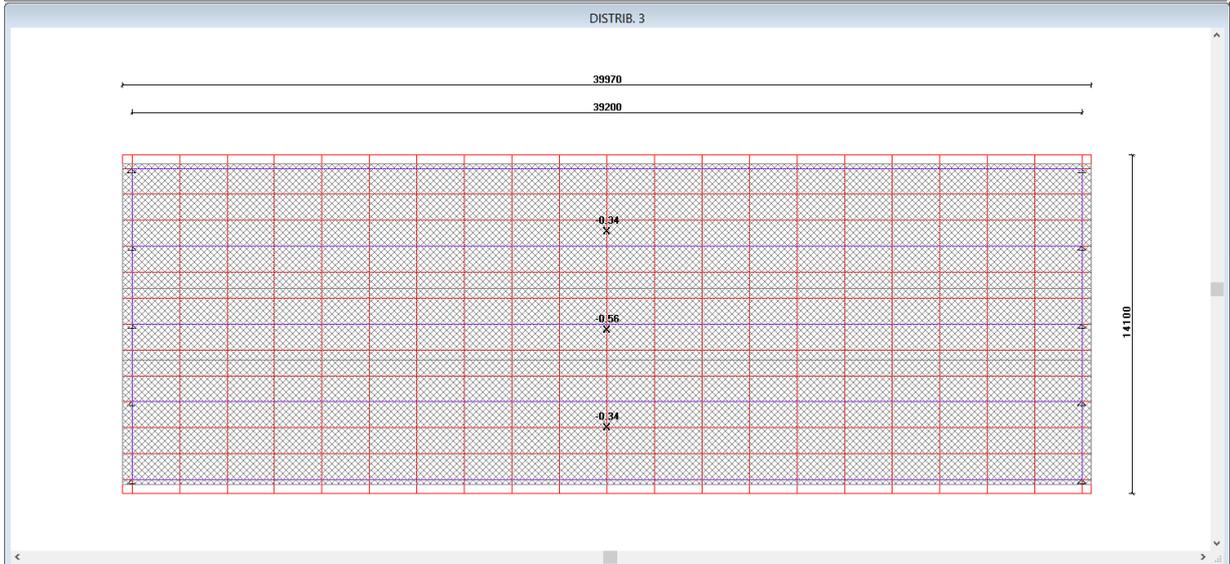
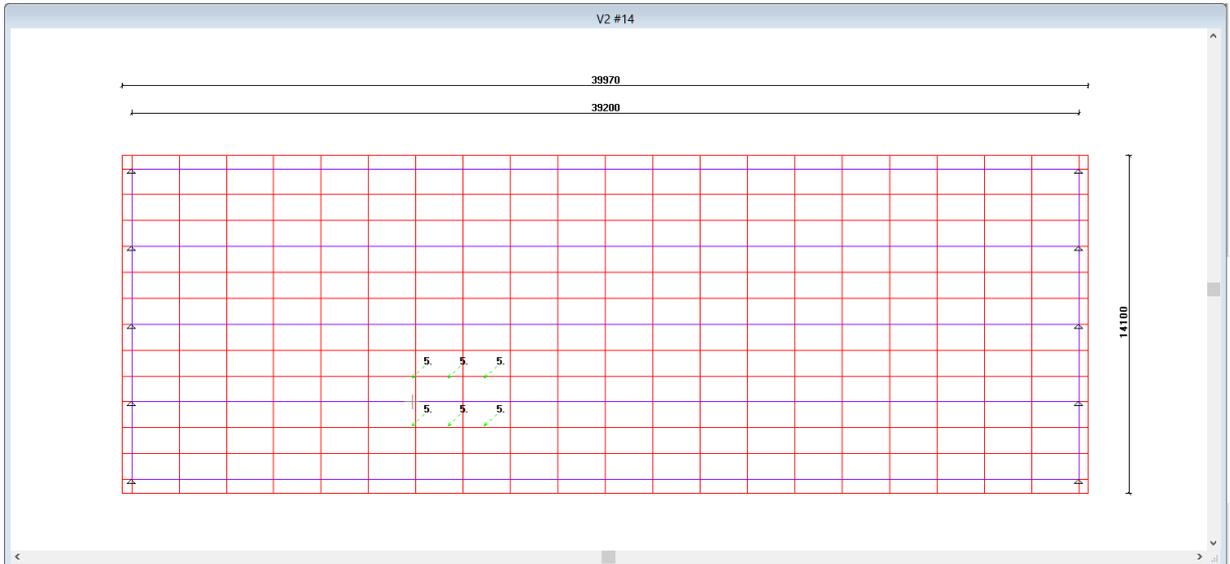


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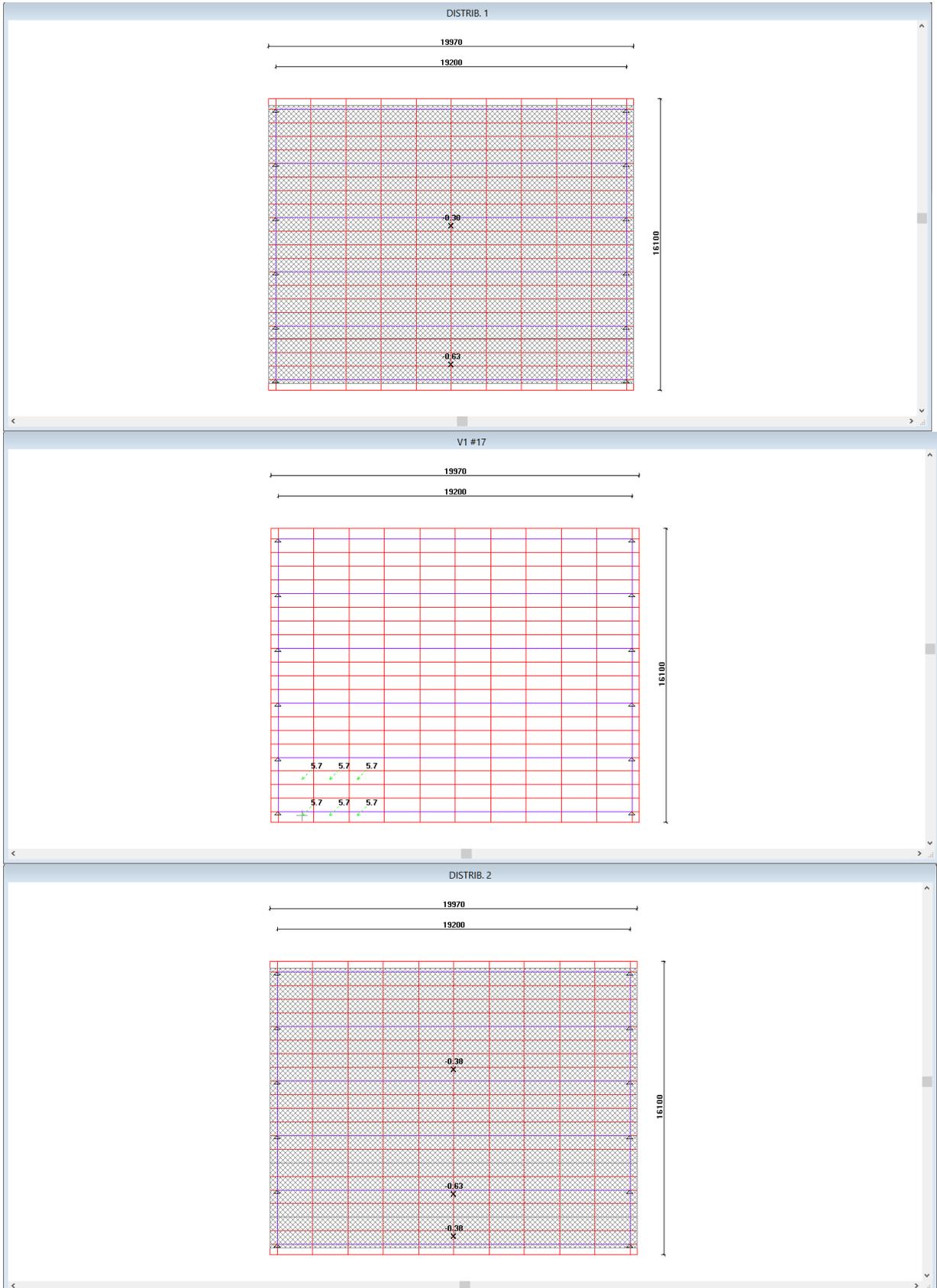
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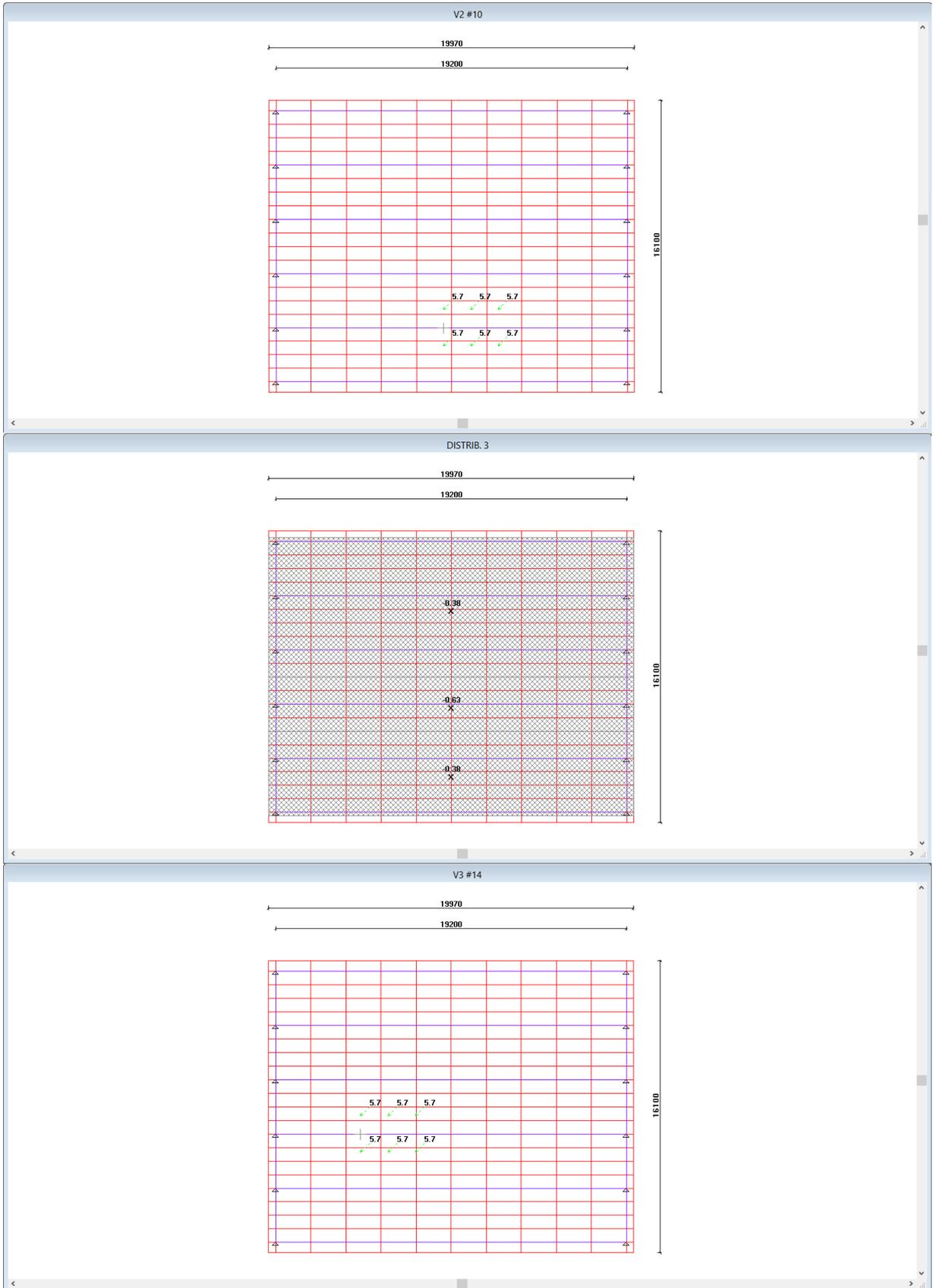
### NOTA TÉCNICA

#### 4.4.4. Tabuleiro 16,10 m



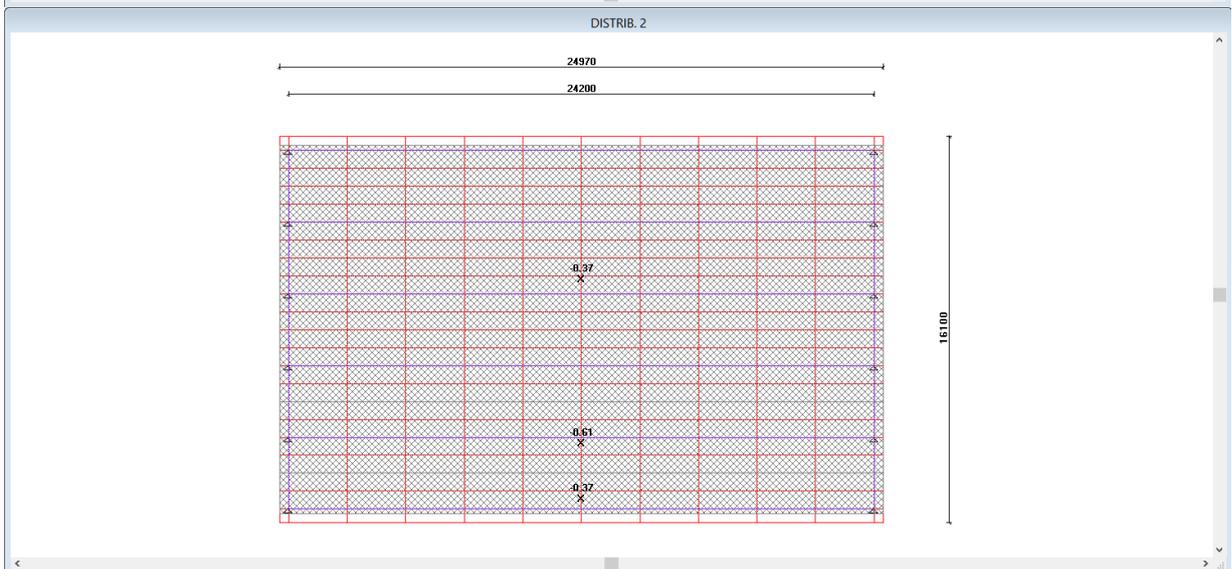
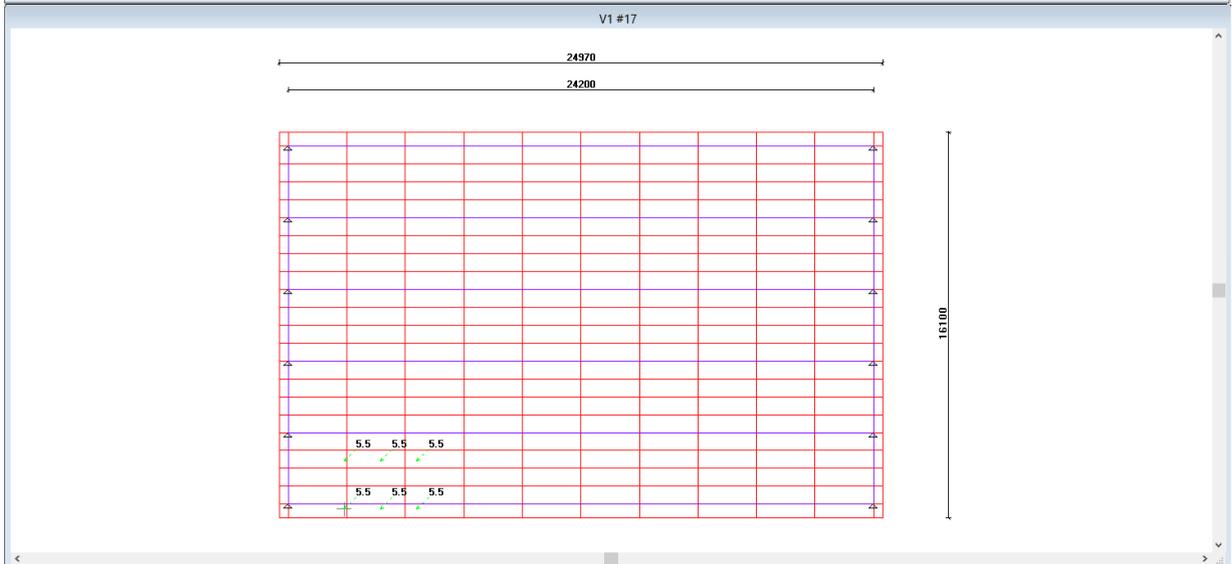
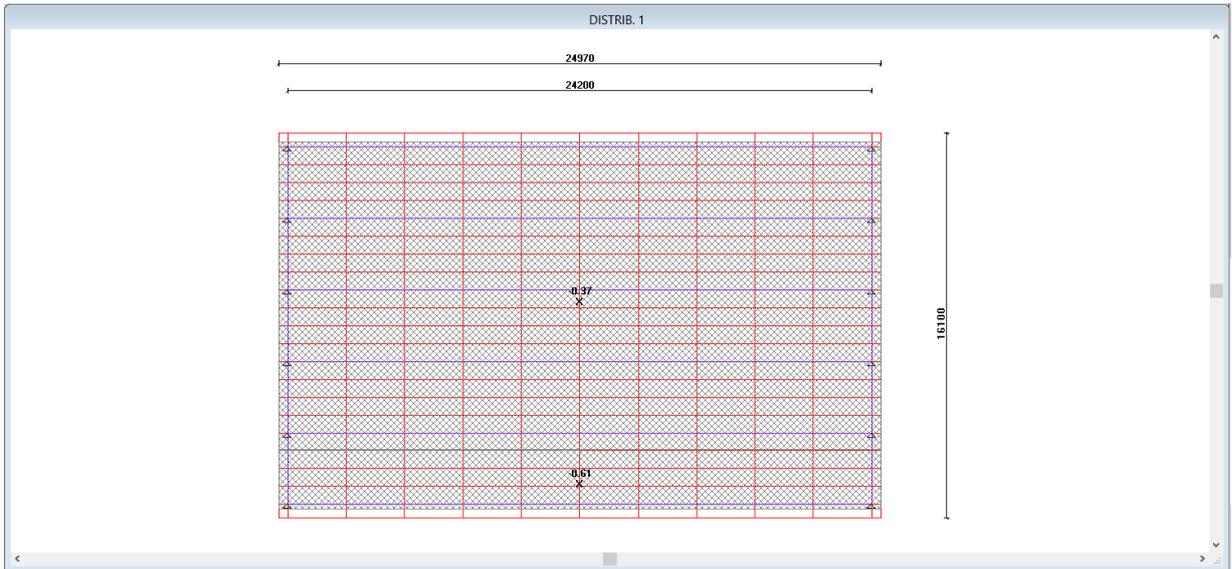


### NOTA TÉCNICA



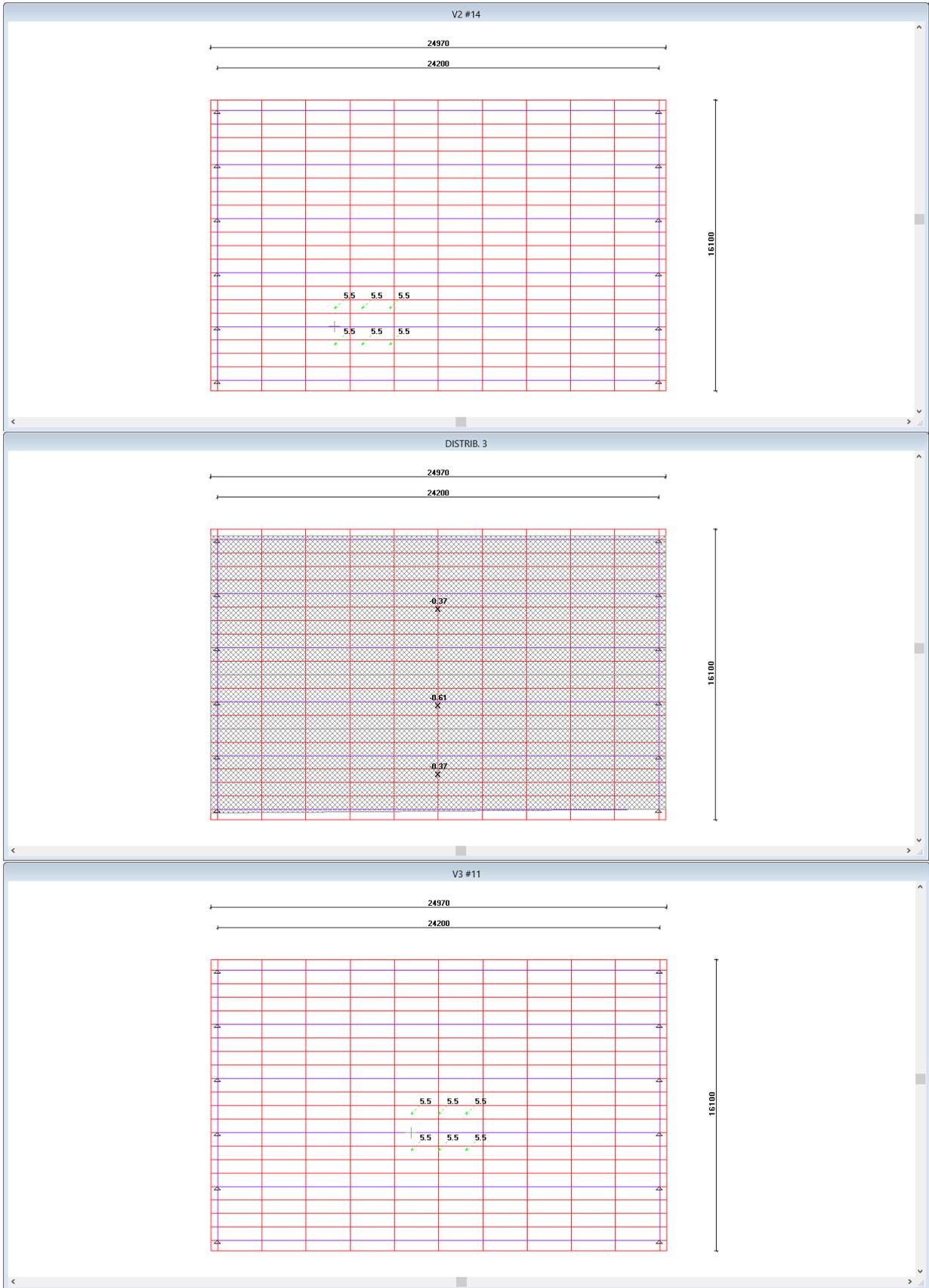


### NOTA TÉCNICA



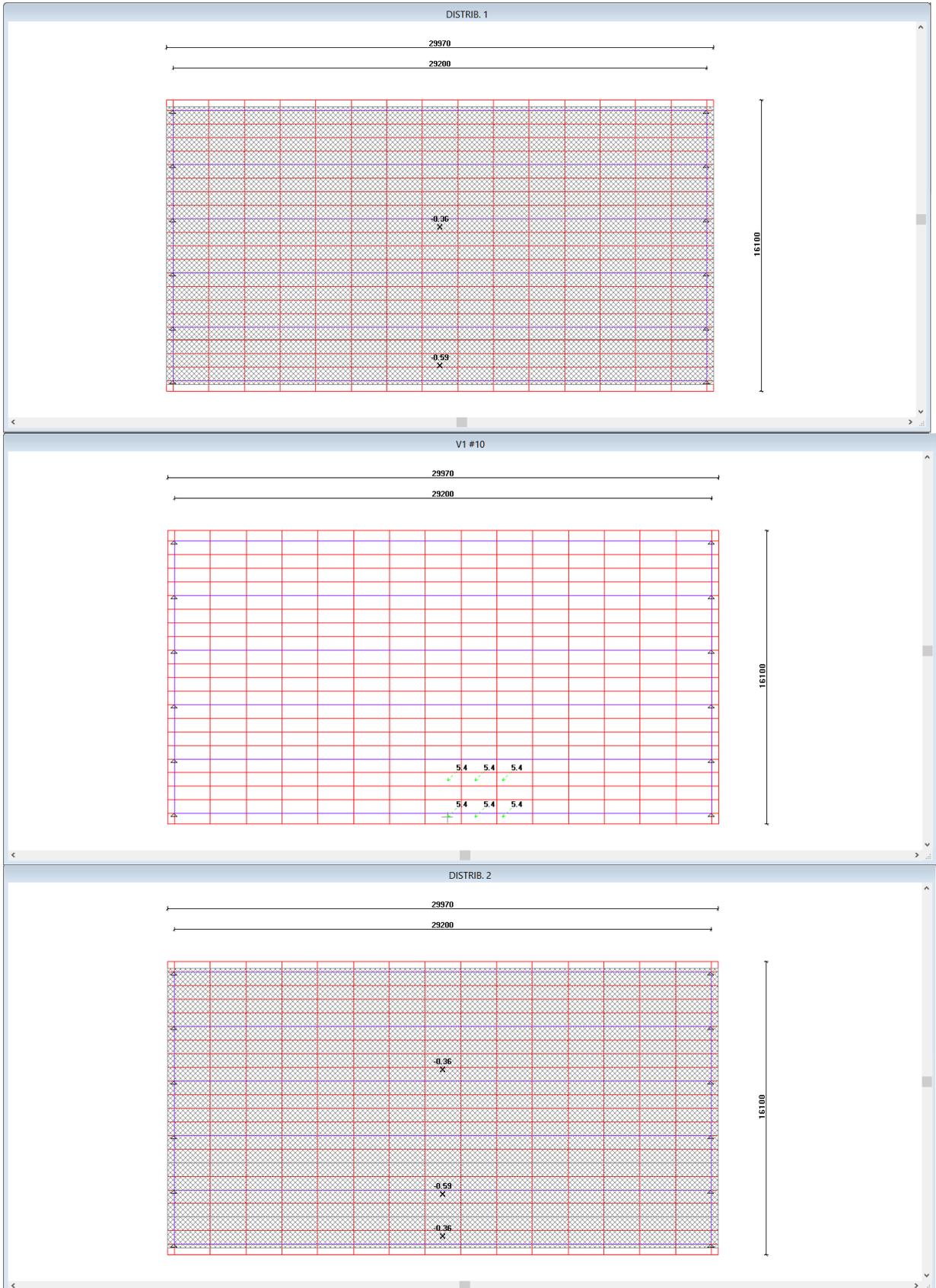


### NOTA TÉCNICA



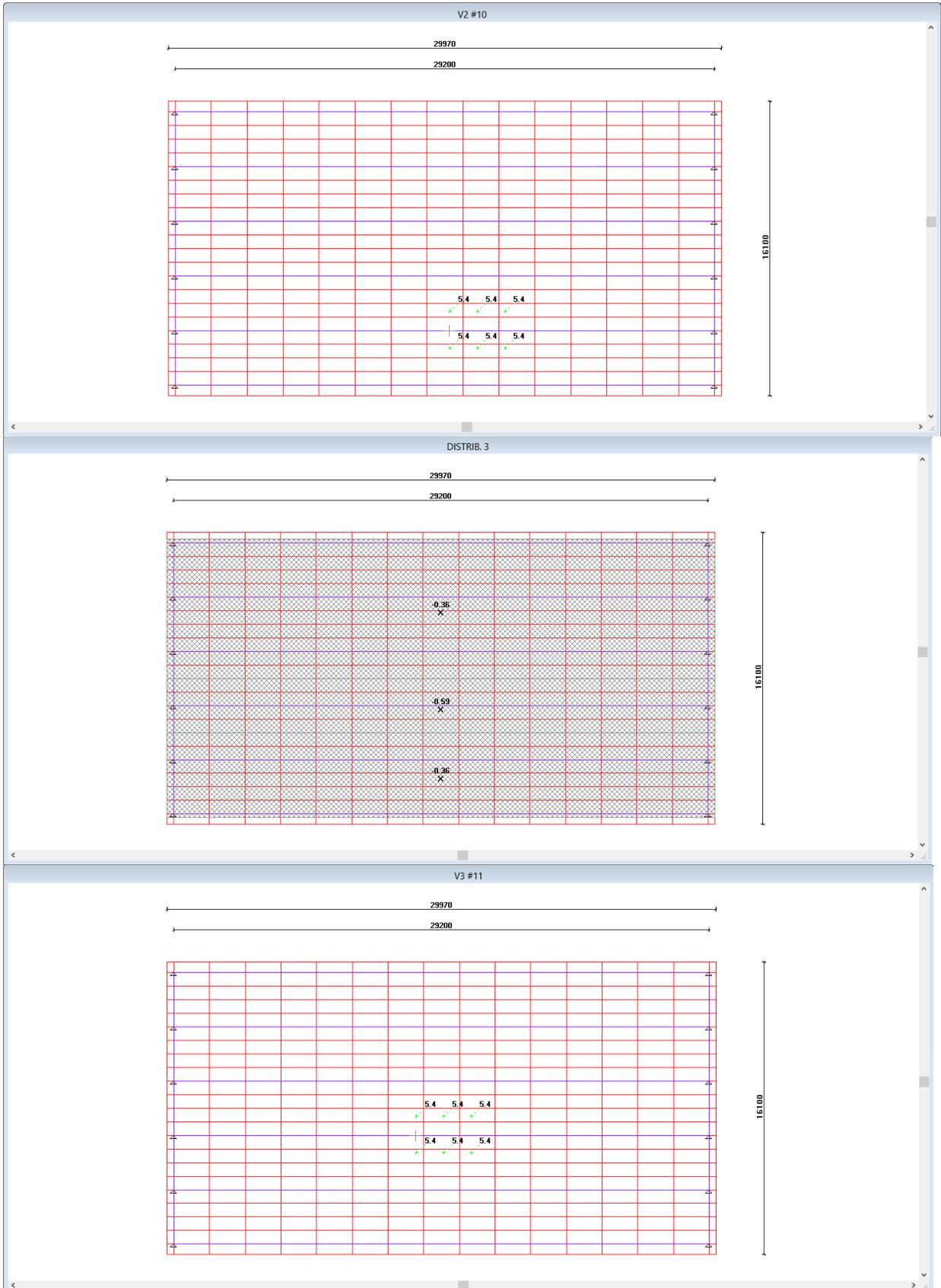


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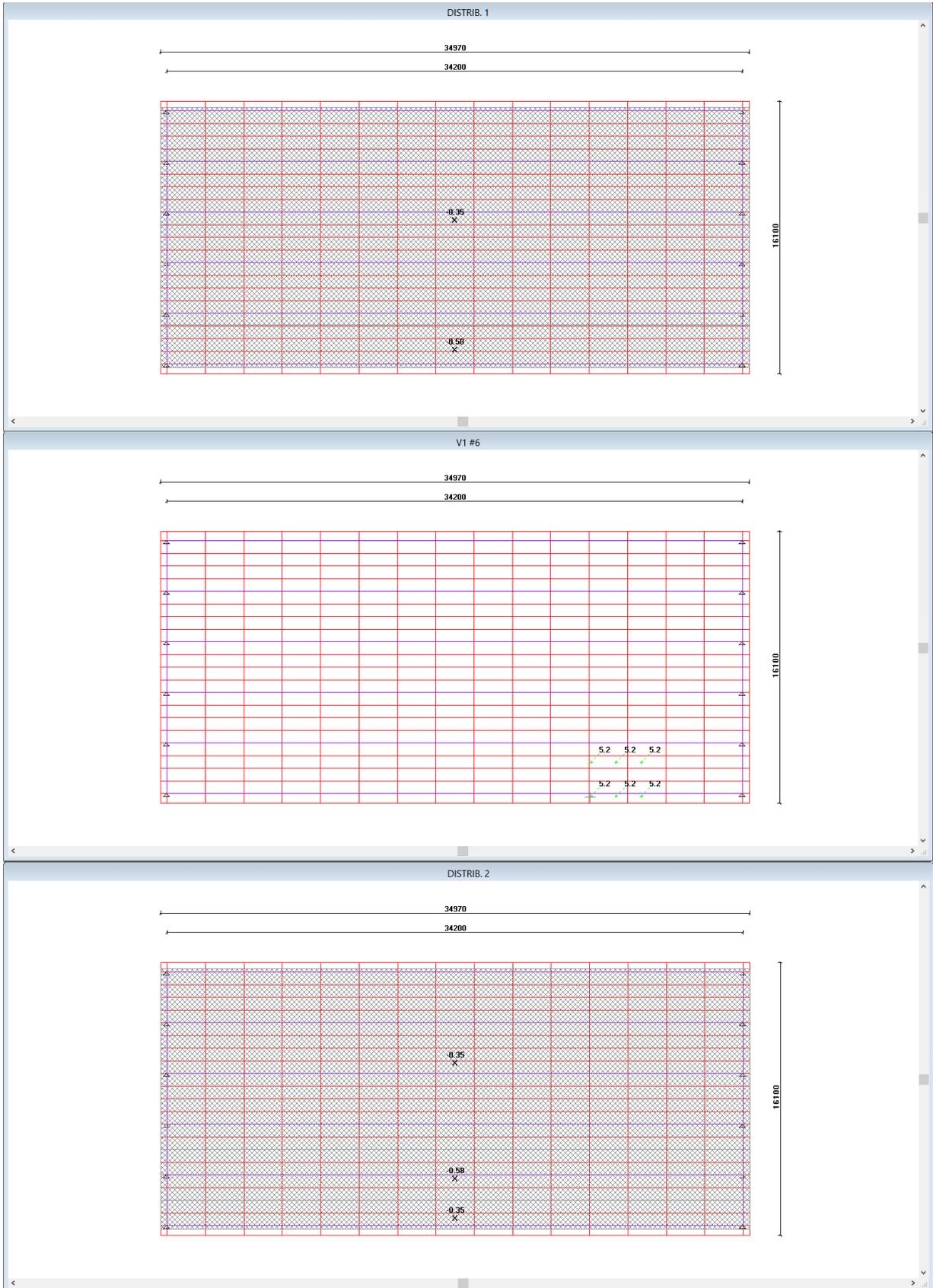


### NOTA TÉCNICA



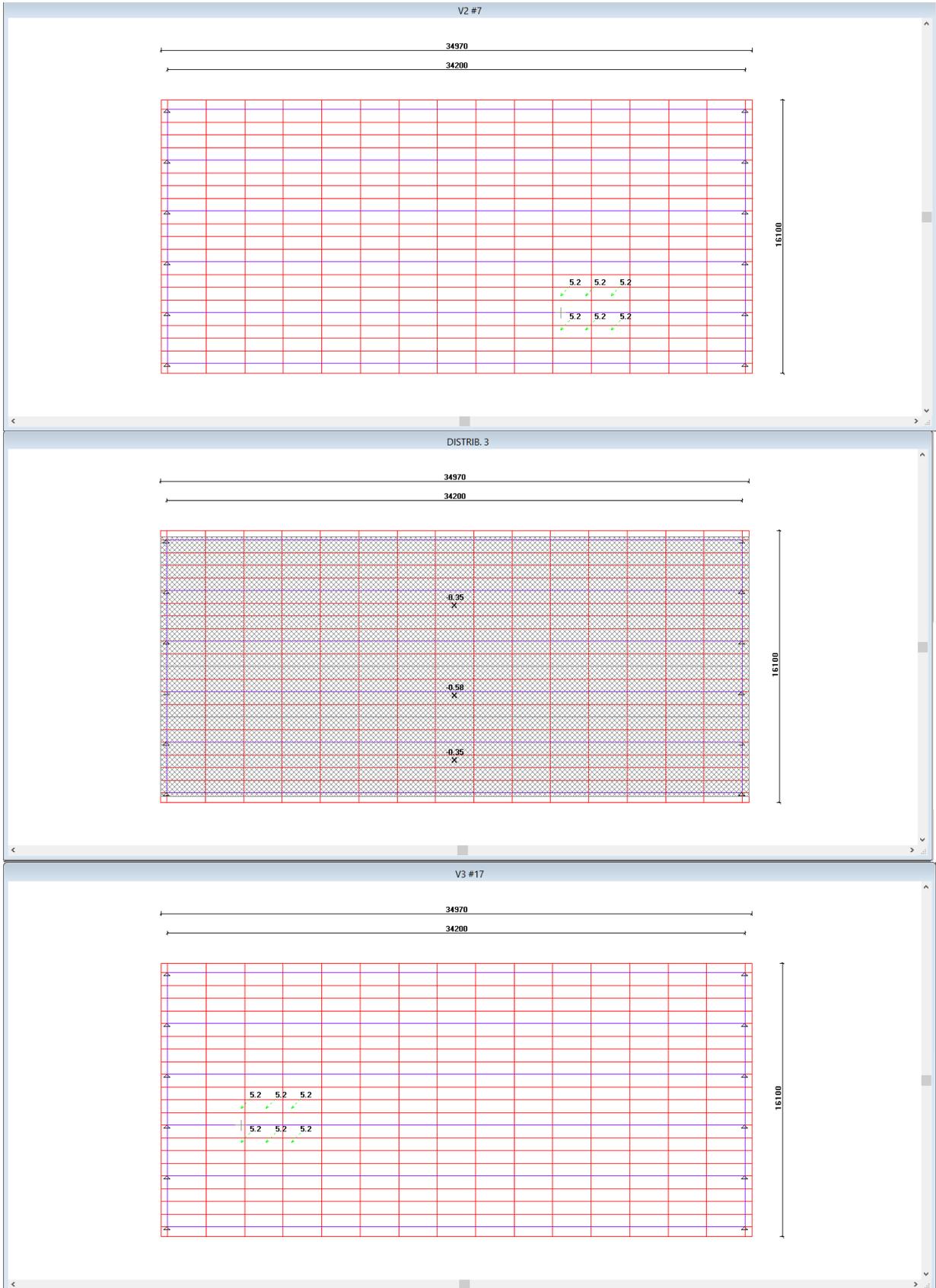


### NOTA TÉCNICA



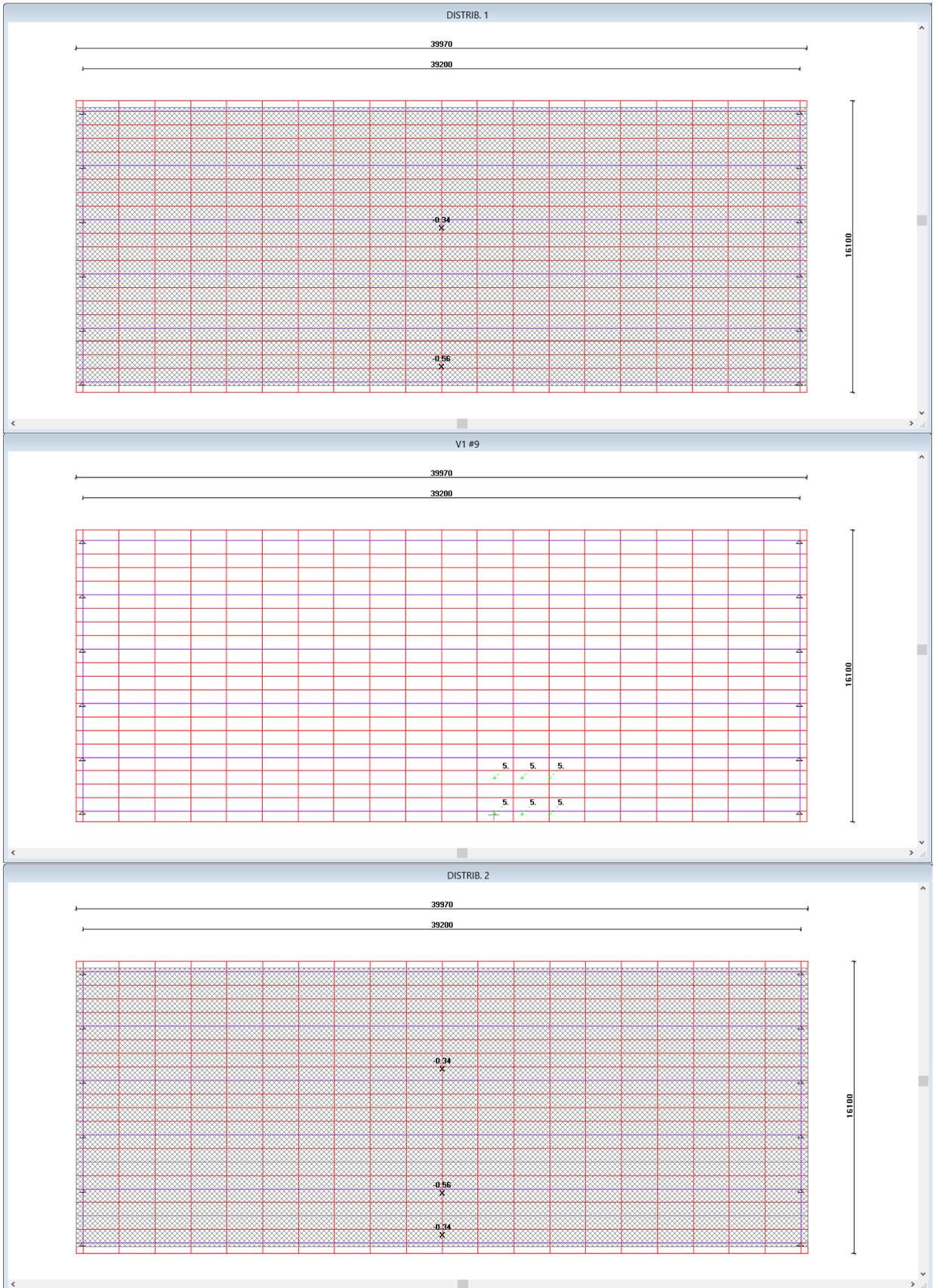


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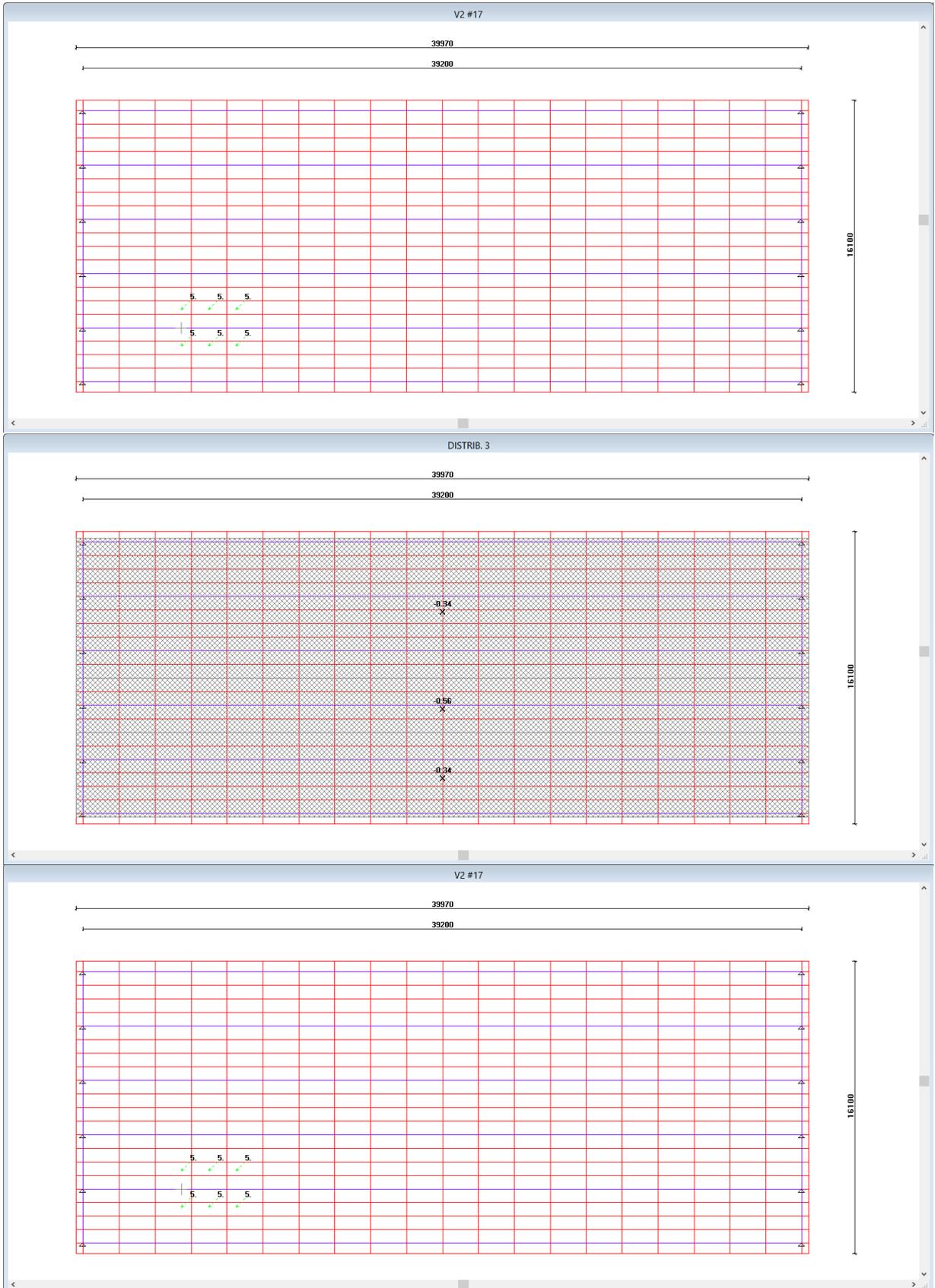


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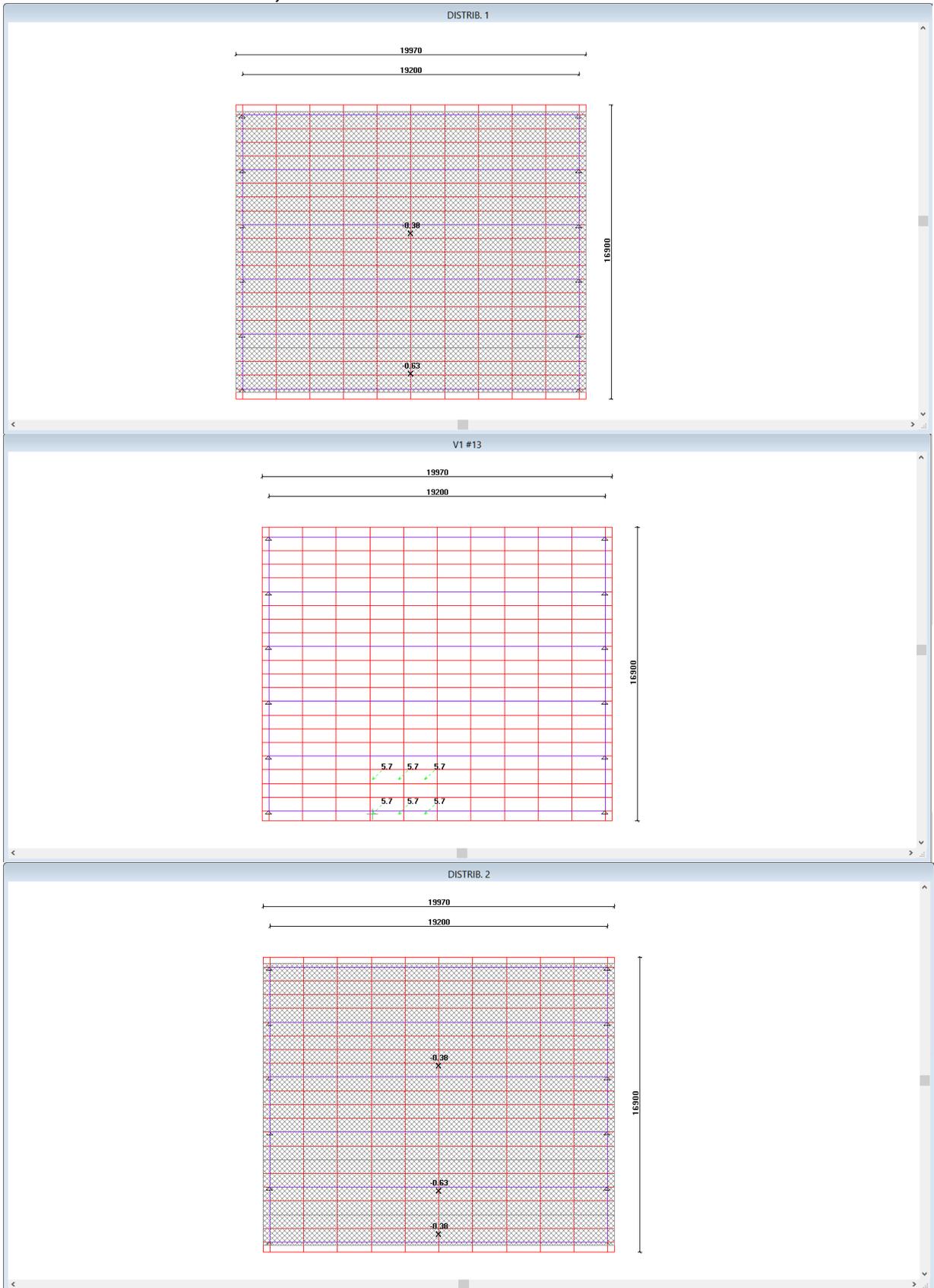
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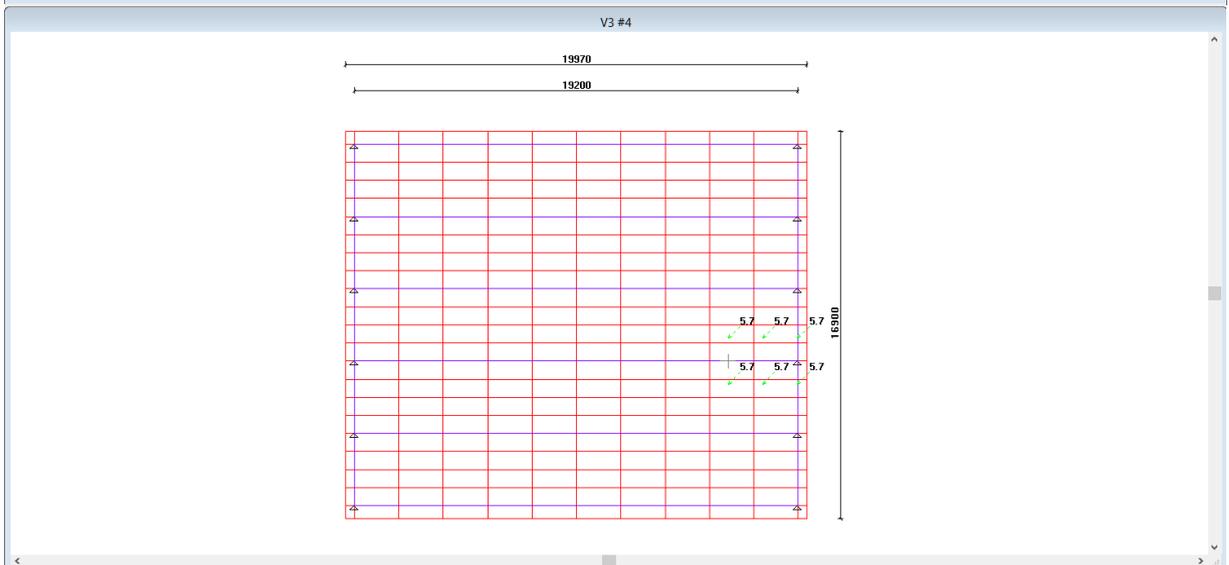
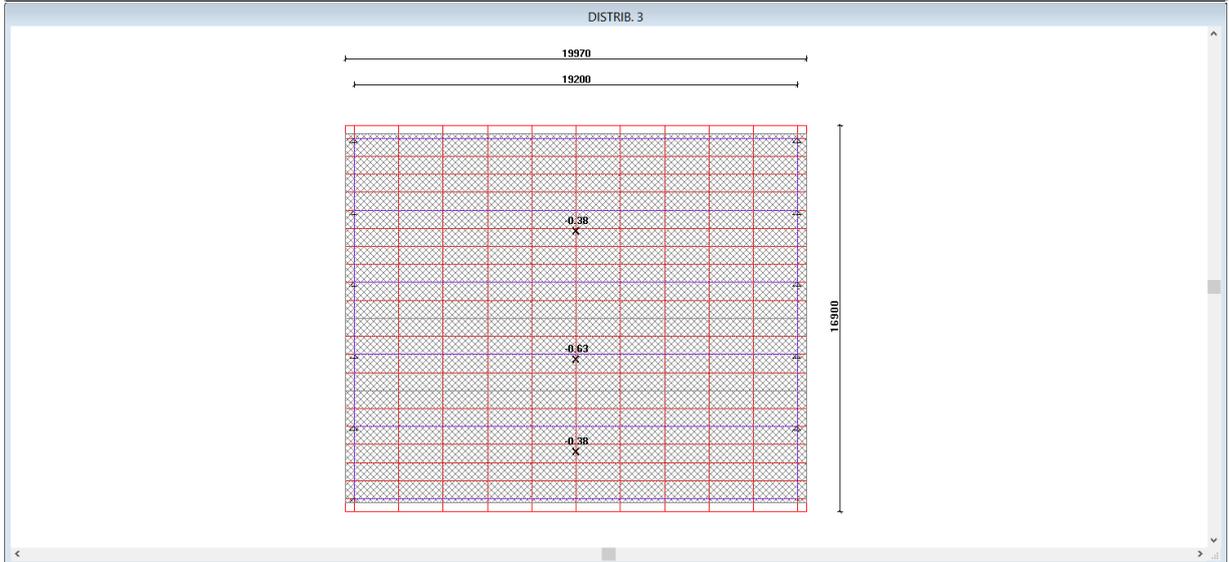
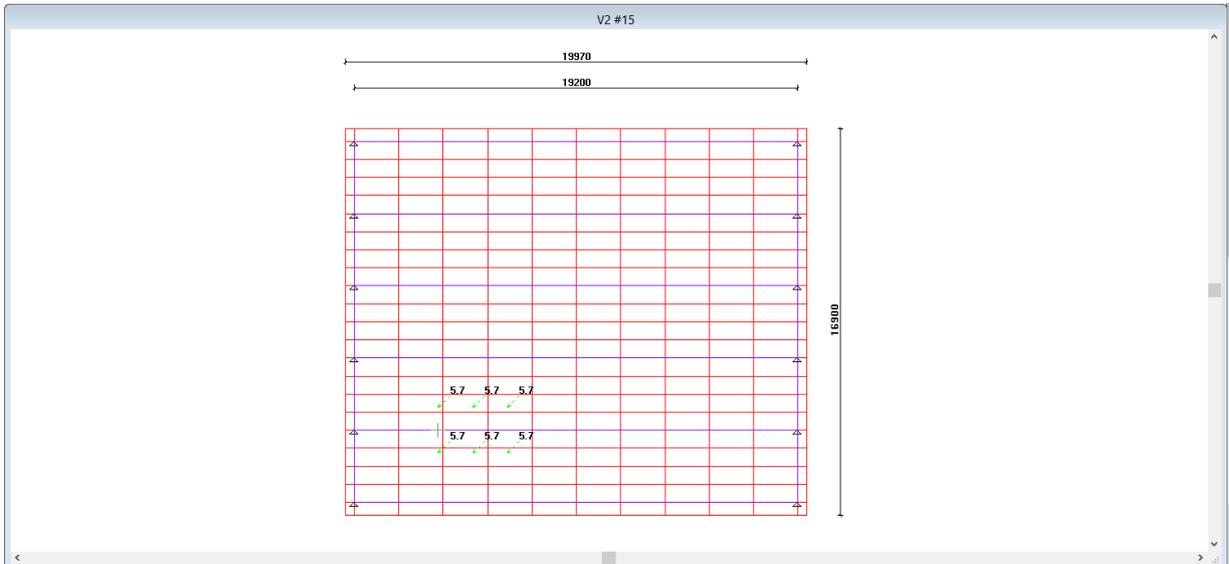
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#### 4.4.5. Tabuleiro 16,90 m



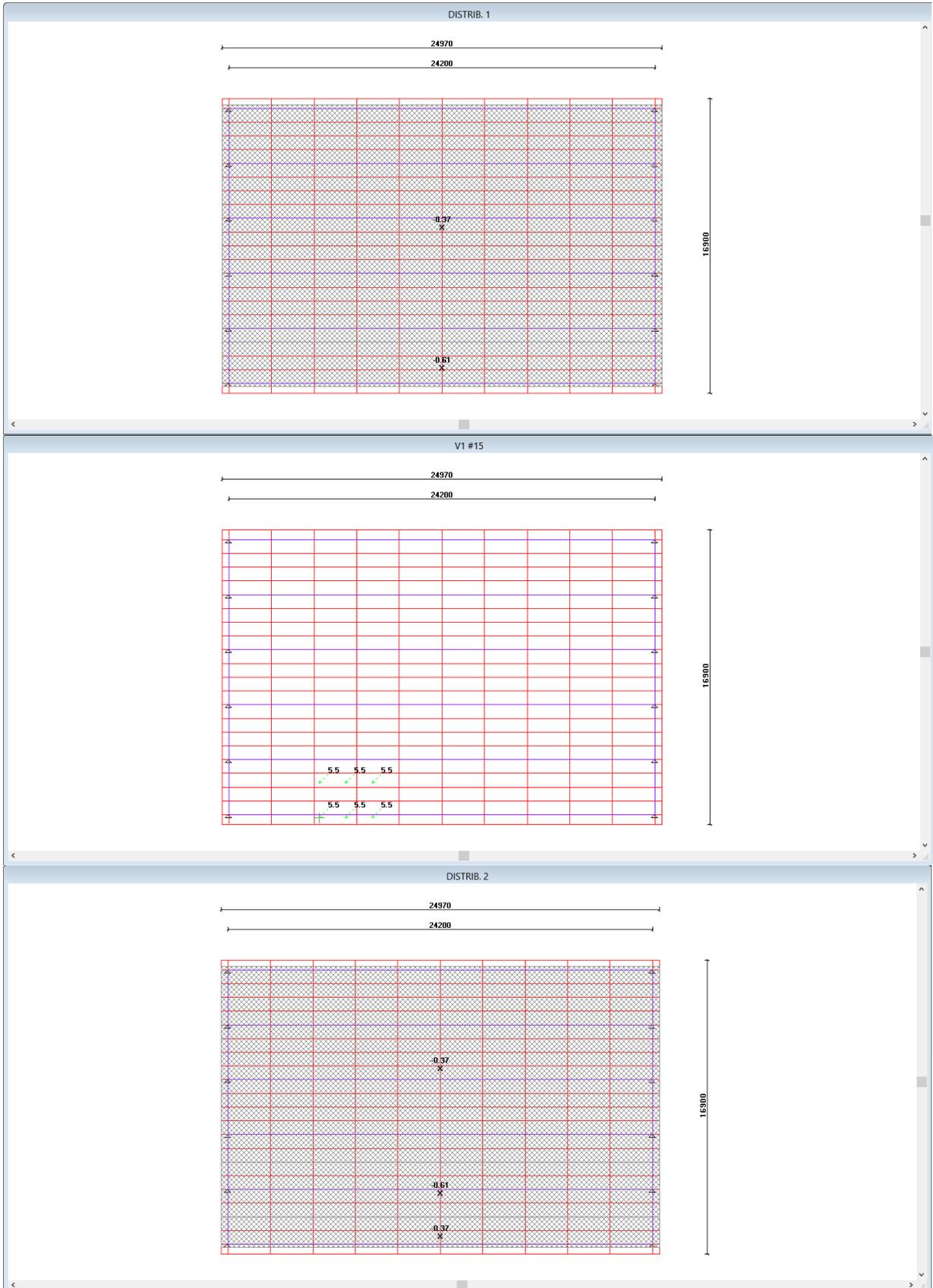


### NOTA TÉCNICA



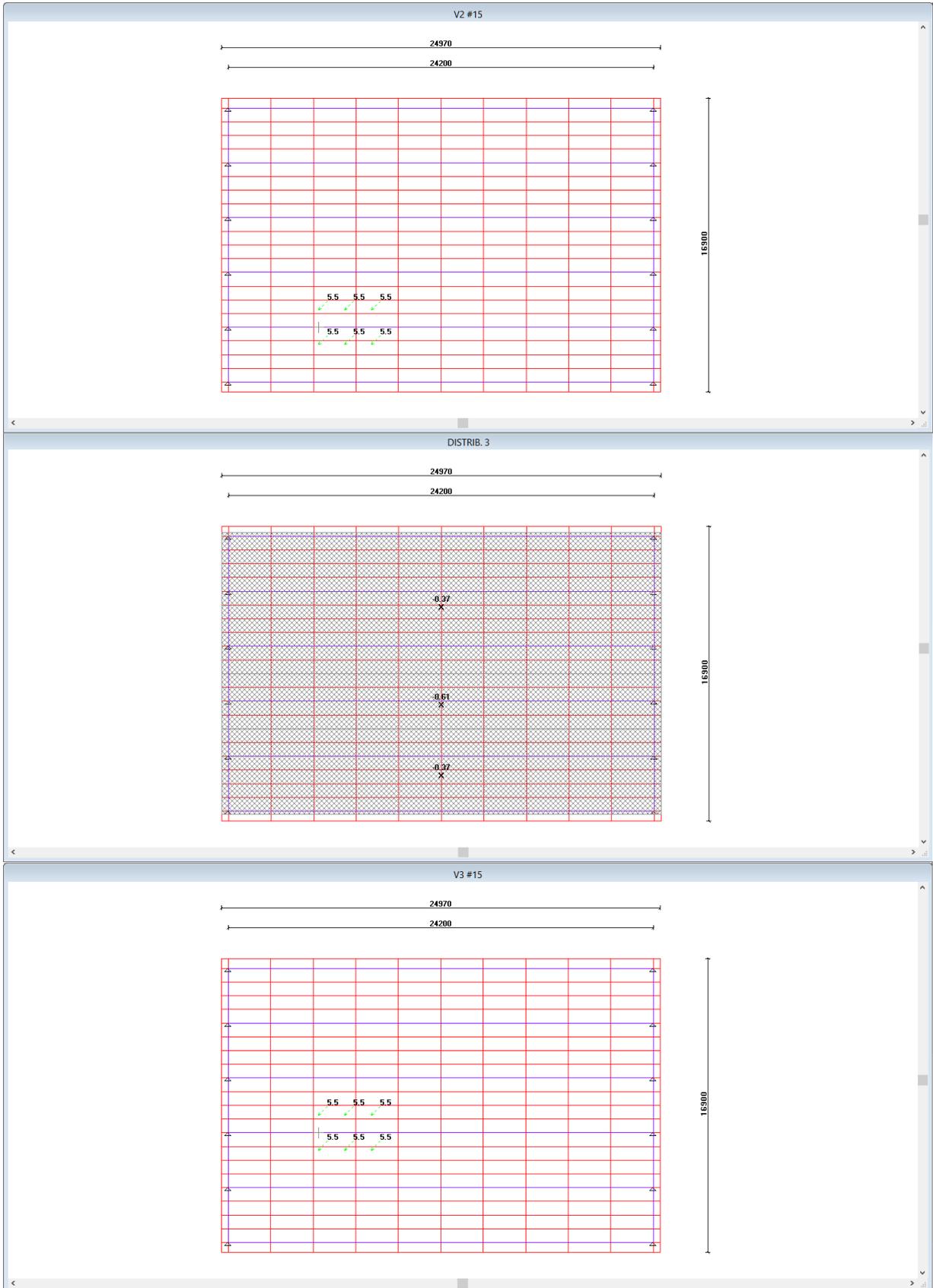


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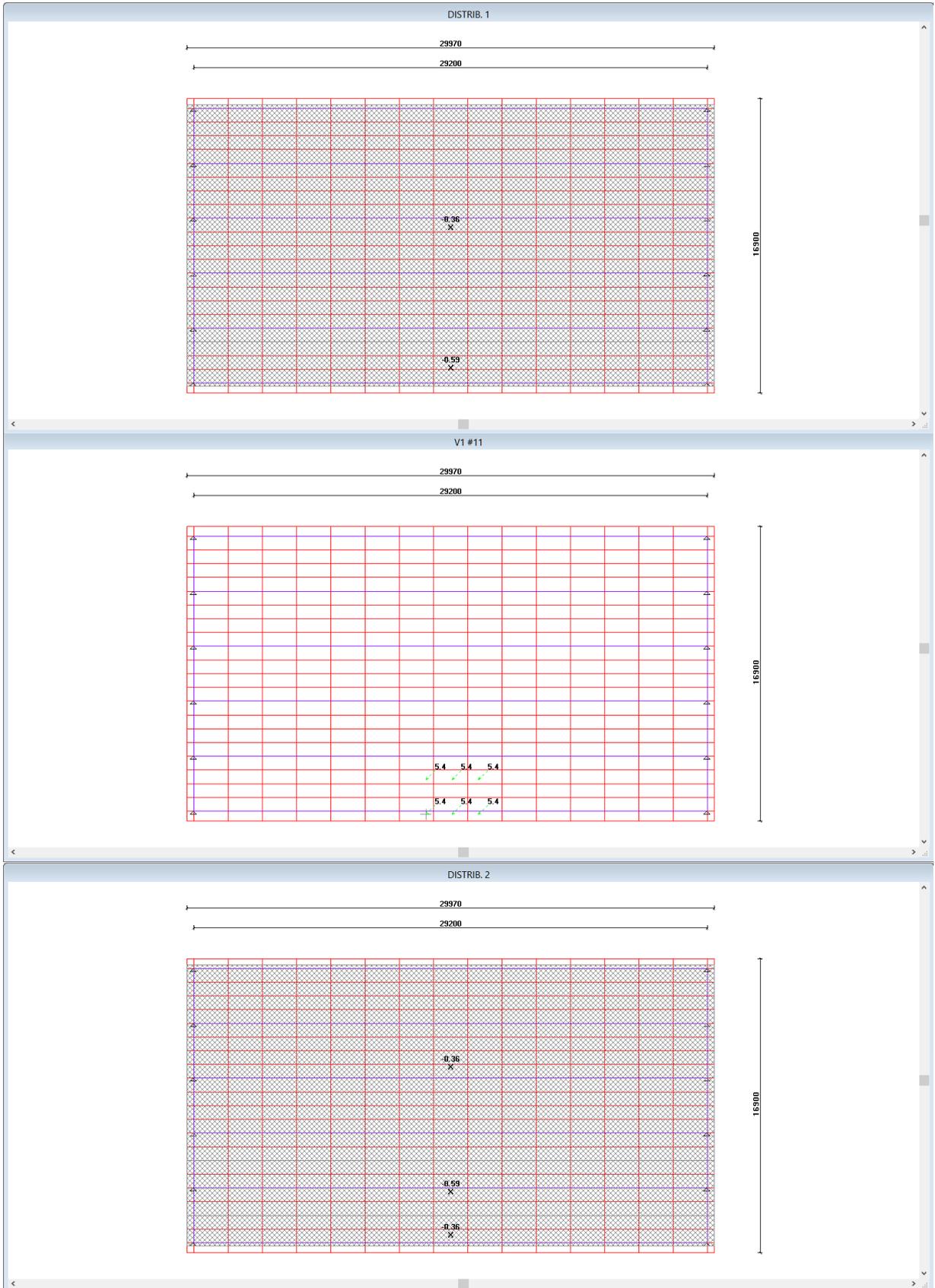


### NOTA TÉCNICA



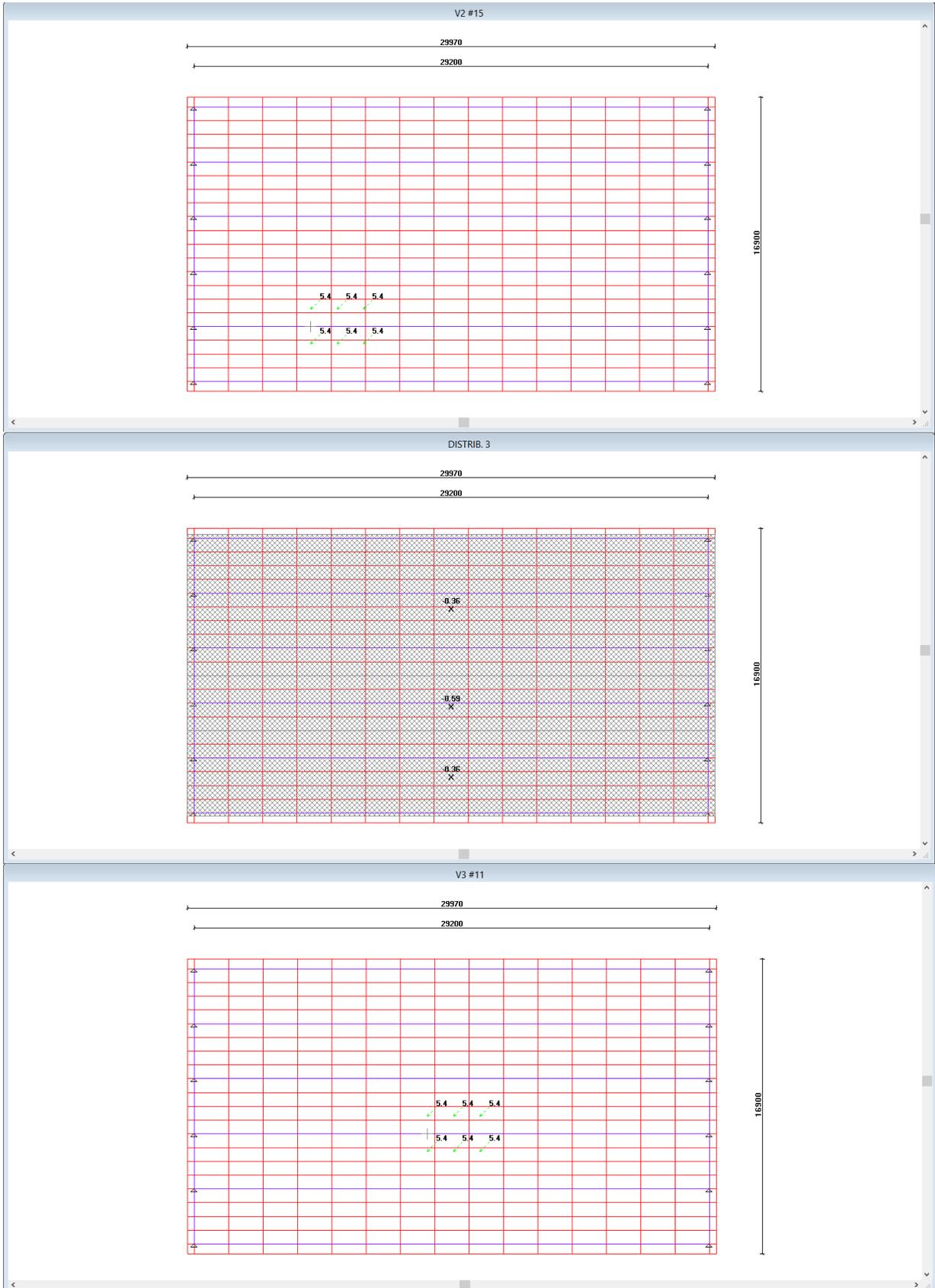


### NOTA TÉCNICA



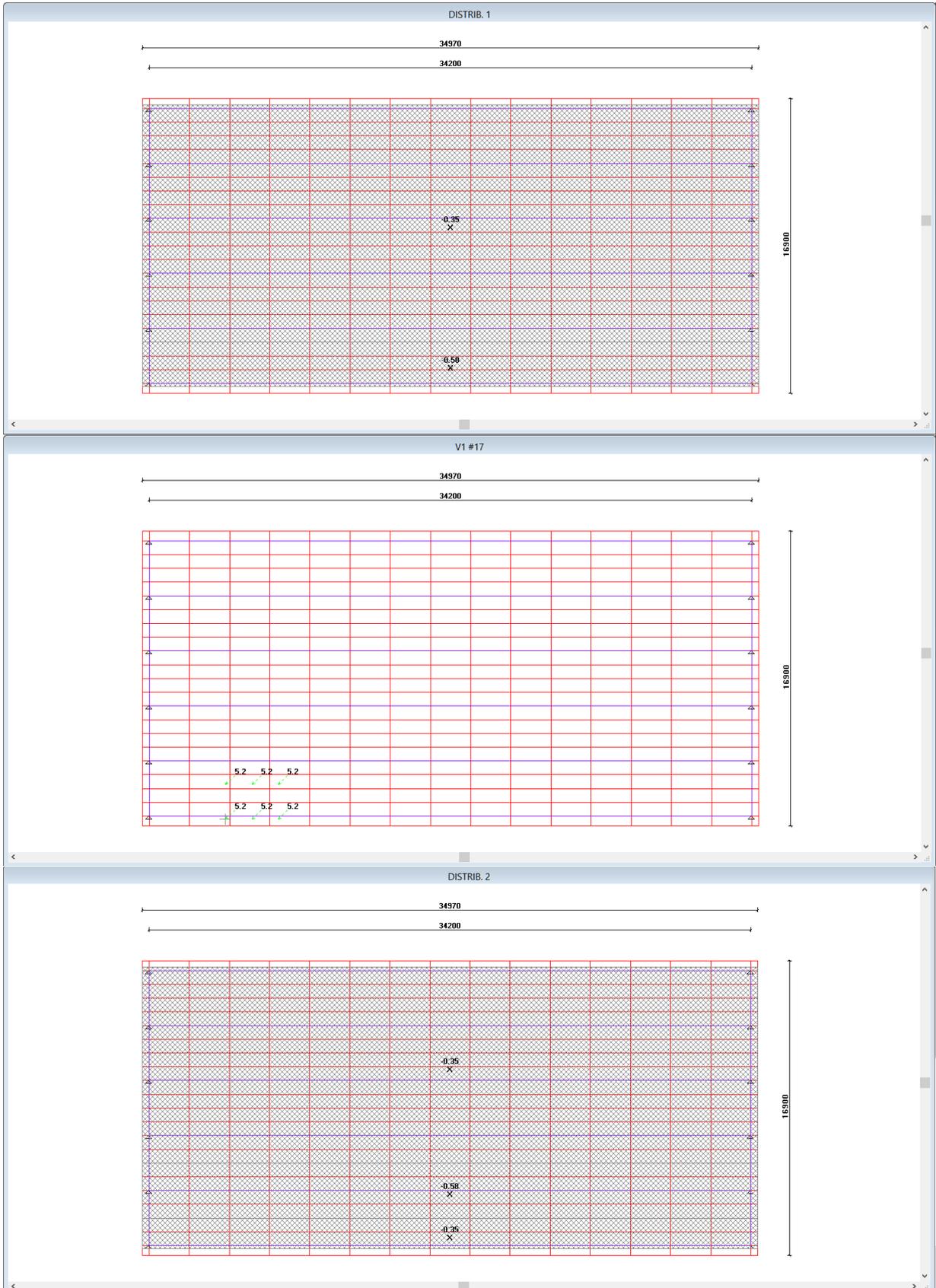


### NOTA TÉCNICA



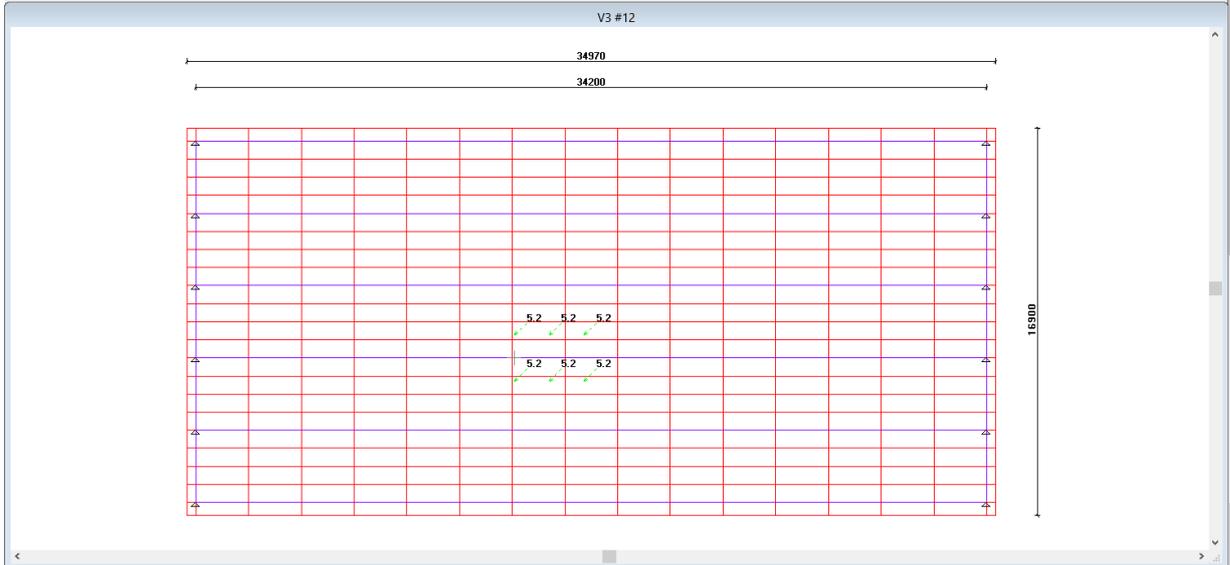
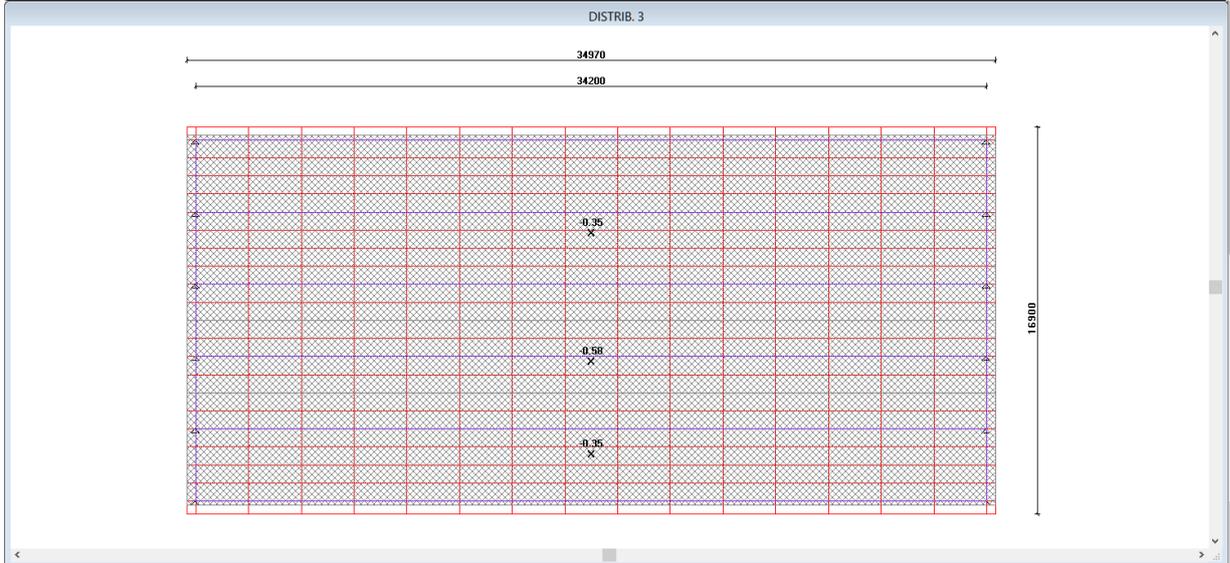
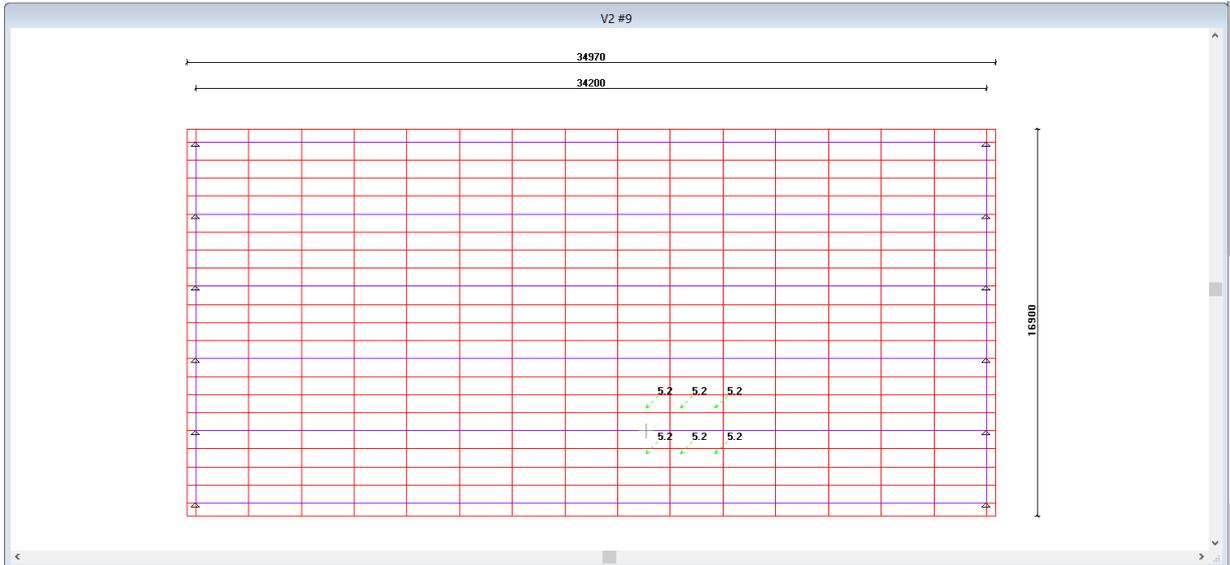


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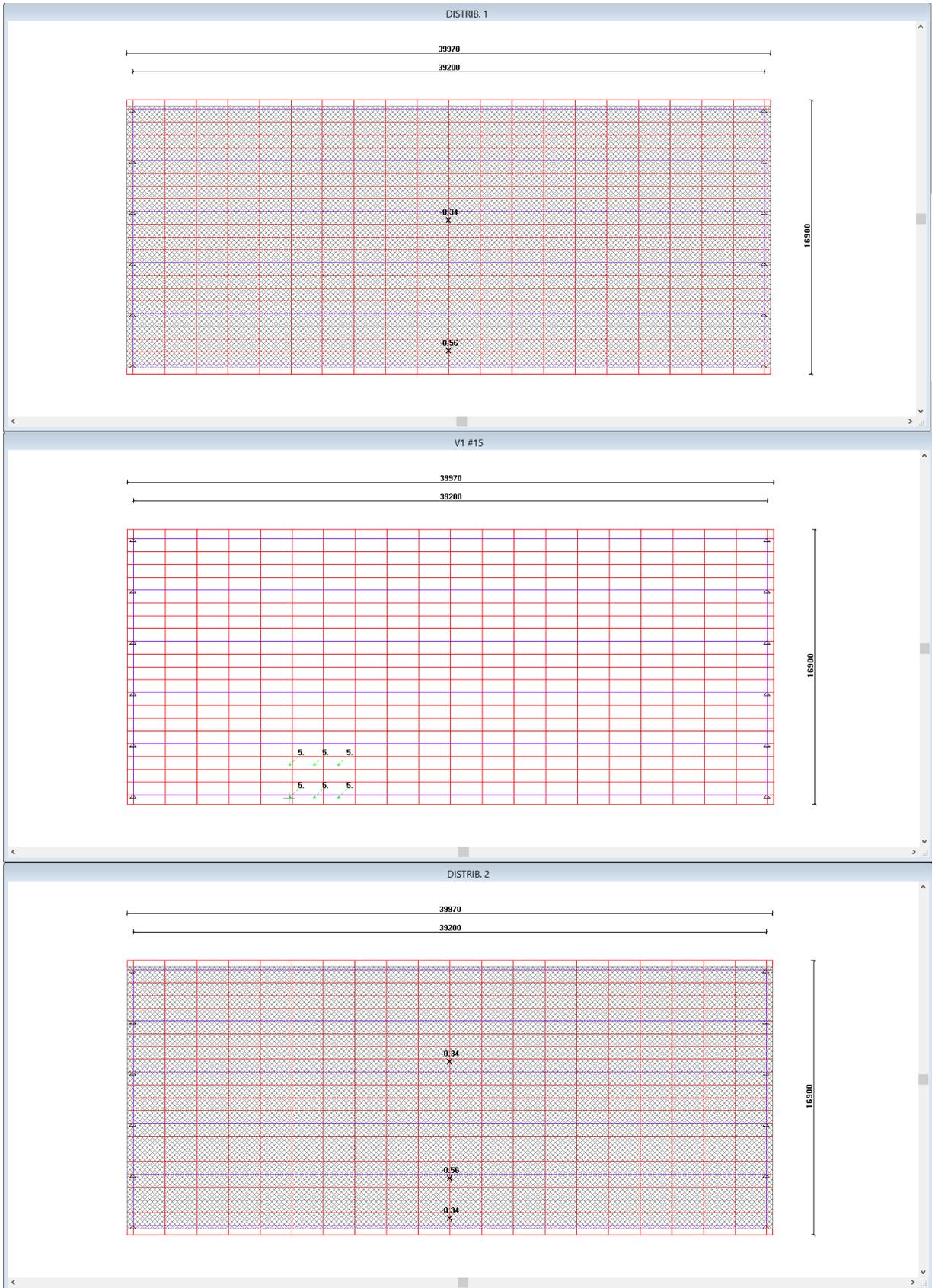


### NOTA TÉCNICA



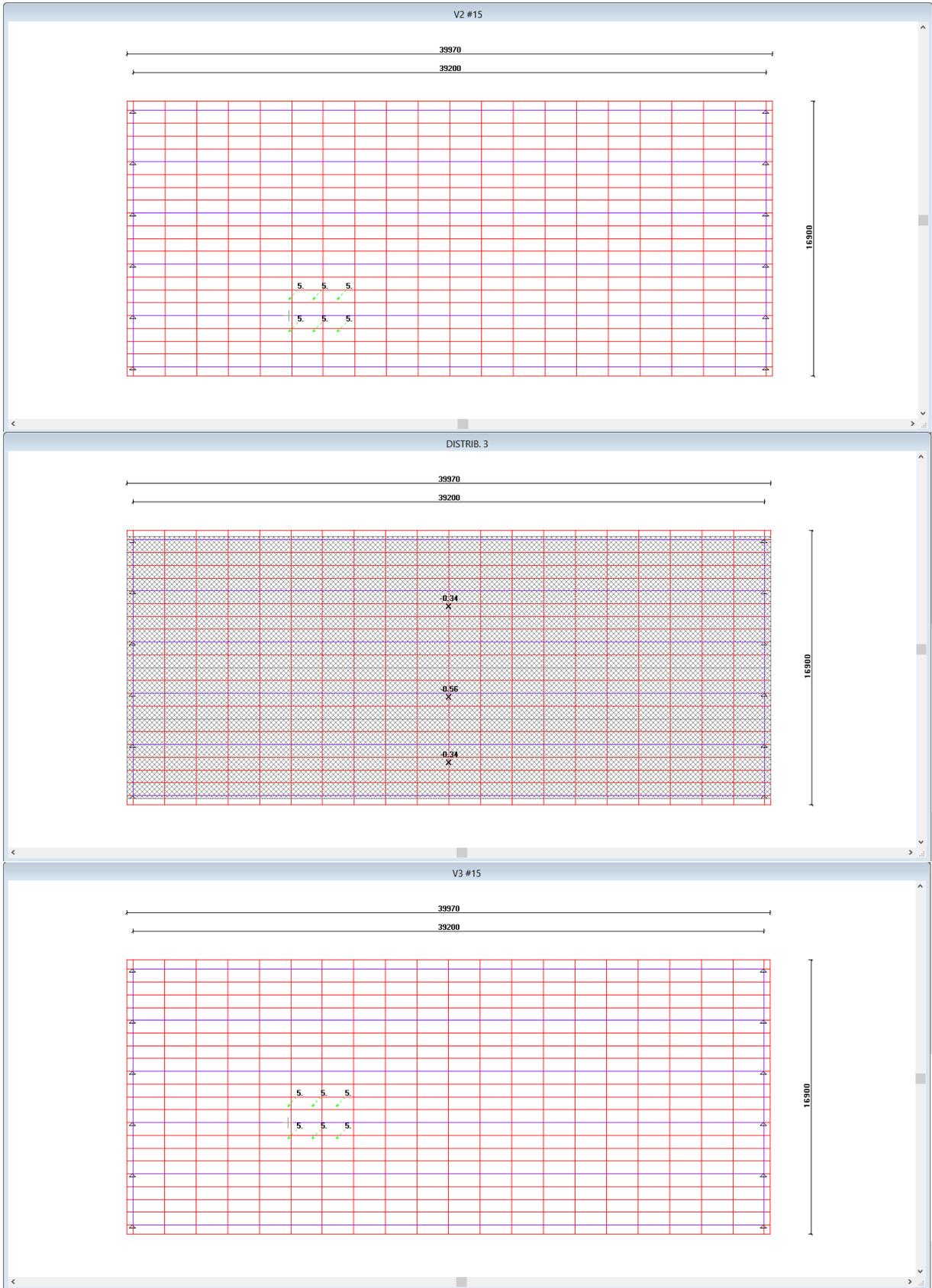


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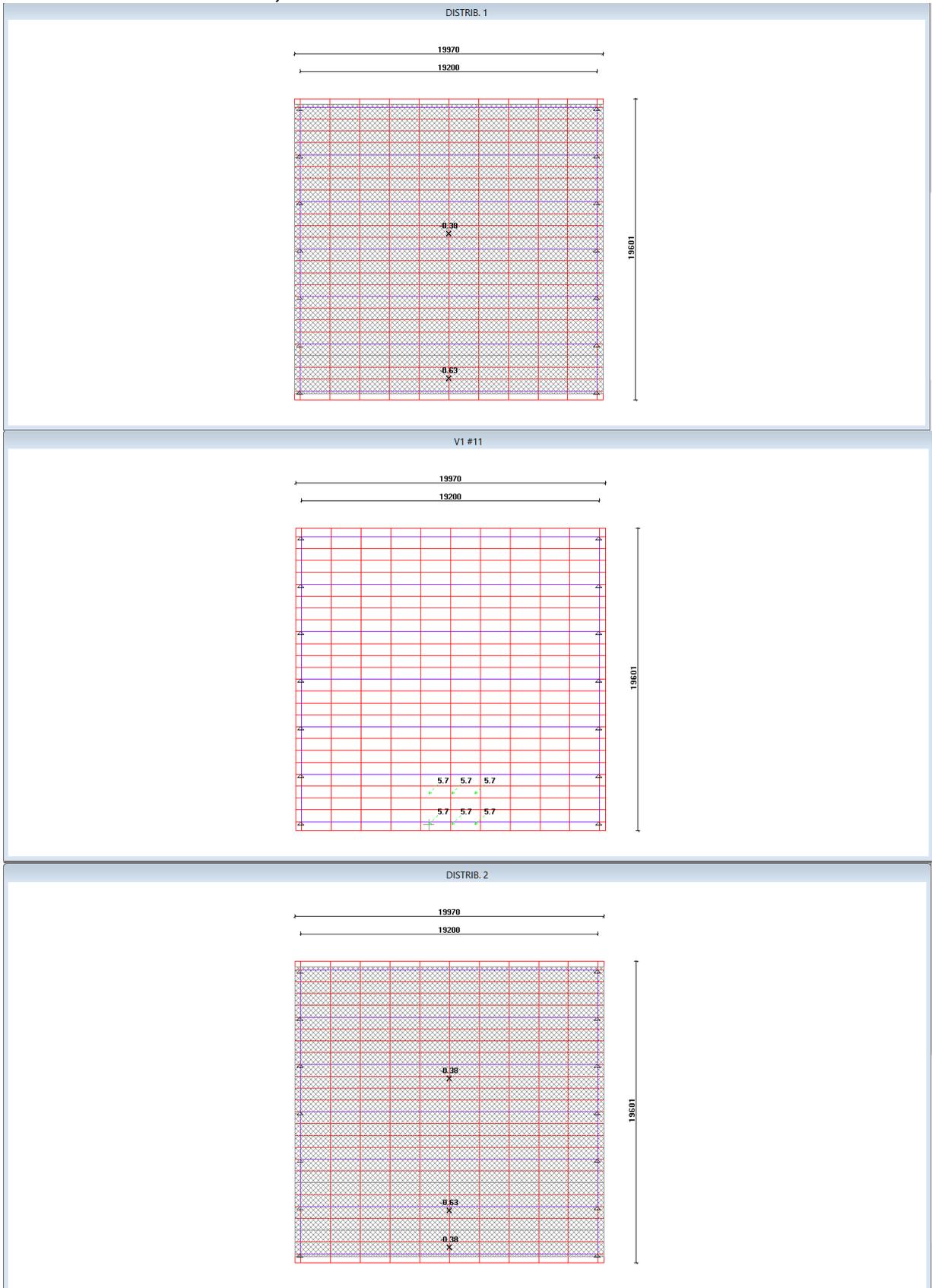
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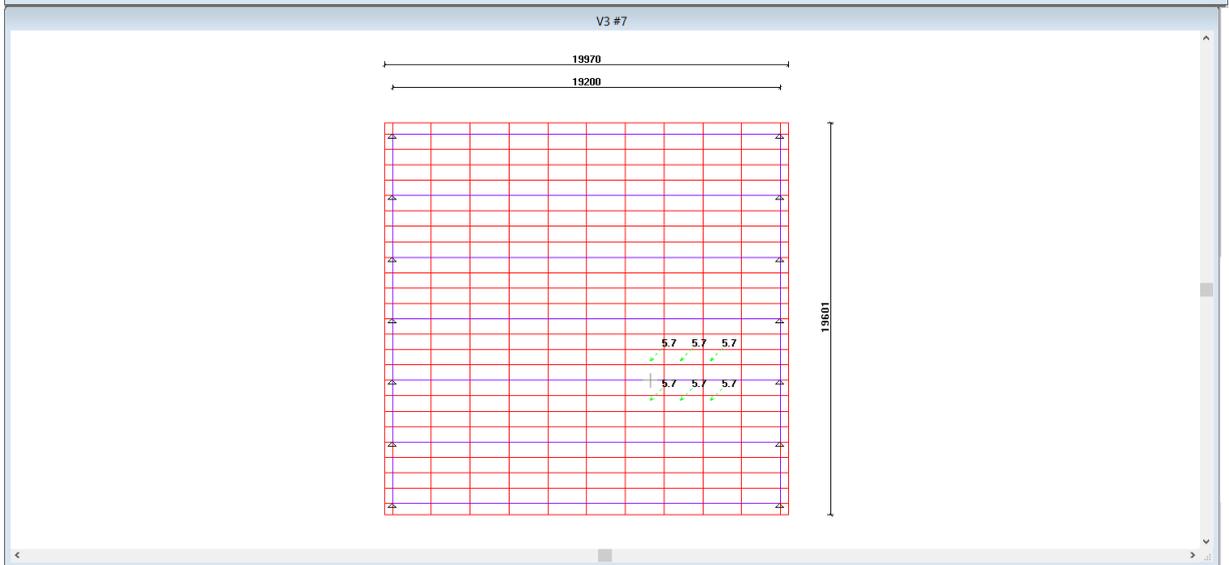
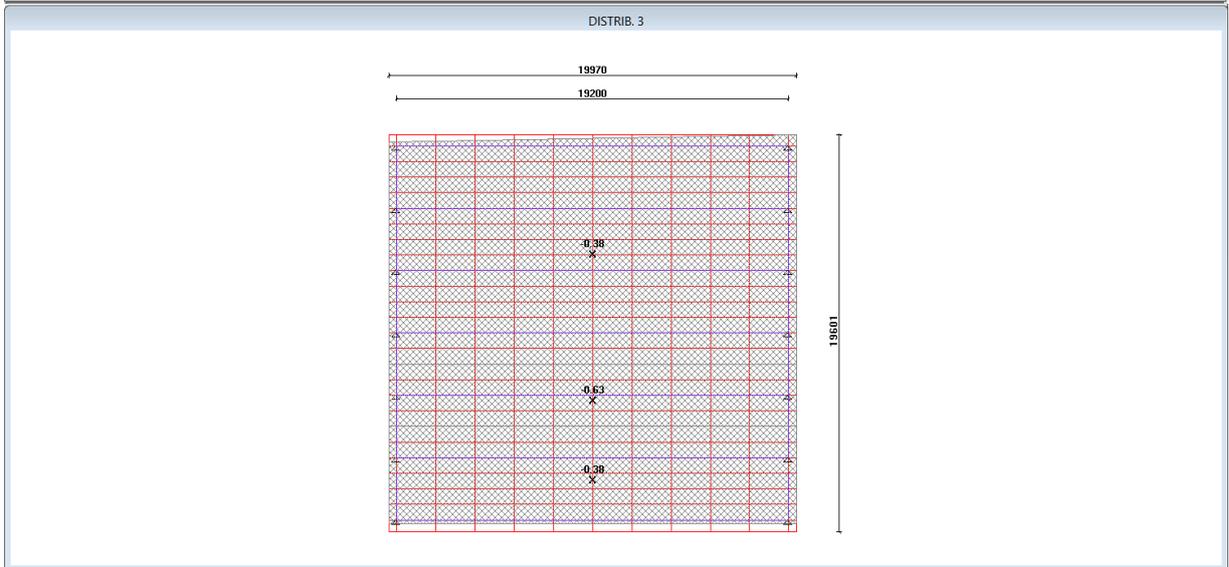
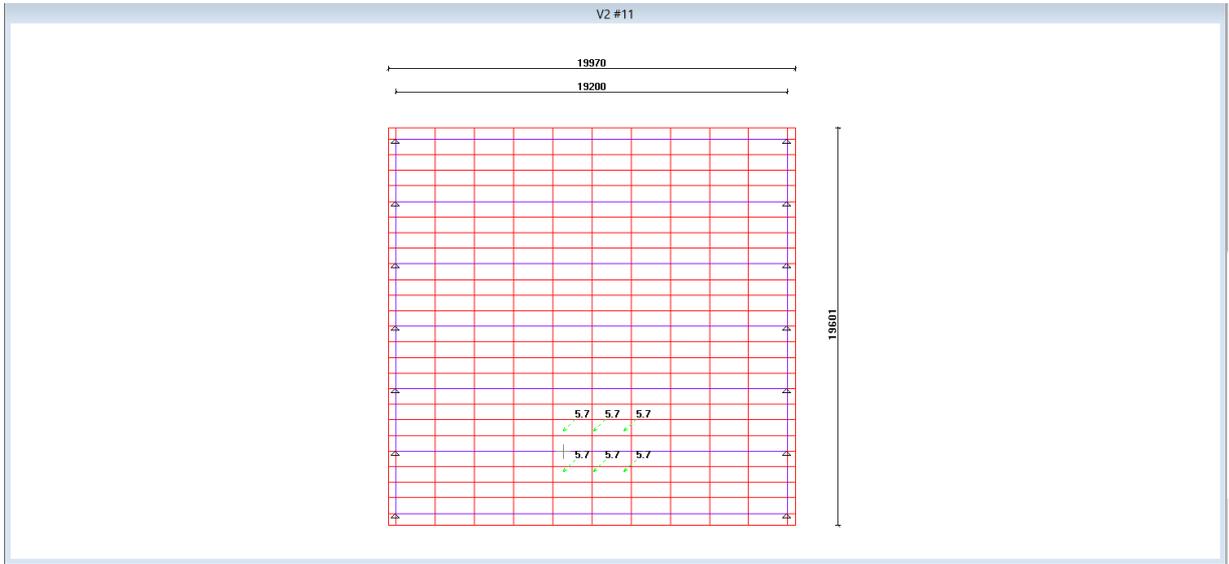
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#### 4.4.6. Tabuleiro 19,60 m



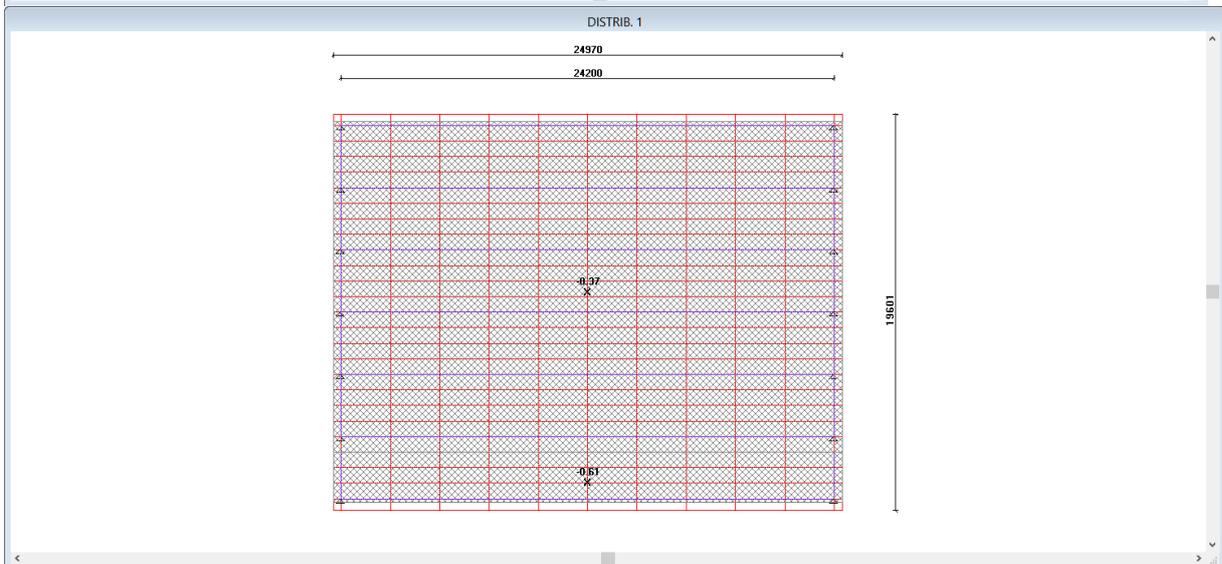
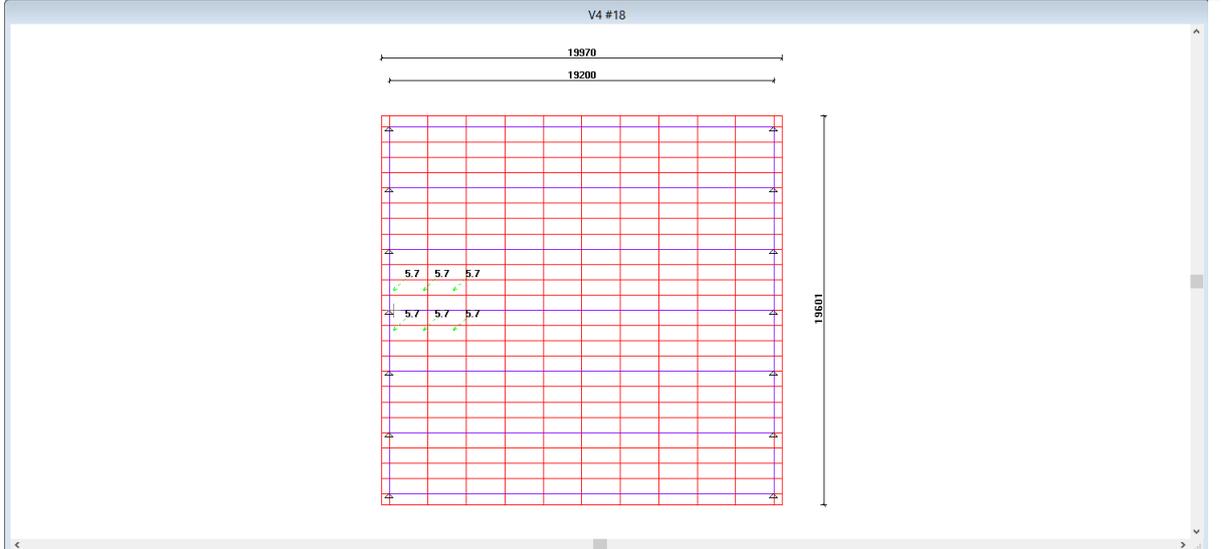
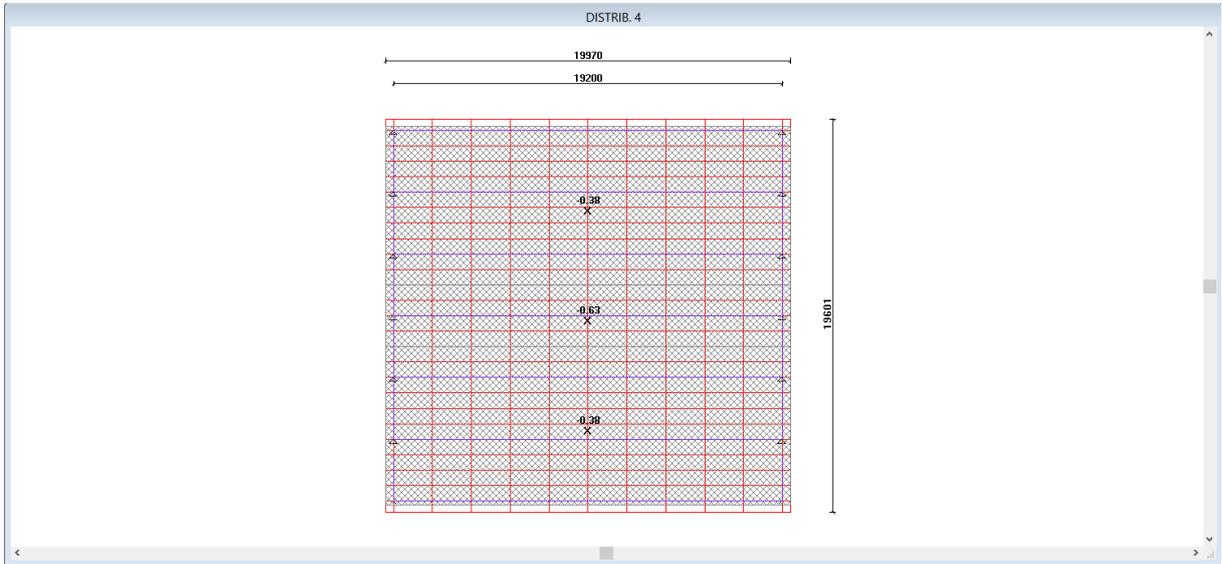


### NOTA TÉCNICA





### NOTA TÉCNICA



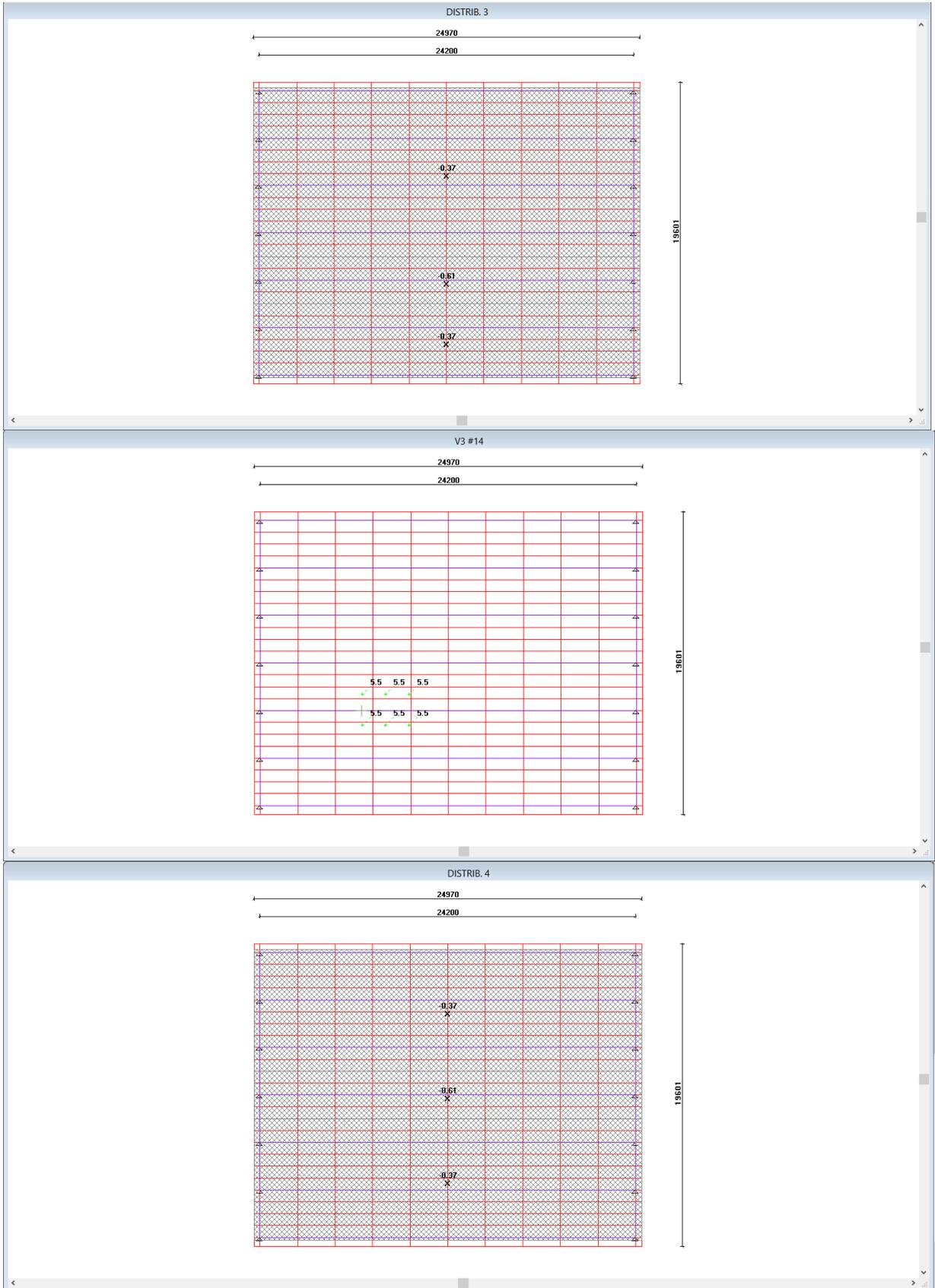


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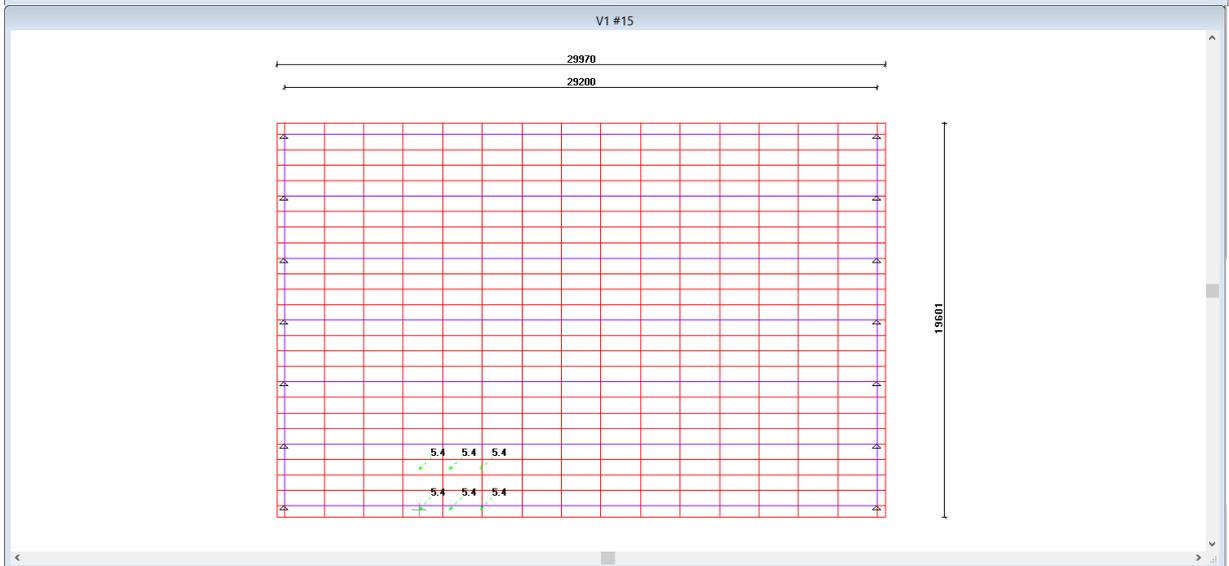
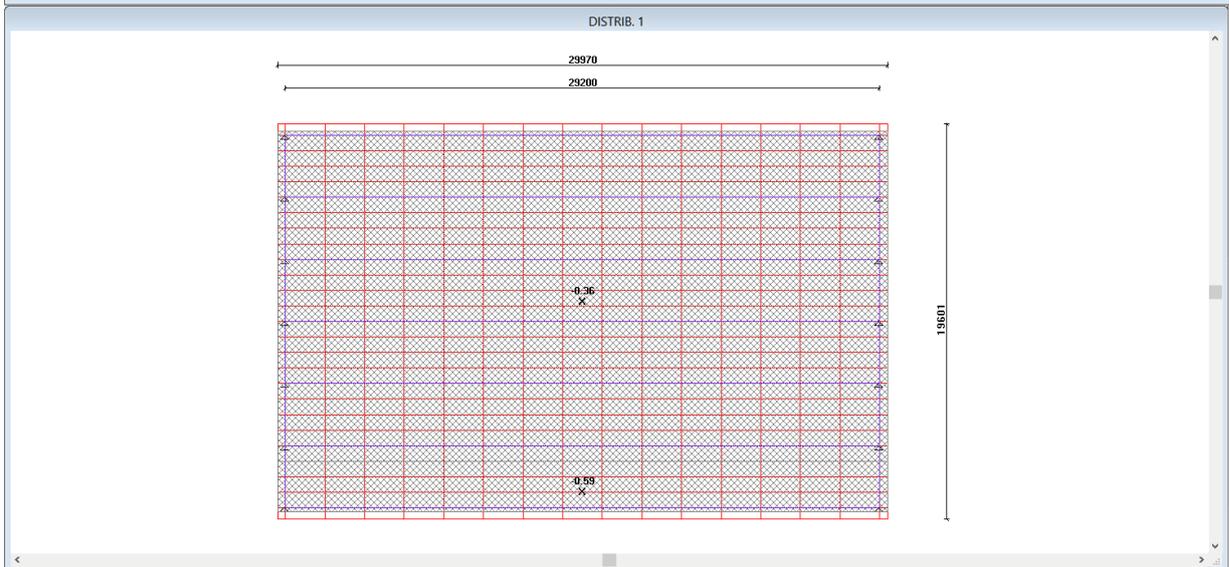
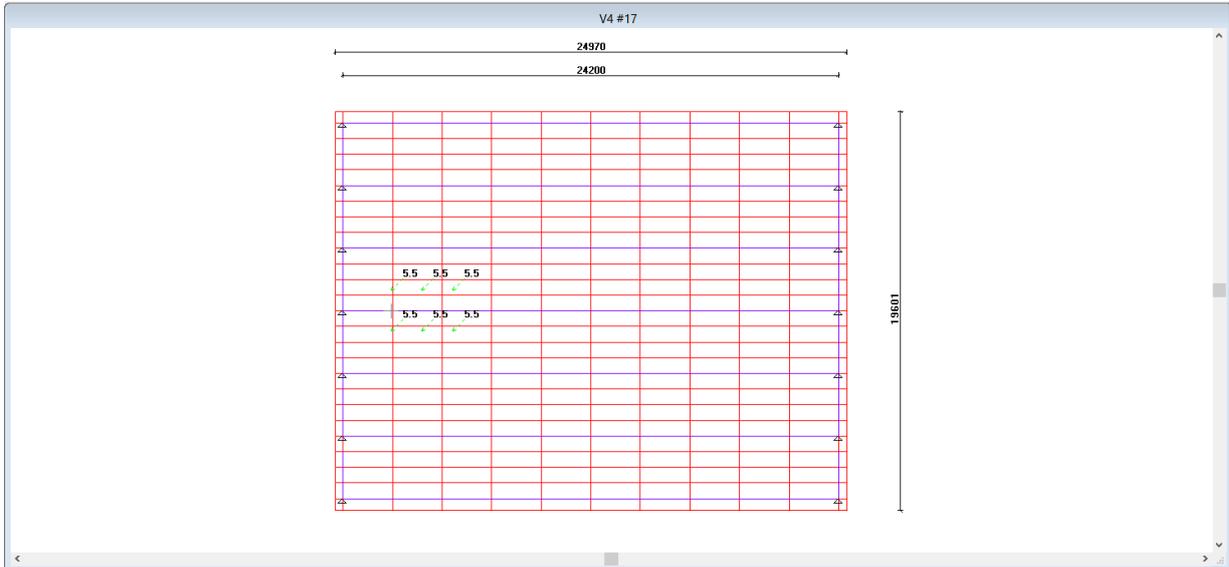


### NOTA TÉCNICA



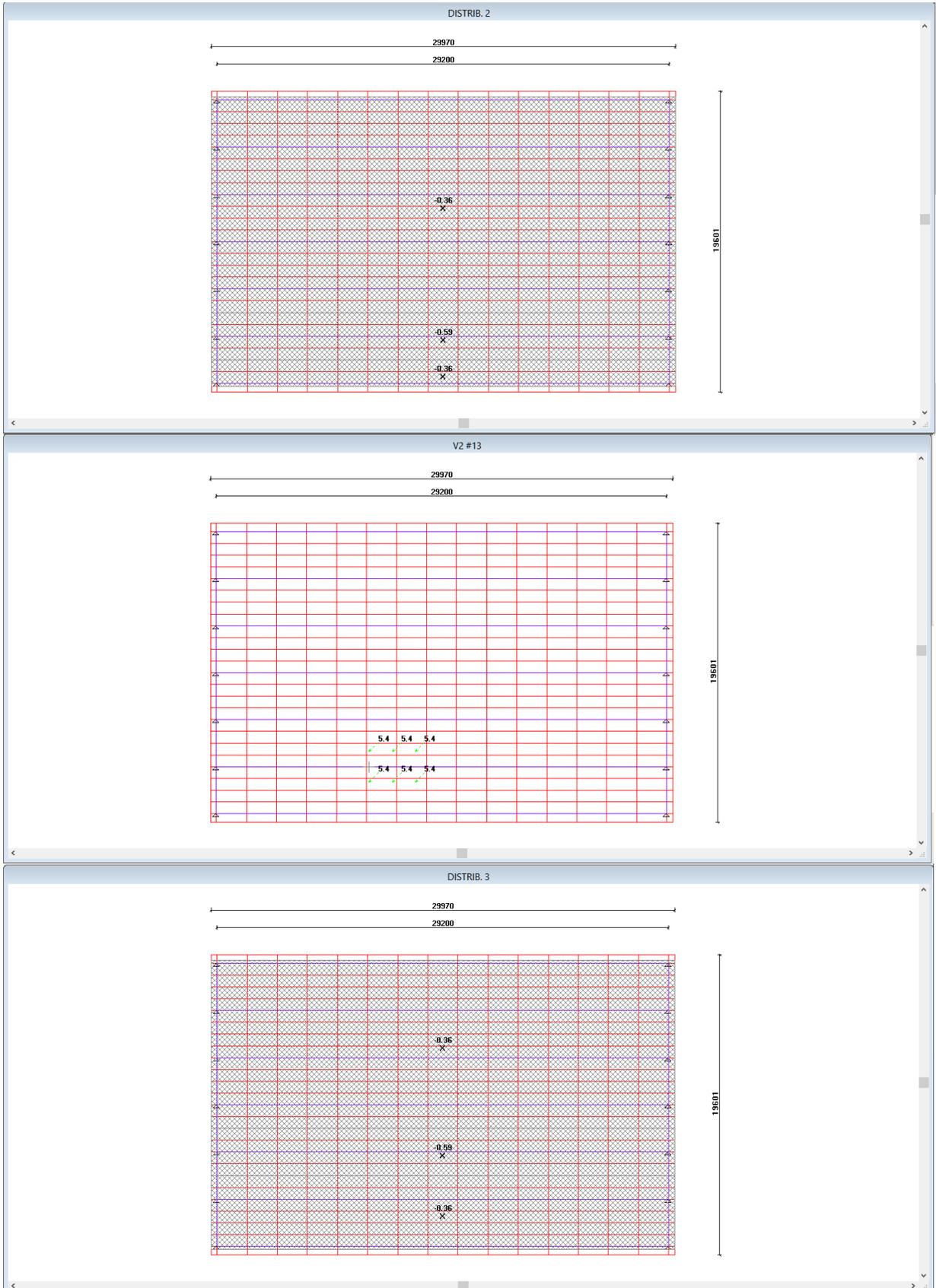


### NOTA TÉCNICA



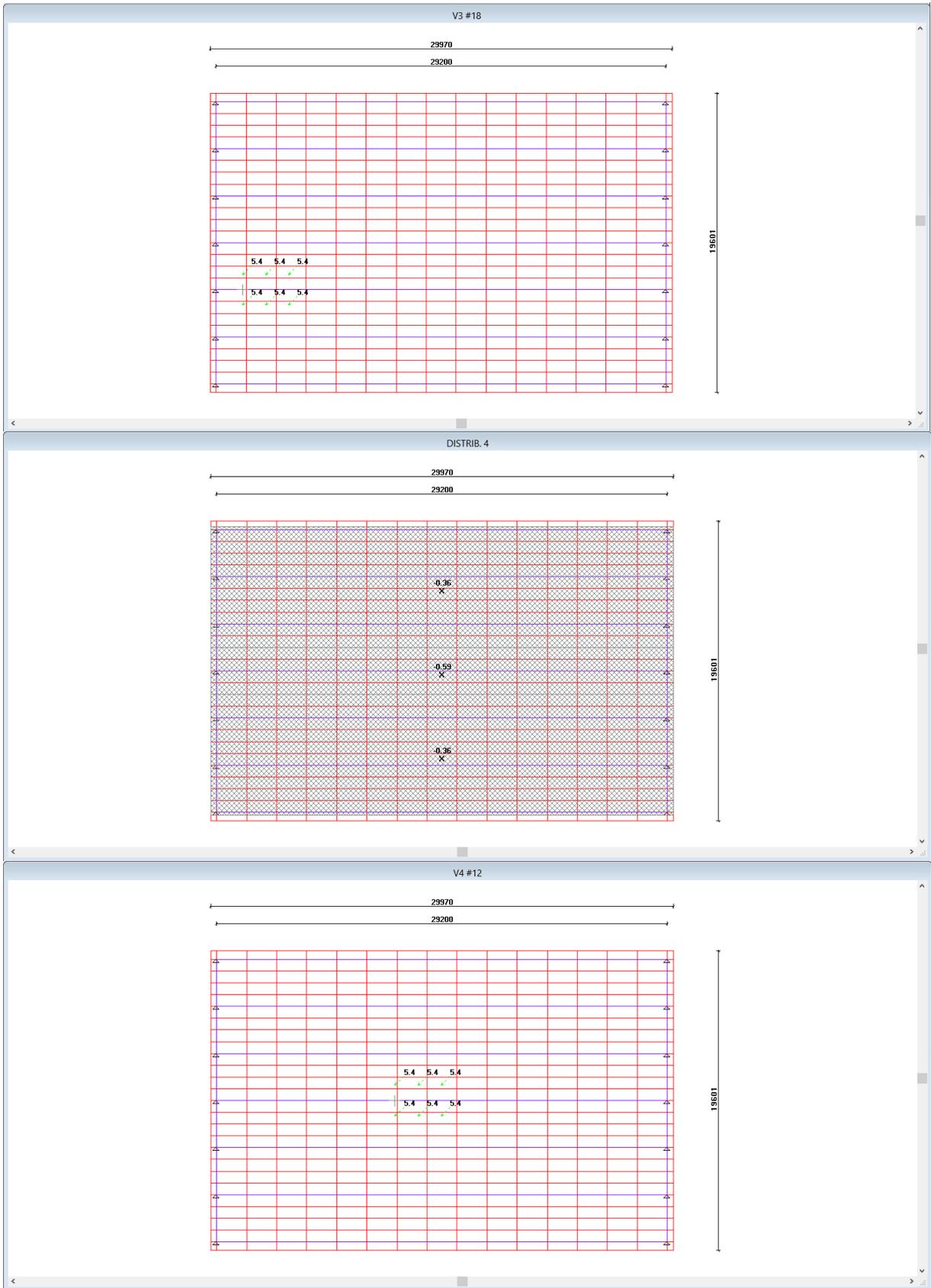


### NOTA TÉCNICA



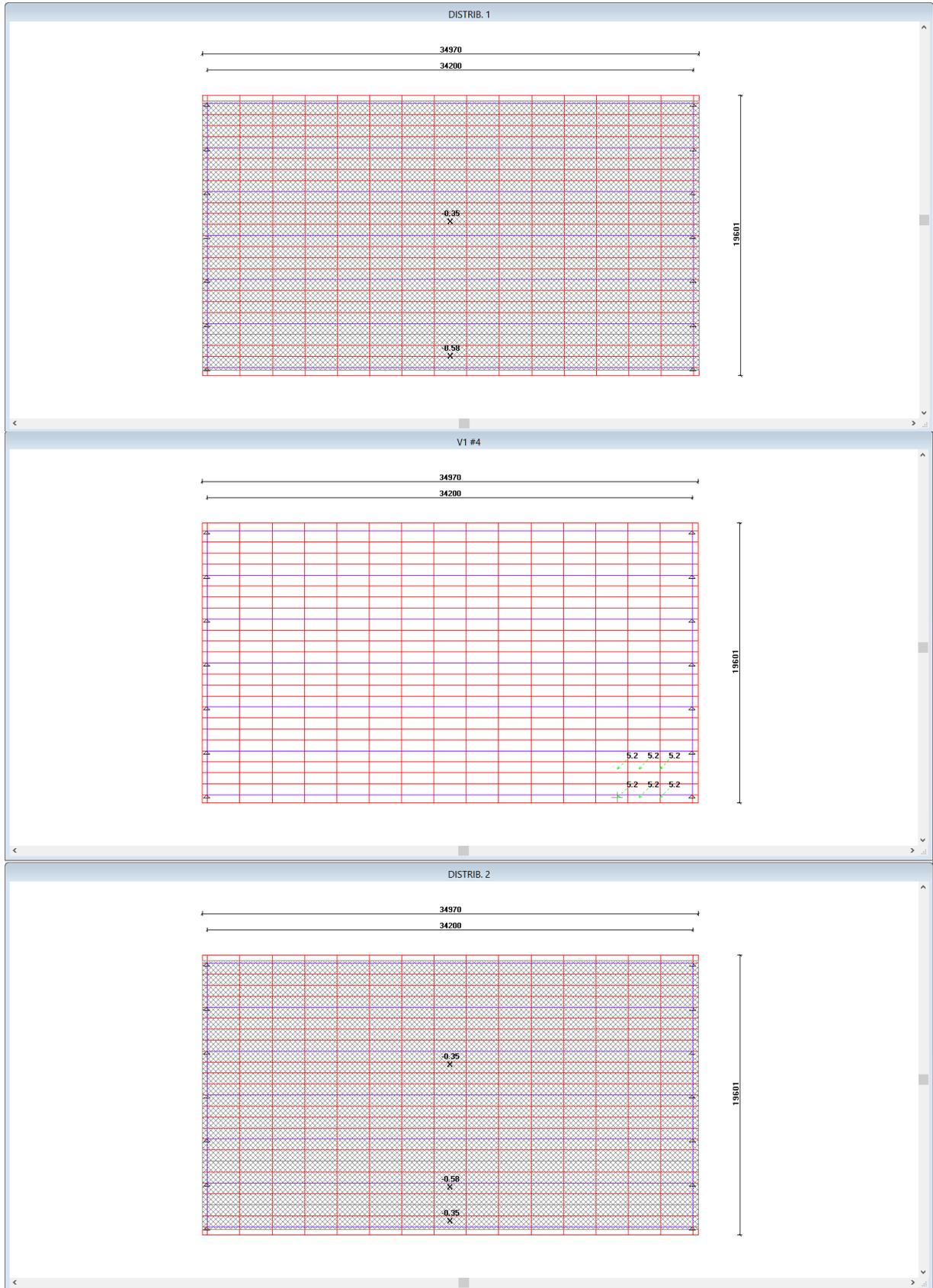


### NOTA TÉCNICA



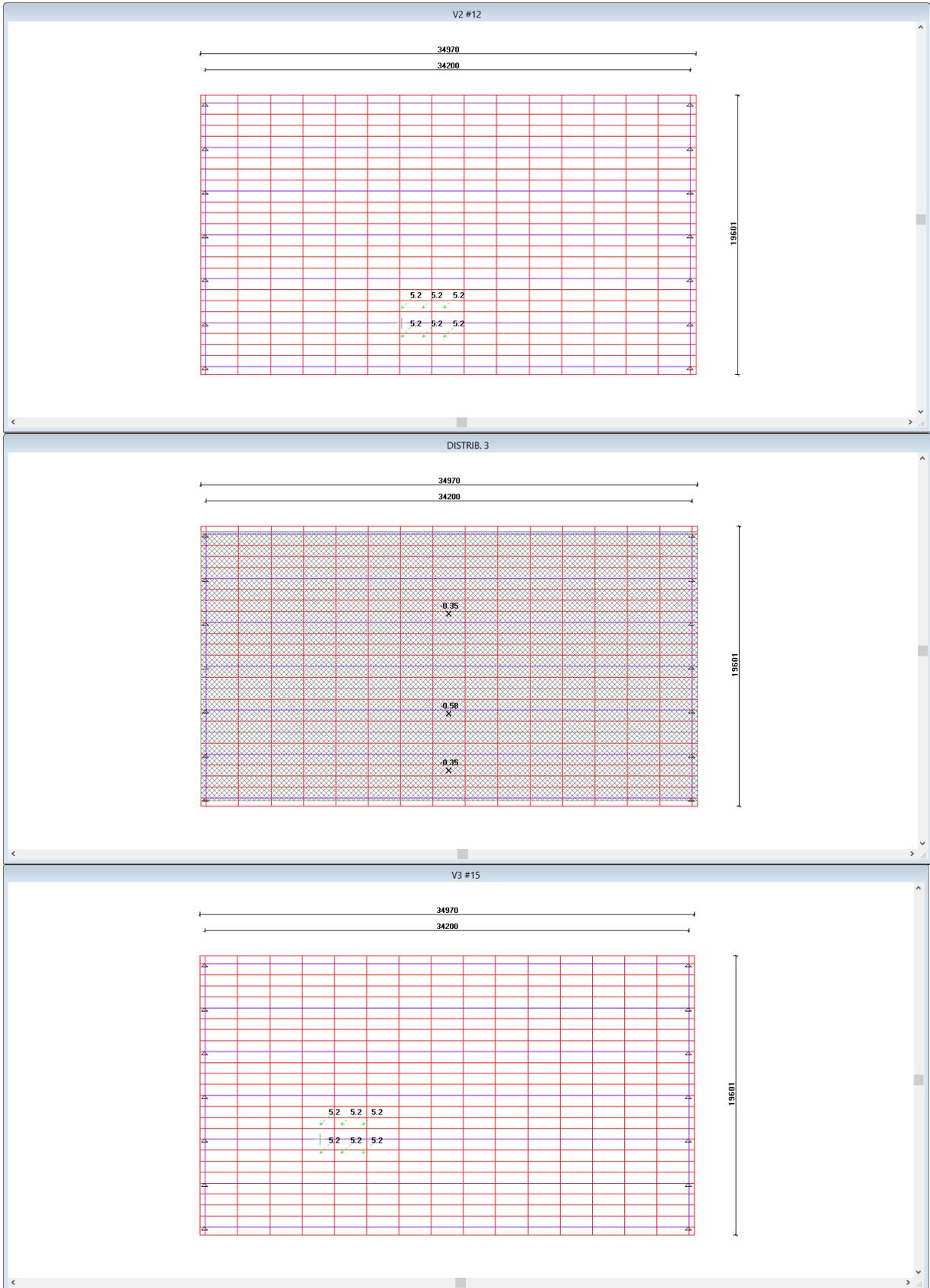


### NOTA TÉCNICA



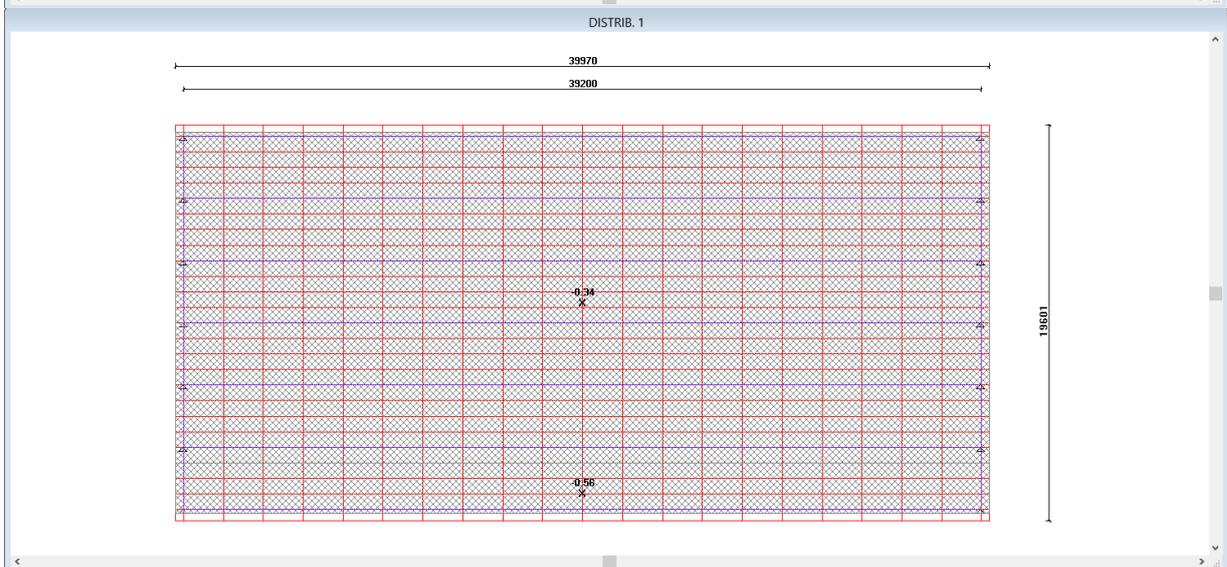
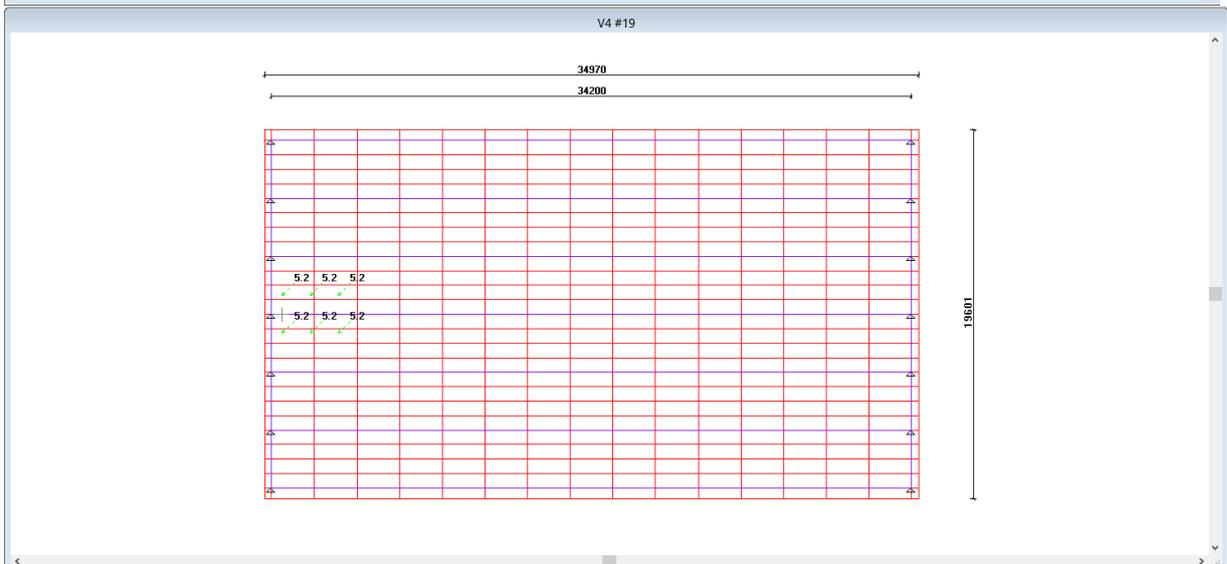
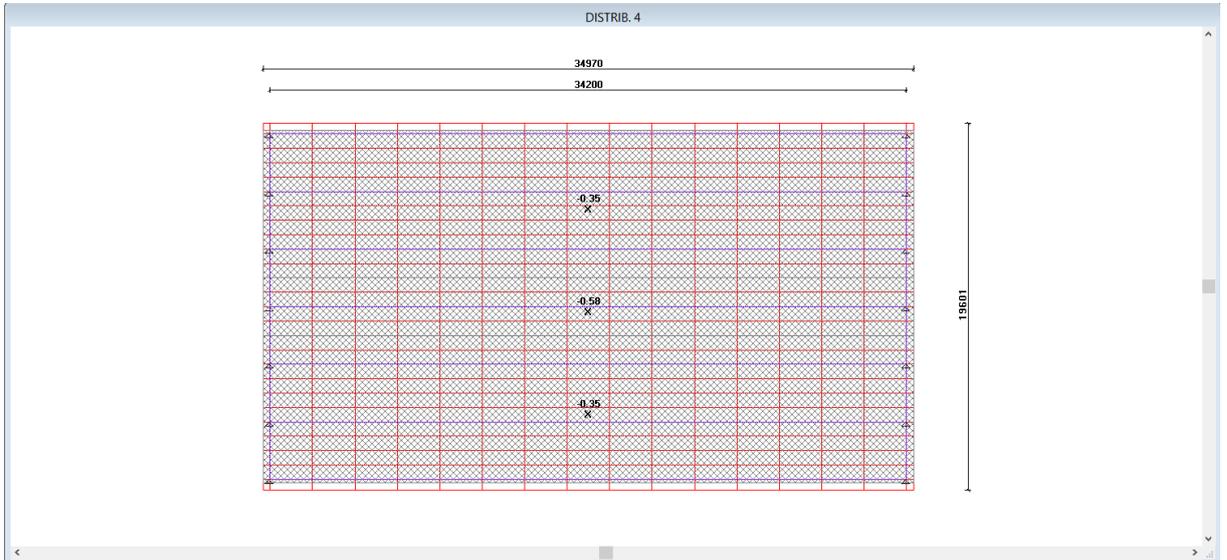


### NOTA TÉCNICA



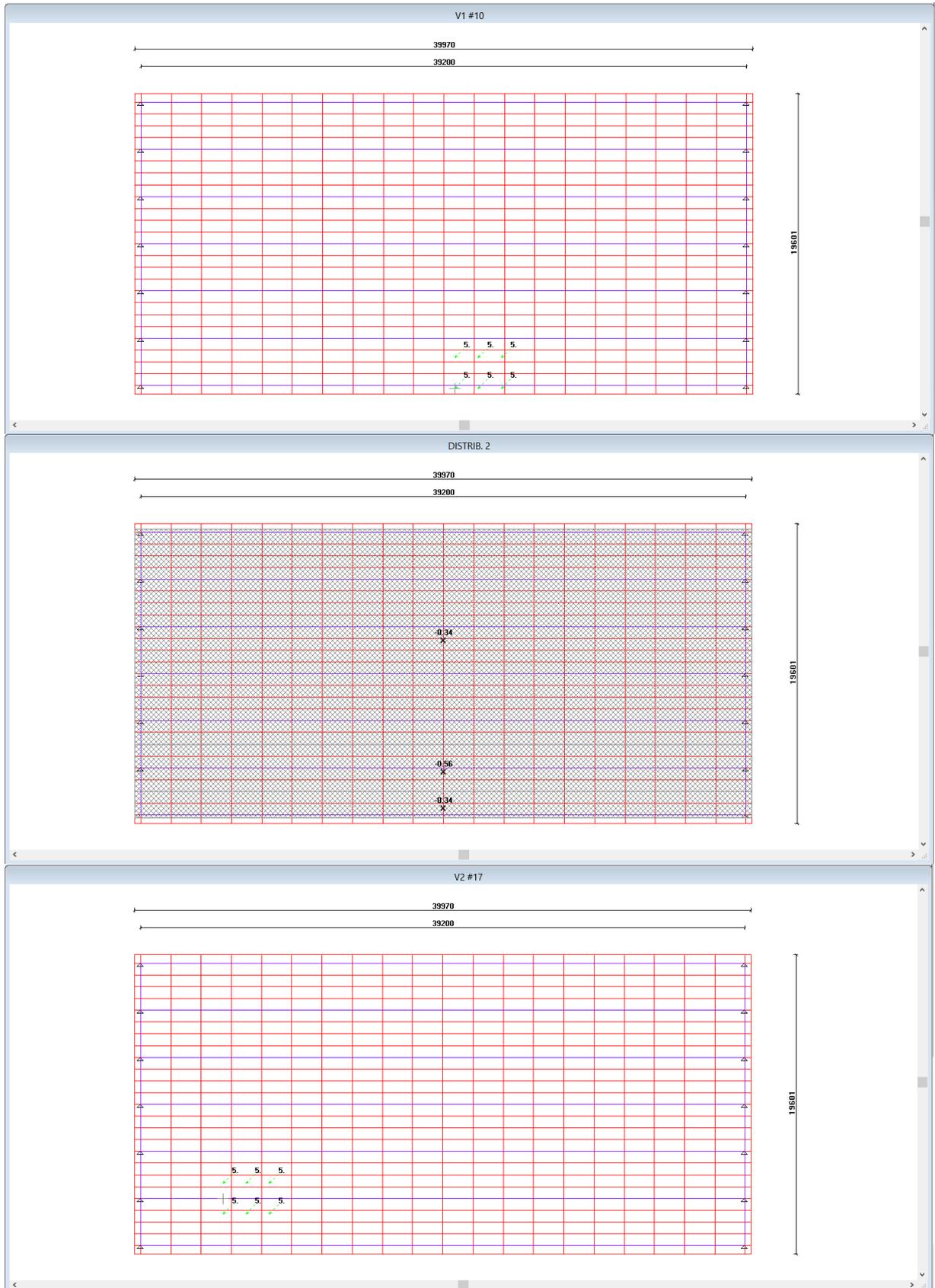


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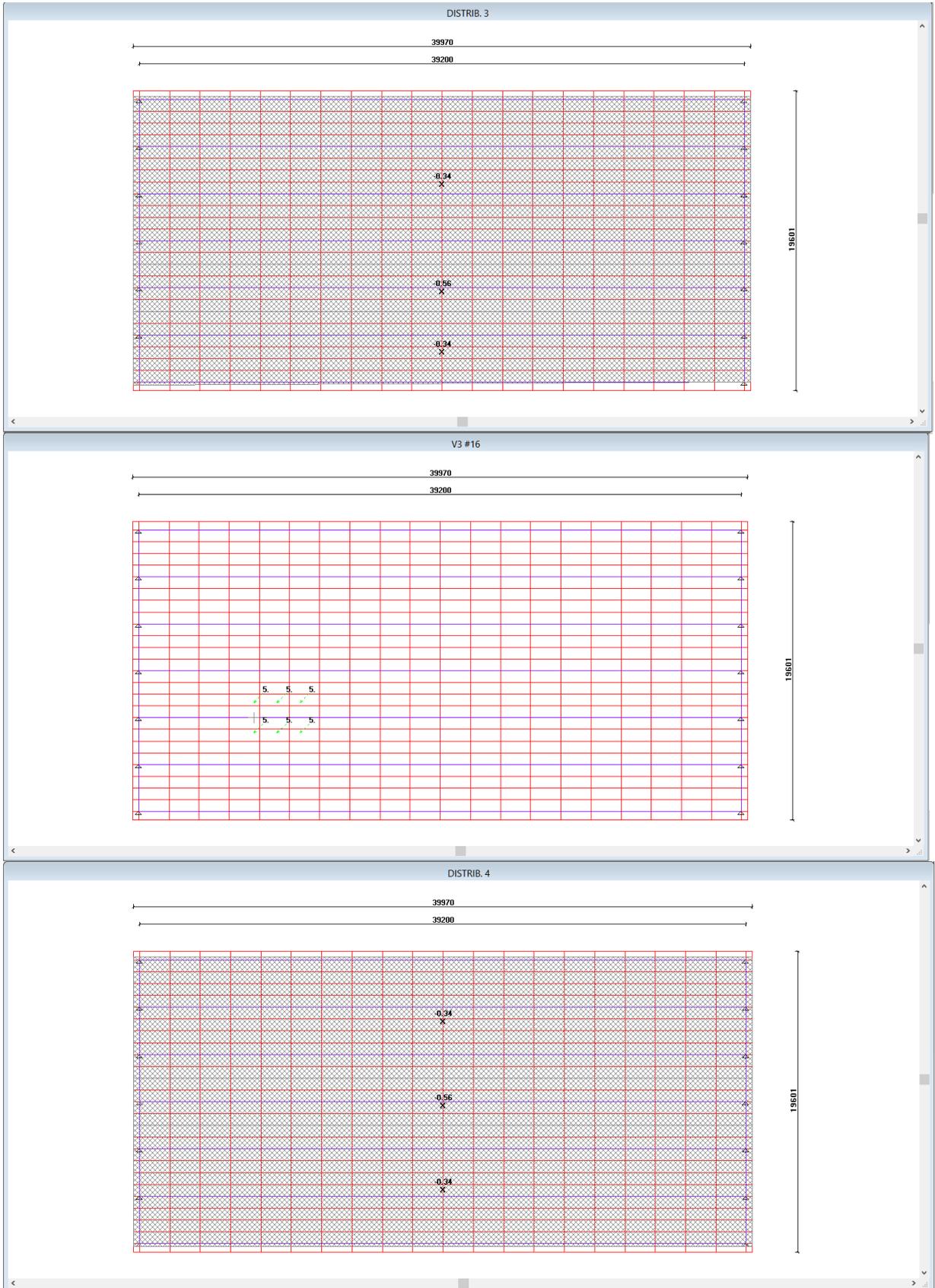


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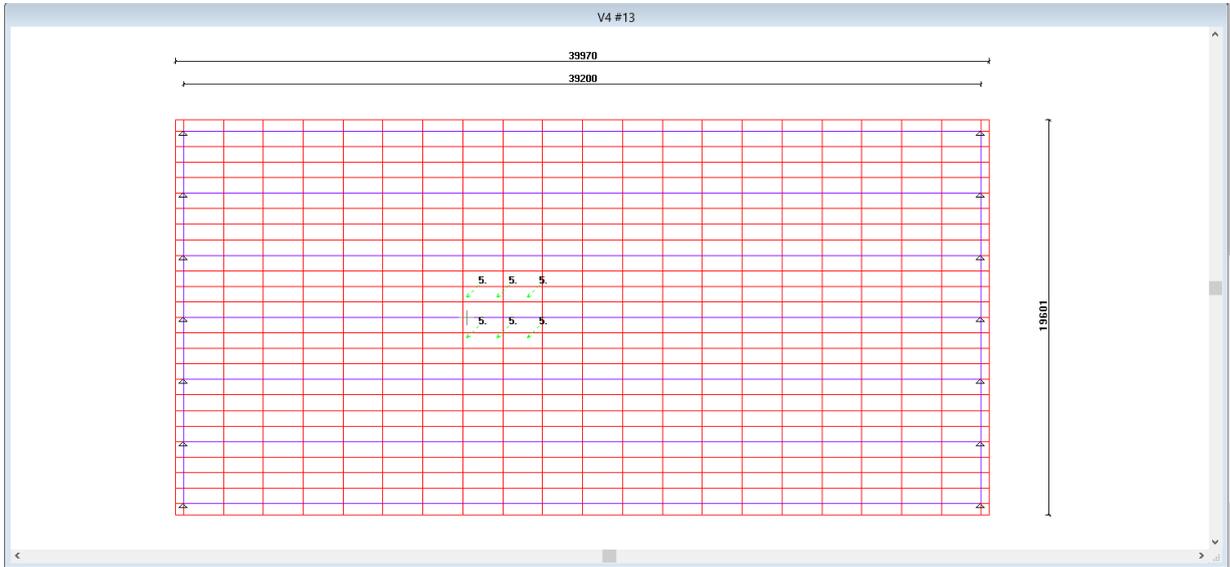


### NOTA TÉCNICA





## NOTA TÉCNICA



### 4.5. Cargas acidentais – Guindaste de 8 eixos e 96 toneladas

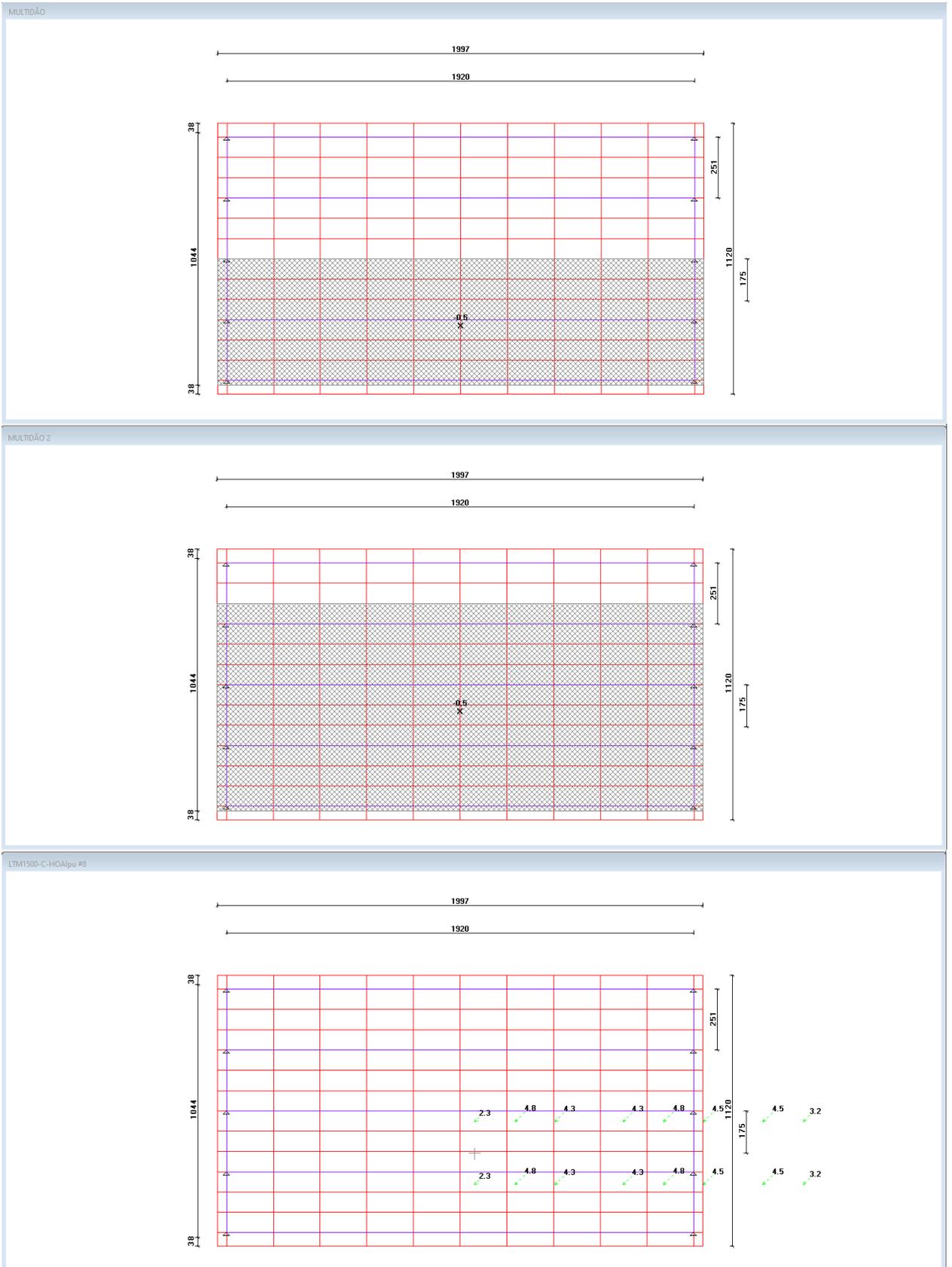
Para o Guindaste de 96 toneladas, o CIV foi aplicado após a obtenção dos momentos e cortantes. Por isso a multidão está com o valor de 0,50 tf/m.

O Liebherr está trafegando homogeneizado conforme foi apresentado no item 2.



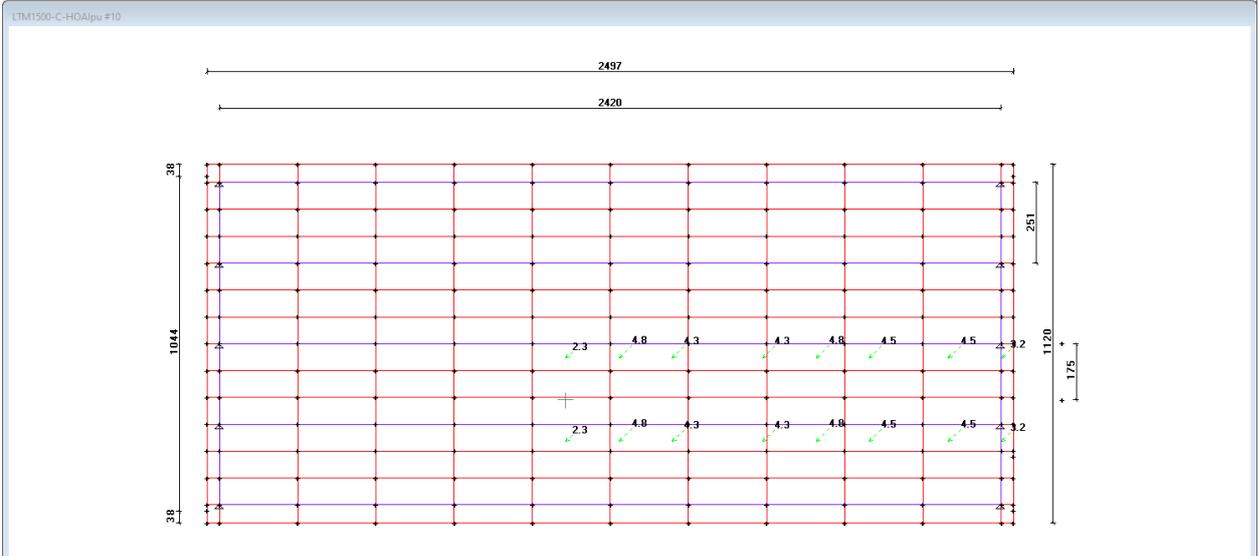
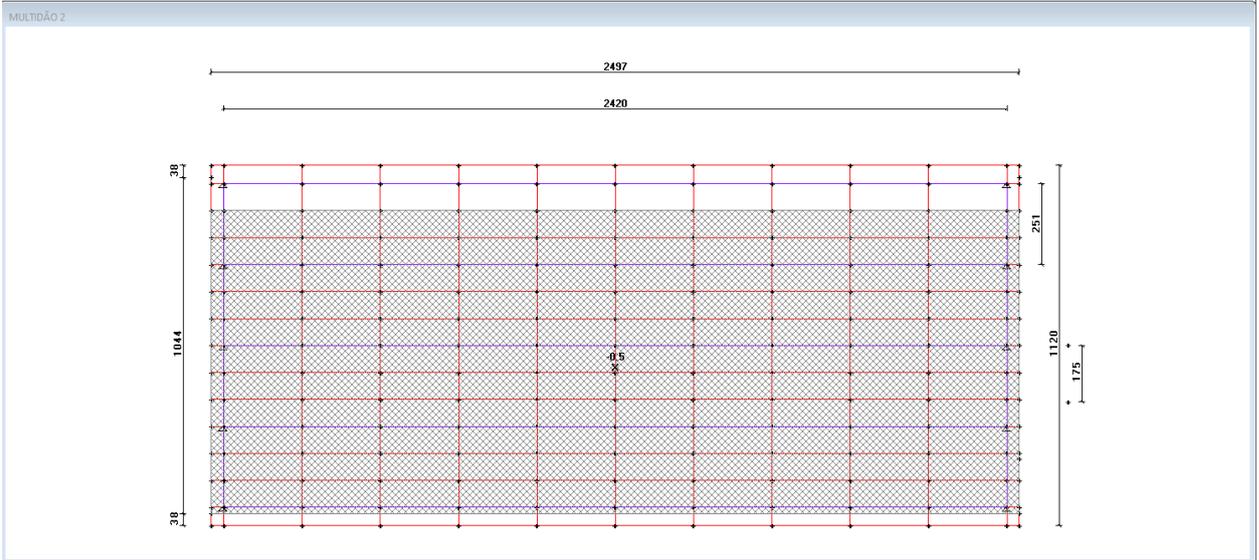
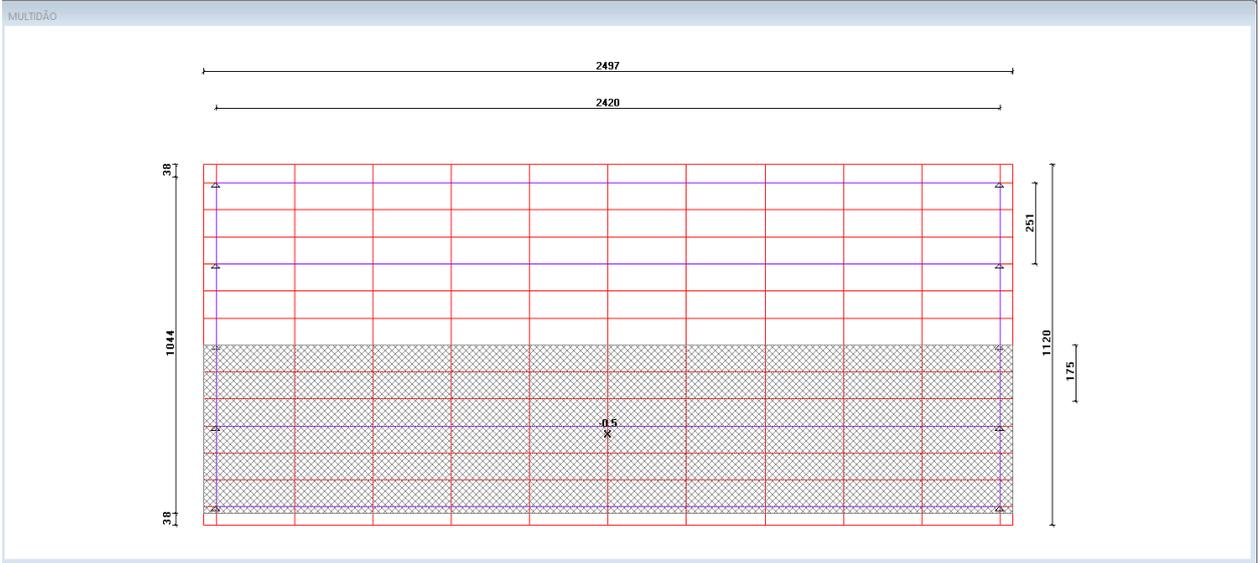
### NOTA TÉCNICA

#### 4.5.1. Tabuleiro 11,20 m



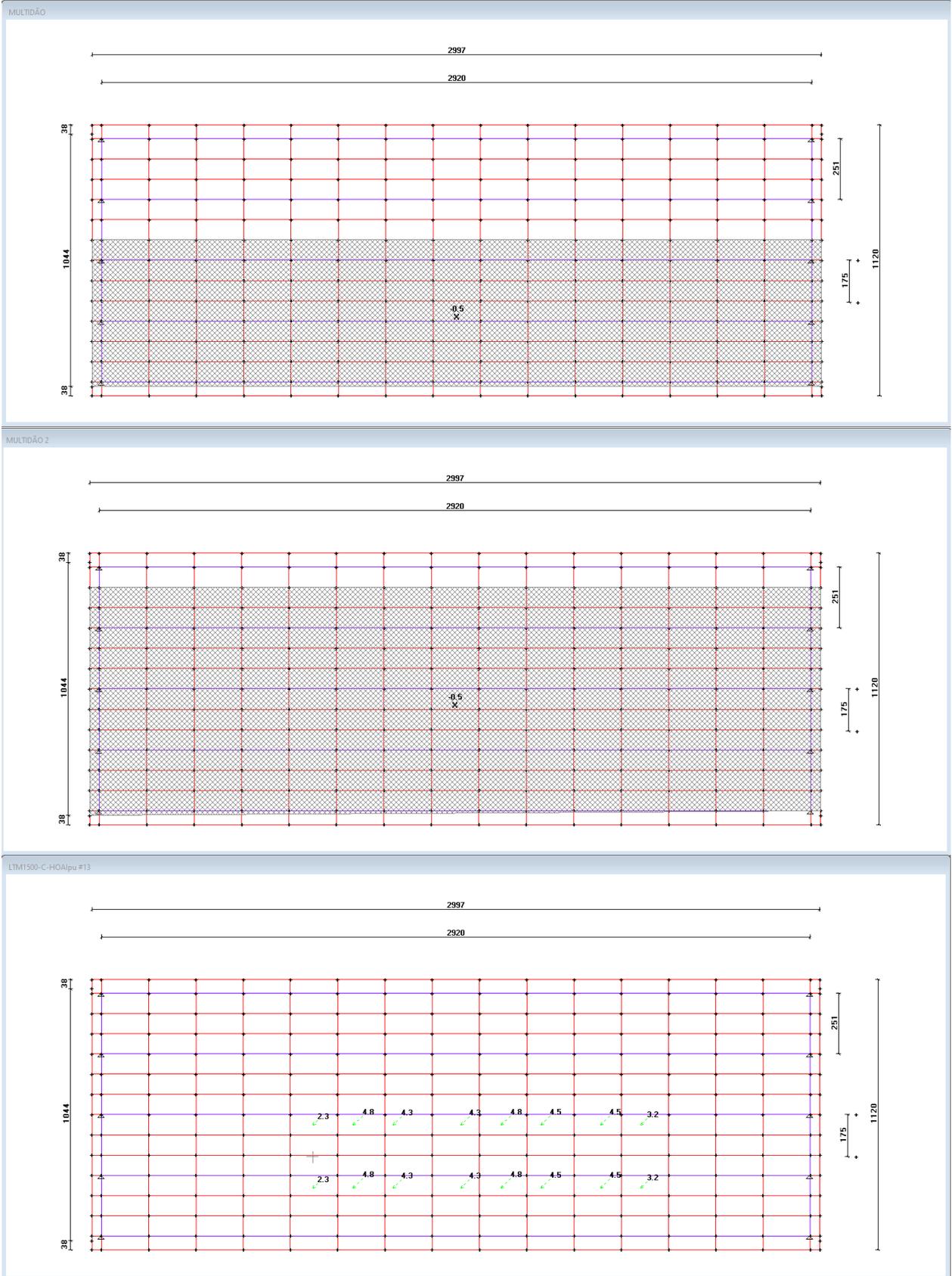


### NOTA TÉCNICA



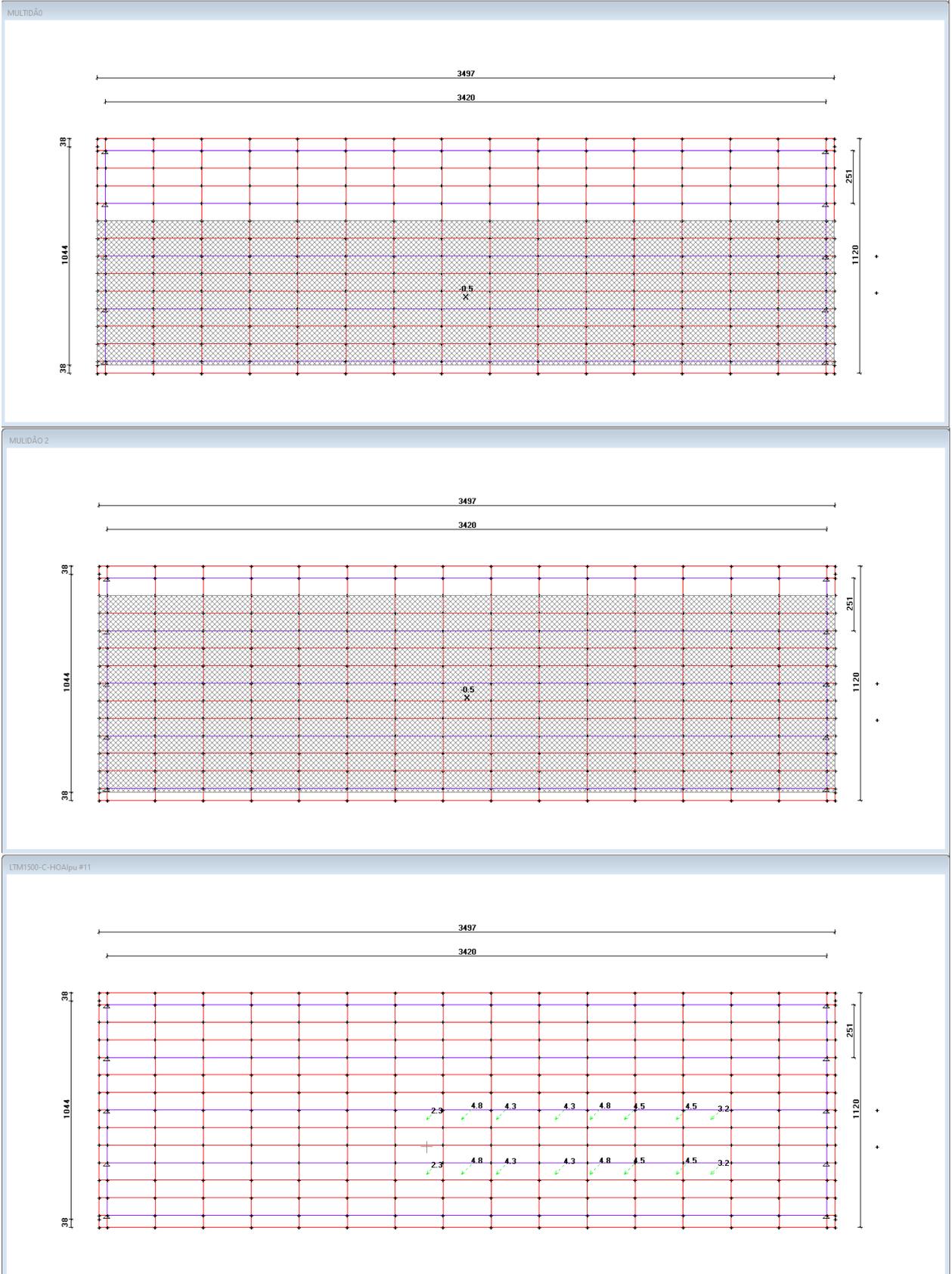


### NOTA TÉCNICA



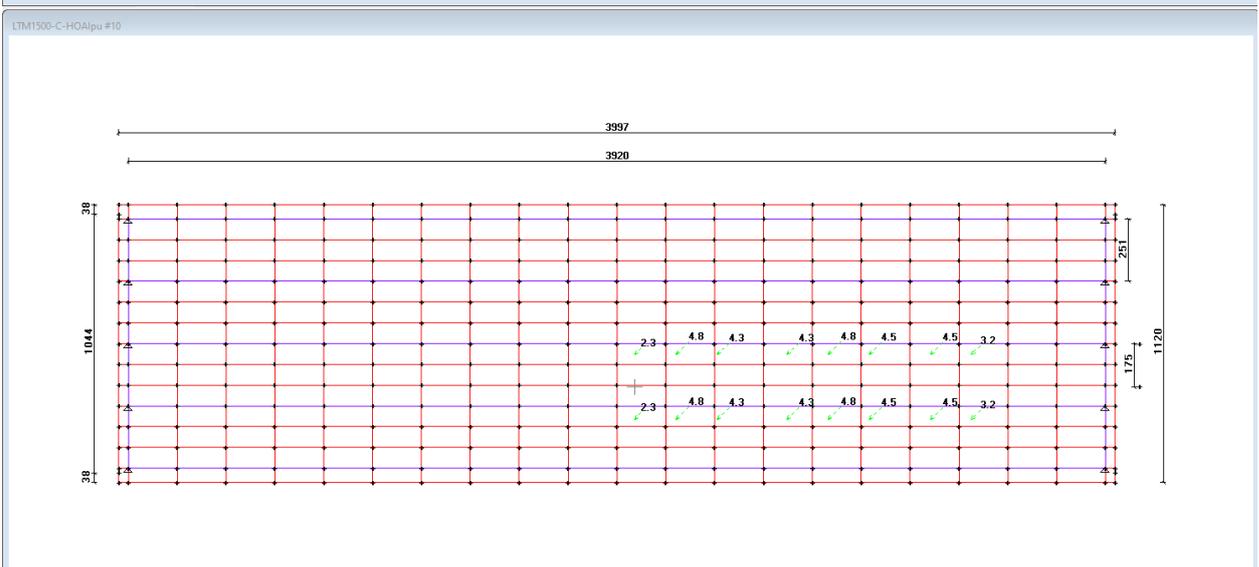
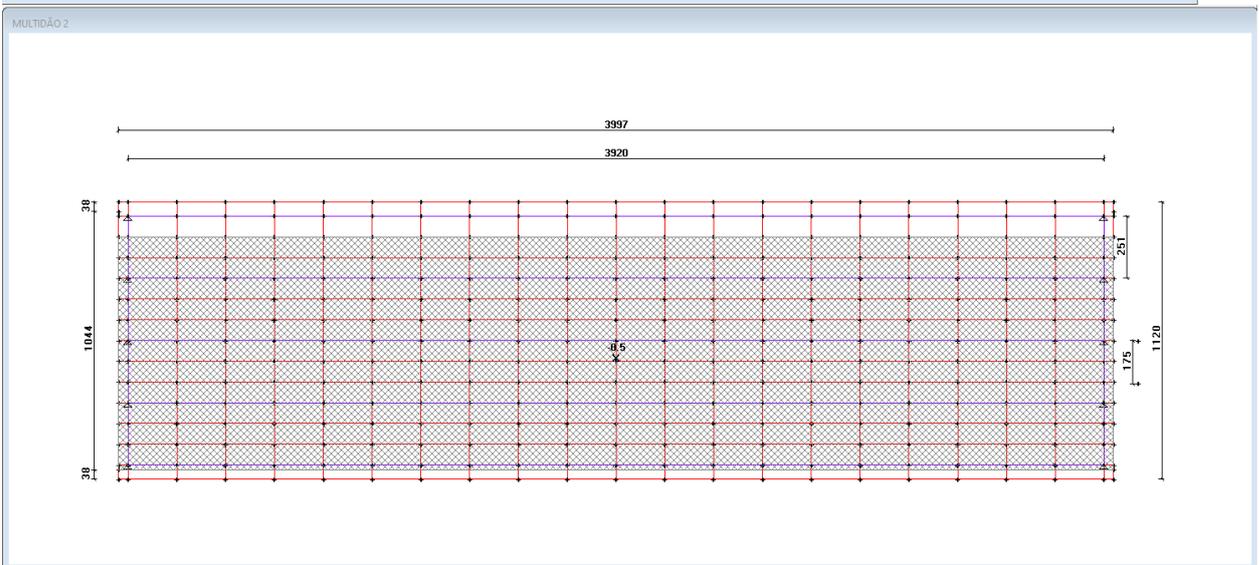
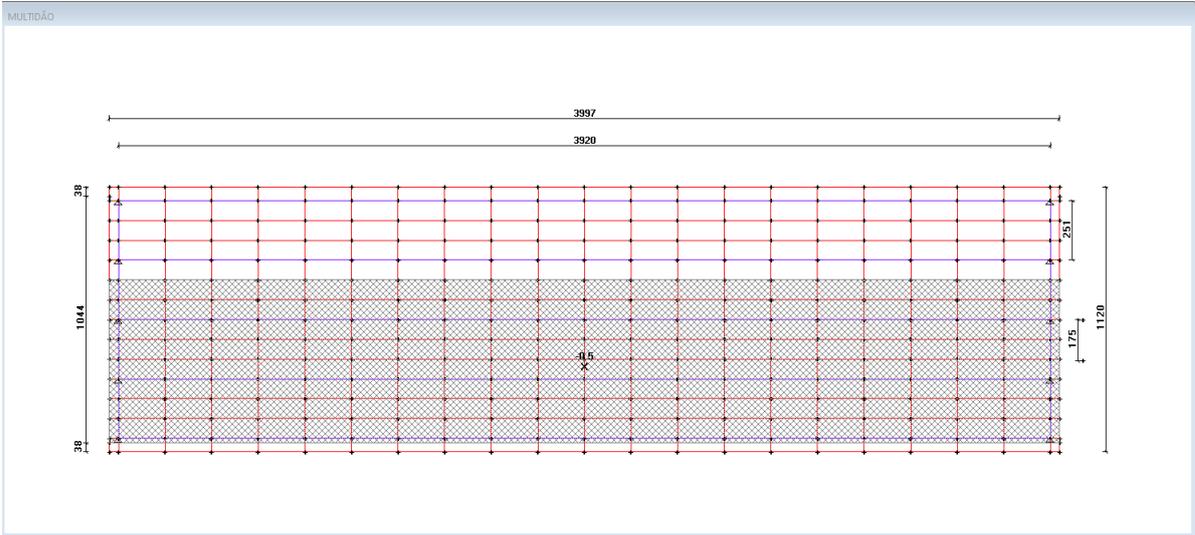


### NOTA TÉCNICA





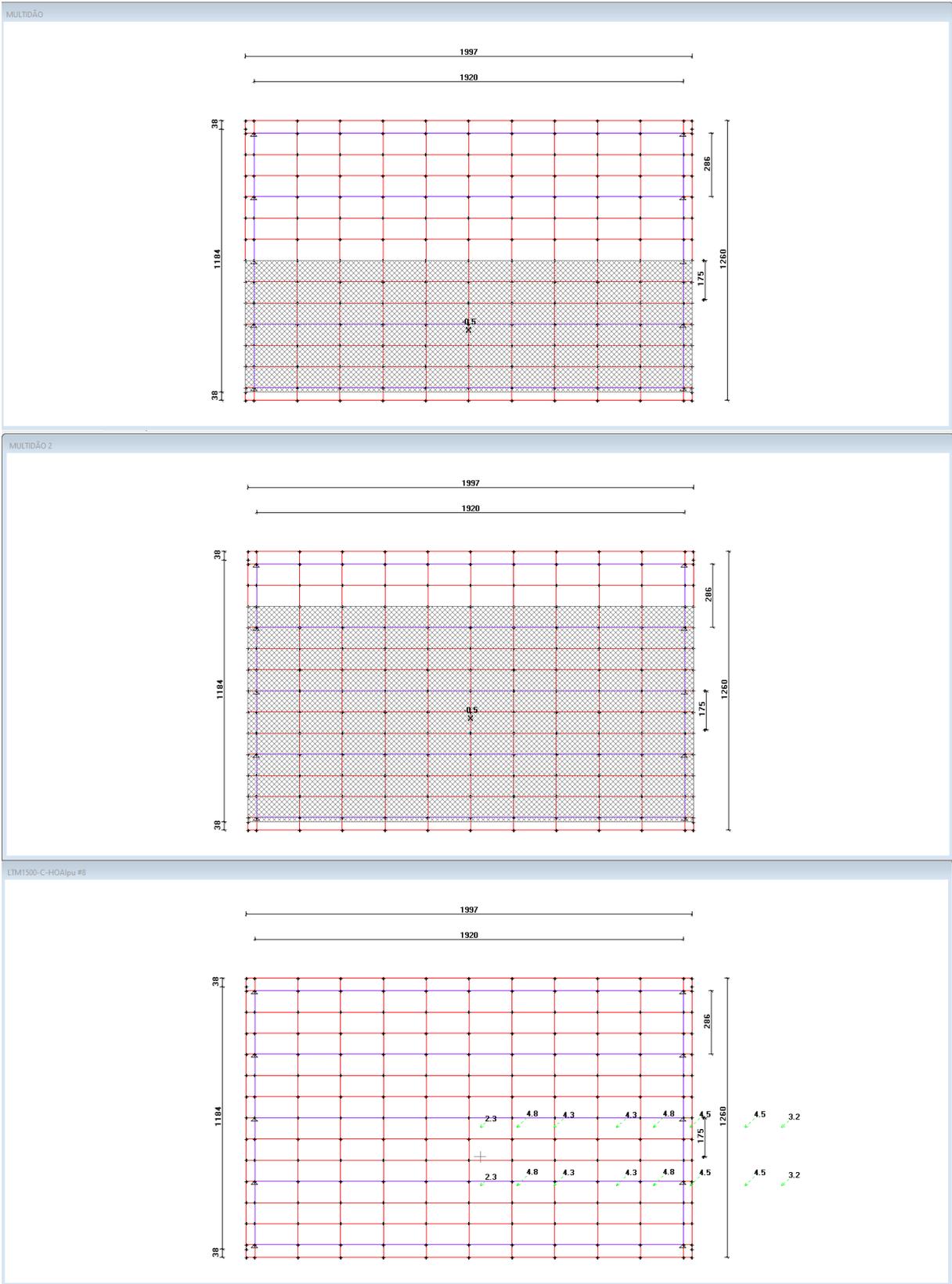
### NOTA TÉCNICA





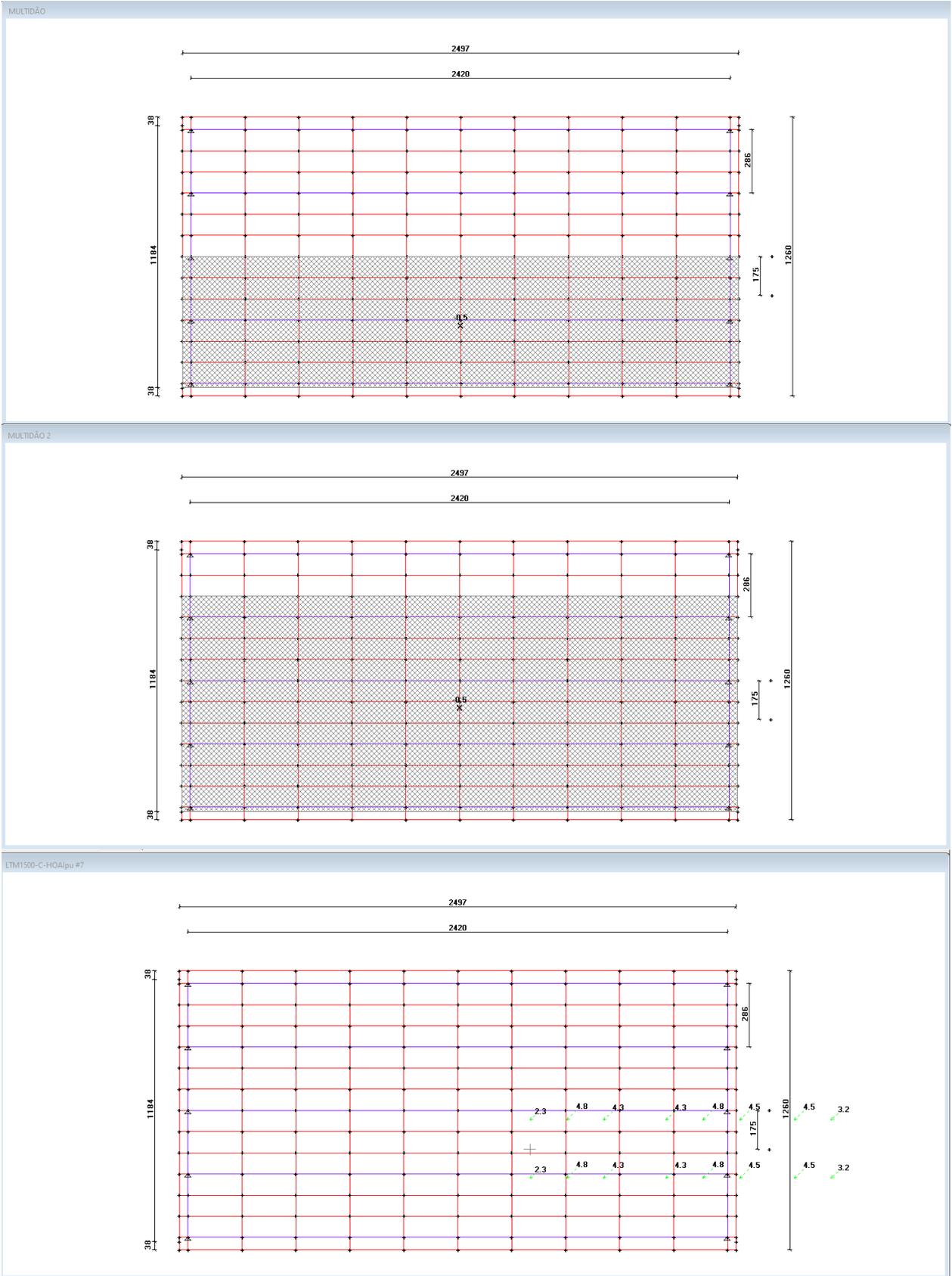
### NOTA TÉCNICA

#### 4.5.2. Tabuleiro 12,60 m



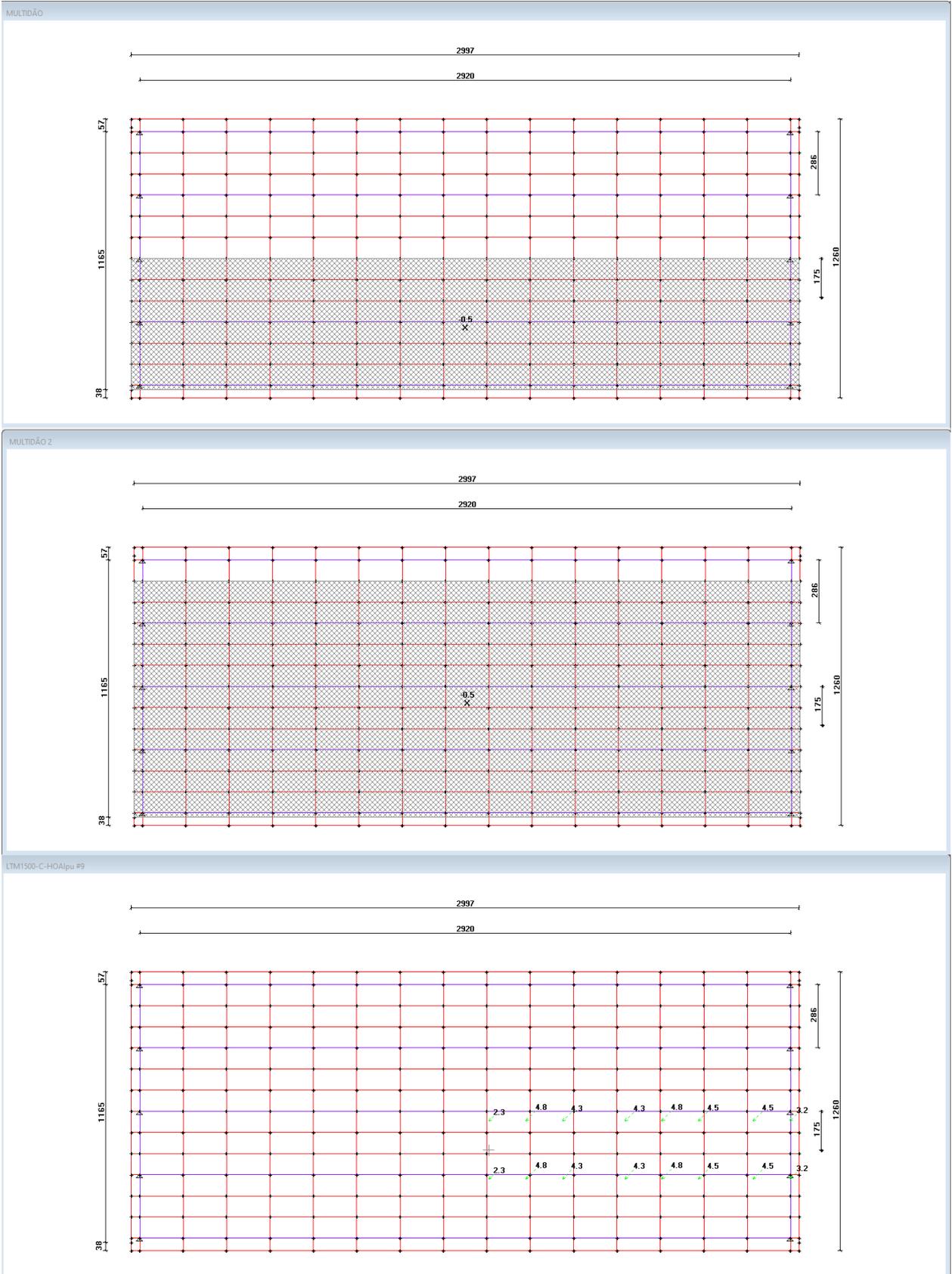


### NOTA TÉCNICA





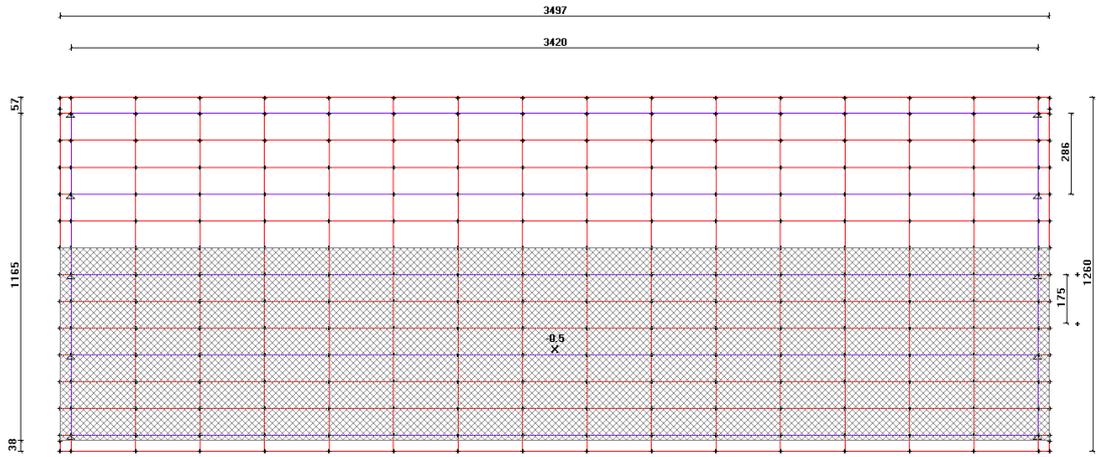
### NOTA TÉCNICA



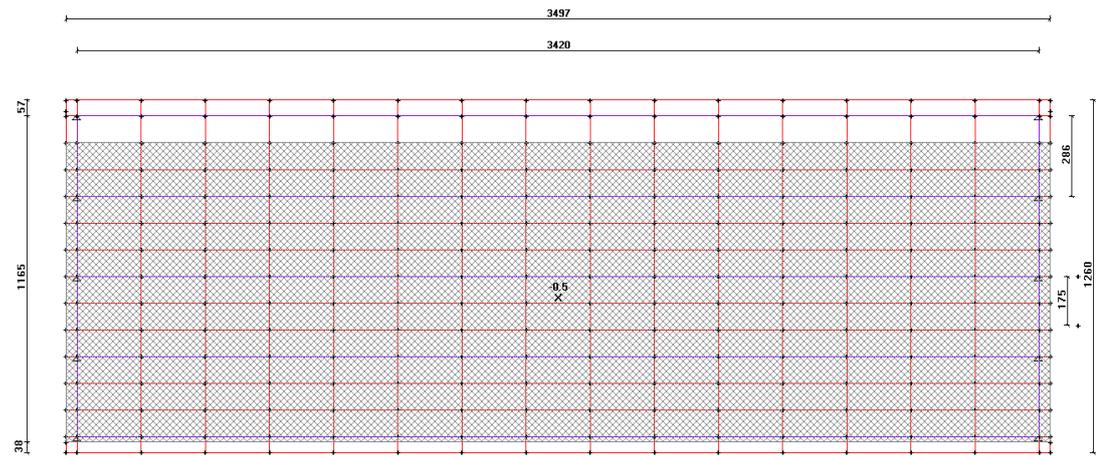


### NOTA TÉCNICA

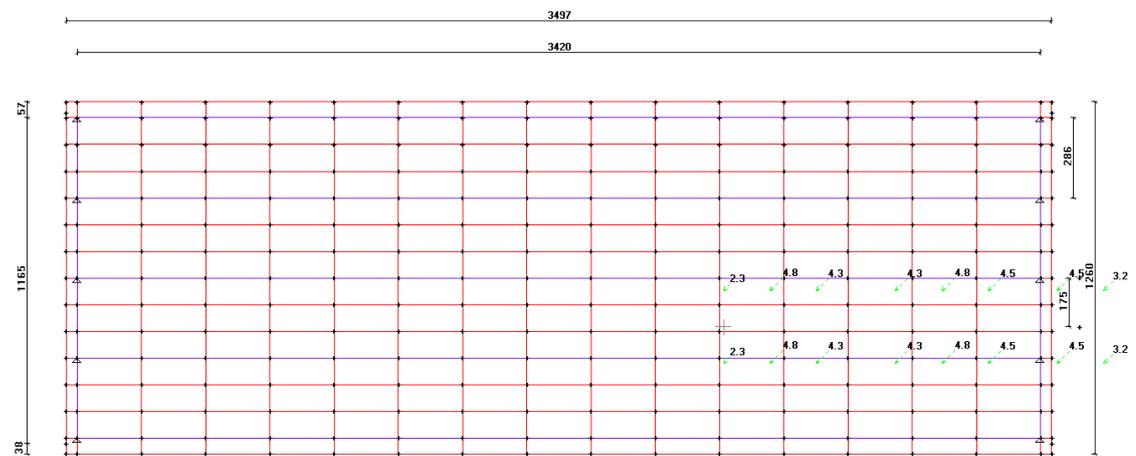
MULTIDÃO



MULTIDÃO 2

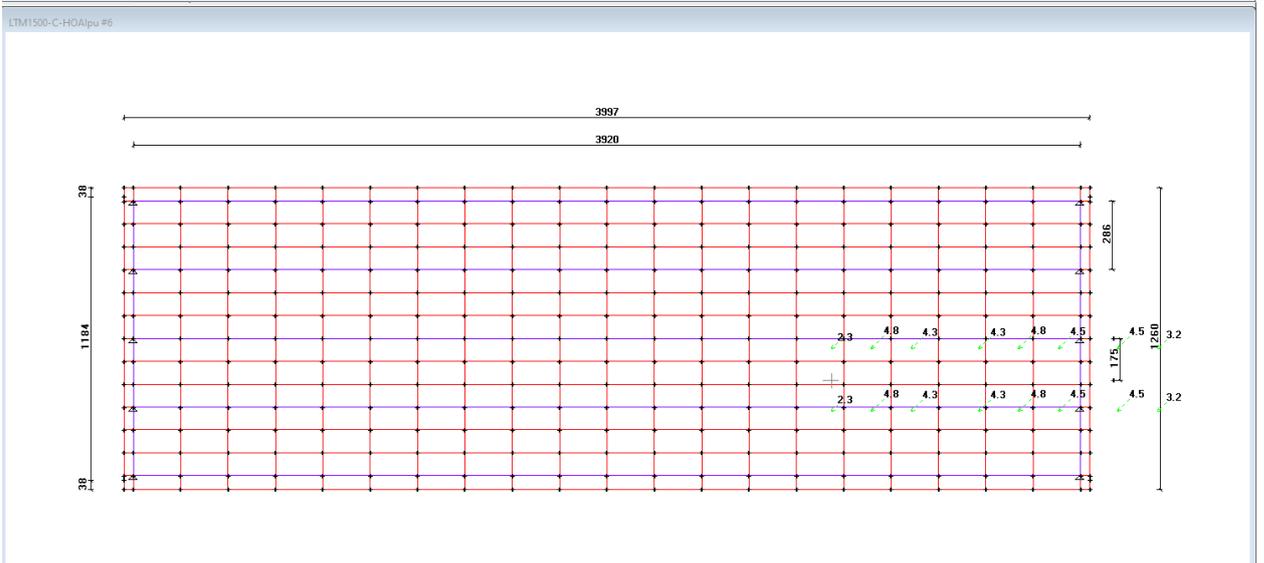
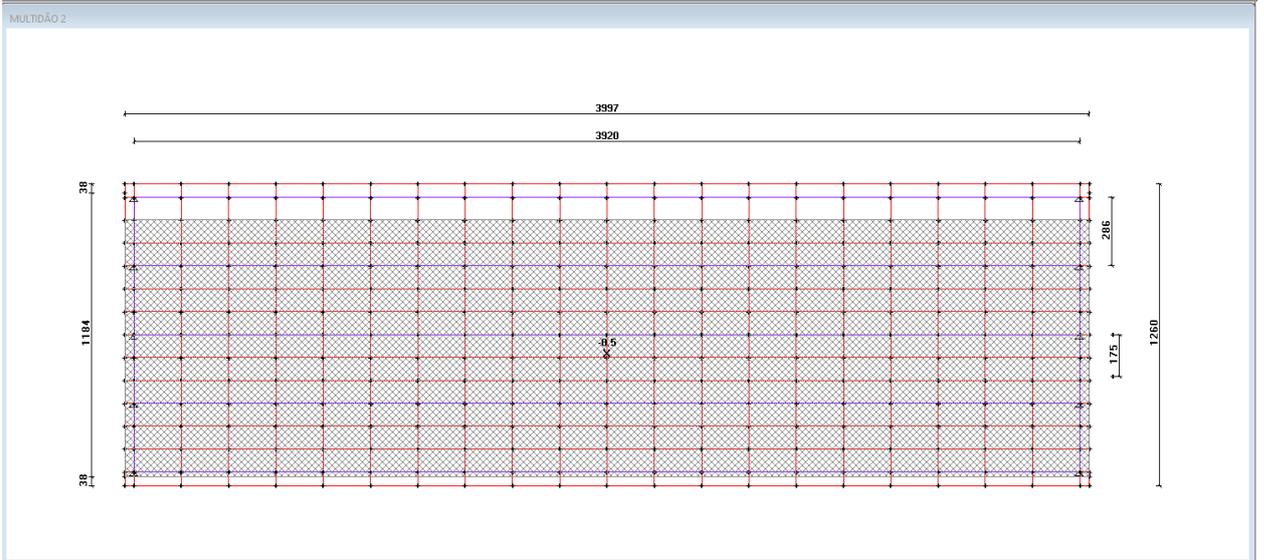
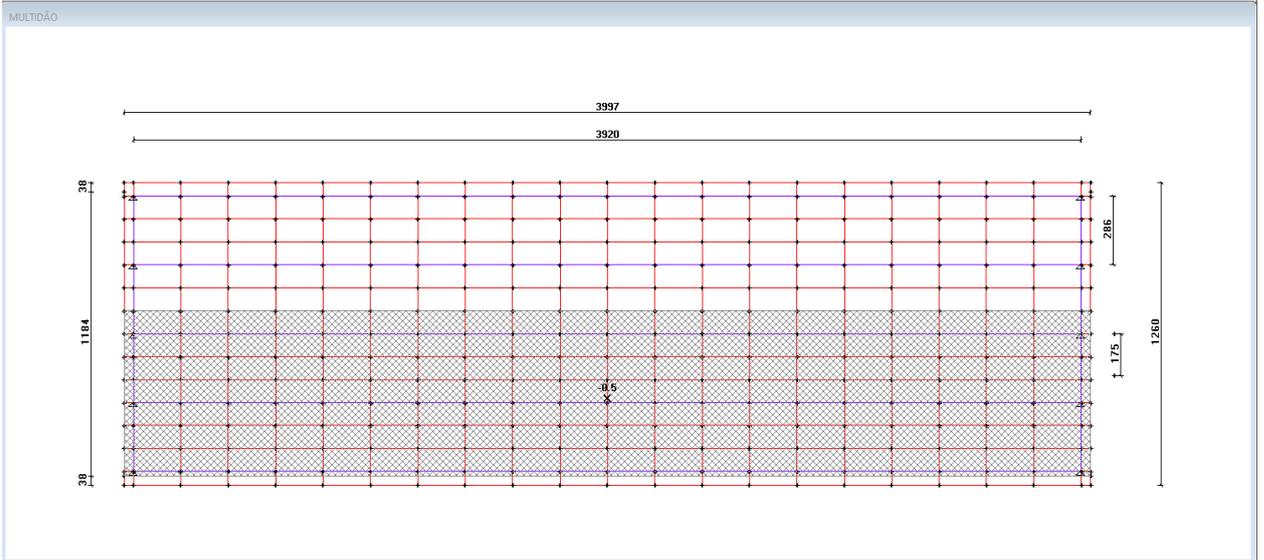


LTM1500-C-HOAlpu #7





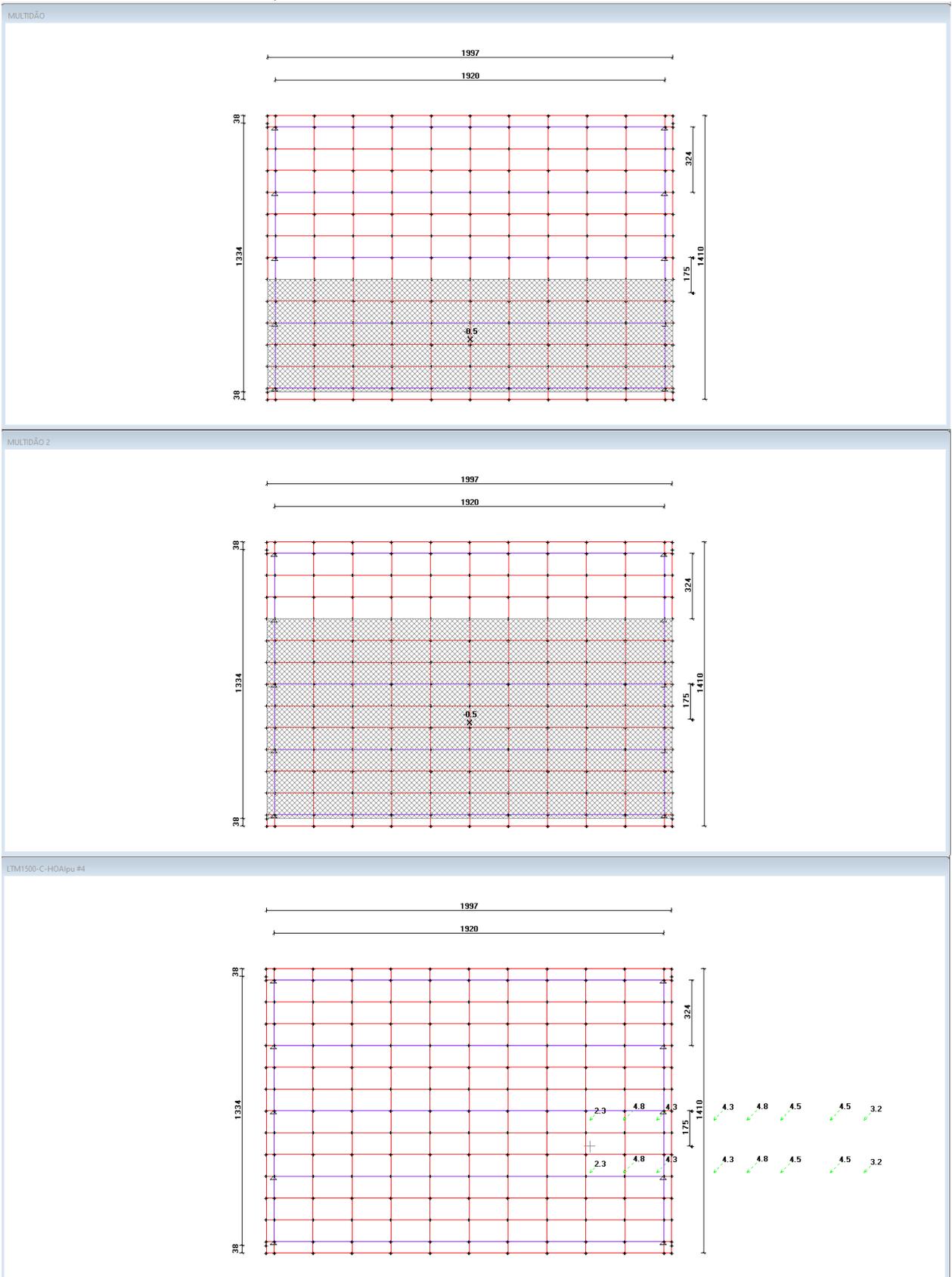
### NOTA TÉCNICA





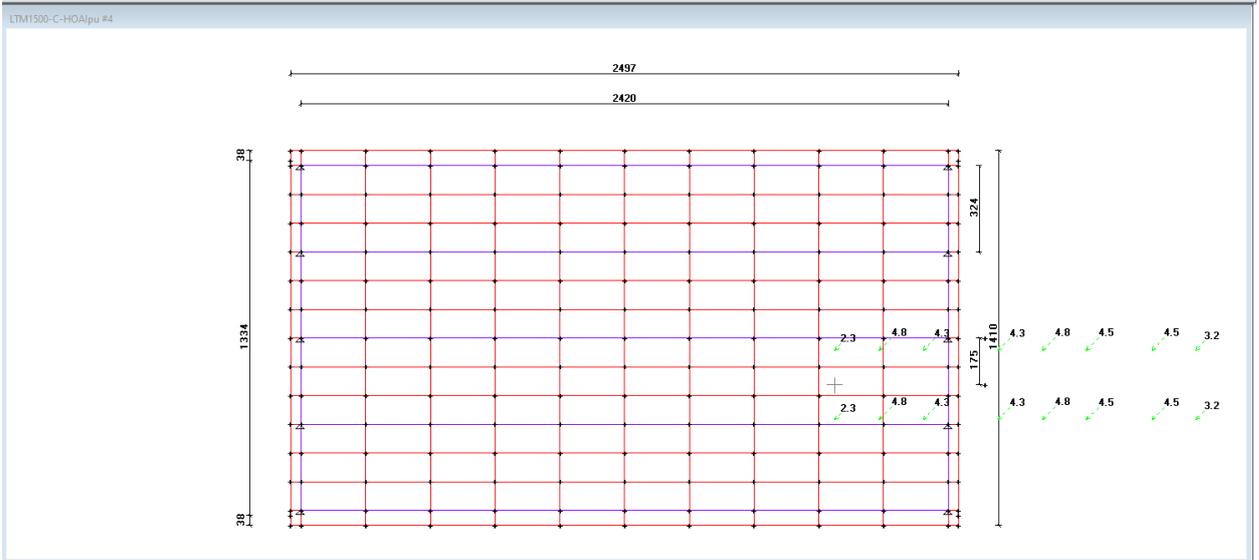
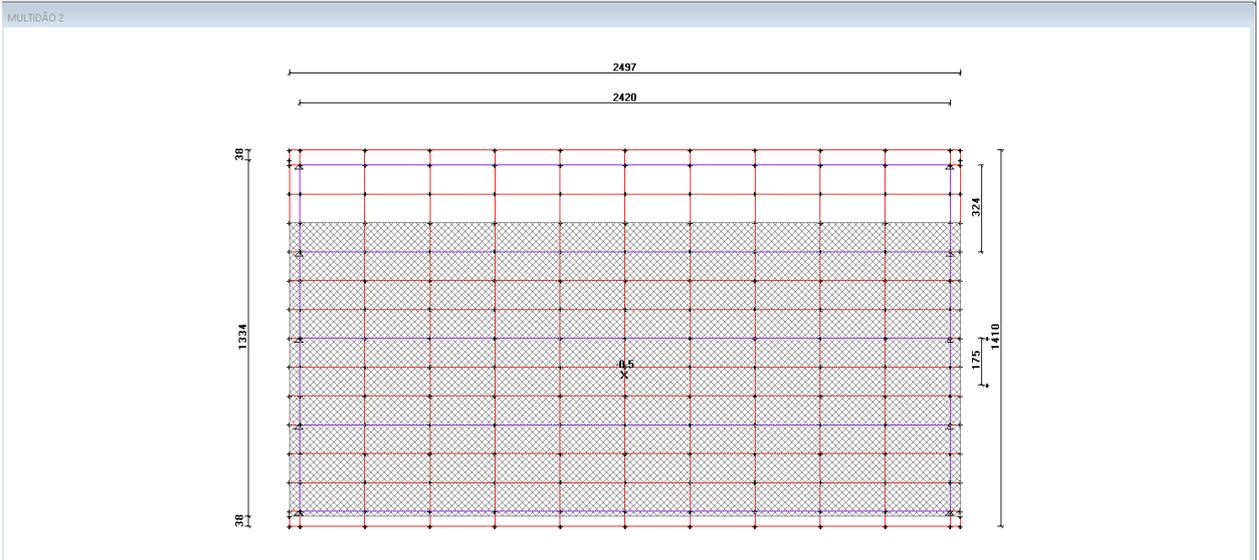
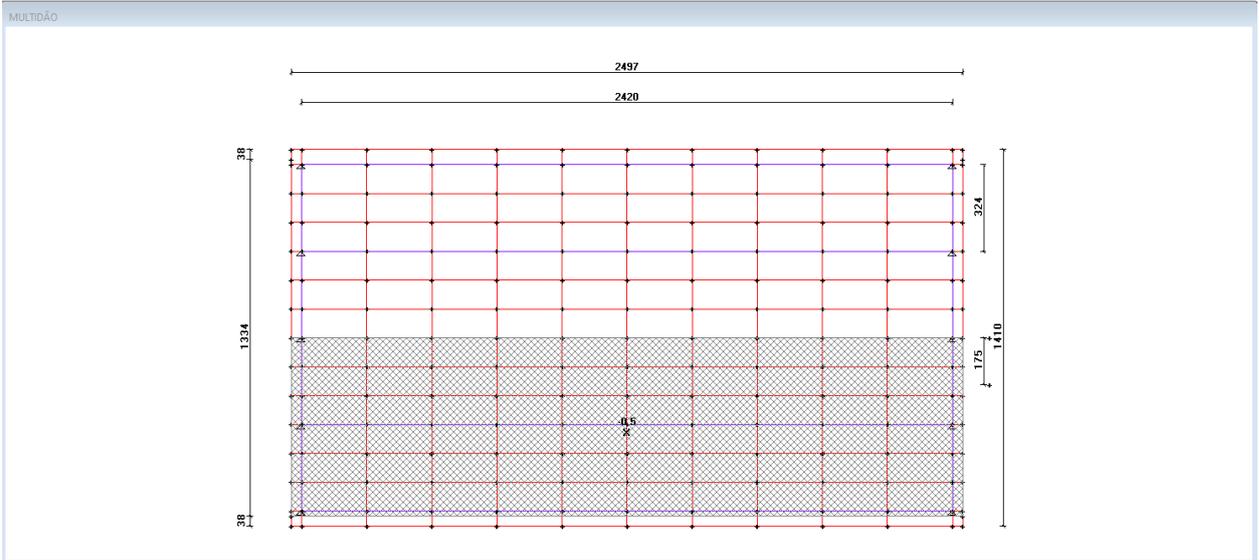
### NOTA TÉCNICA

#### 4.5.3. Tabuleiro 14,10 m



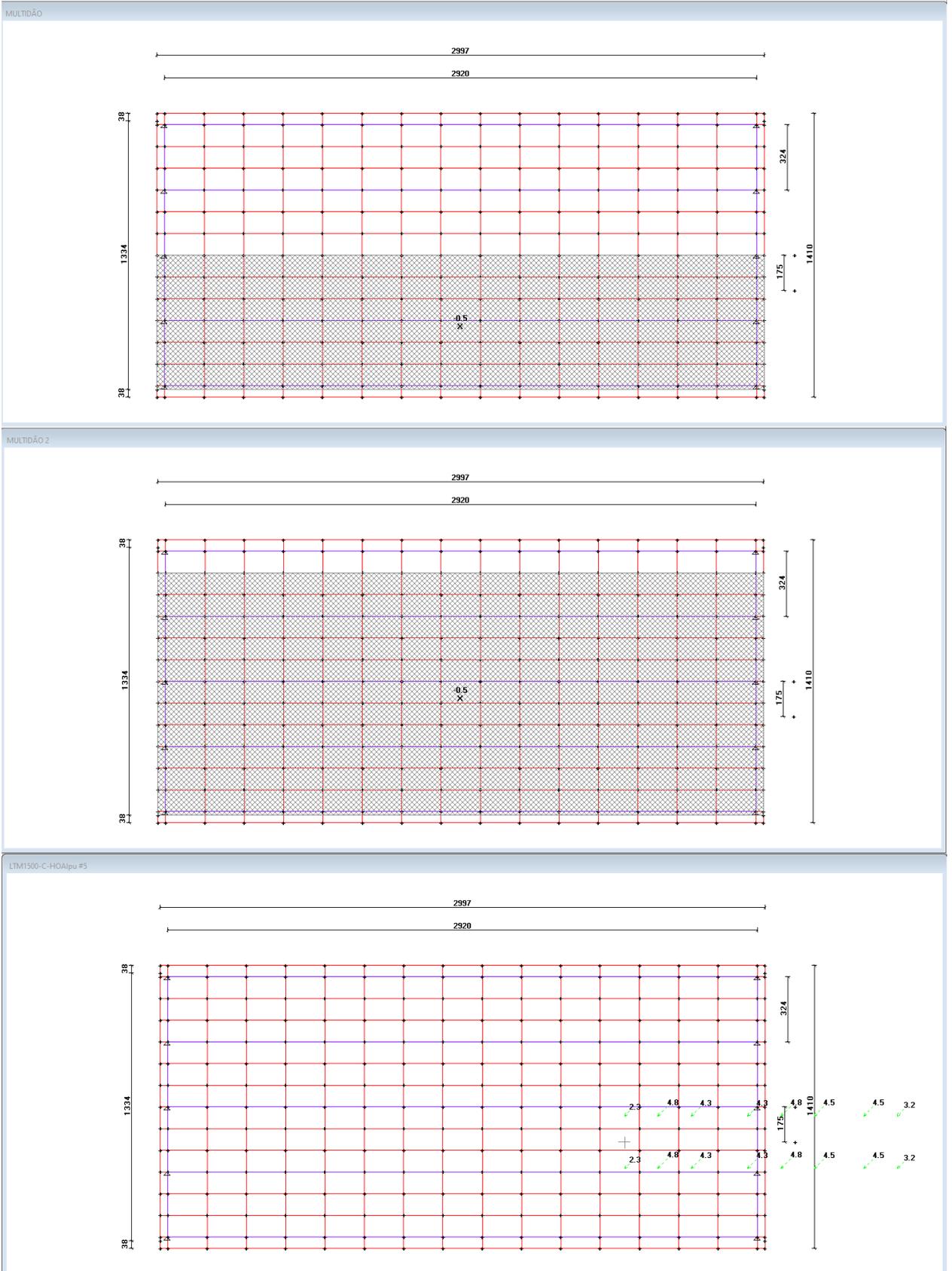


### NOTA TÉCNICA





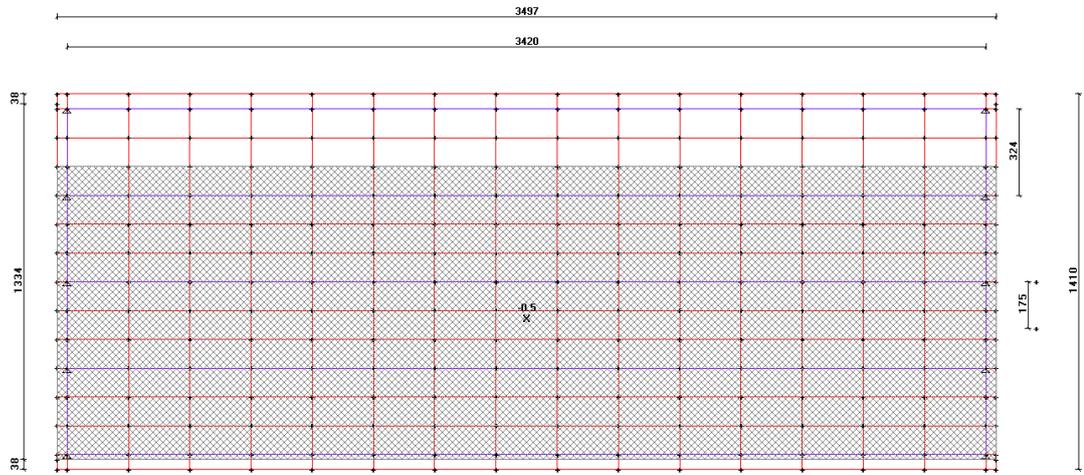
### NOTA TÉCNICA



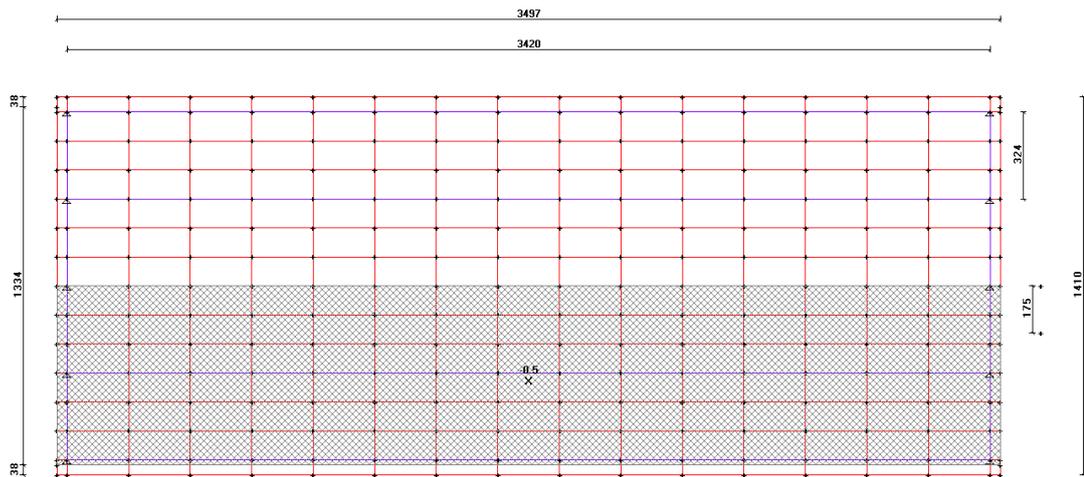


### NOTA TÉCNICA

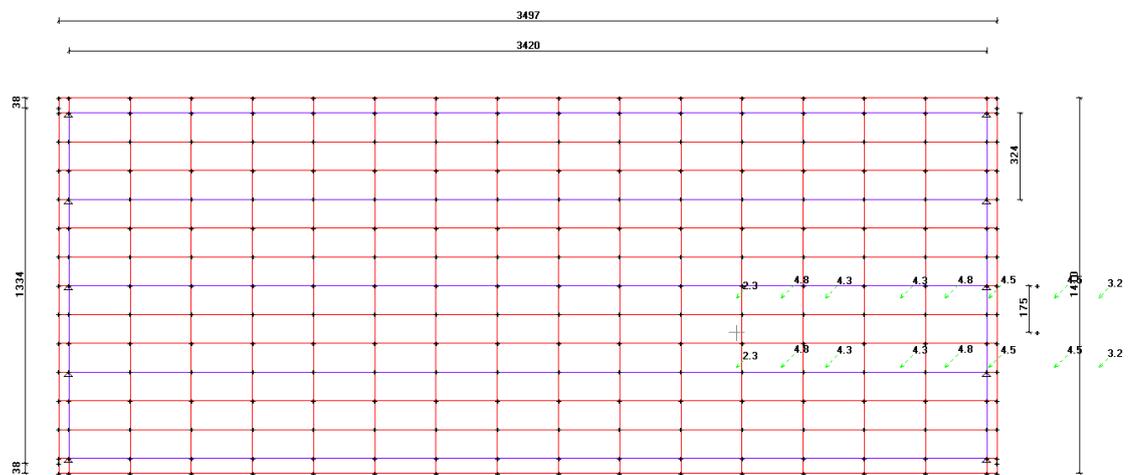
MULTIDÃO



MULTIDÃO 2

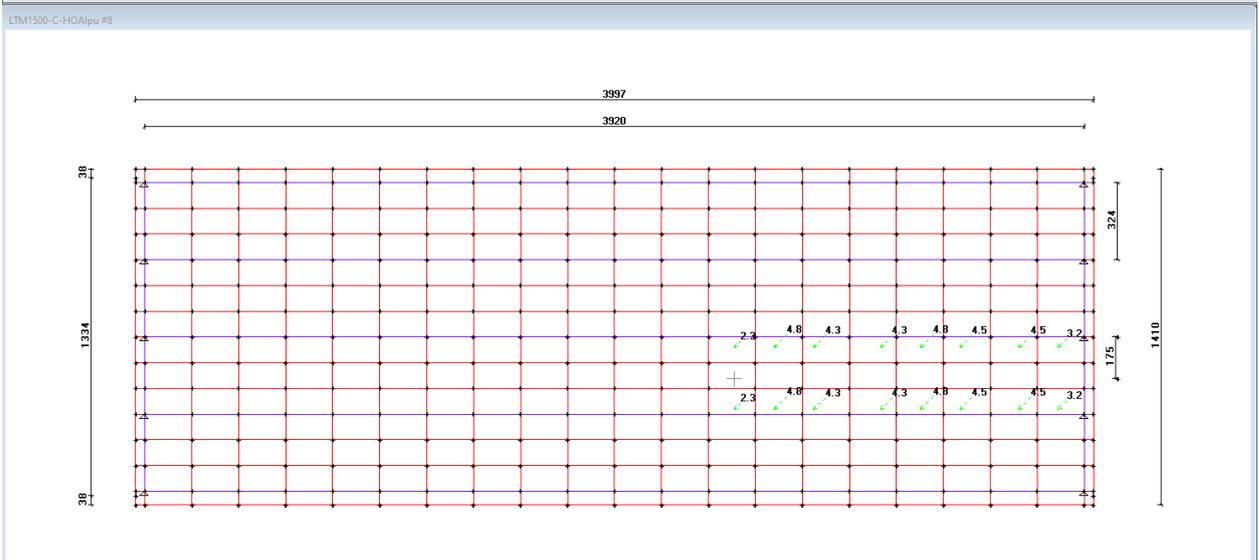
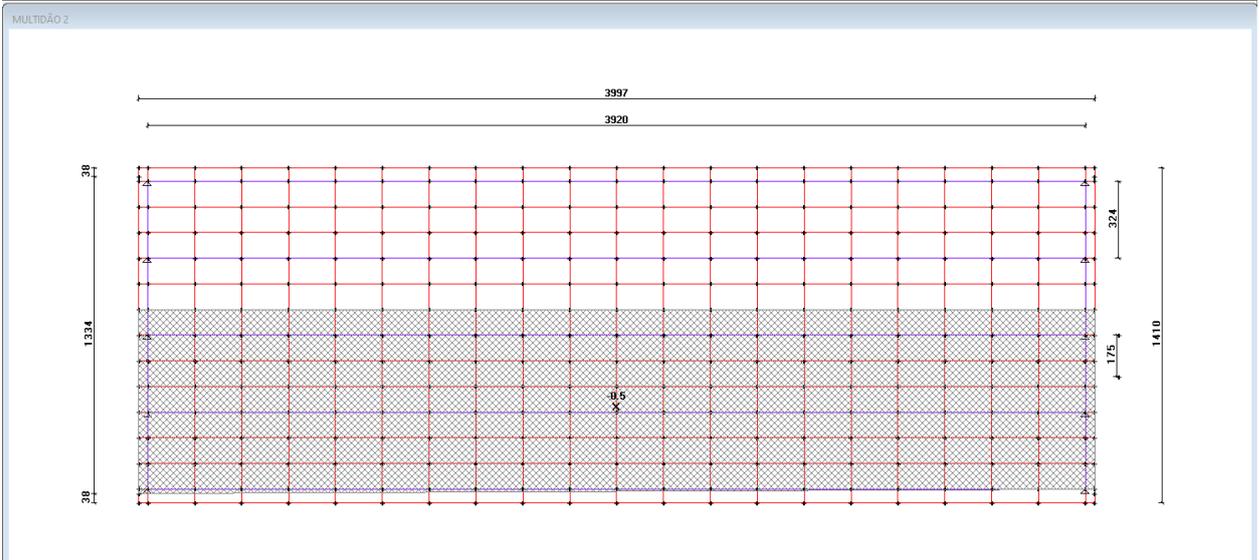
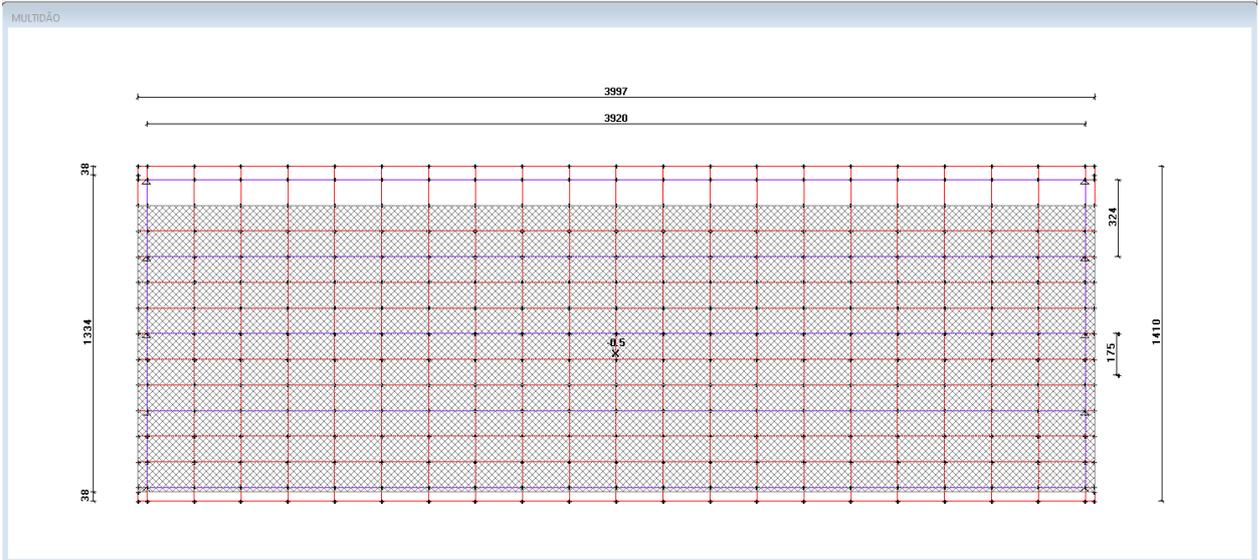


LTM1500-C-HOAlpu #6





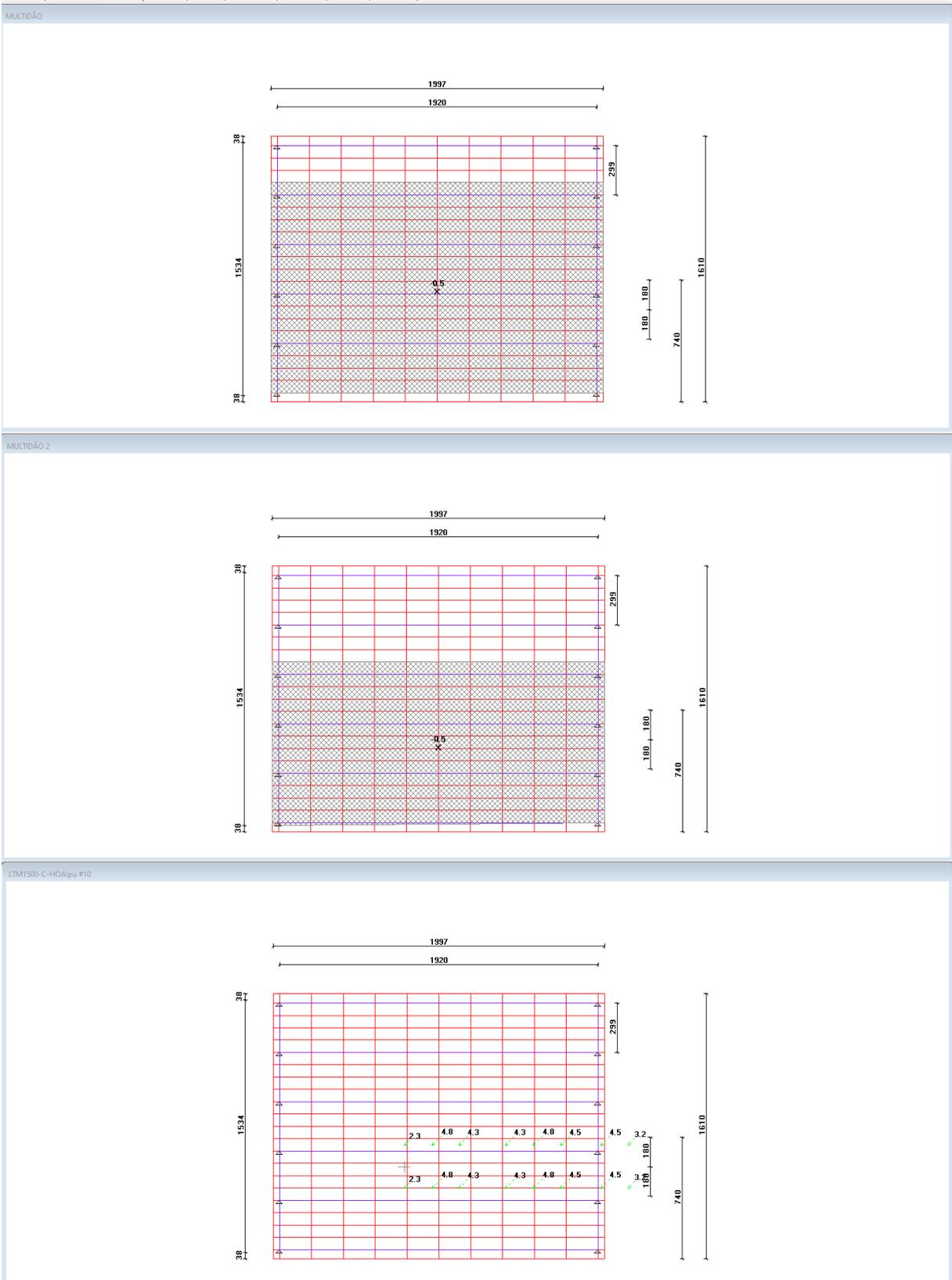
### NOTA TÉCNICA





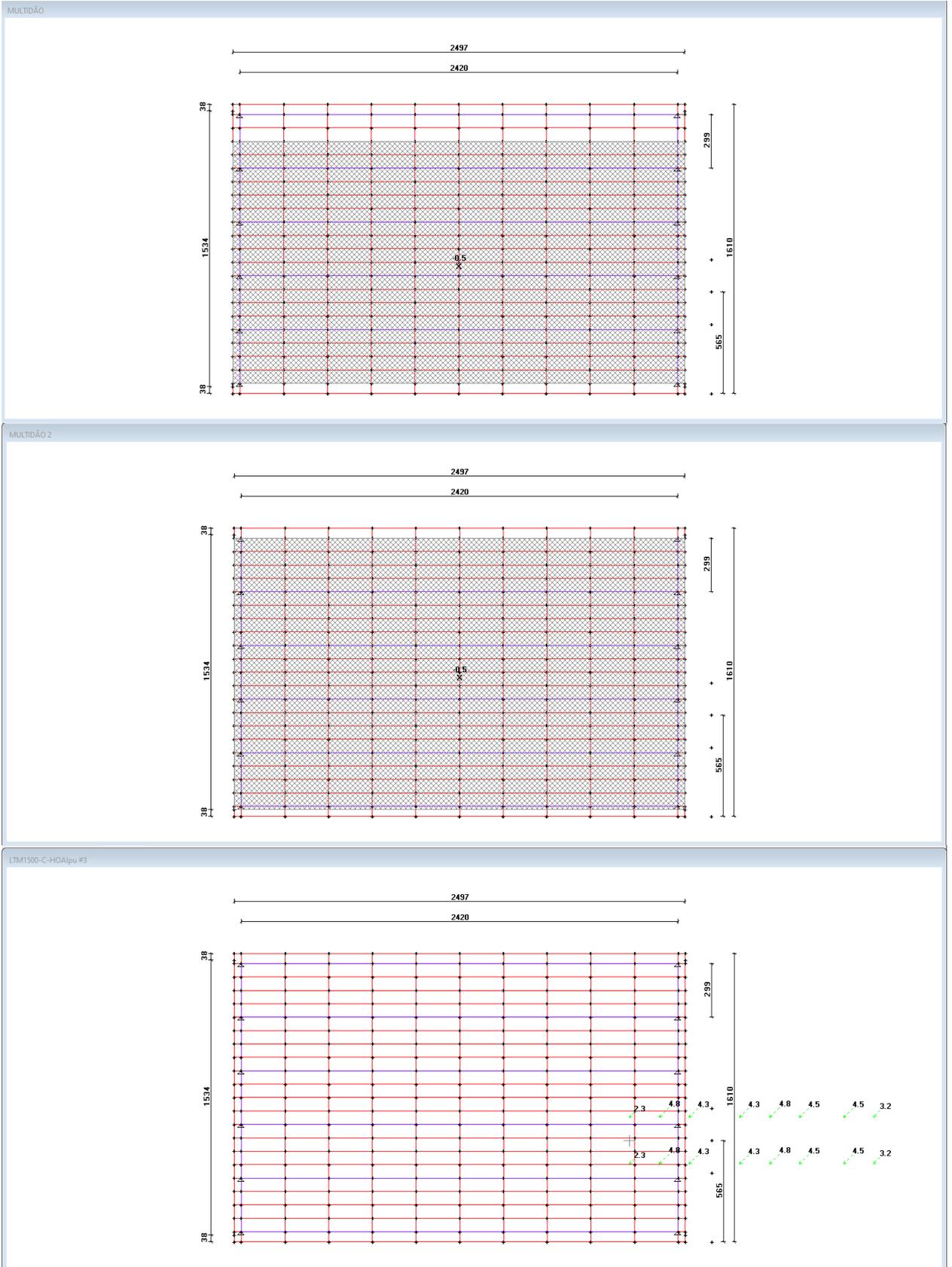
### NOTA TÉCNICA

#### 4.5.4. Tabuleiro 16,10 m



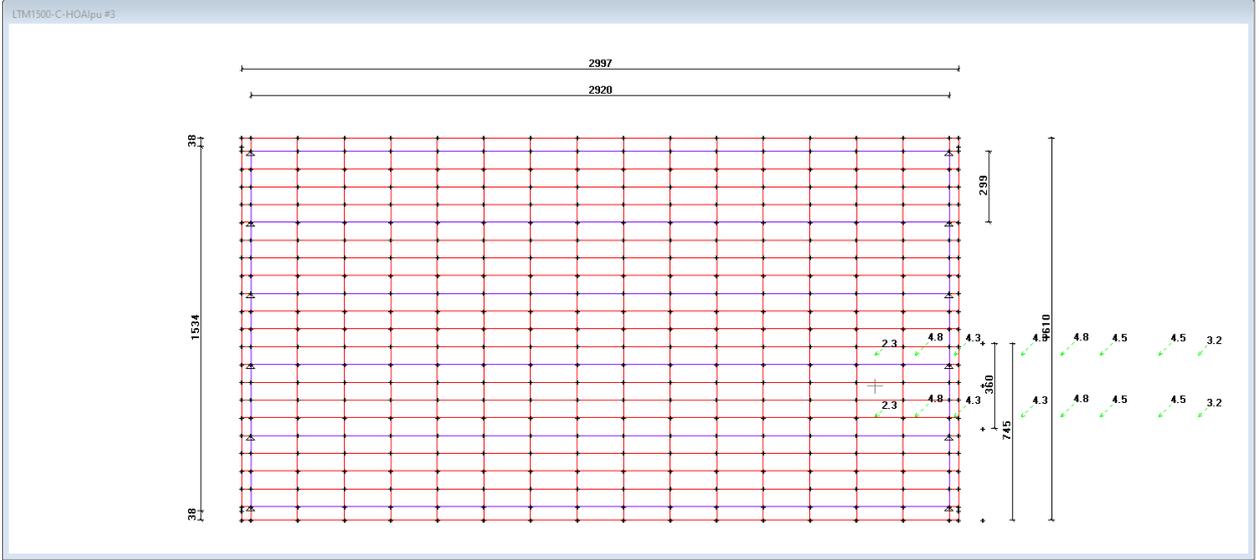
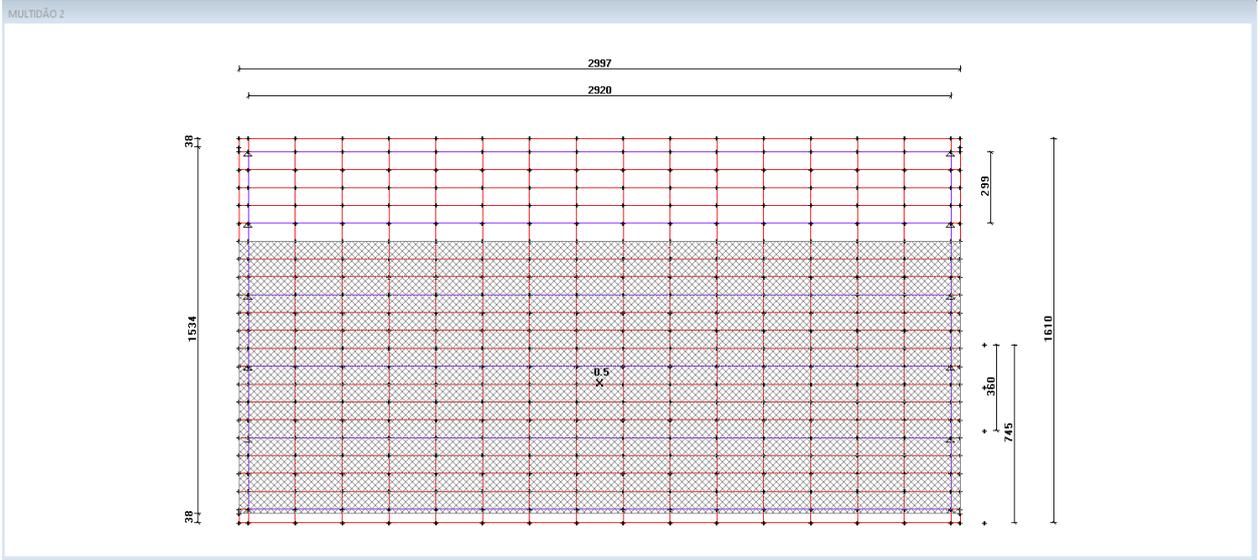
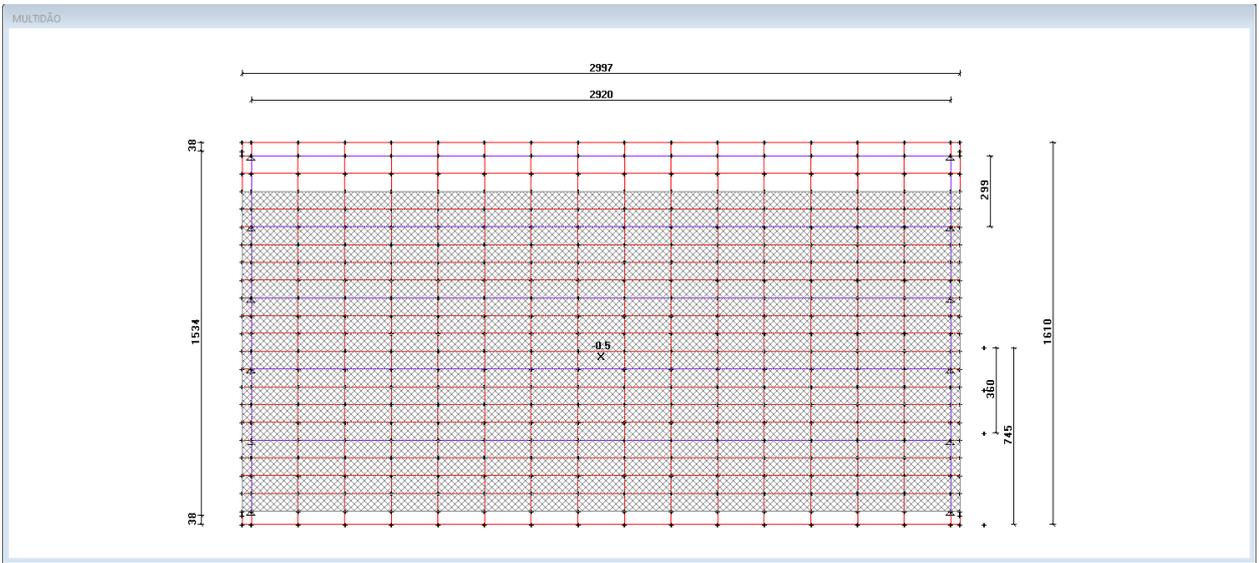


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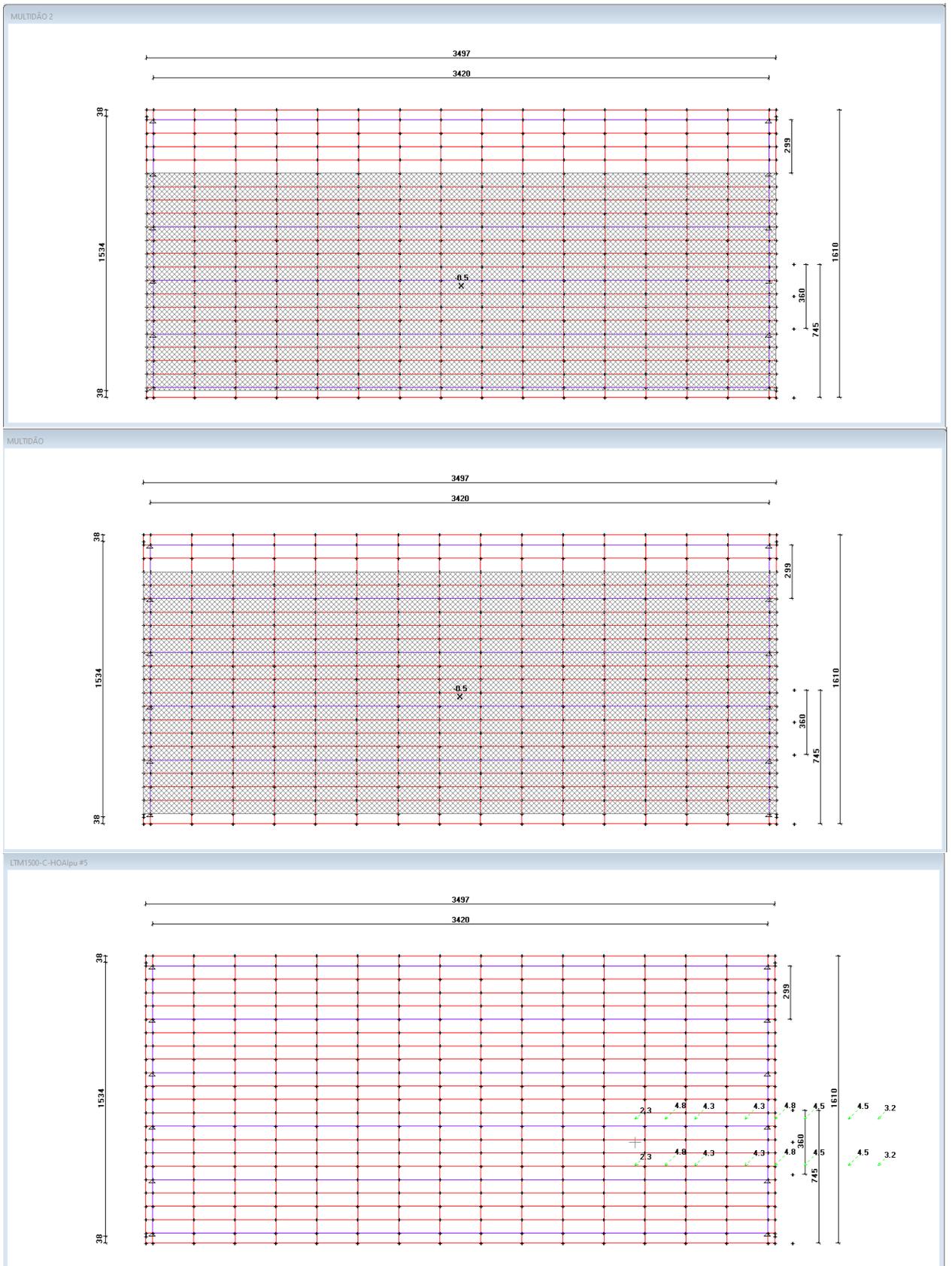


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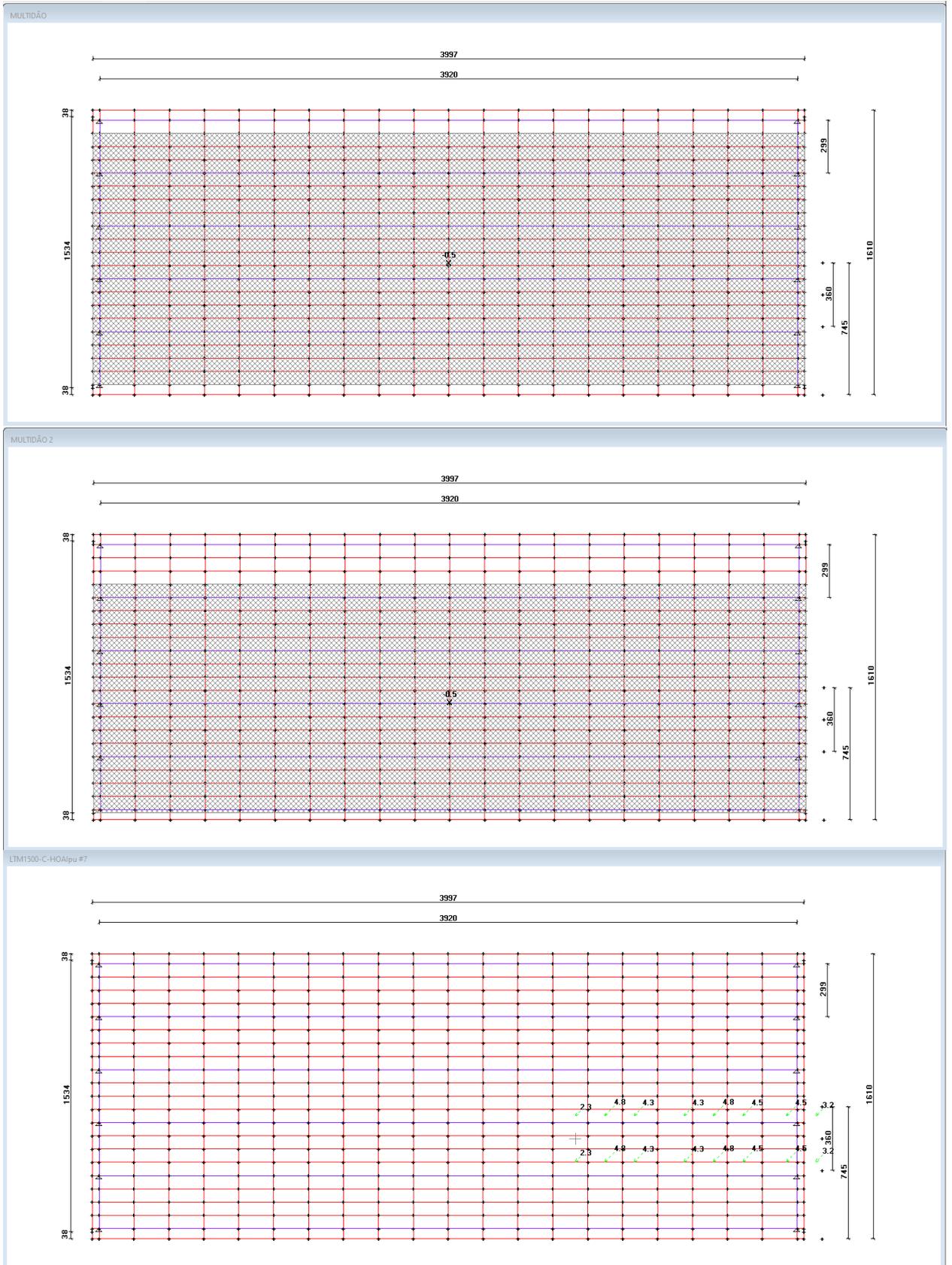


### NOTA TÉCNICA





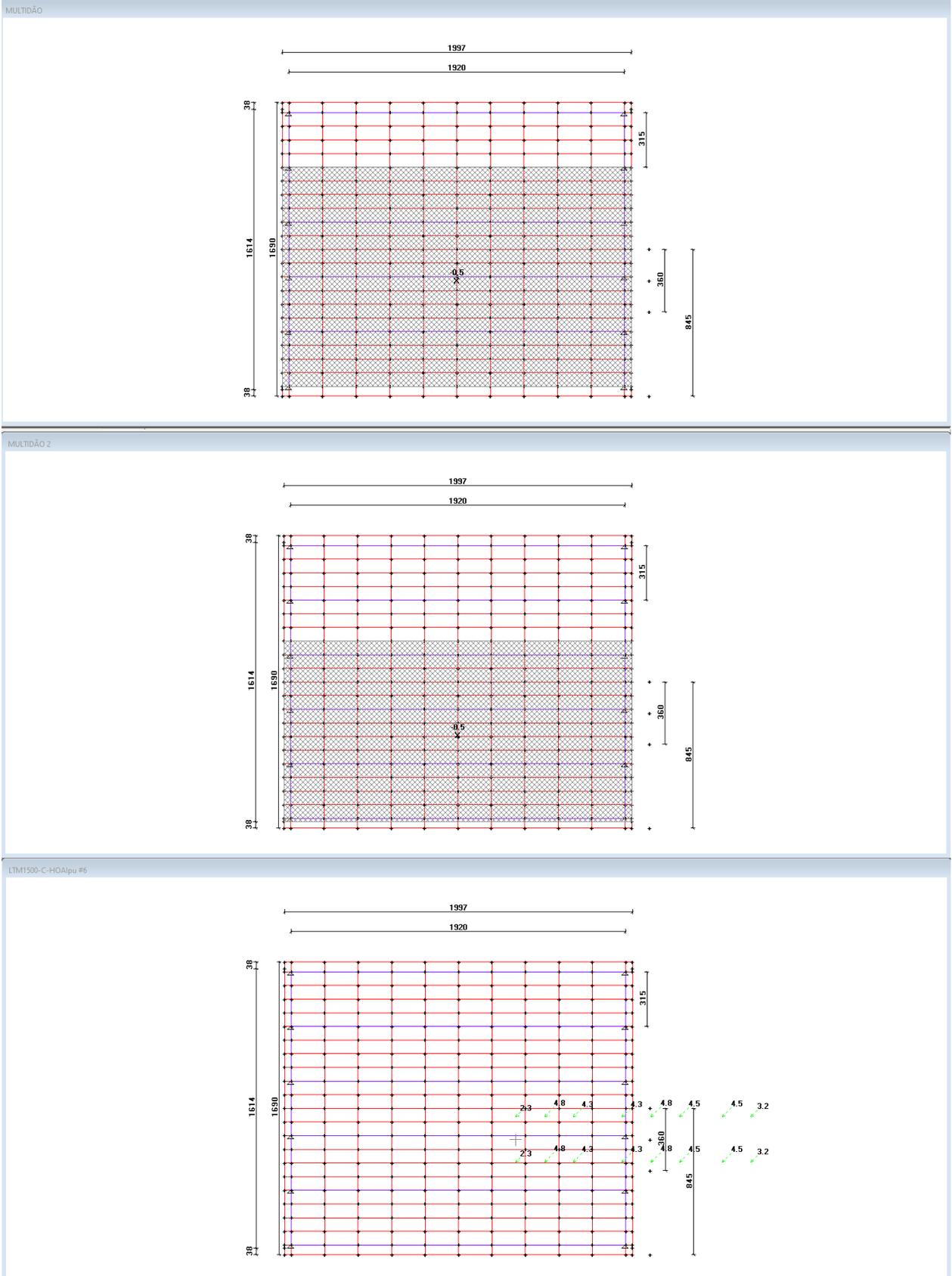
### NOTA TÉCNICA





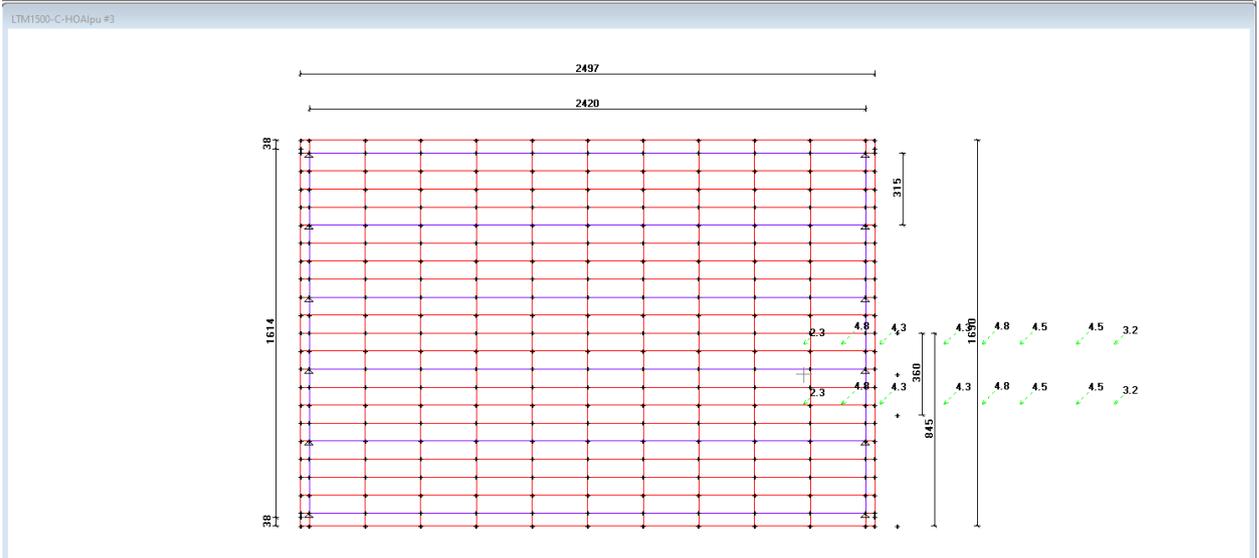
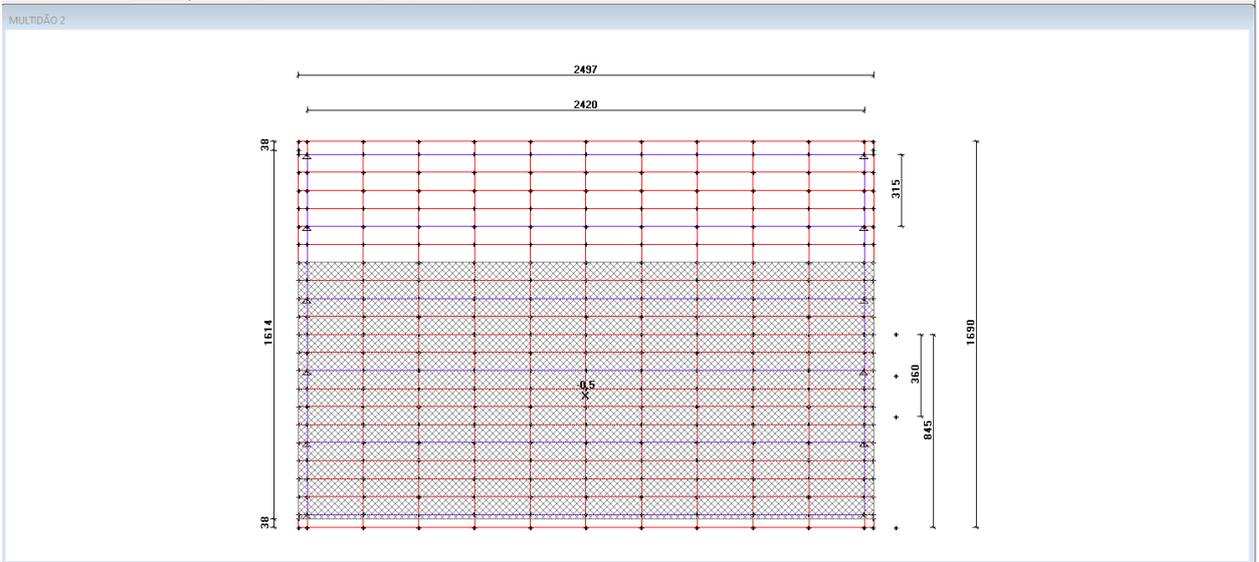
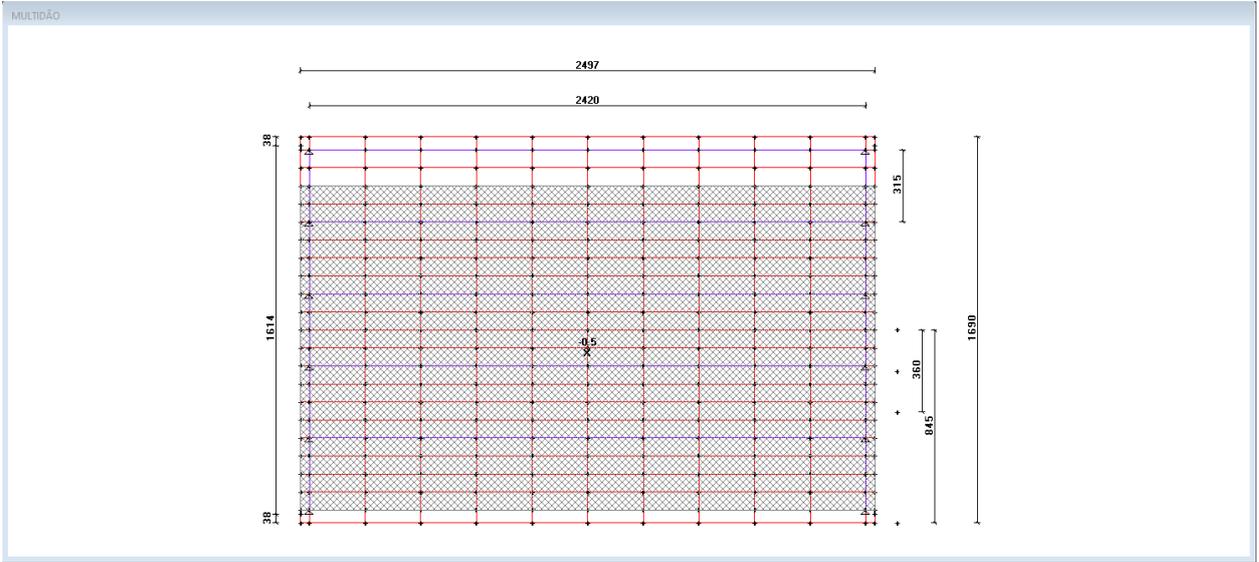
### NOTA TÉCNICA

#### 4.5.5. Tabuleiro 16,90 m



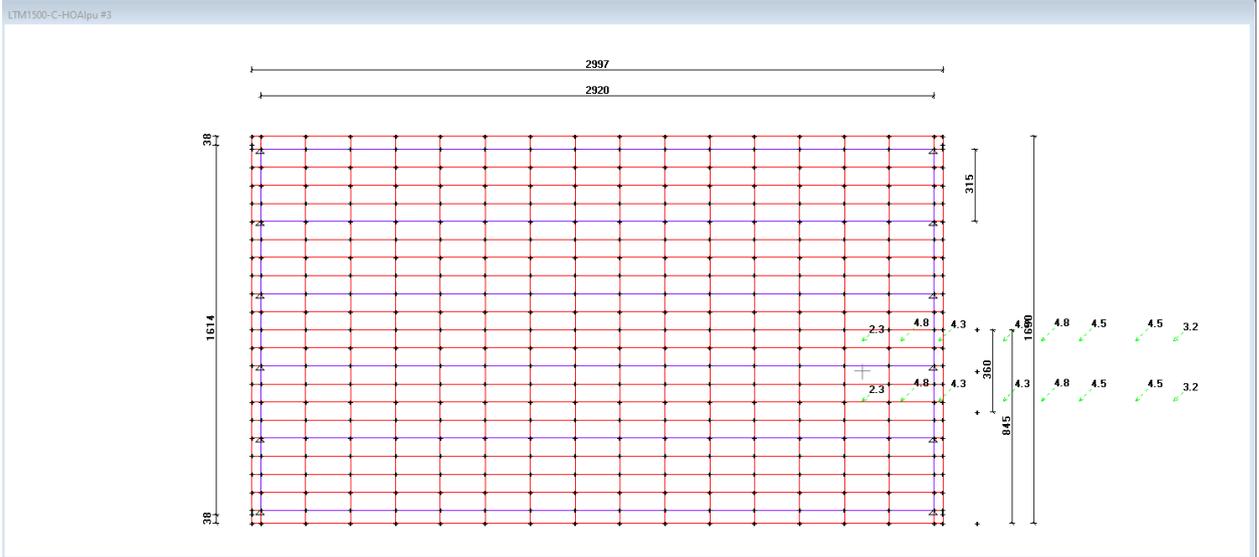
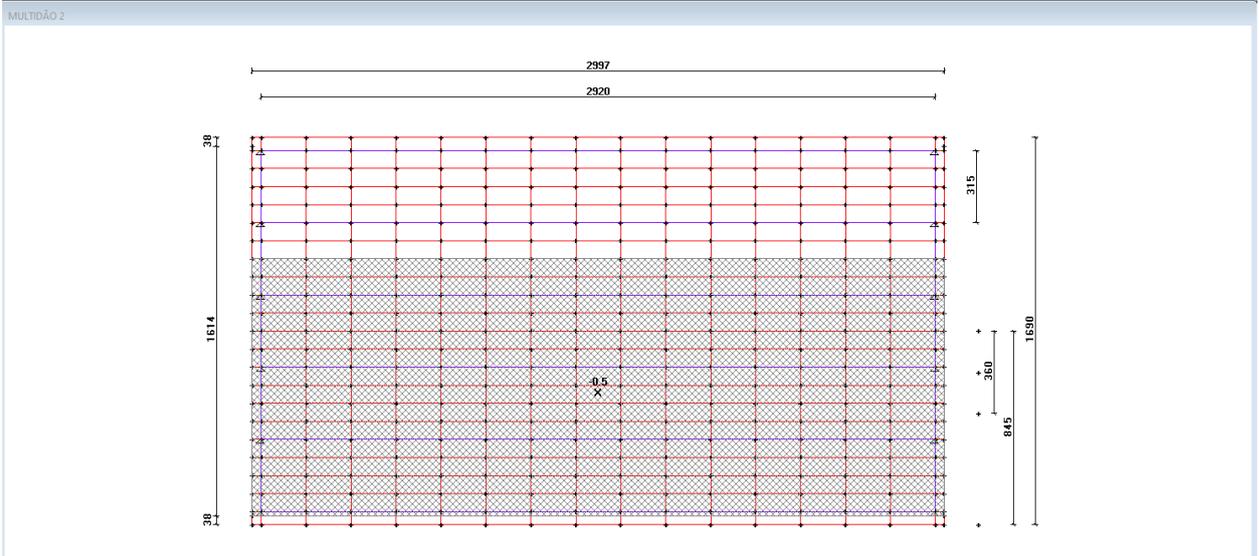
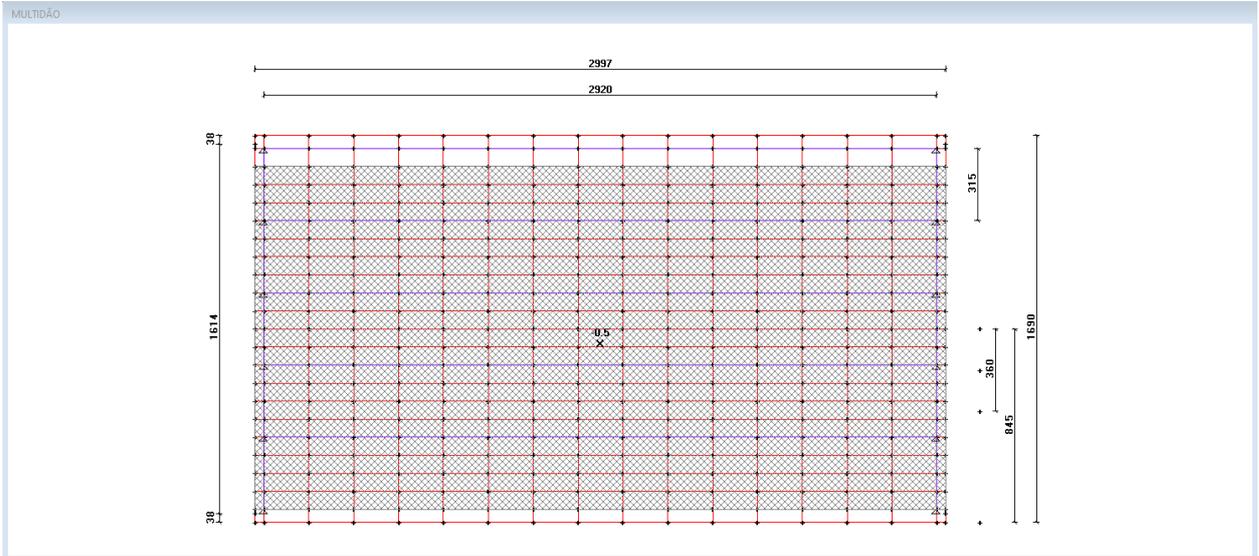


### NOTA TÉCNICA



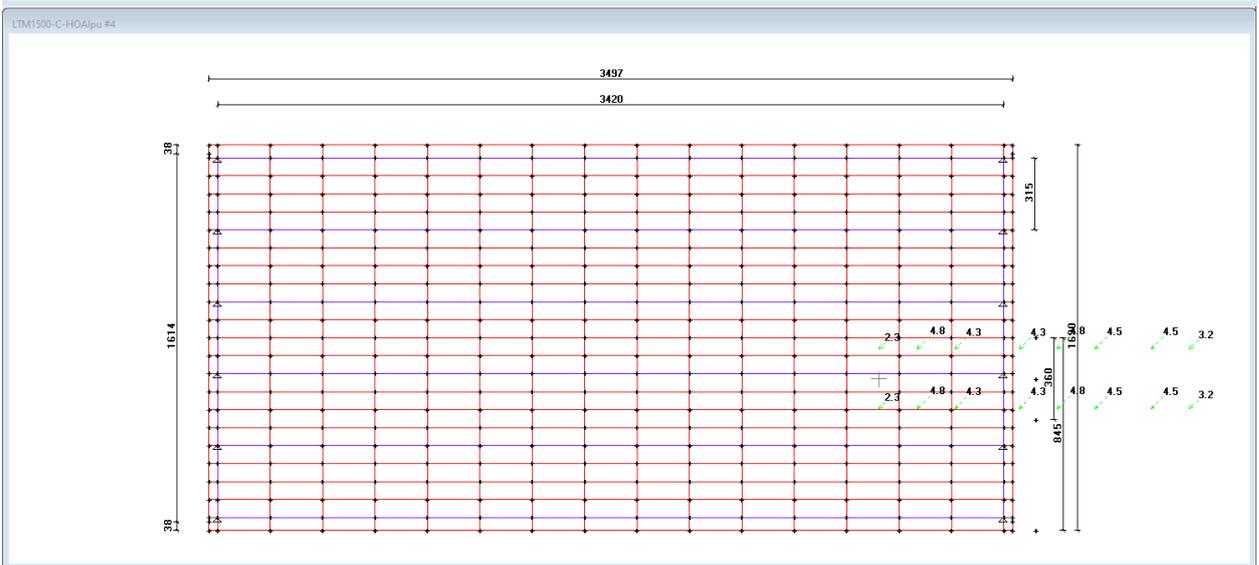
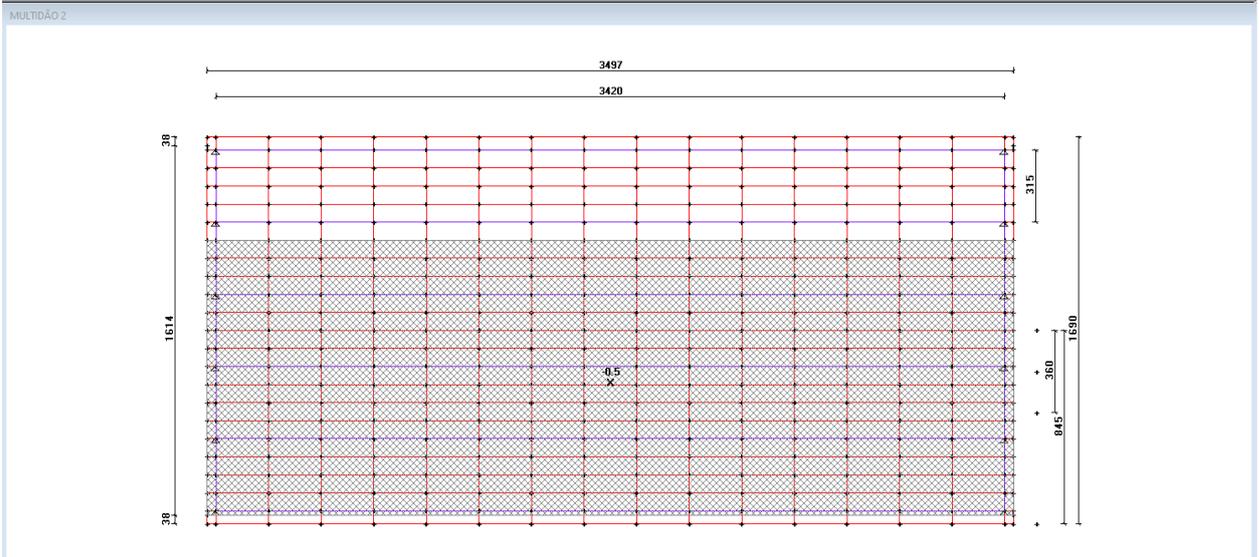
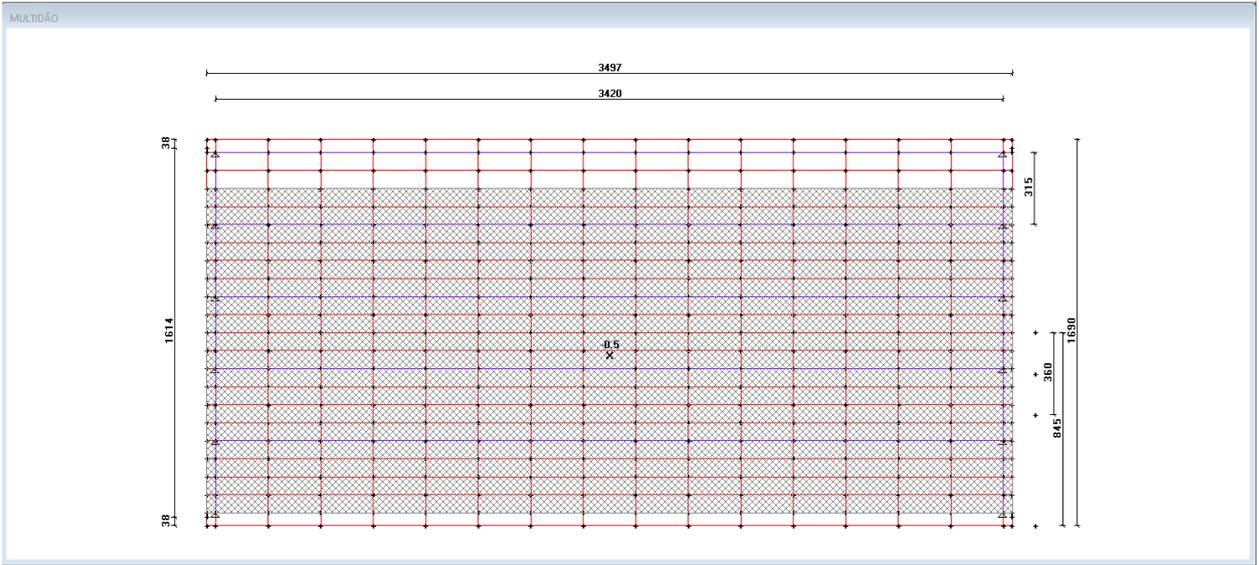


### NOTA TÉCNICA



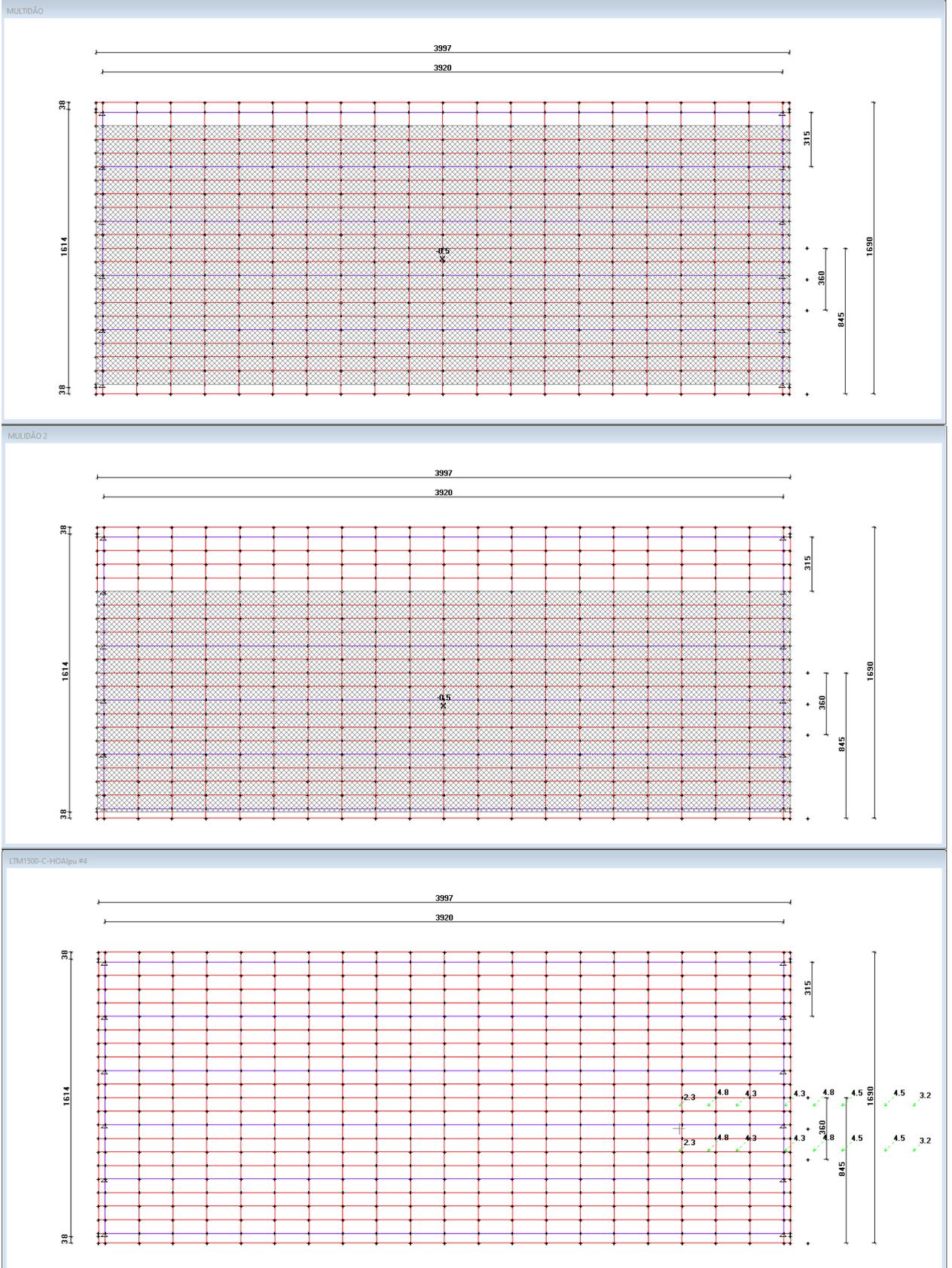


### NOTA TÉCNICA





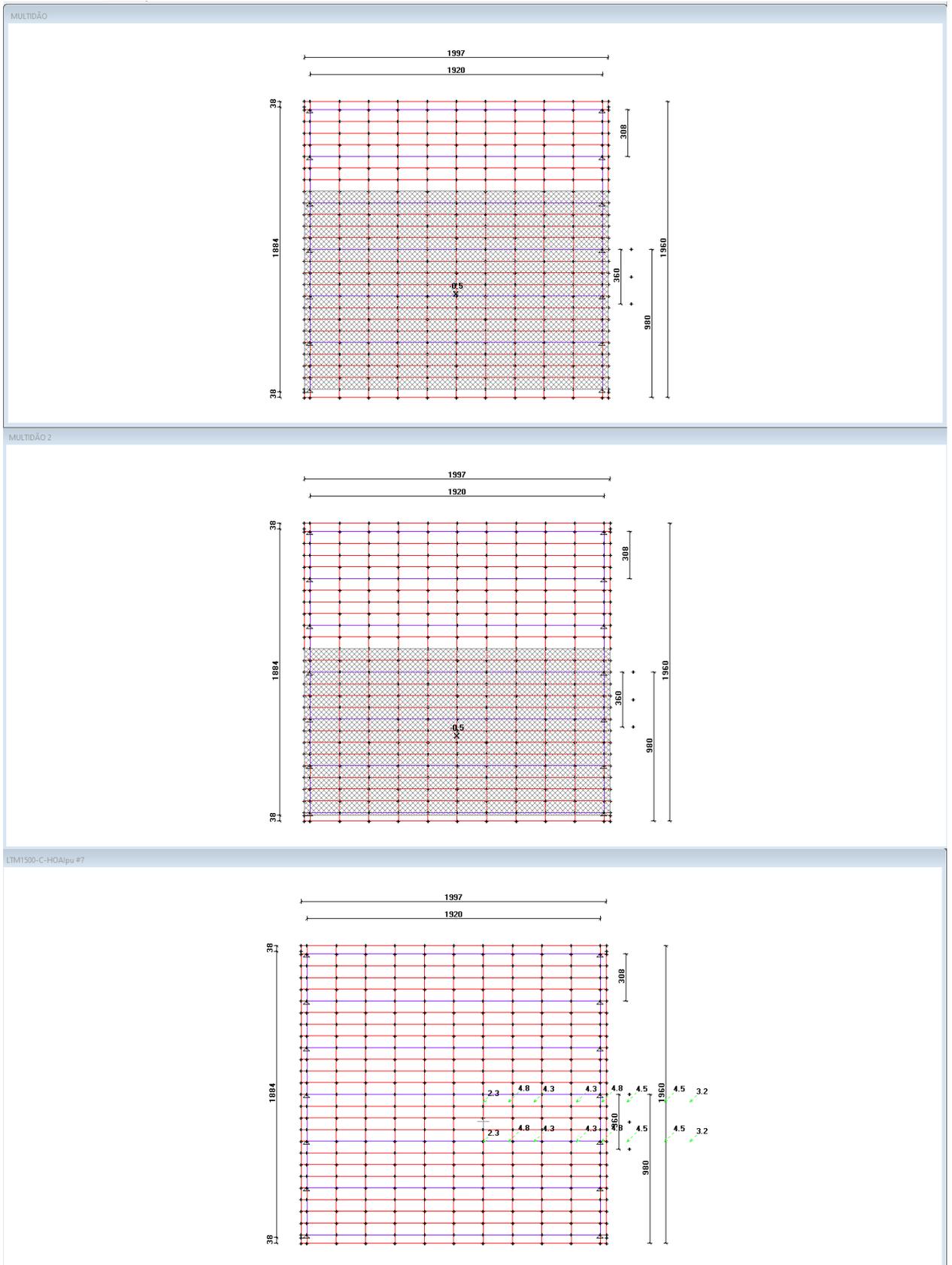
NOTA TÉCNICA





### NOTA TÉCNICA

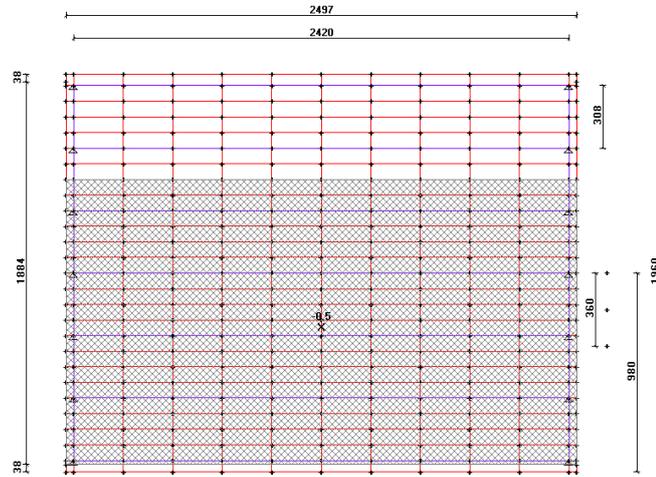
#### 4.5.6. Tabuleiro 19,60 m



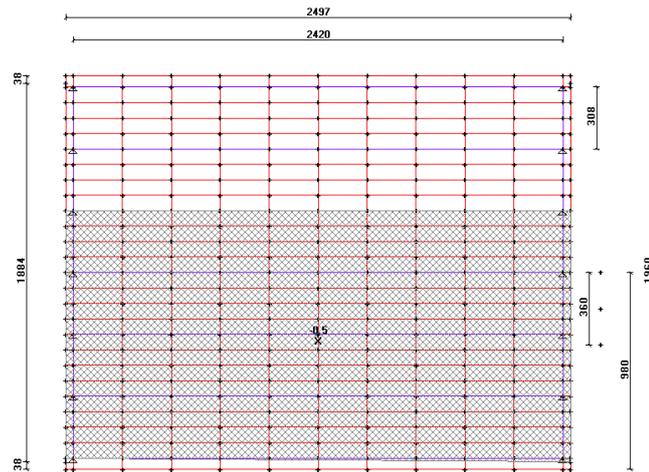


### NOTA TÉCNICA

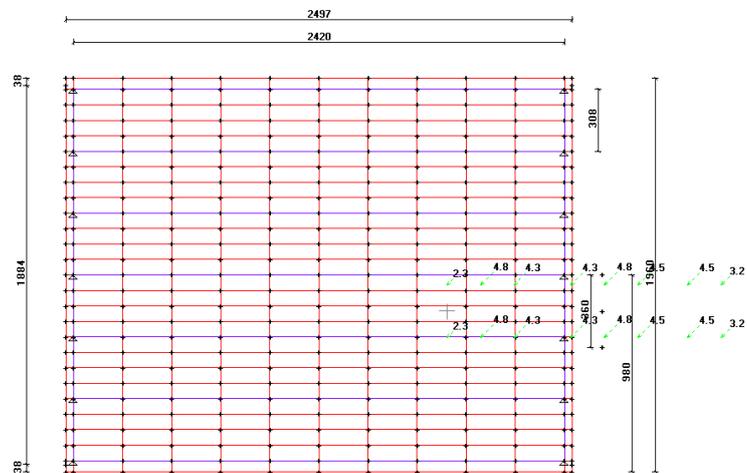
MULTIDÃO



MULTIDÃO 2



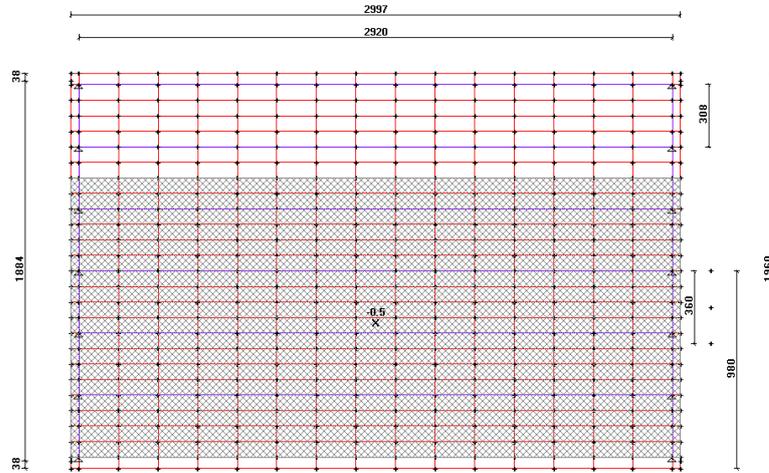
LTM1500-C-HQAlpu #5



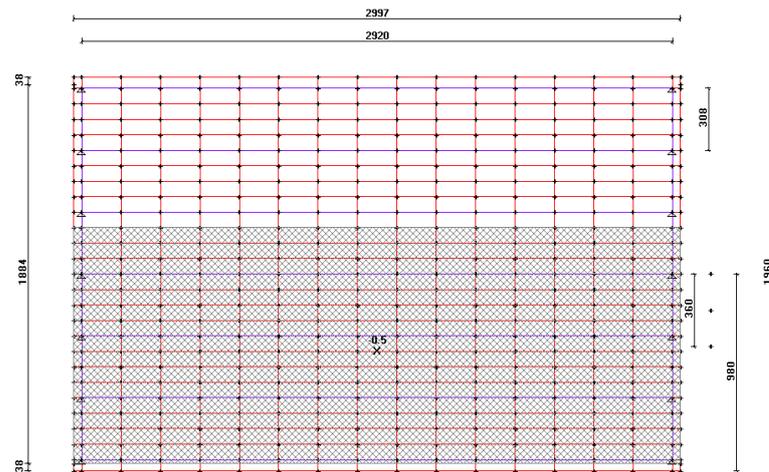


### NOTA TÉCNICA

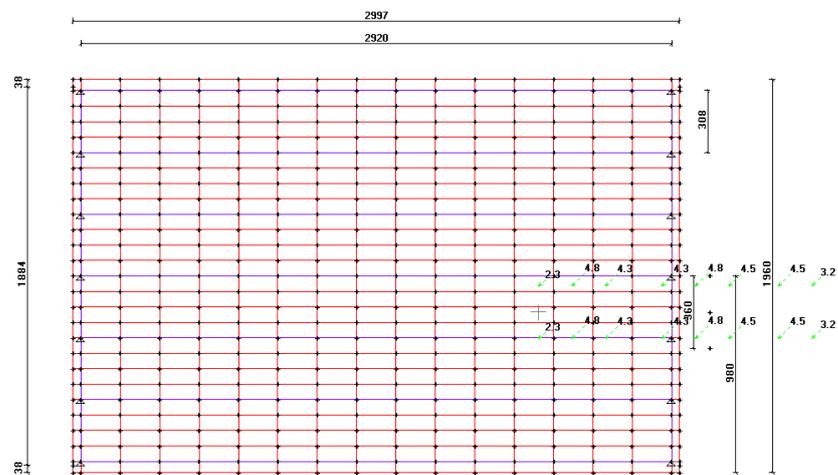
MULTIDÃO



MULTIDÃO 2

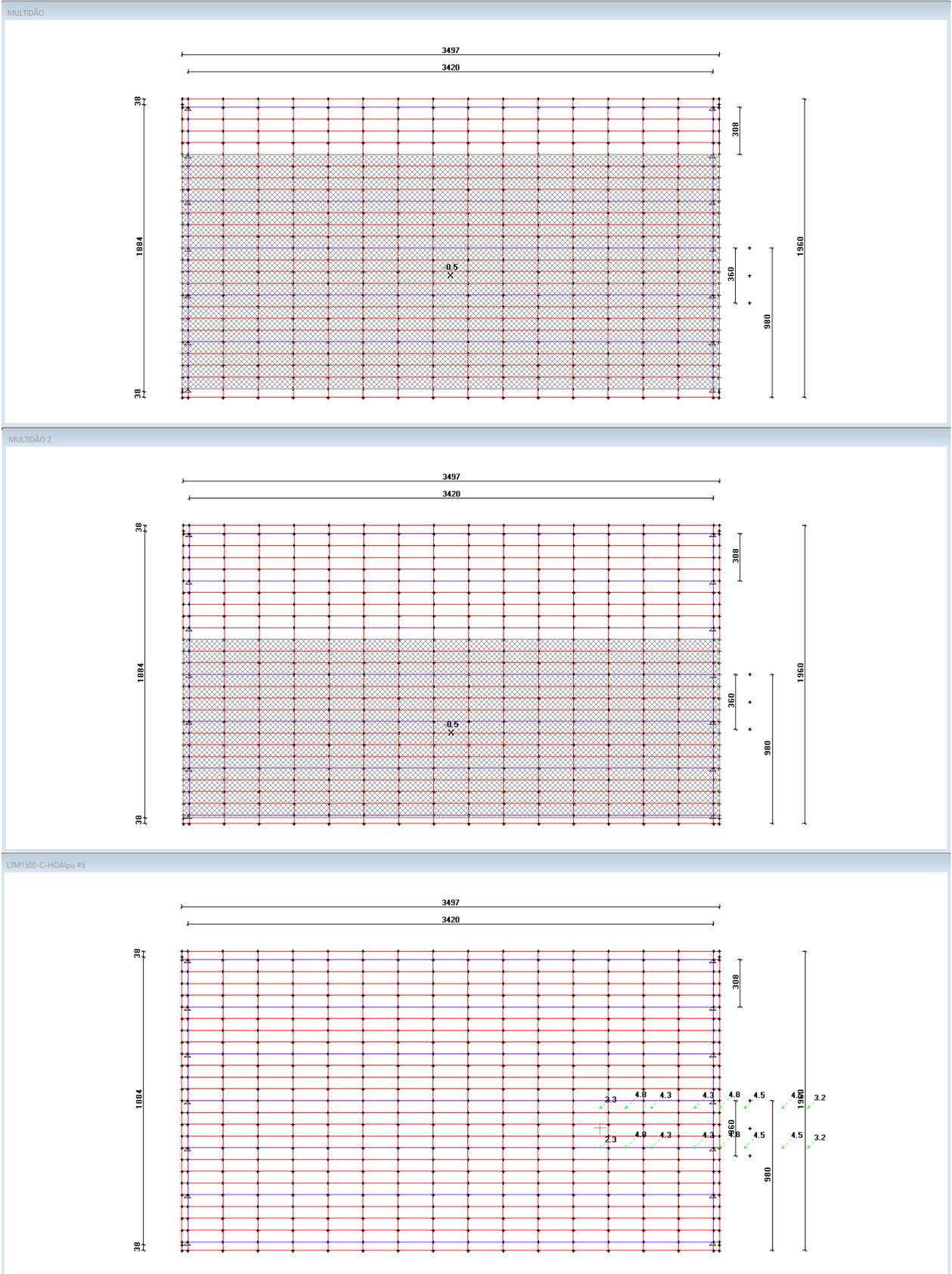


LTM1500-C-HOAlpu #5



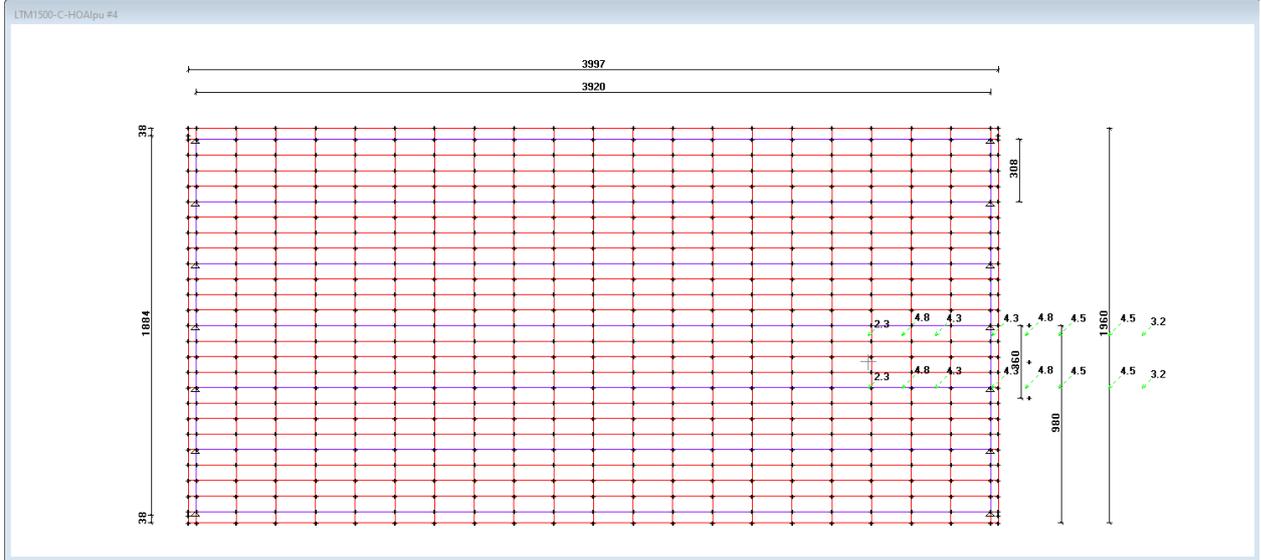
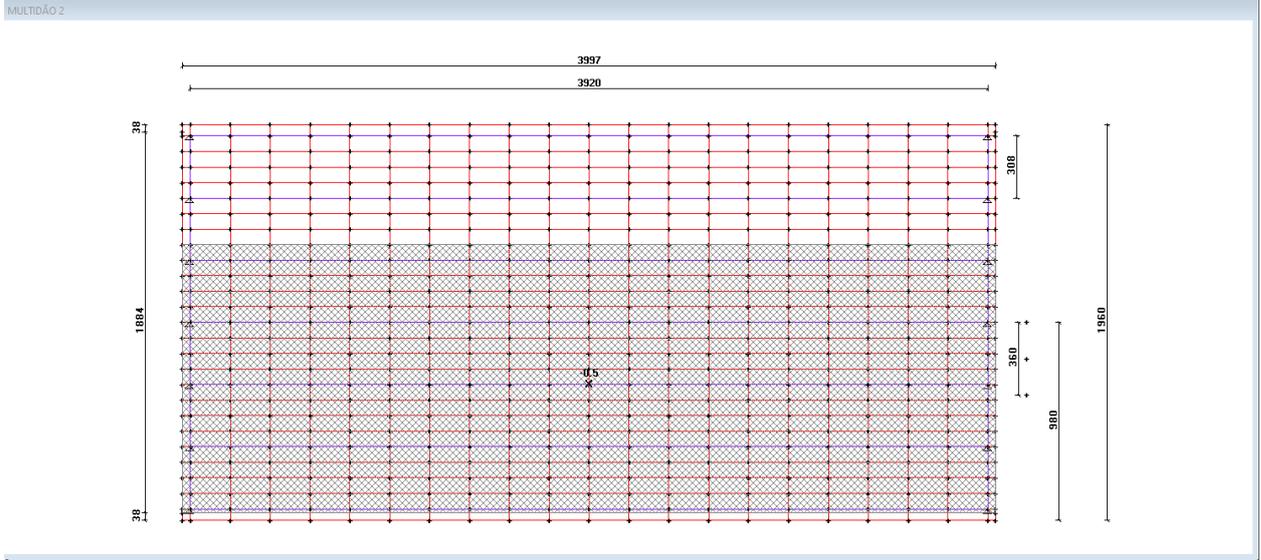
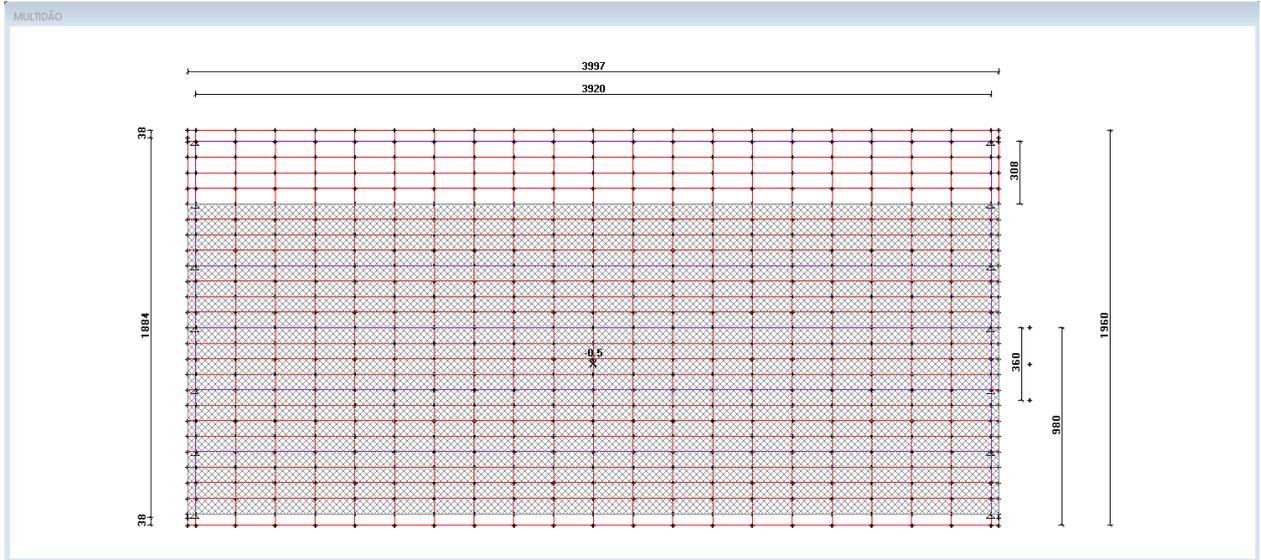


### NOTA TÉCNICA





### NOTA TÉCNICA

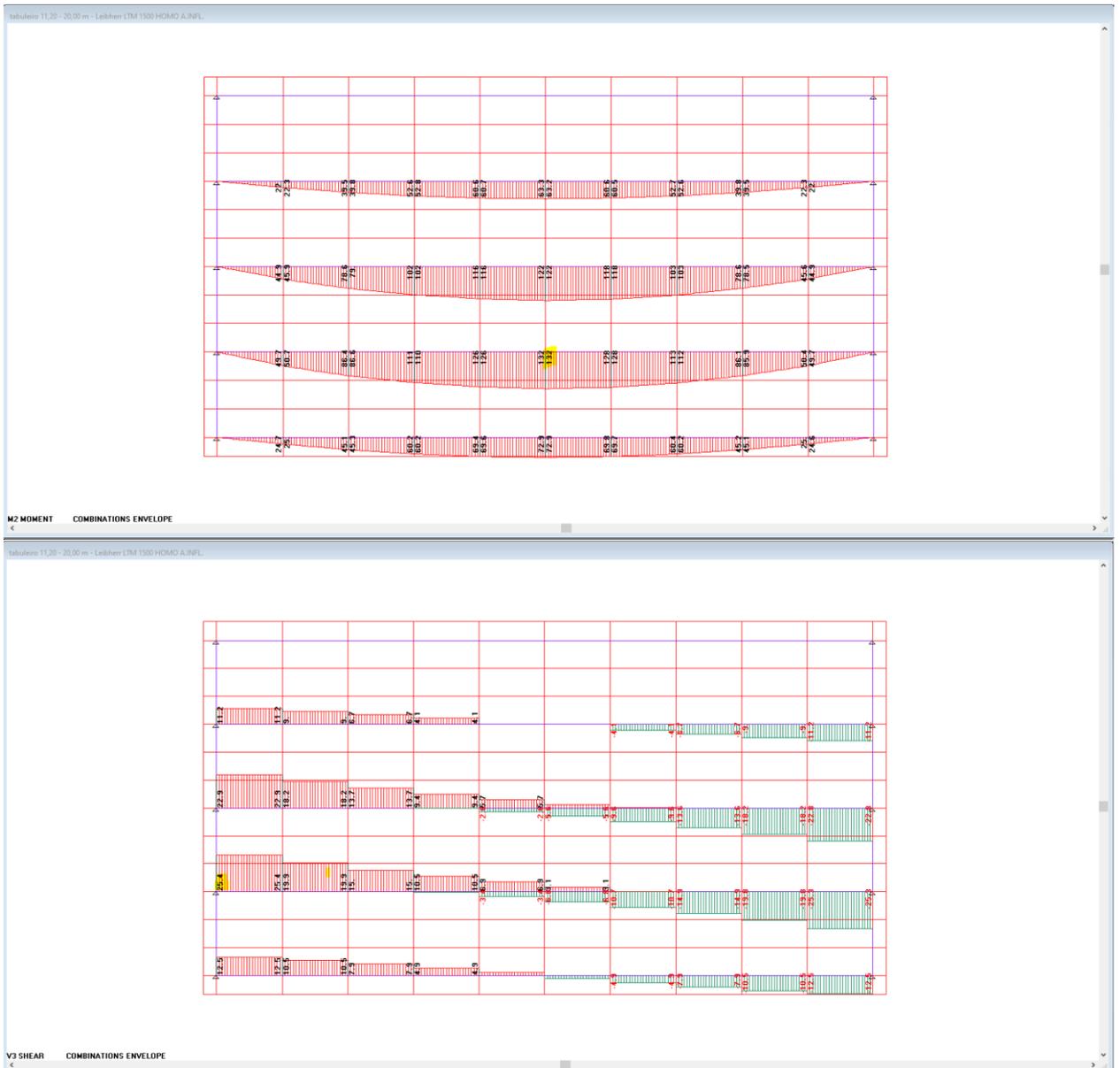




## NOTA TÉCNICA

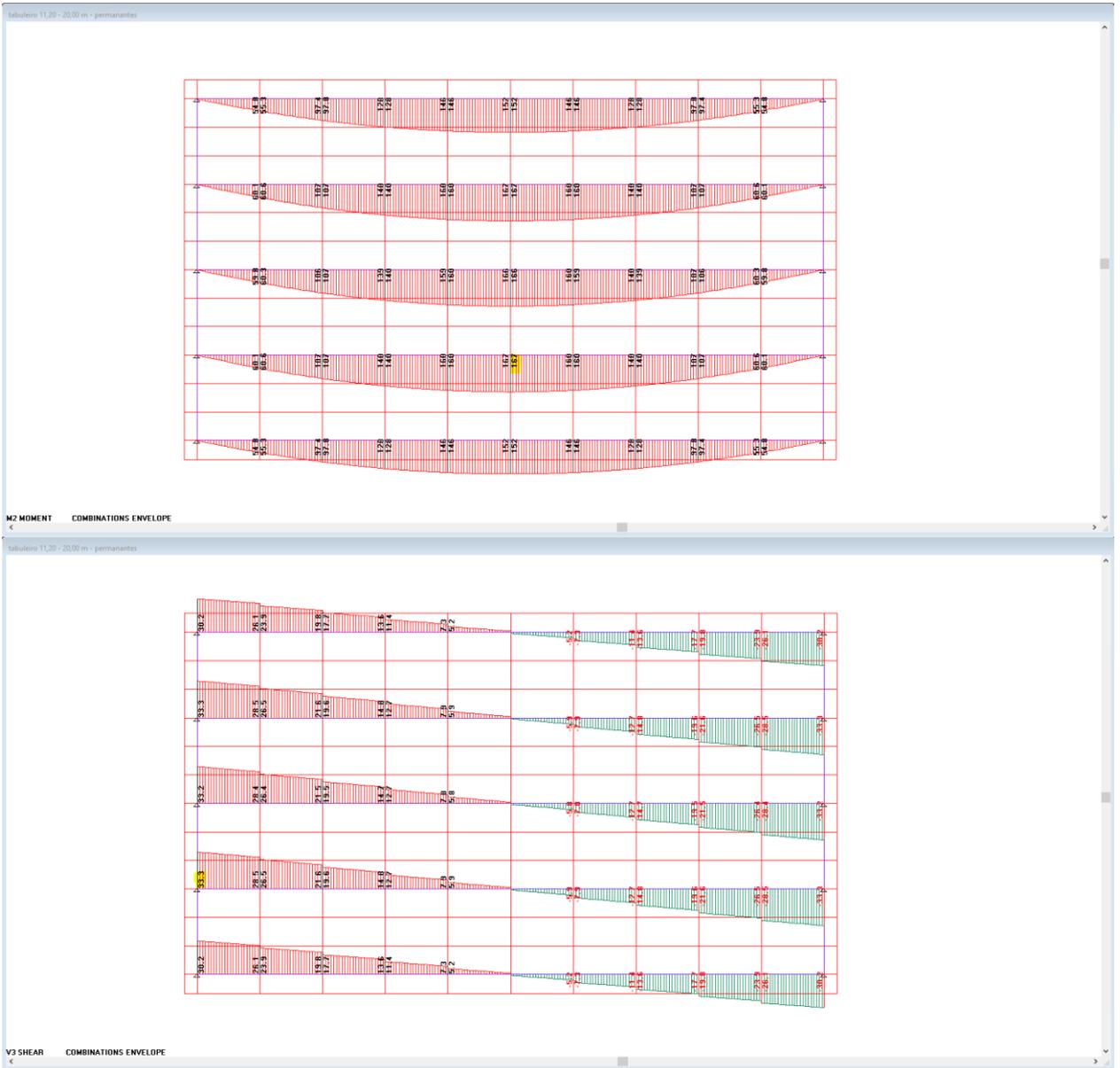
### 4.6. Momentos e cortantes (cargas permanentes, TB-36 e Liebherr)

#### 4.6.1. Tabuleiro 11,20 m



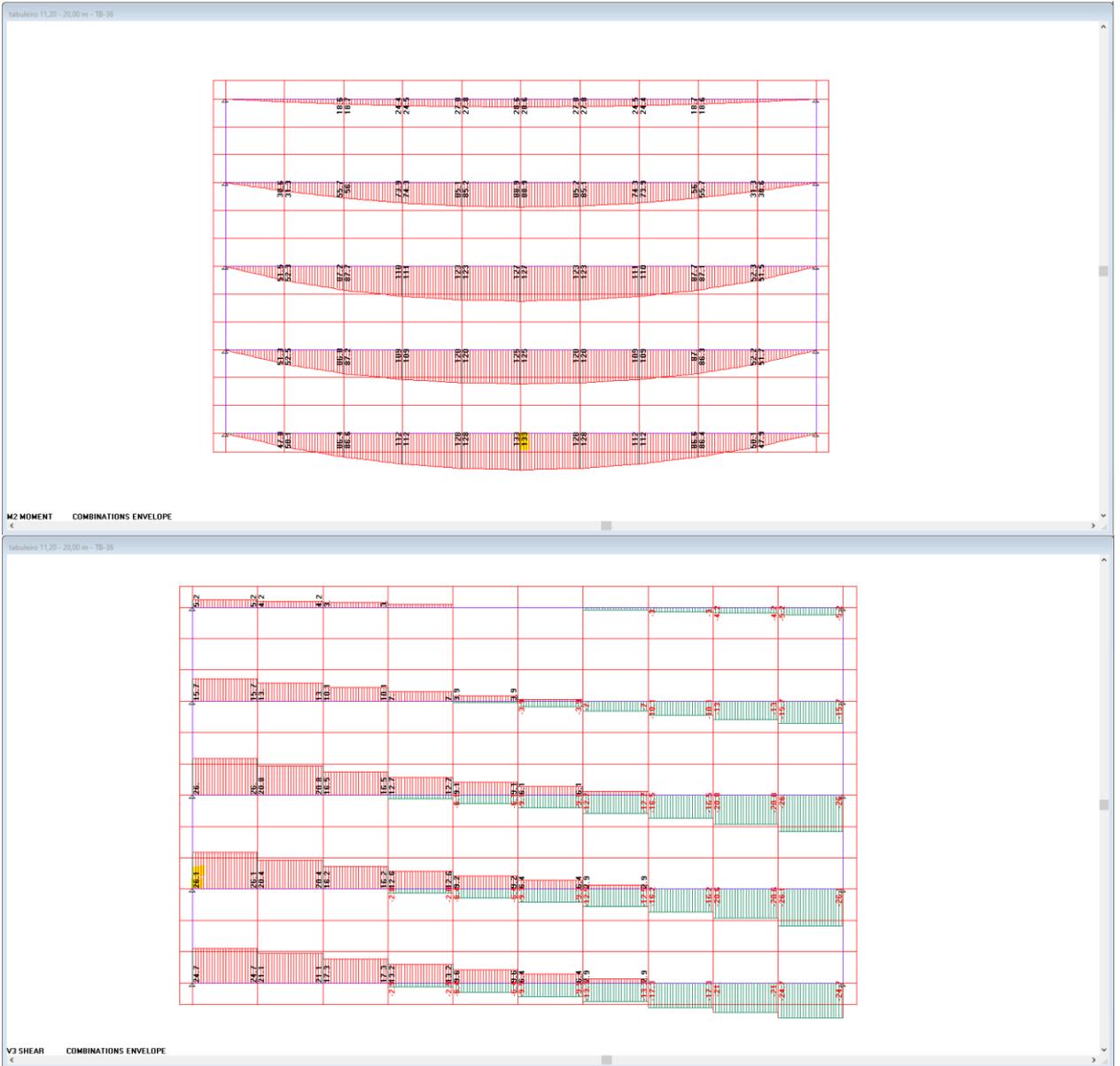


### NOTA TÉCNICA



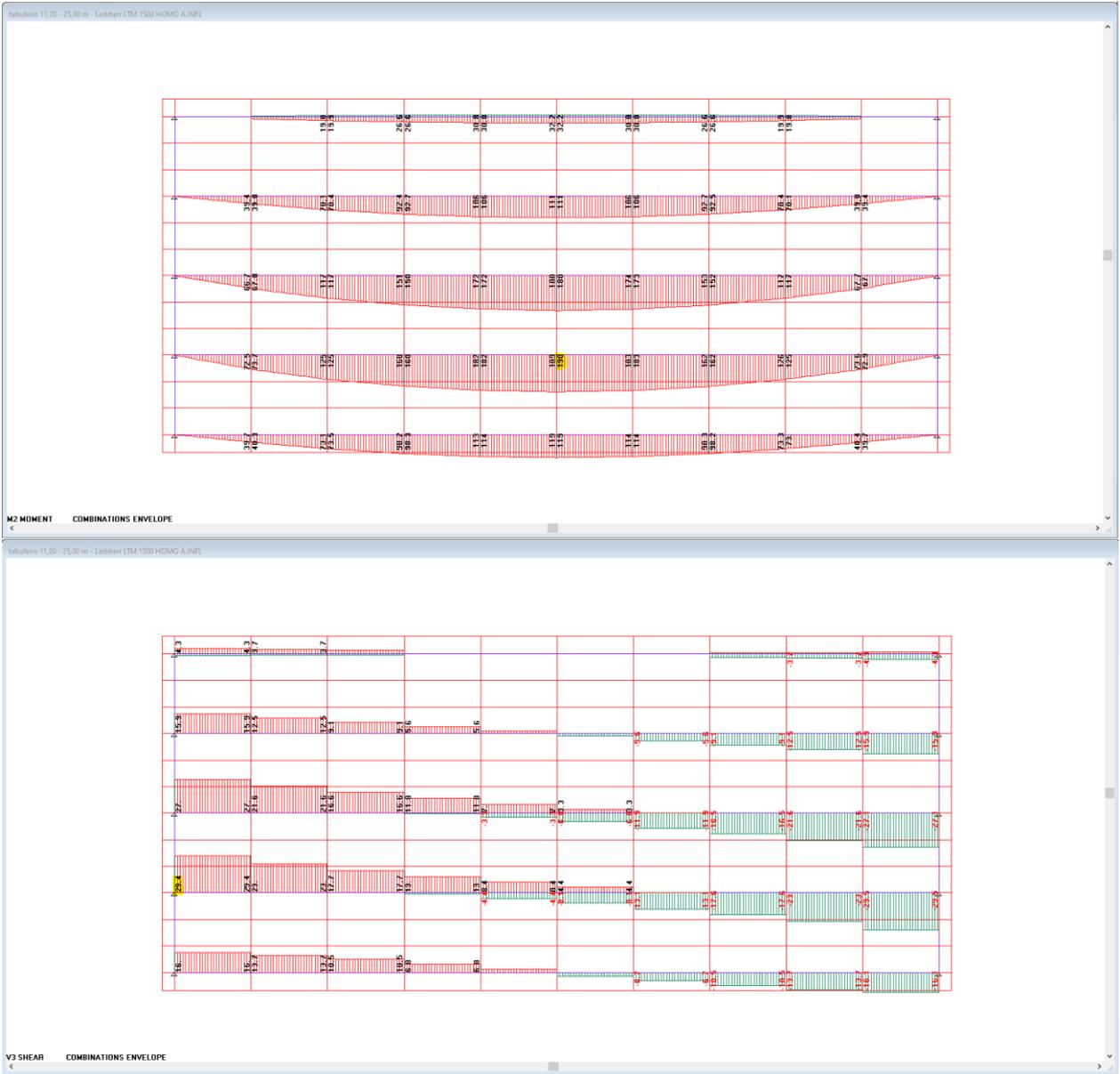


### NOTA TÉCNICA



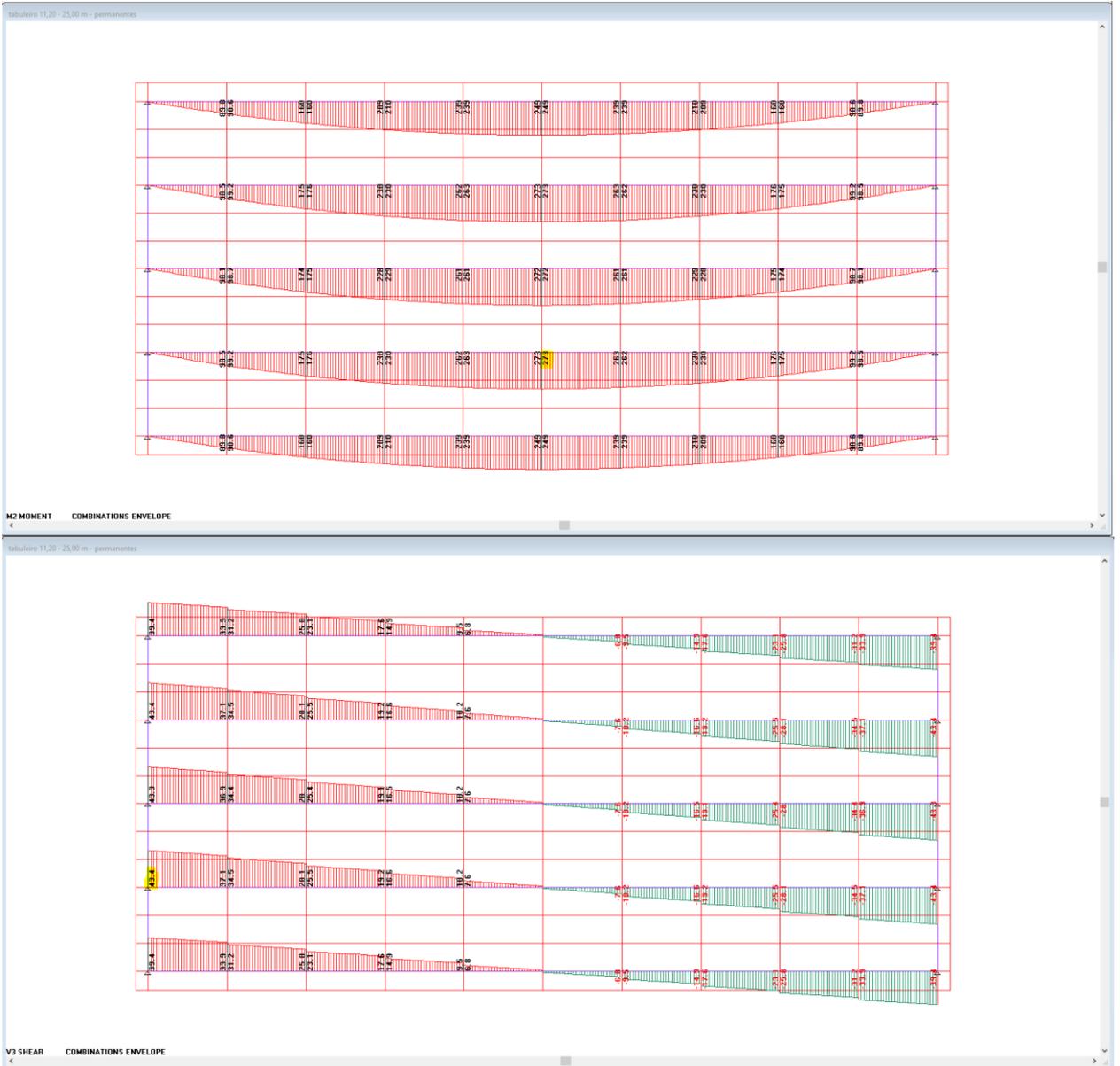


### NOTA TÉCNICA



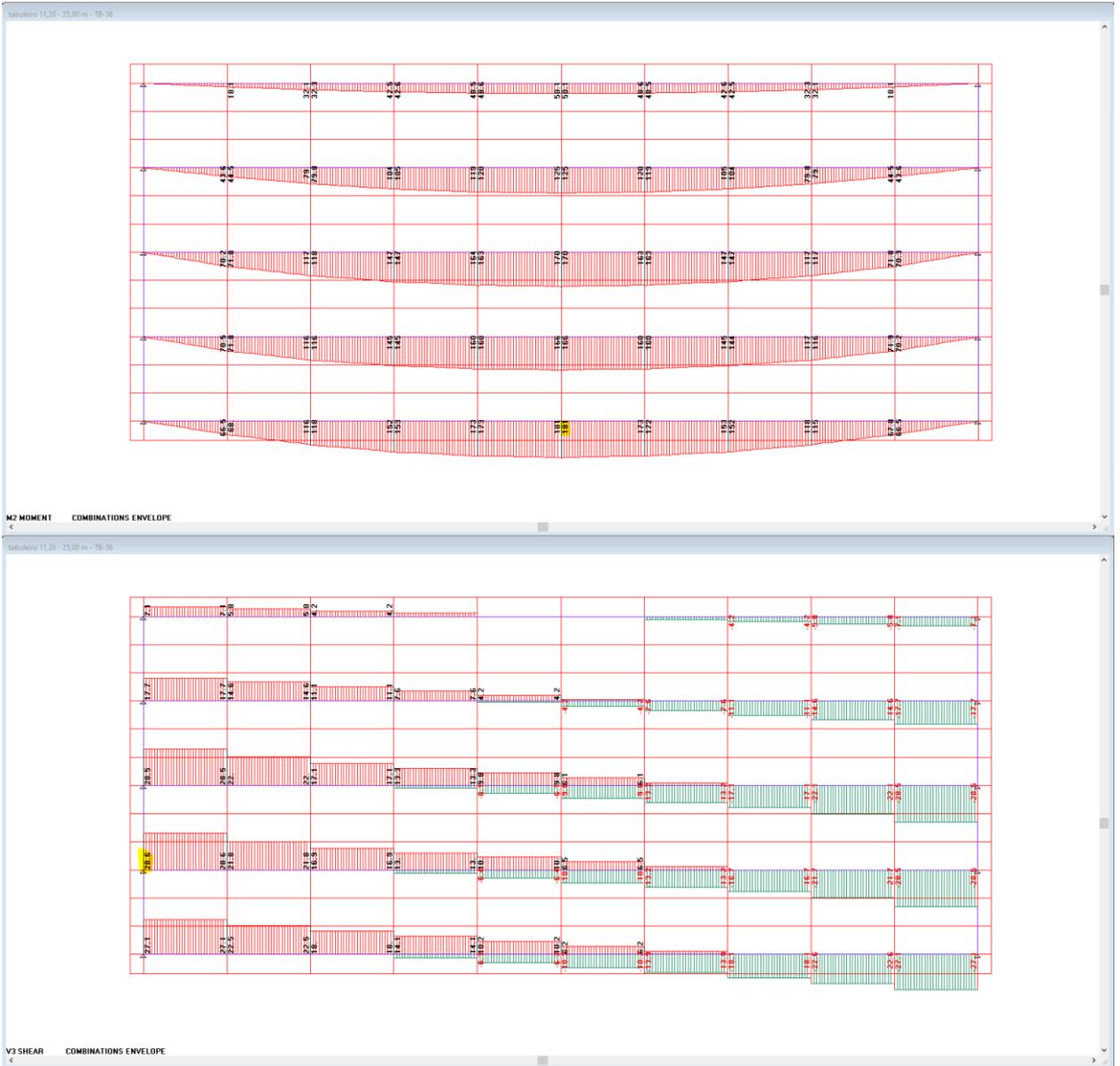


### NOTA TÉCNICA



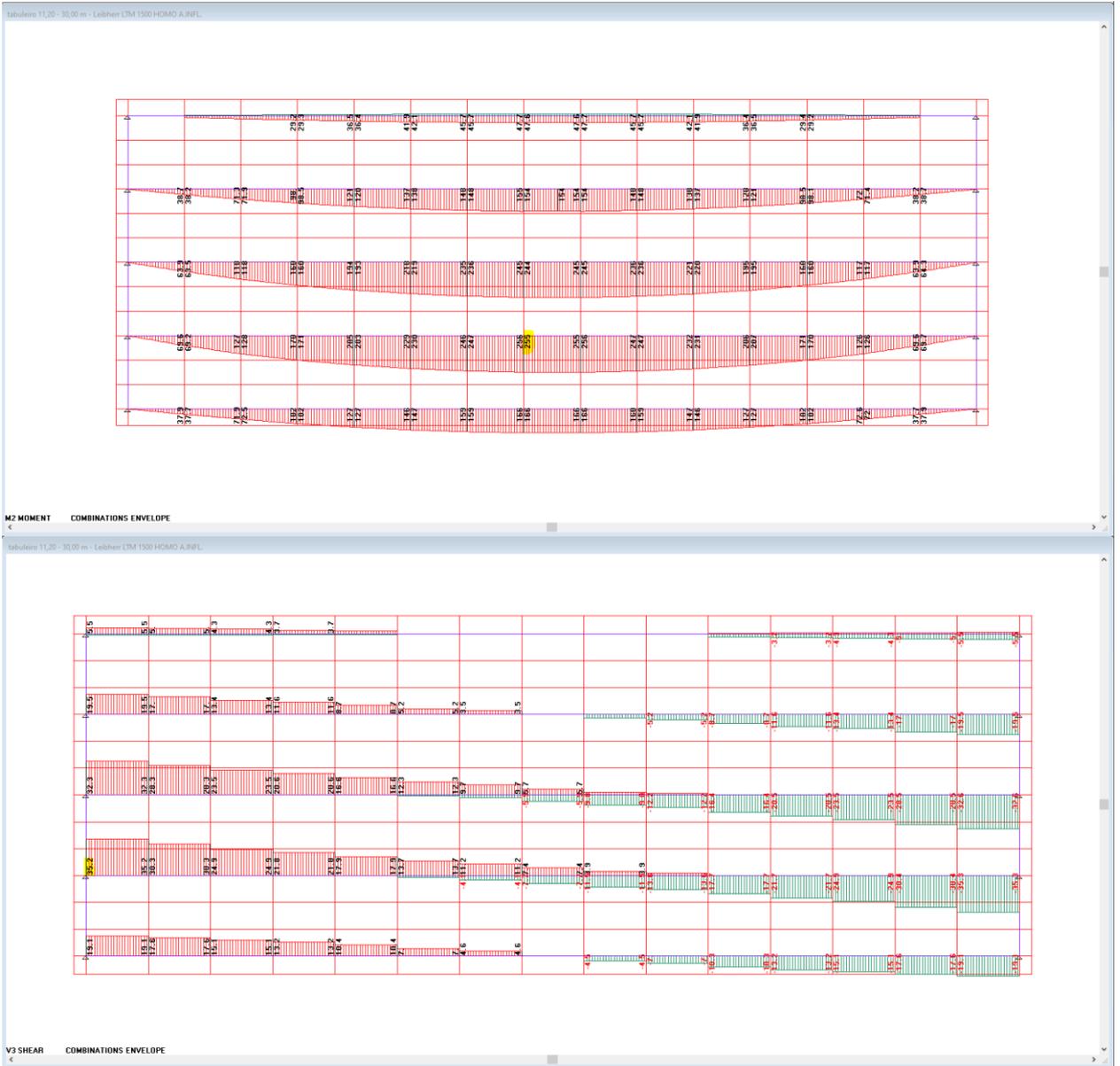


### NOTA TÉCNICA



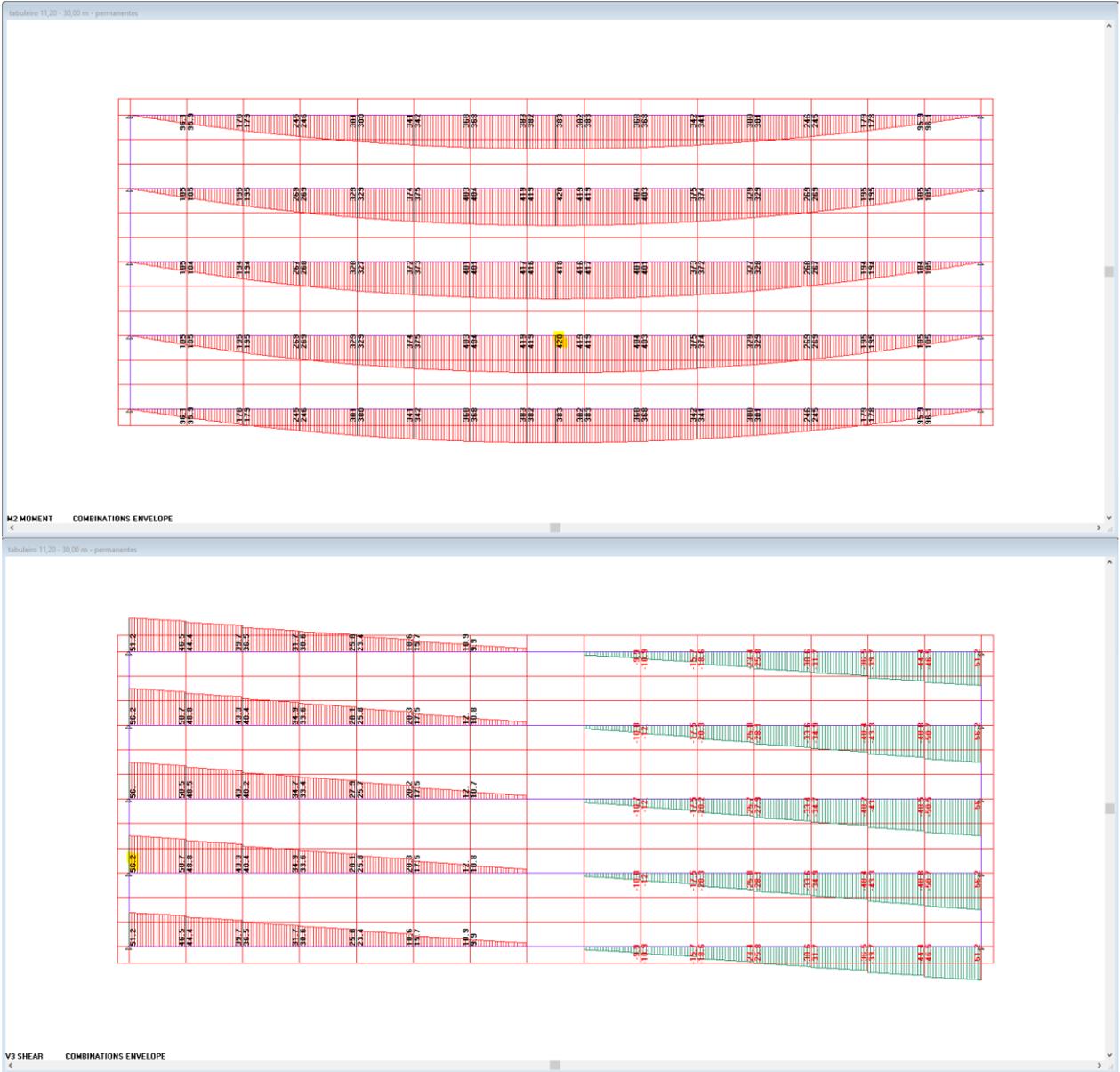


### NOTA TÉCNICA



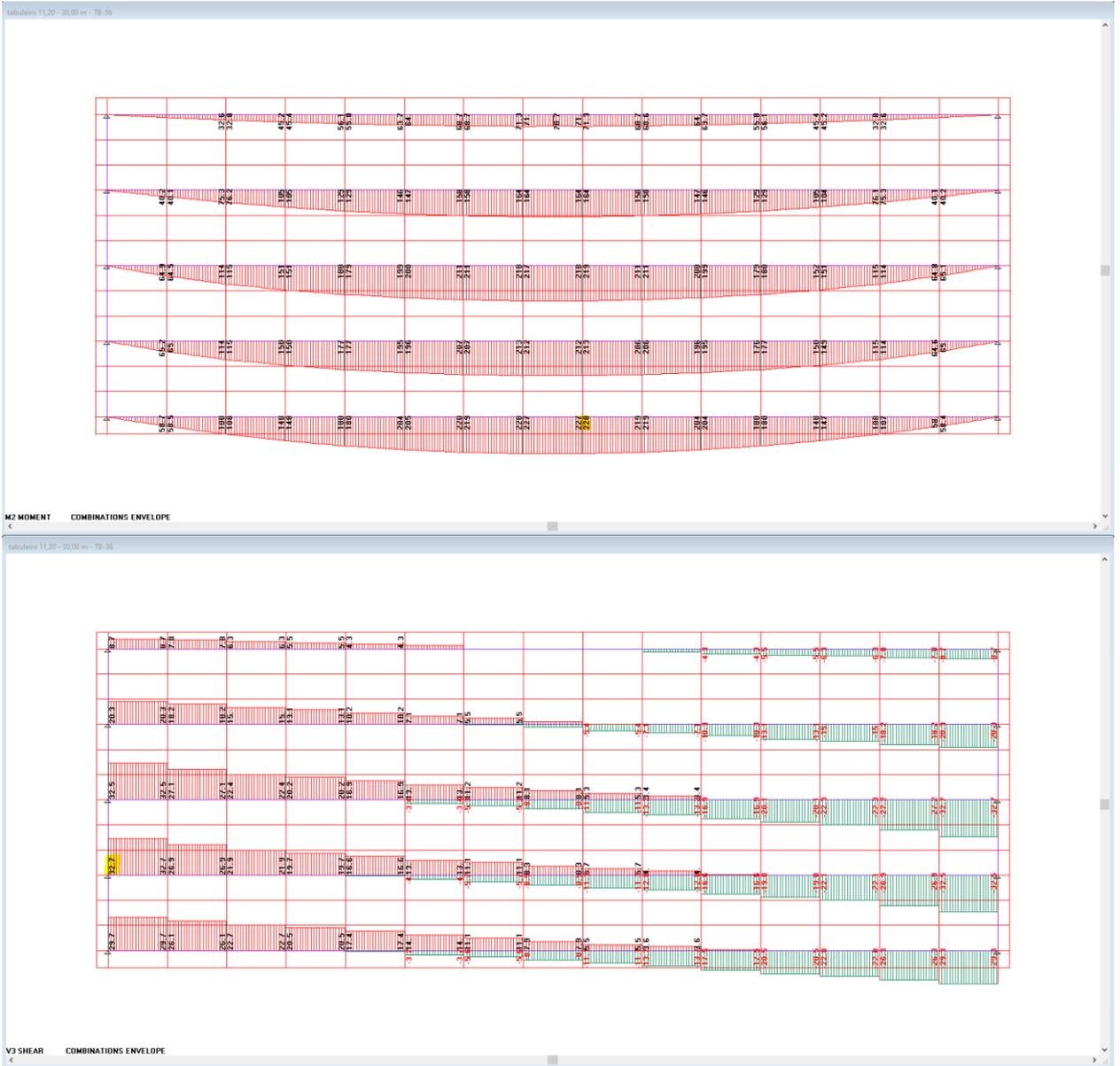


### NOTA TÉCNICA



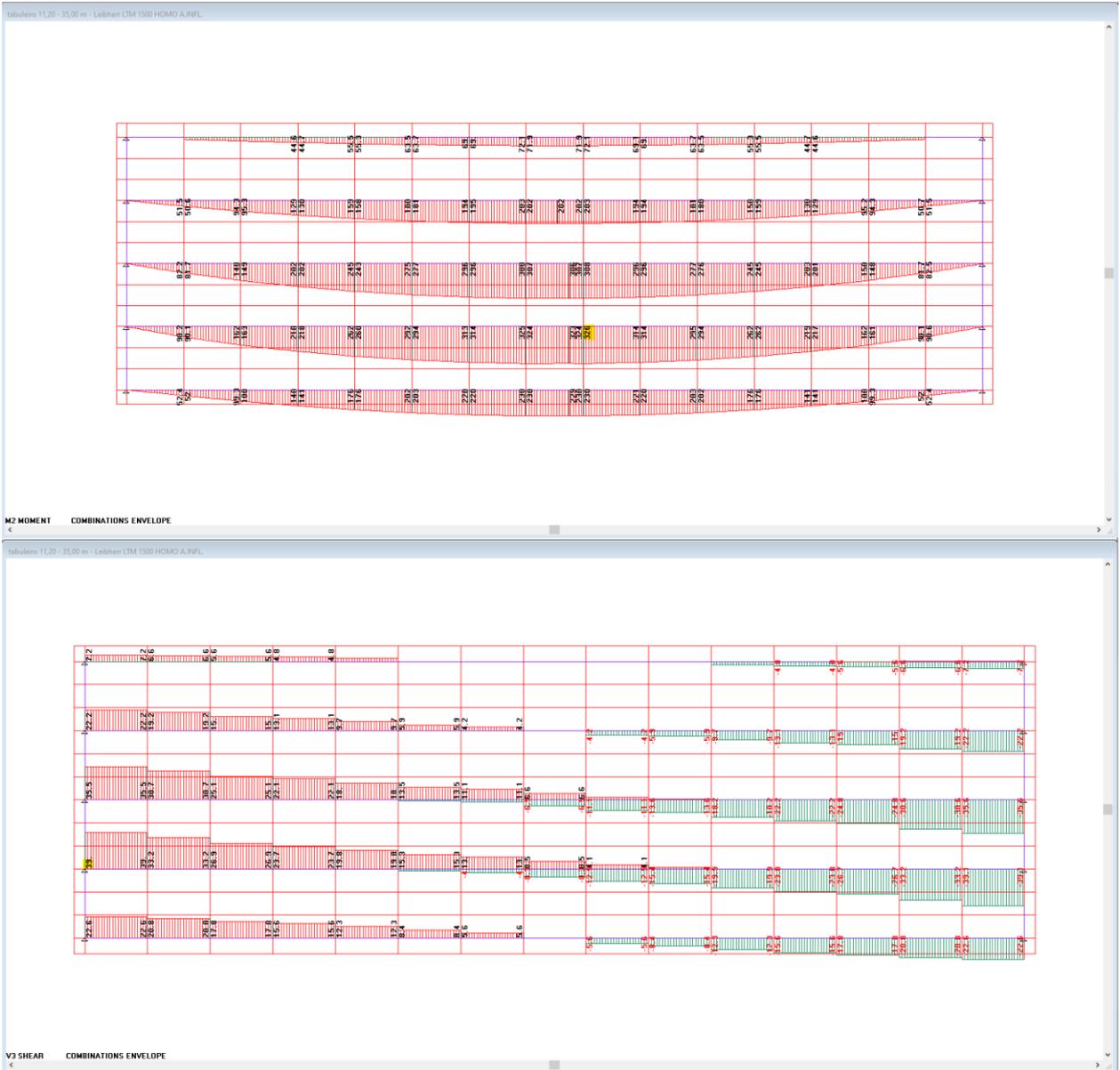


### NOTA TÉCNICA



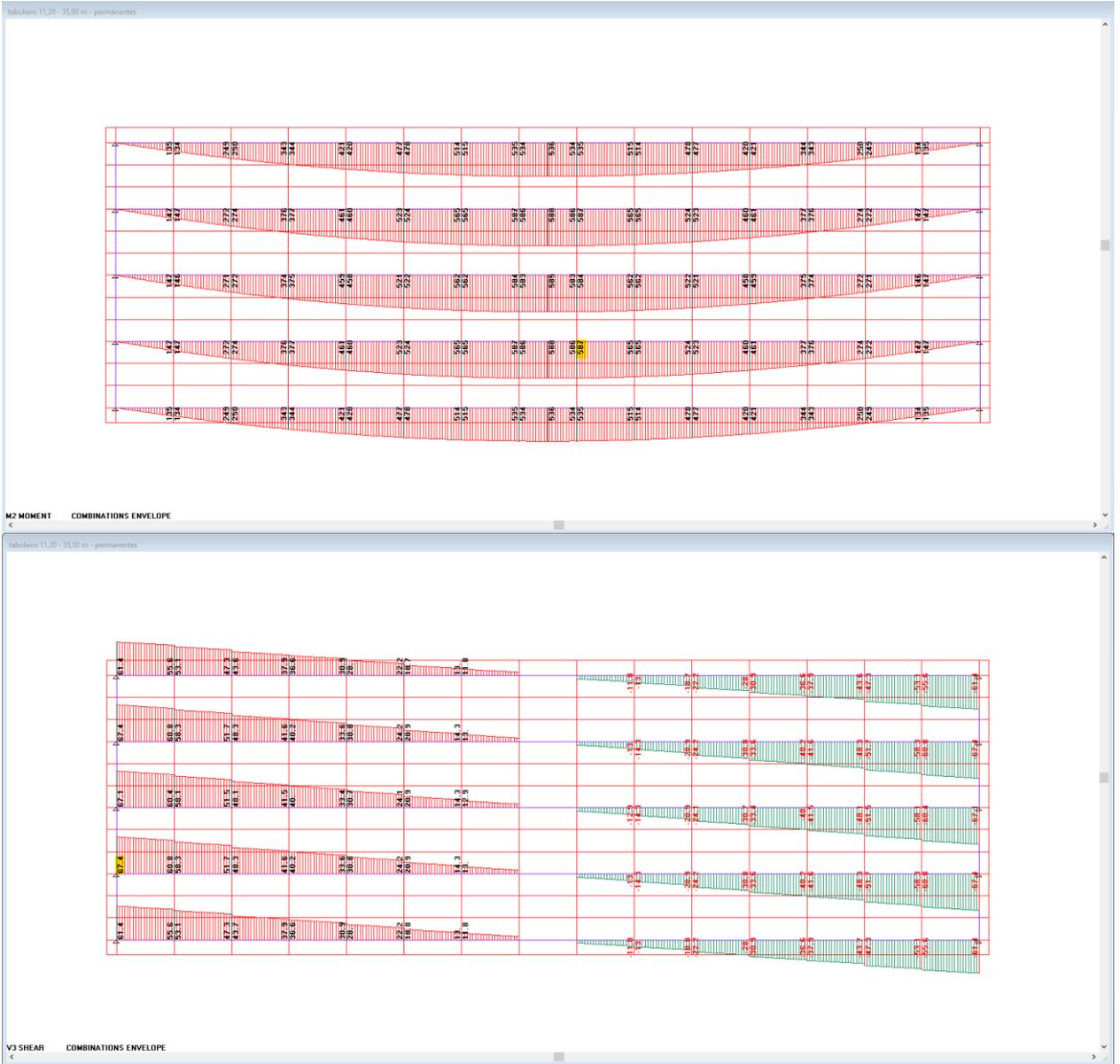


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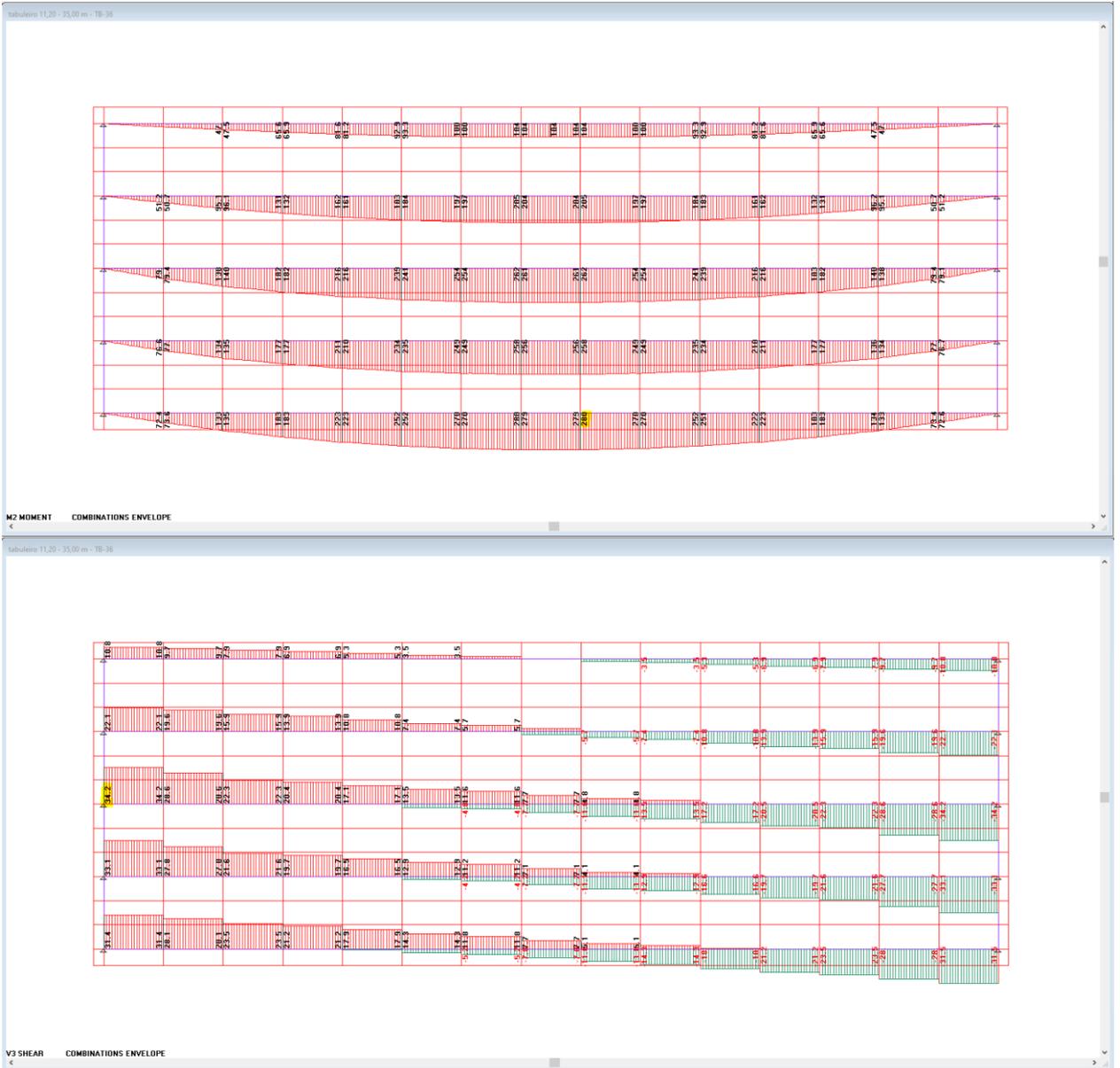


### NOTA TÉCNICA



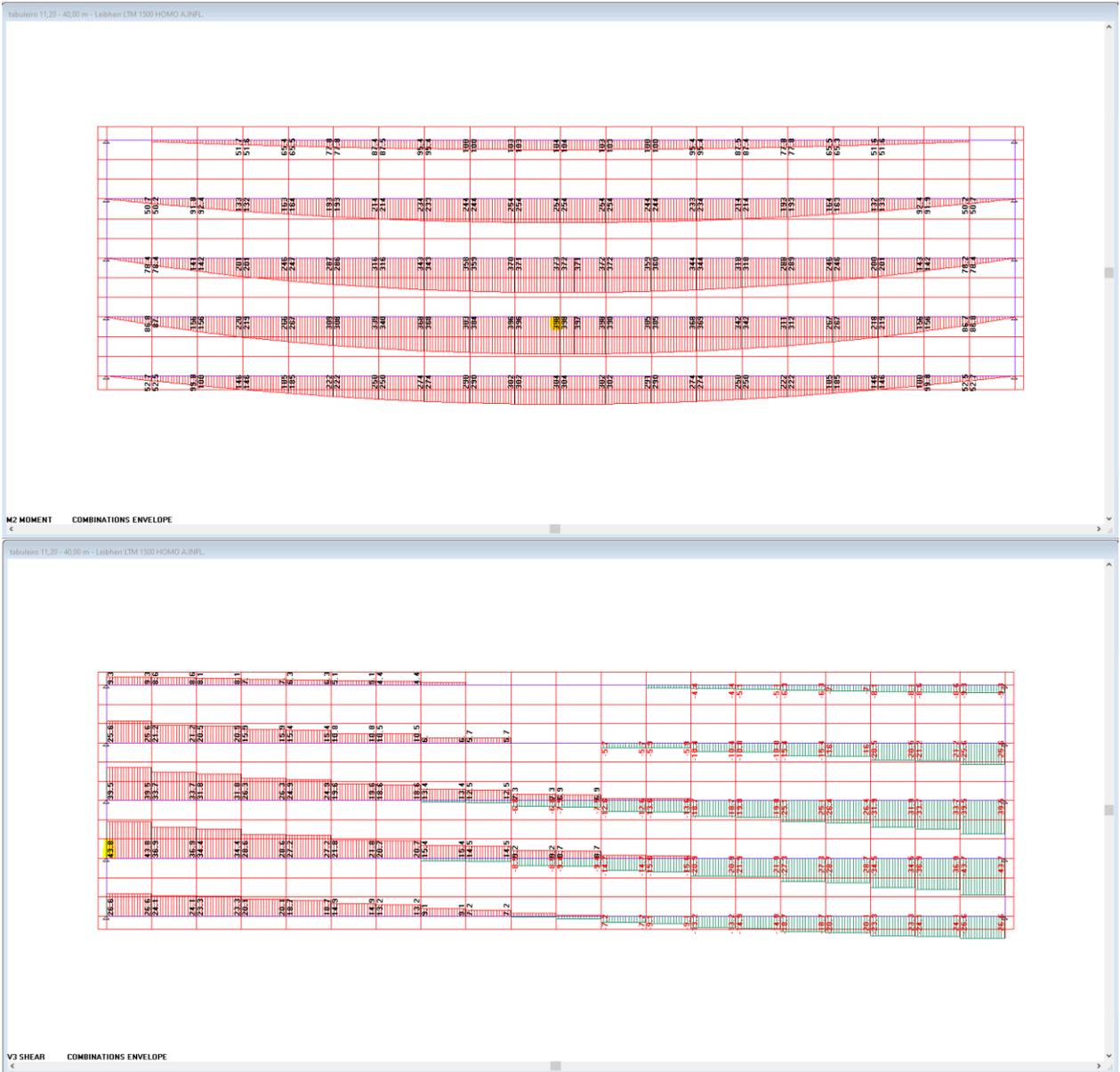


### NOTA TÉCNICA



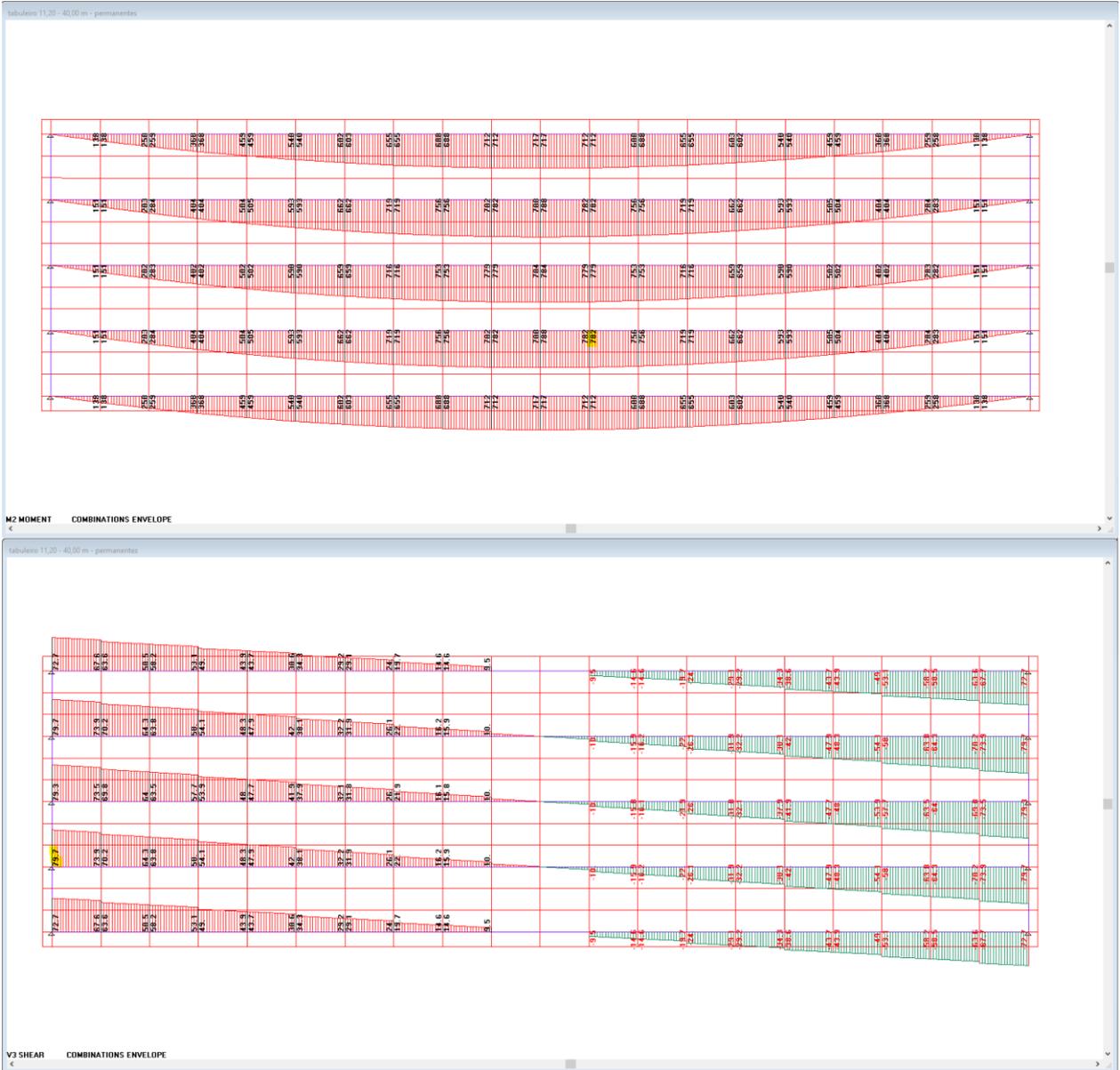


### NOTA TÉCNICA



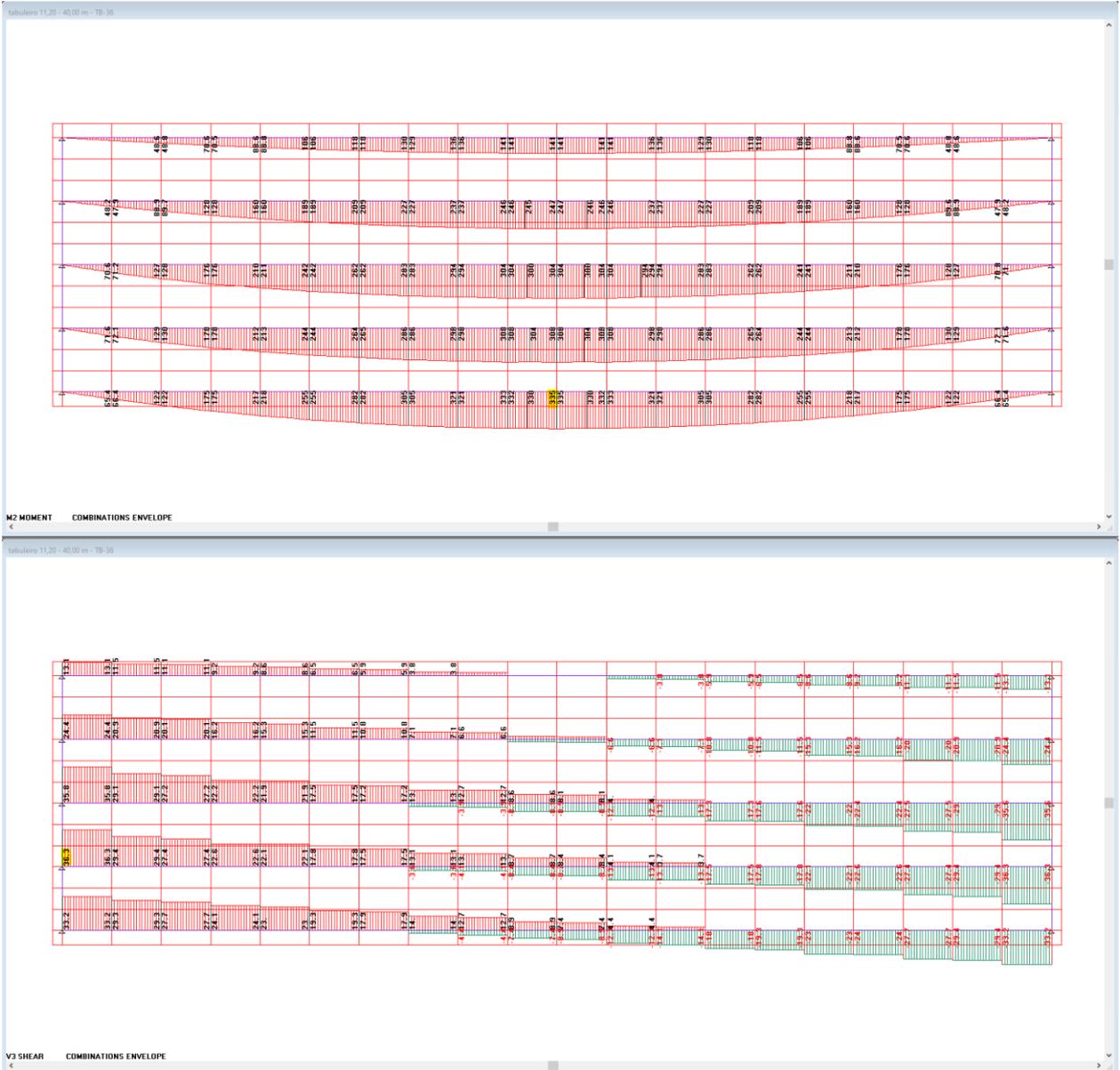


### NOTA TÉCNICA





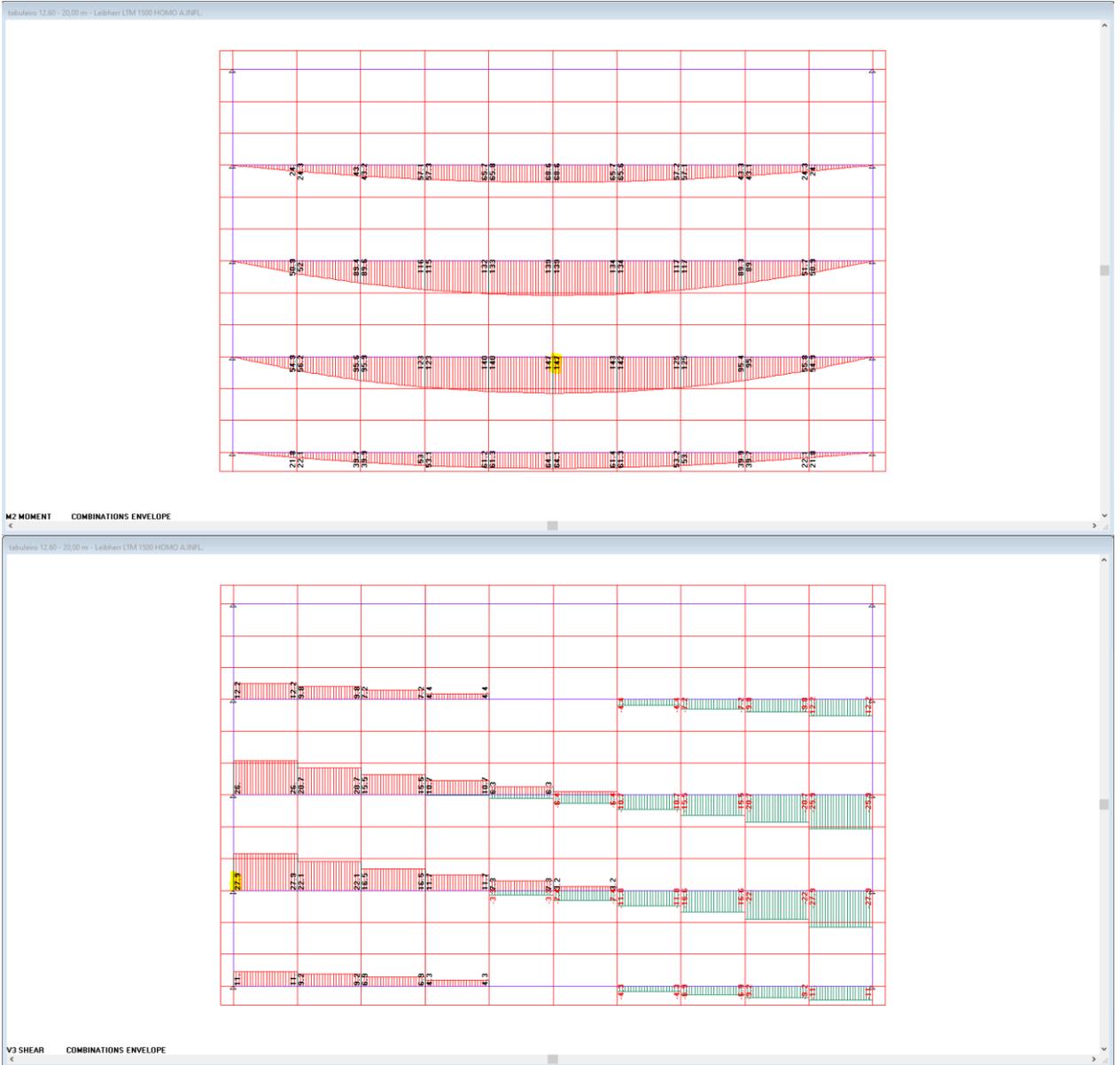
### NOTA TÉCNICA





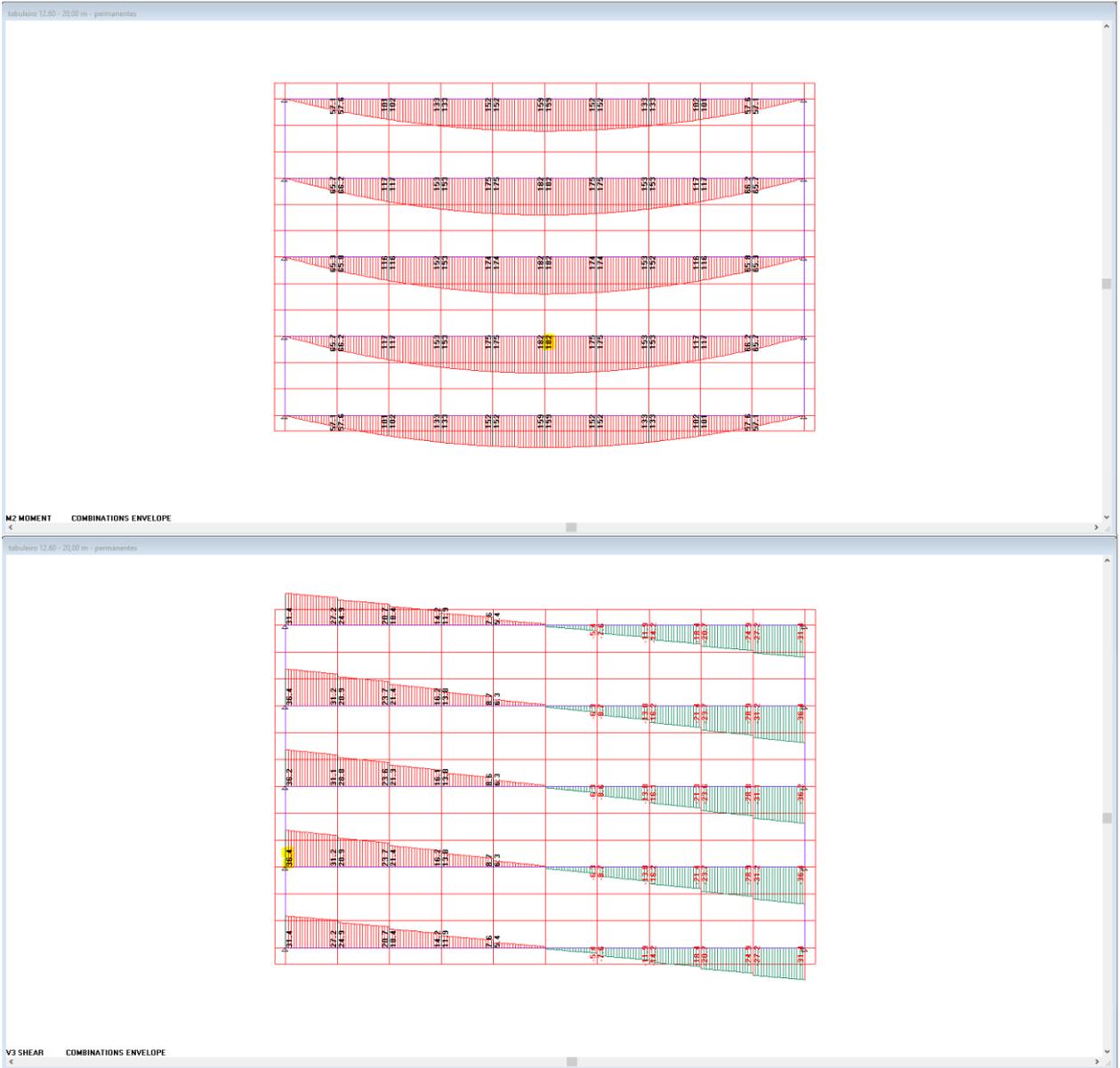
### NOTA TÉCNICA

#### 4.6.2. Tabuleiro 12,60 m



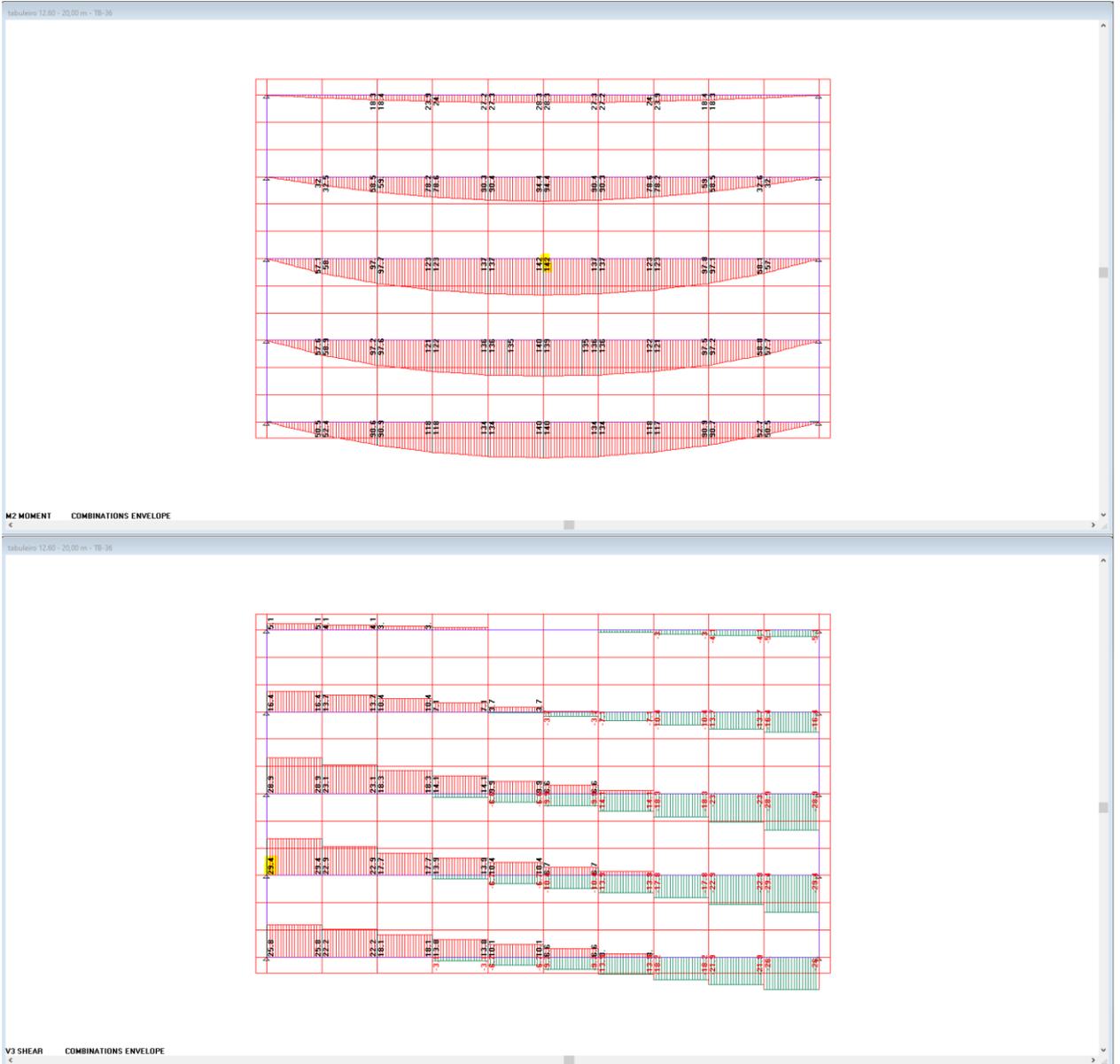


### NOTA TÉCNICA



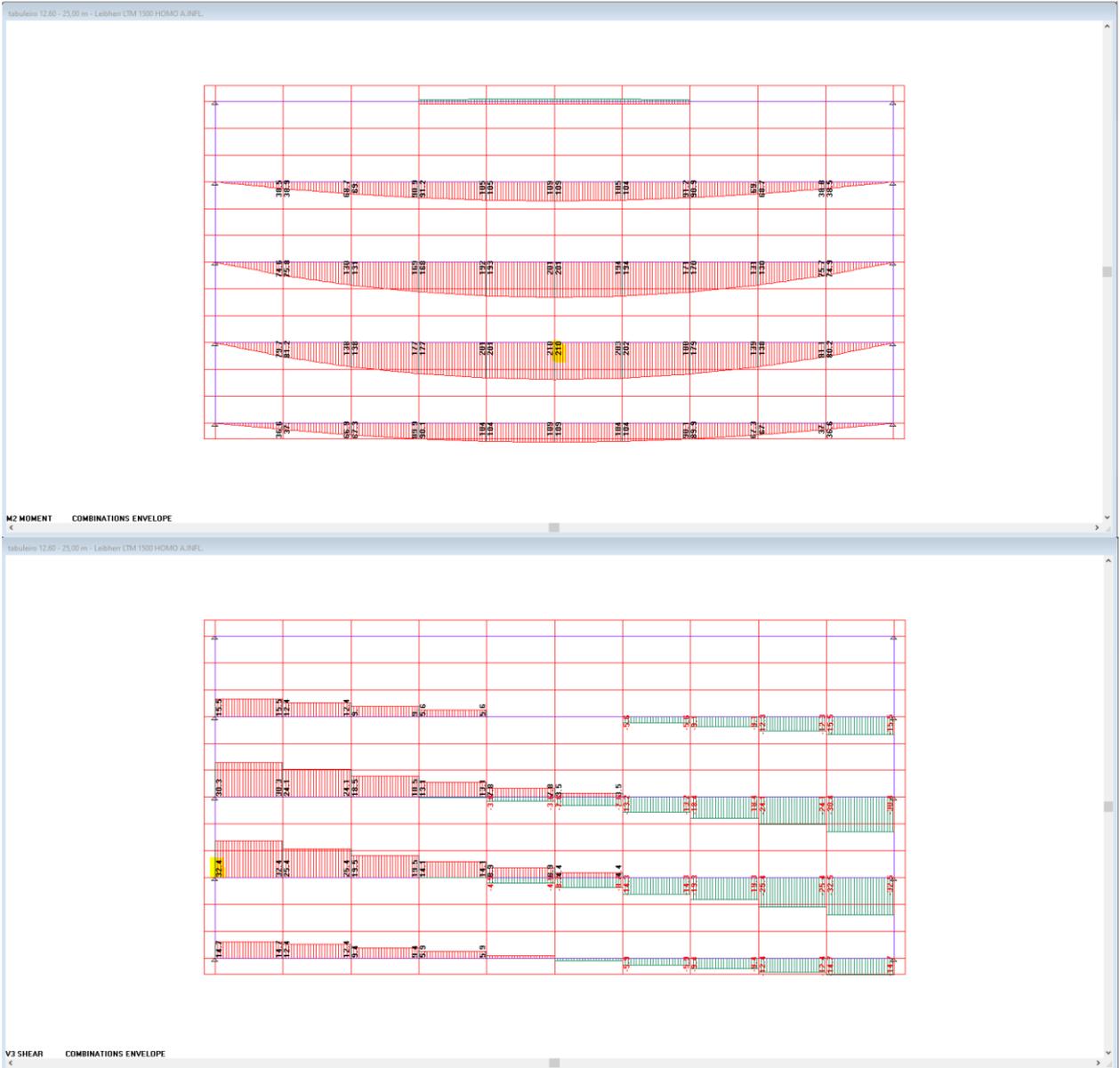


### NOTA TÉCNICA



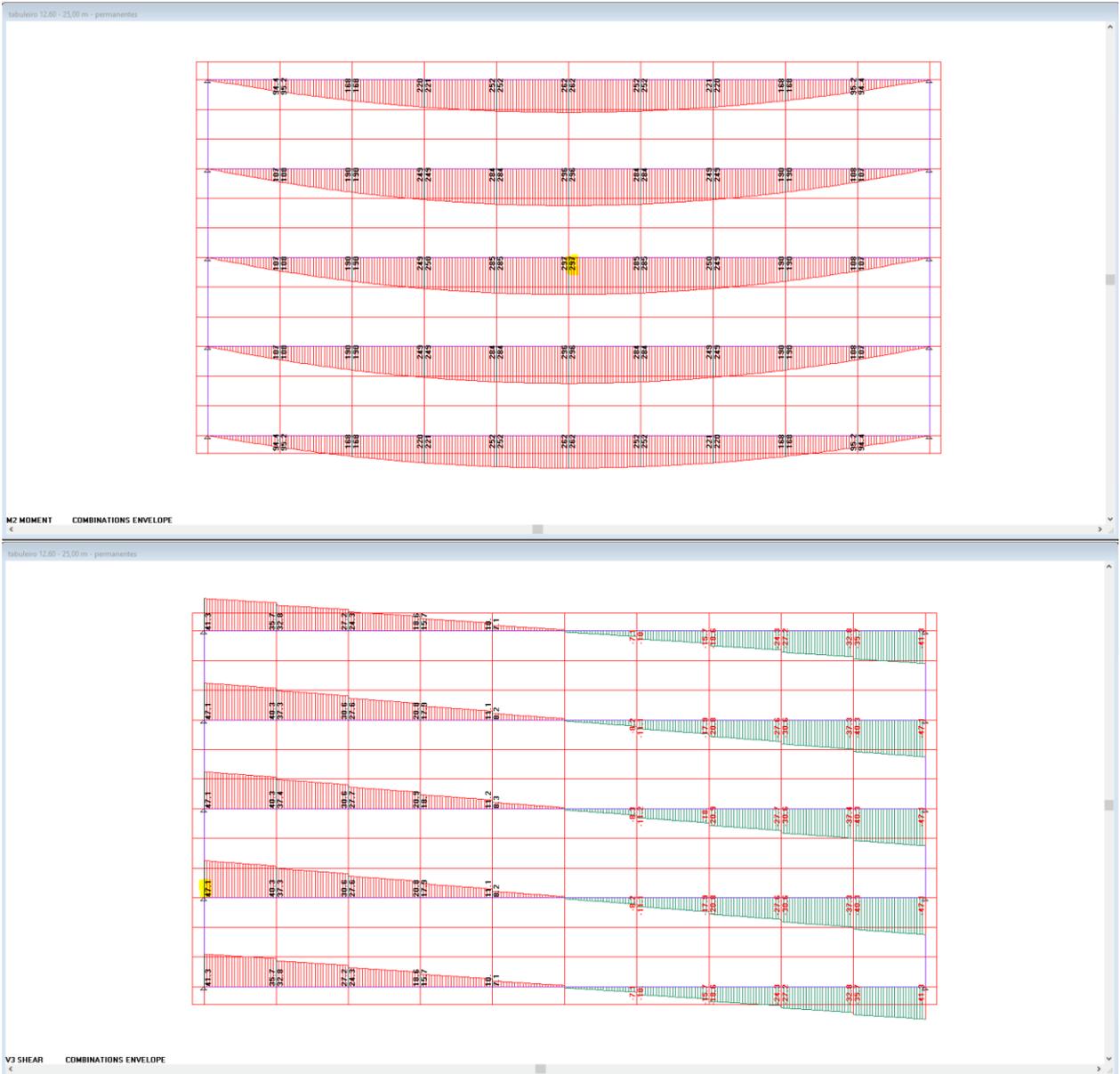


### NOTA TÉCNICA



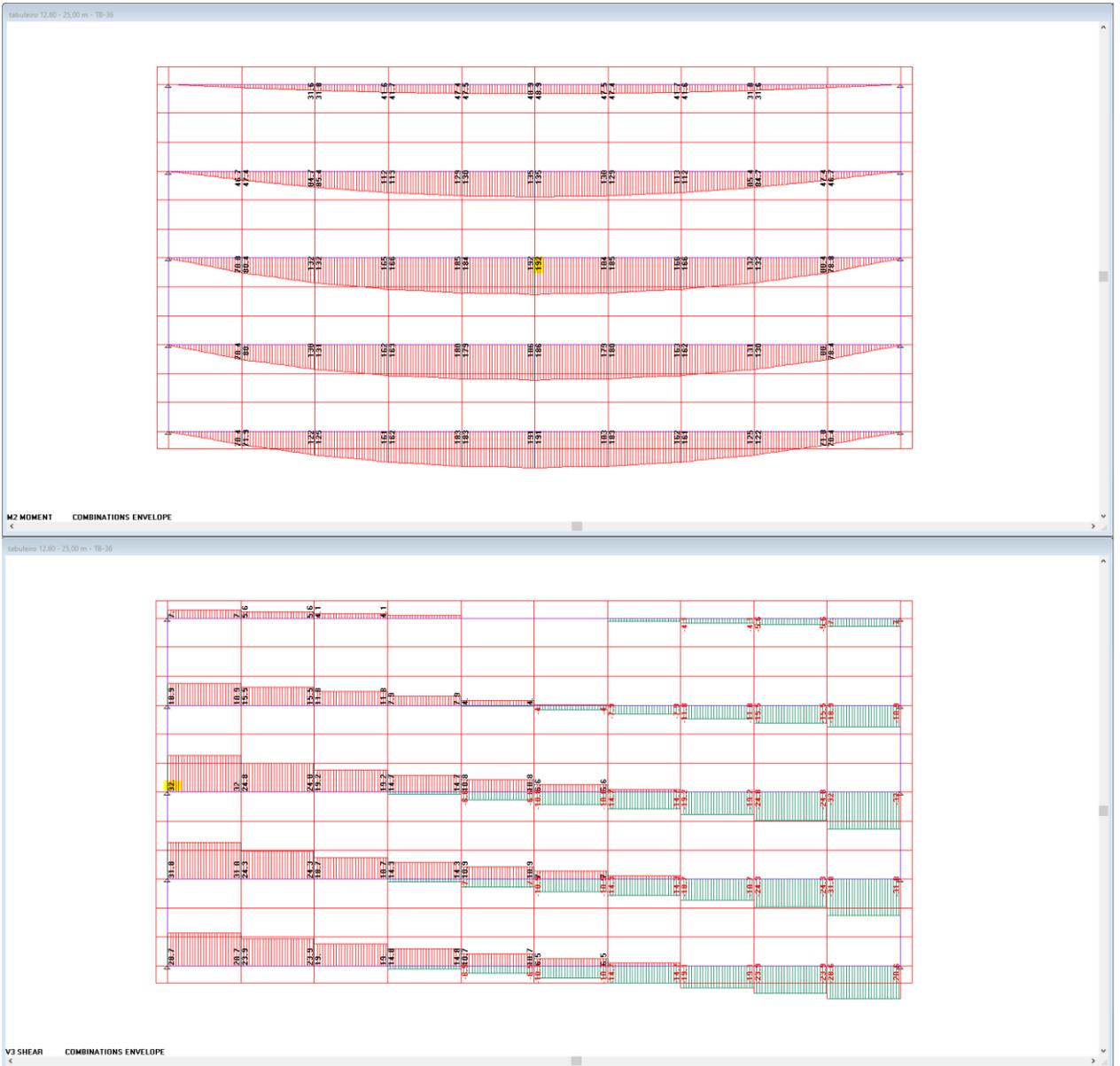


### NOTA TÉCNICA



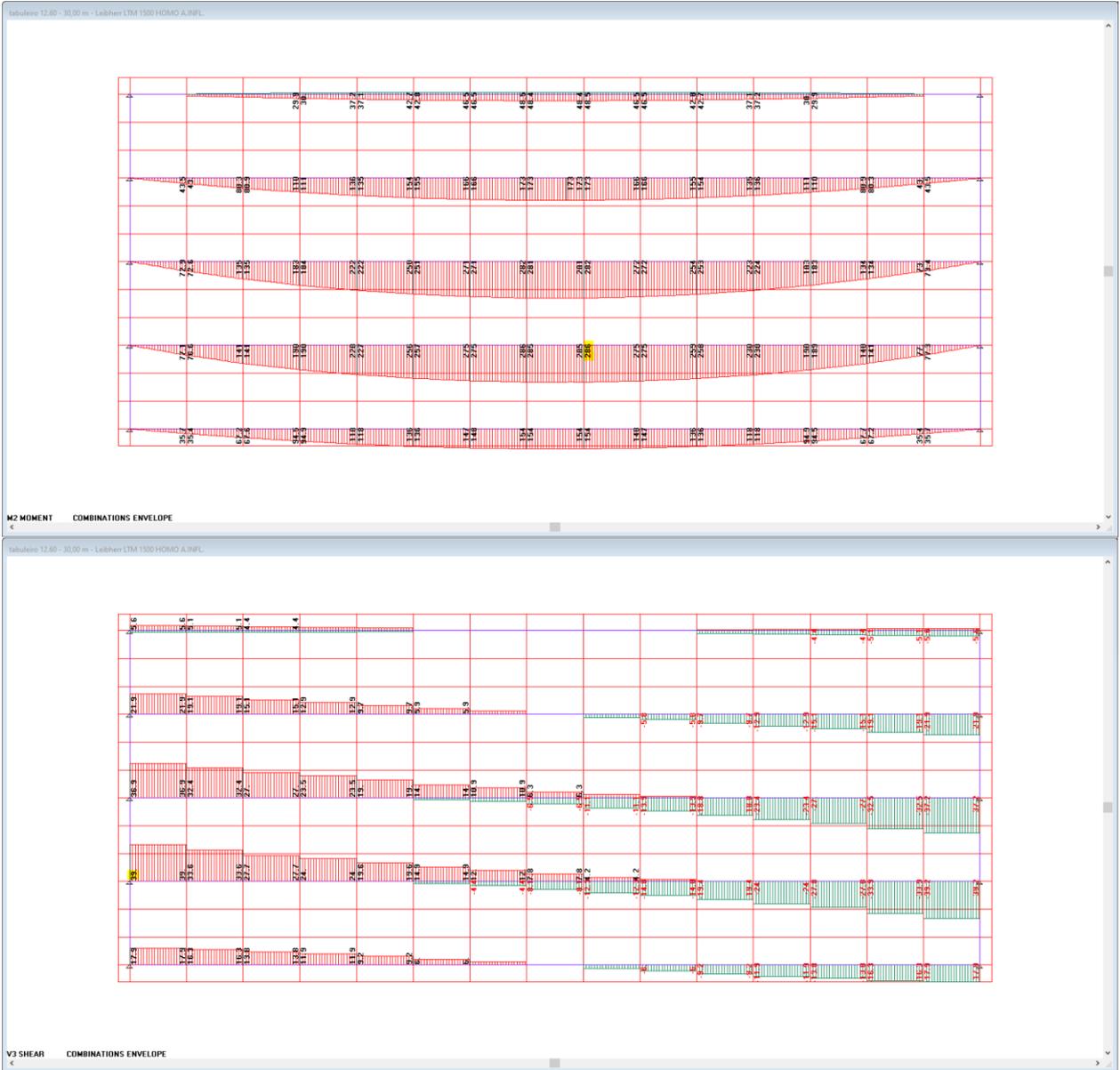


### NOTA TÉCNICA



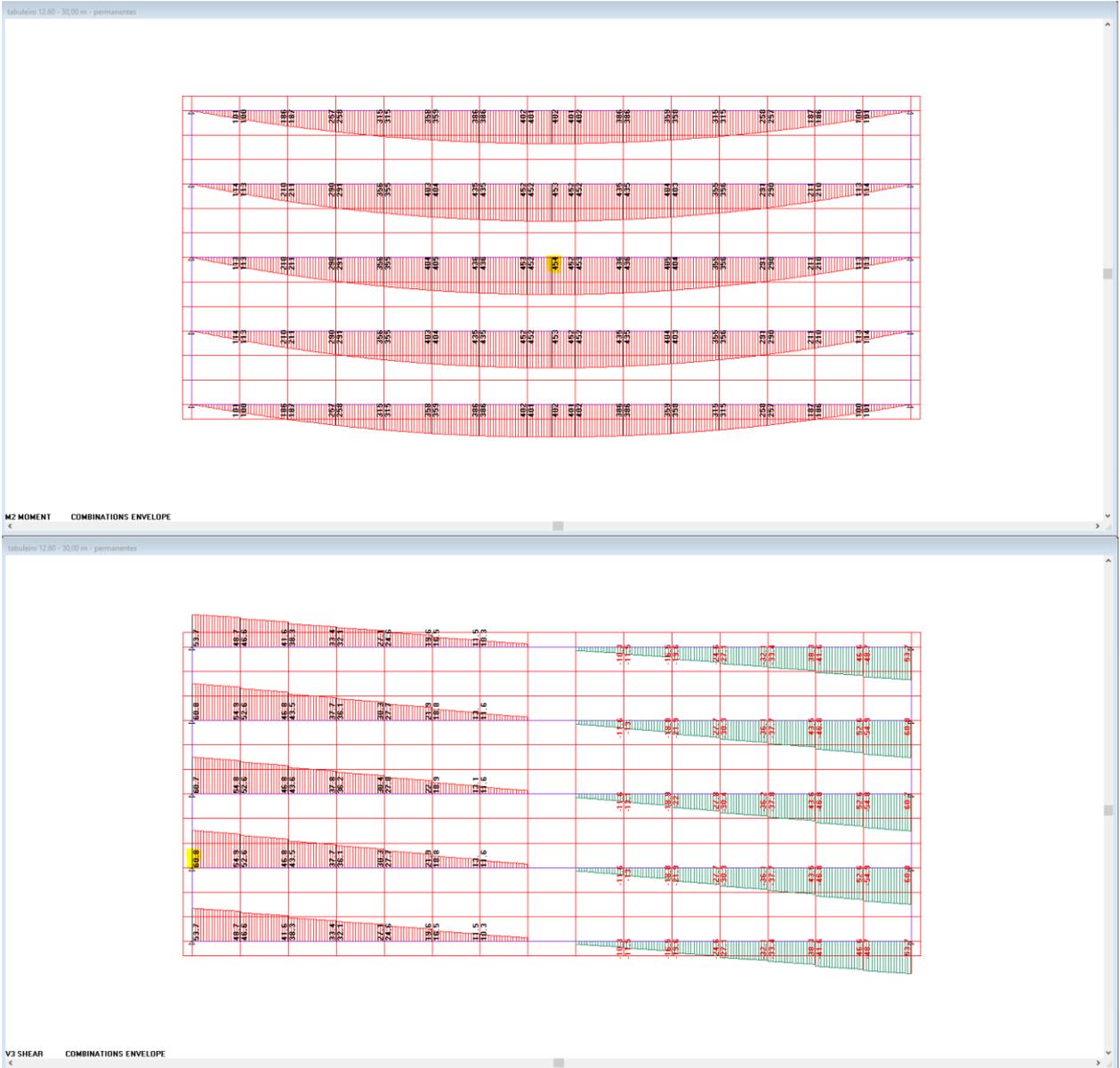


### NOTA TÉCNICA



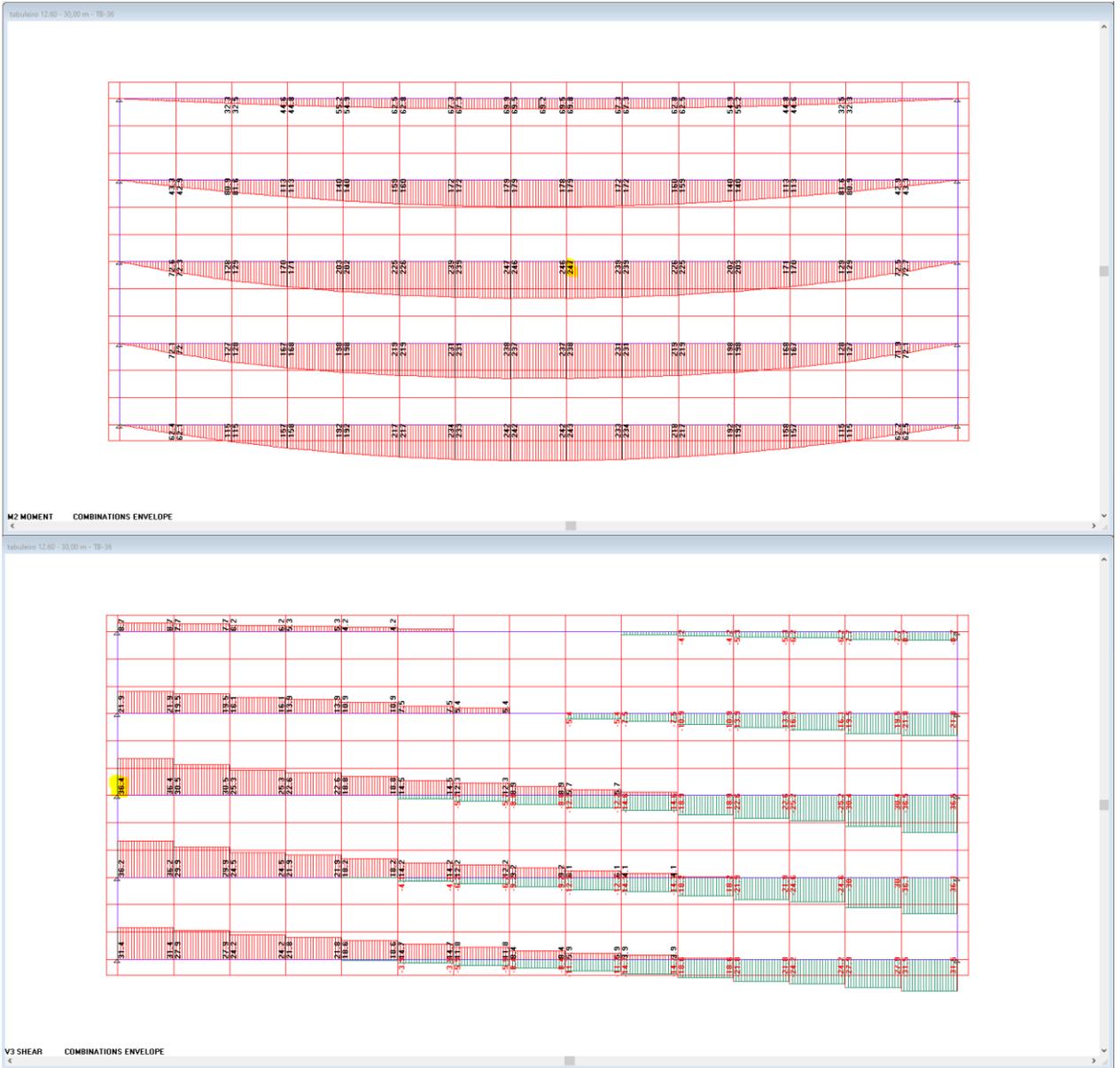


### NOTA TÉCNICA





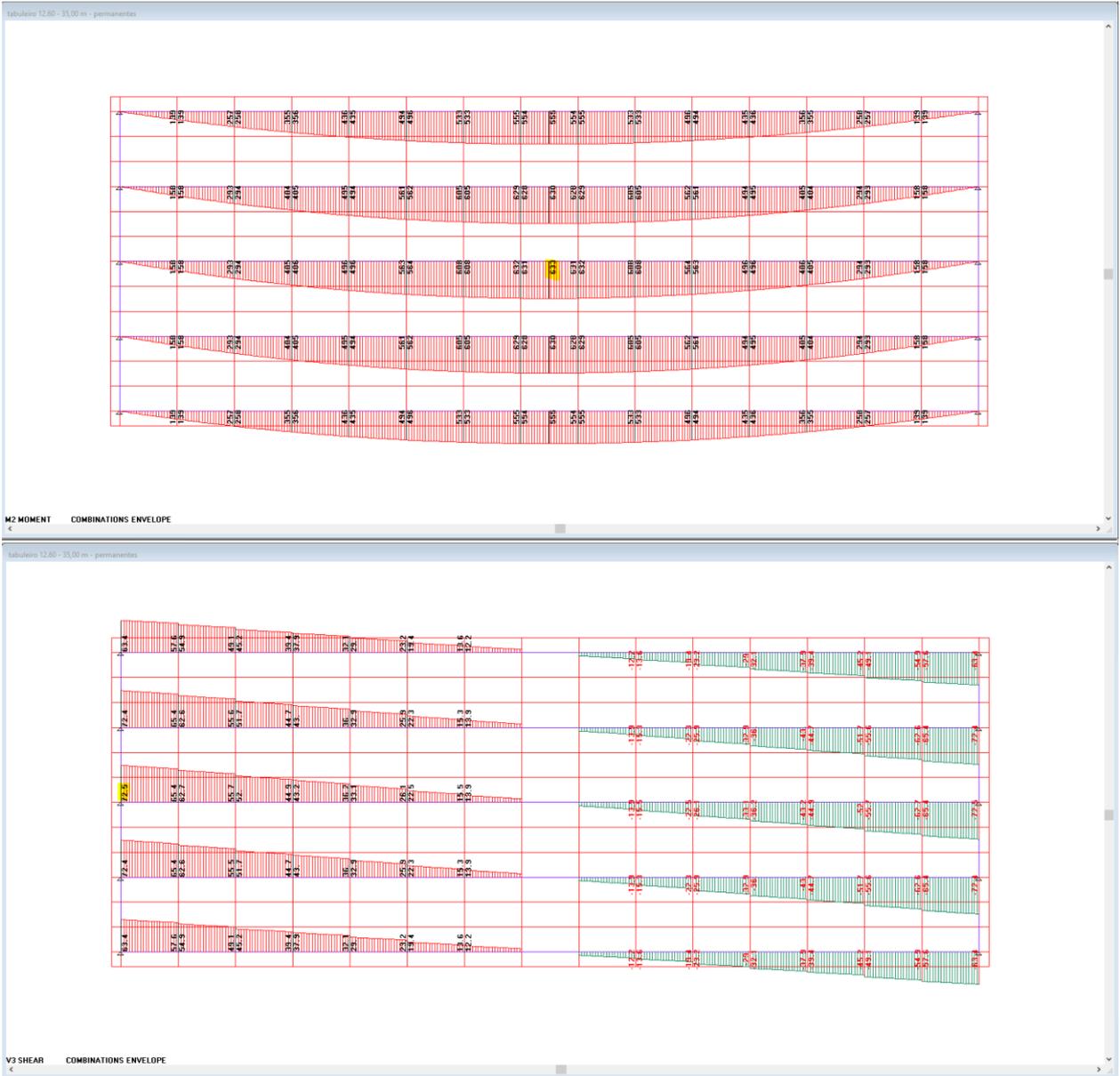
### NOTA TÉCNICA





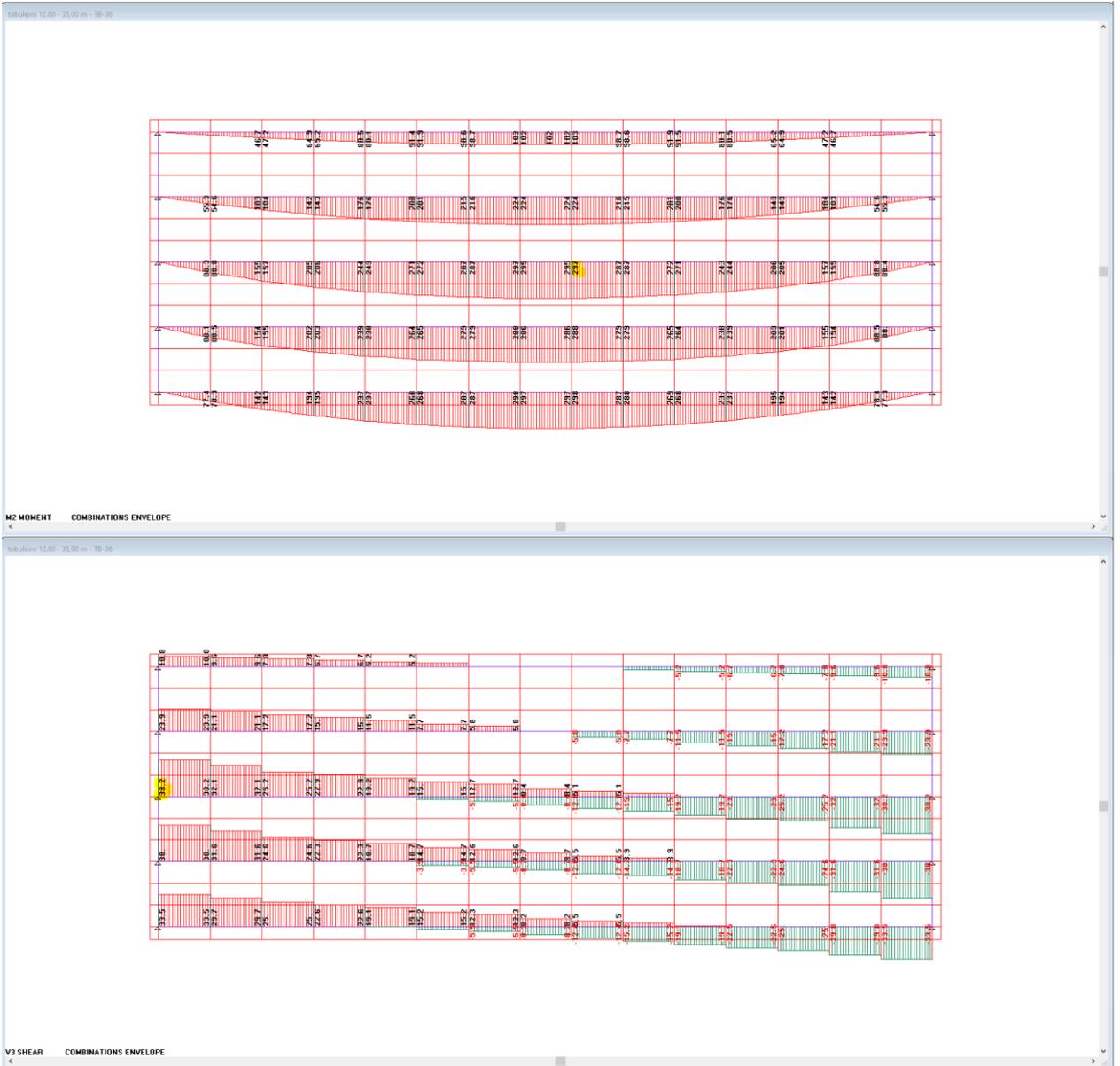


### NOTA TÉCNICA



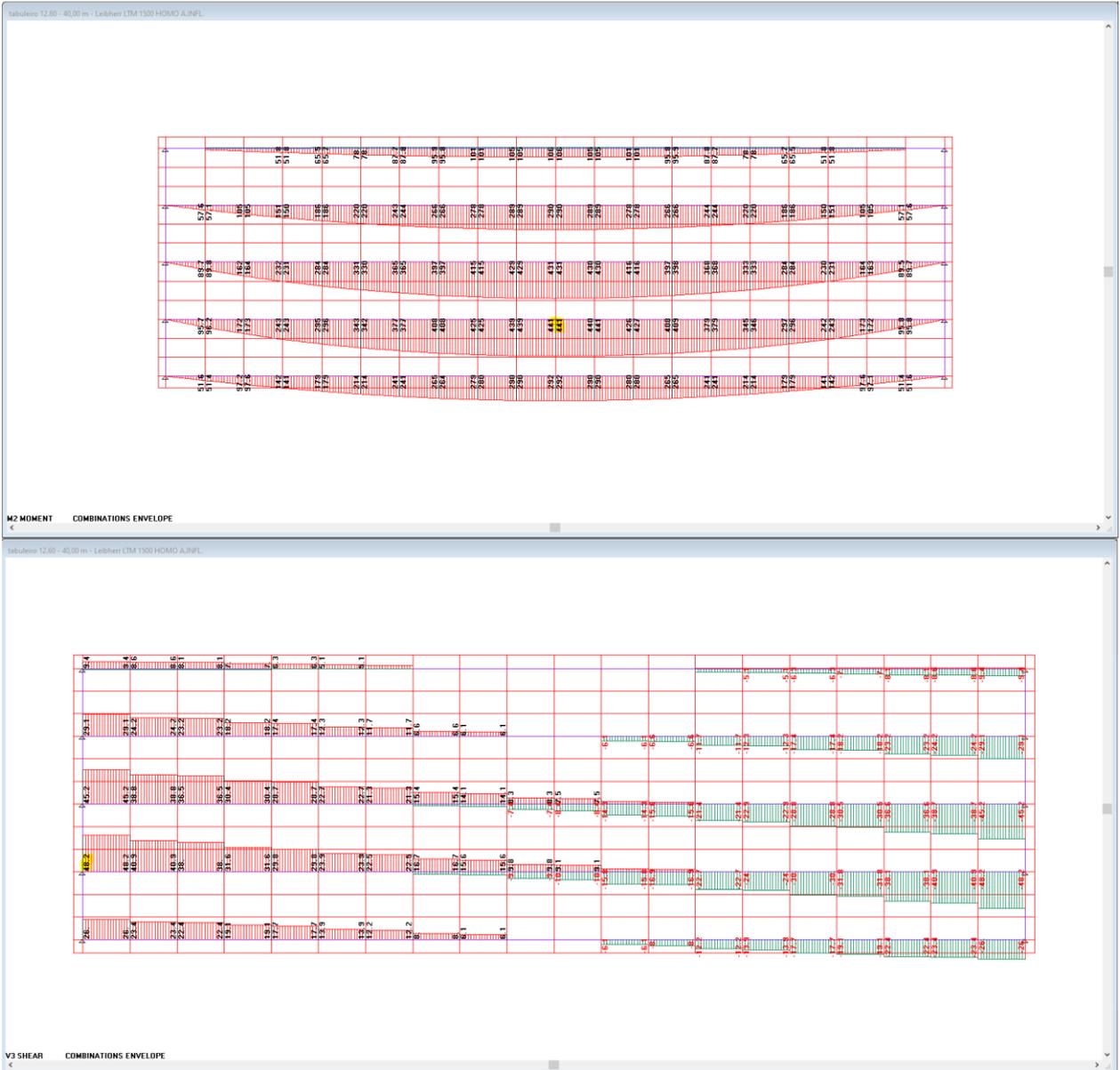


### NOTA TÉCNICA



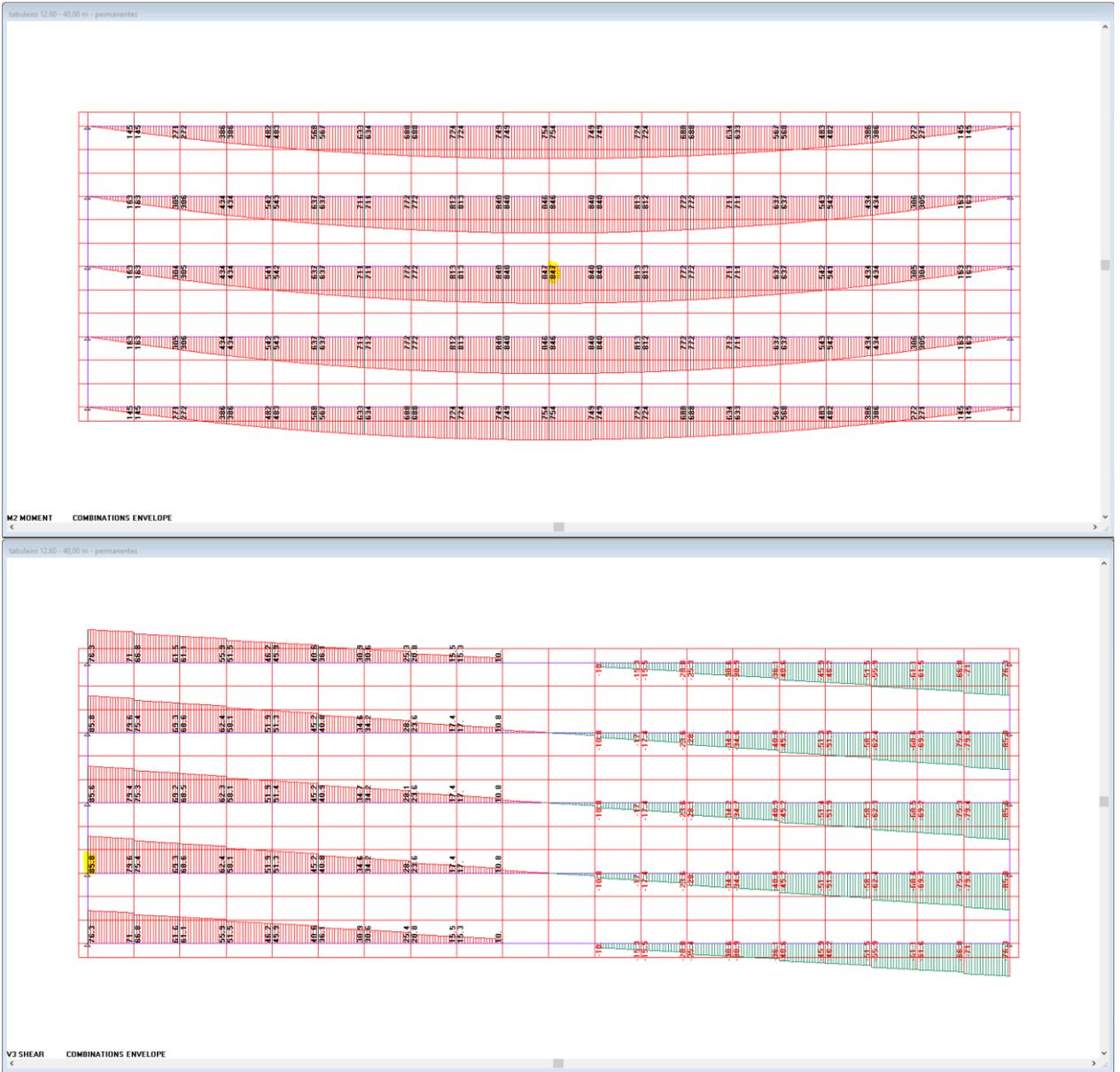


### NOTA TÉCNICA



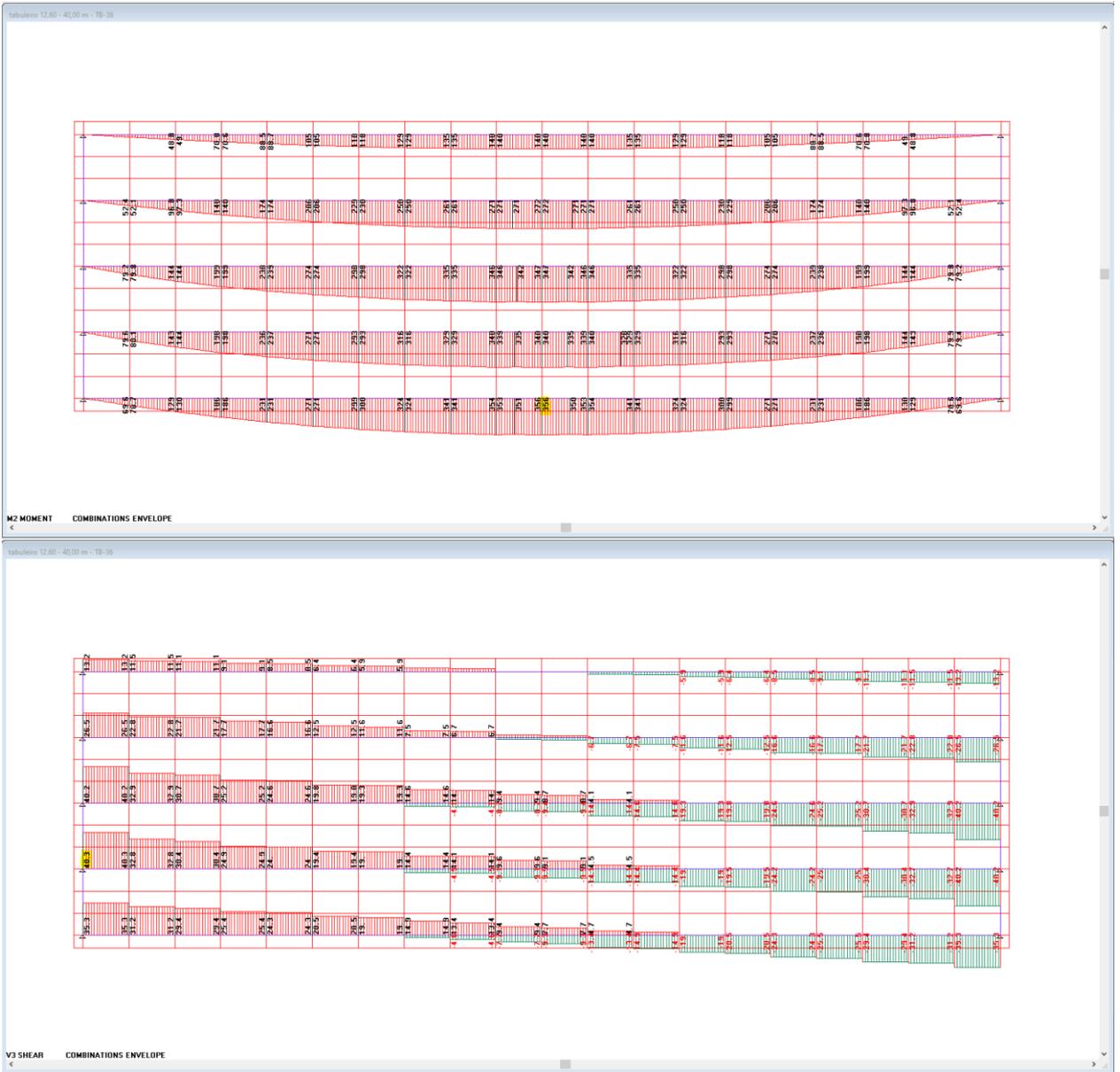


### NOTA TÉCNICA





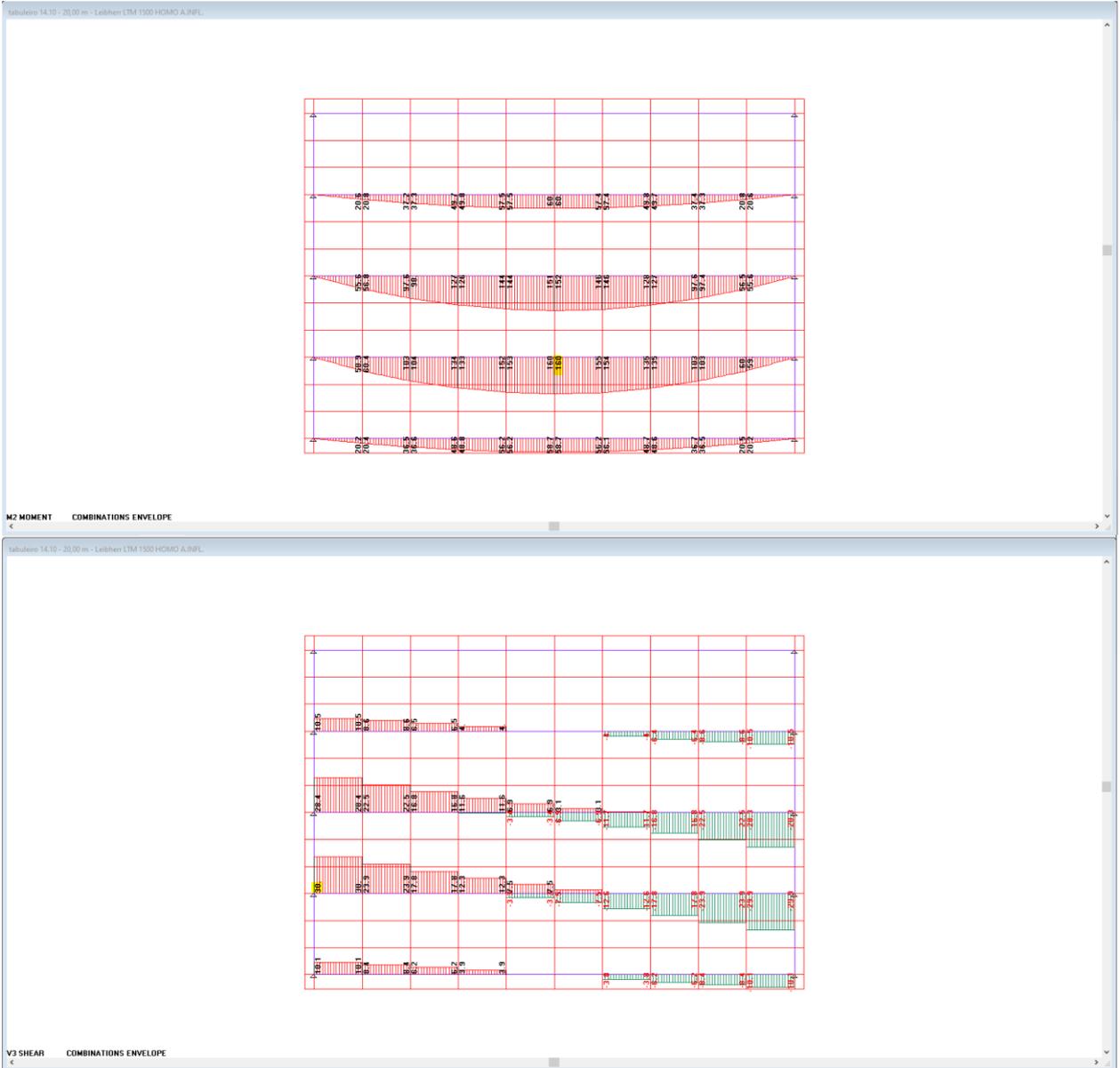
### NOTA TÉCNICA





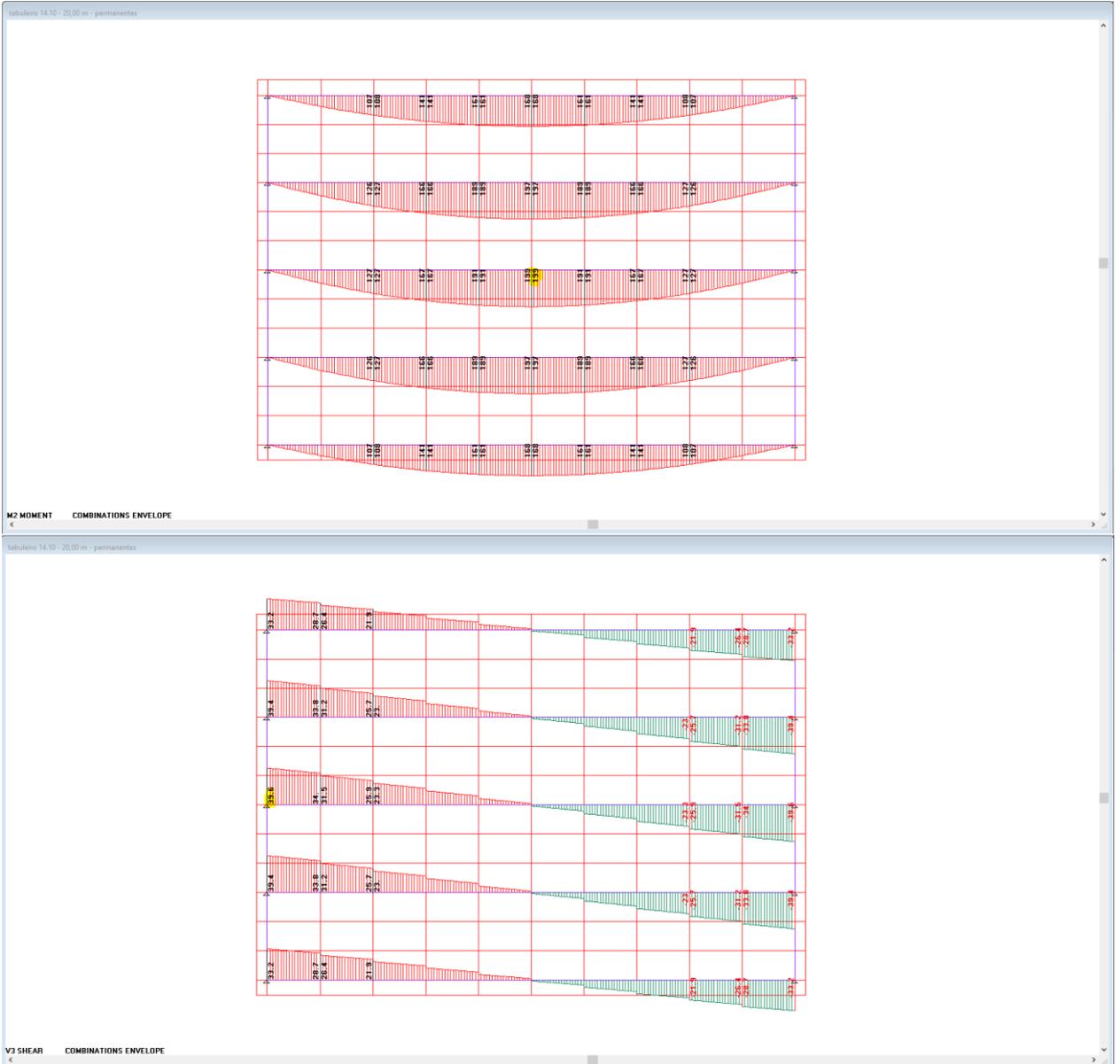
### NOTA TÉCNICA

#### 4.6.3. Tabuleiro 14,10 m



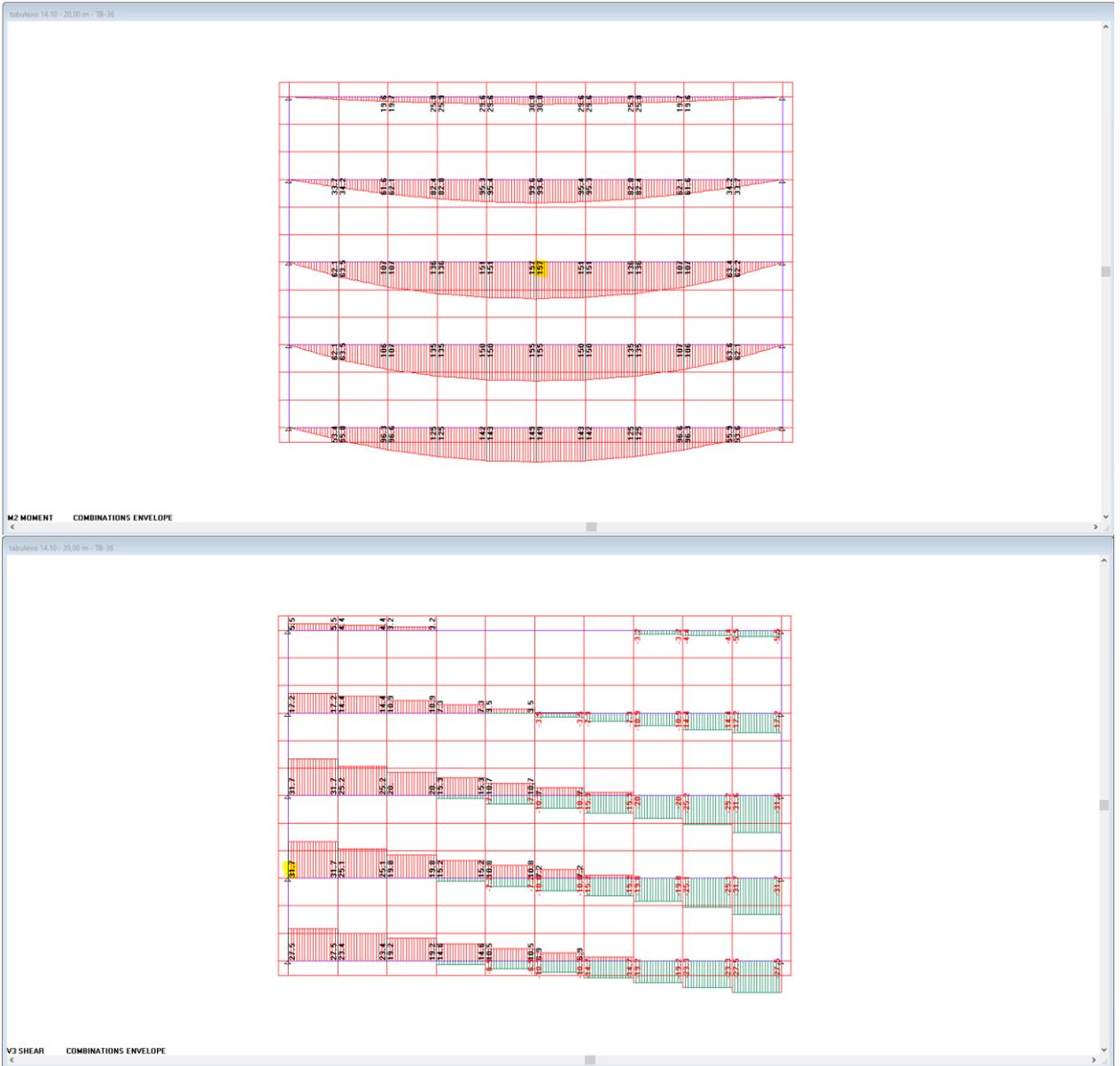


### NOTA TÉCNICA



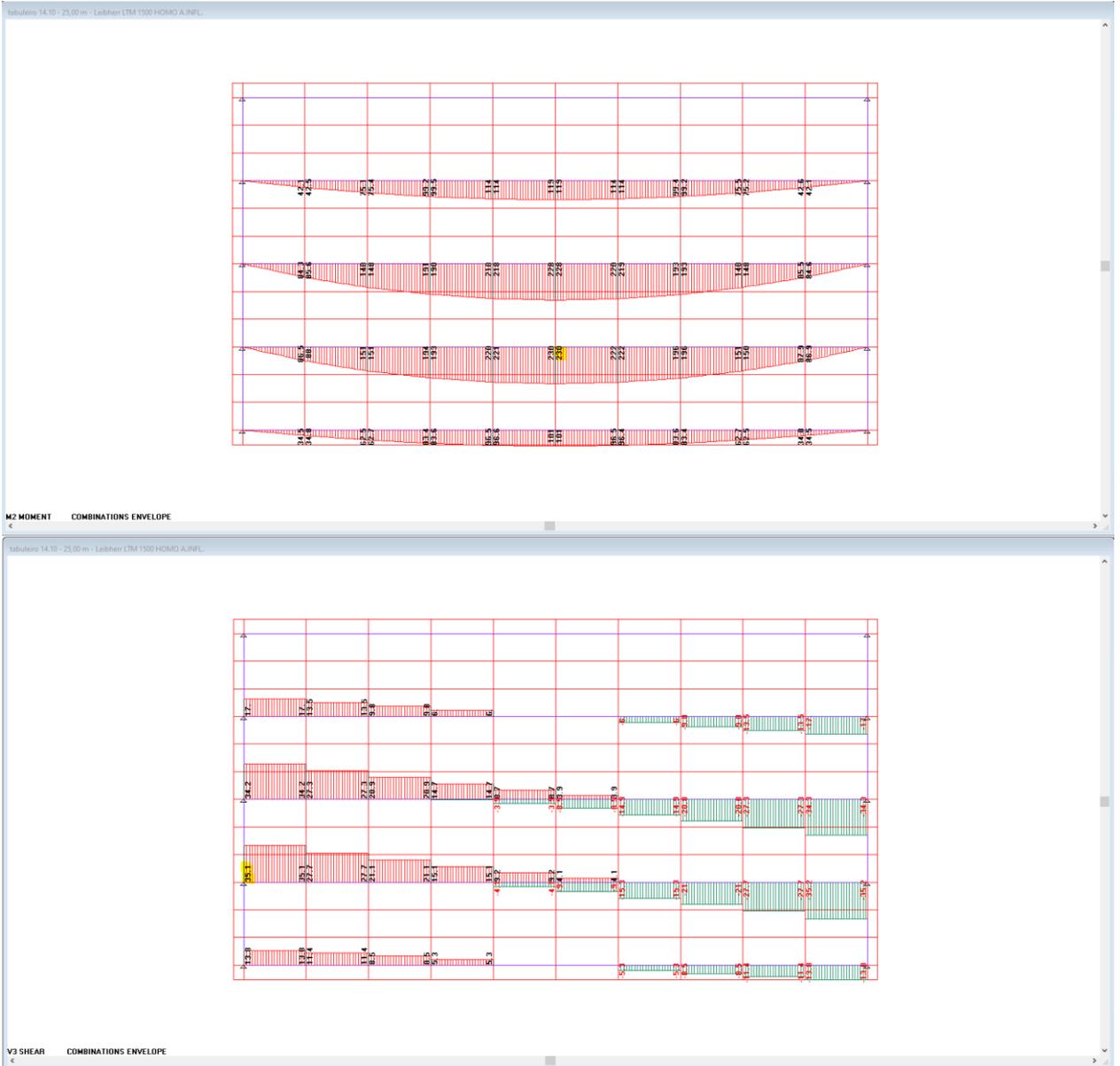


### NOTA TÉCNICA



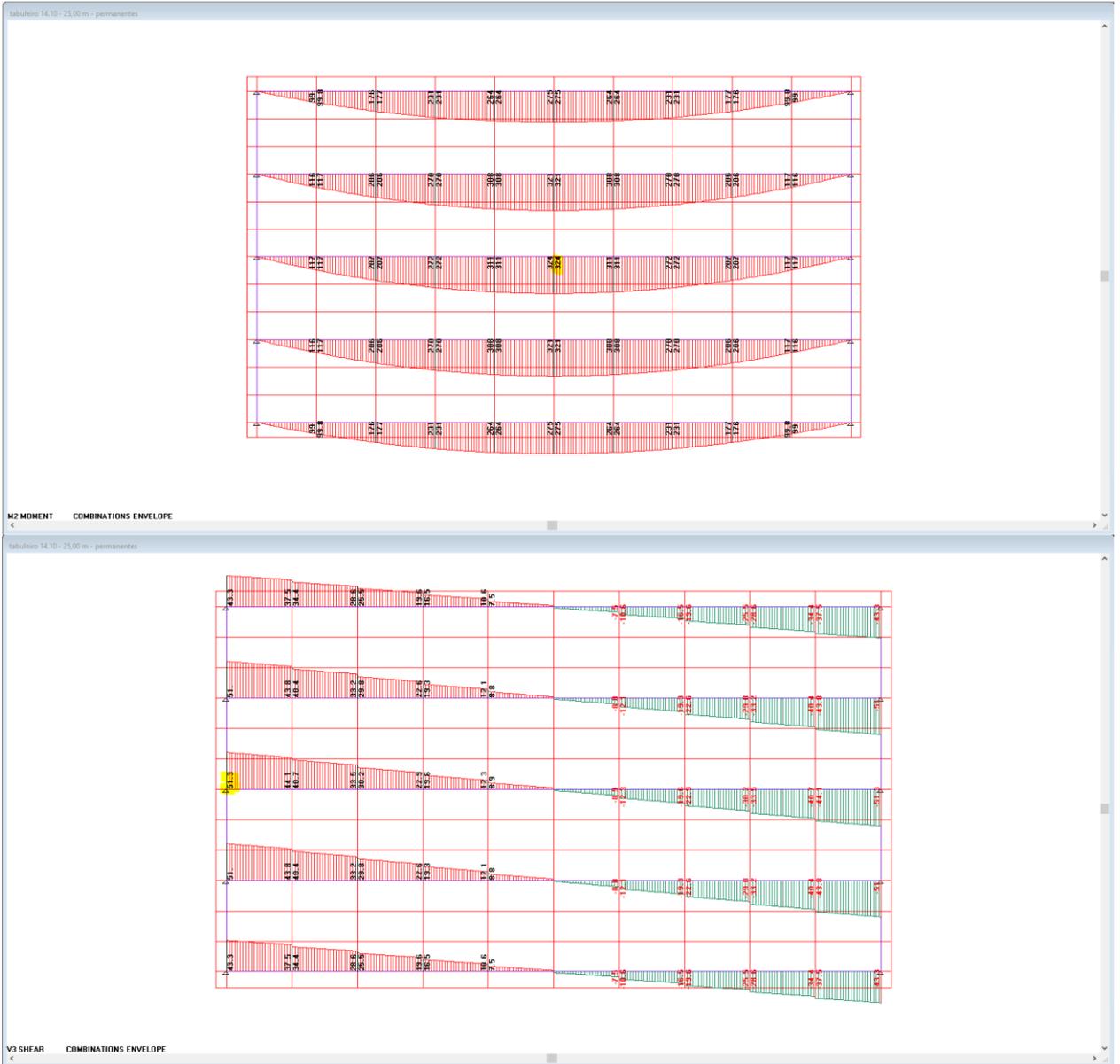


### NOTA TÉCNICA



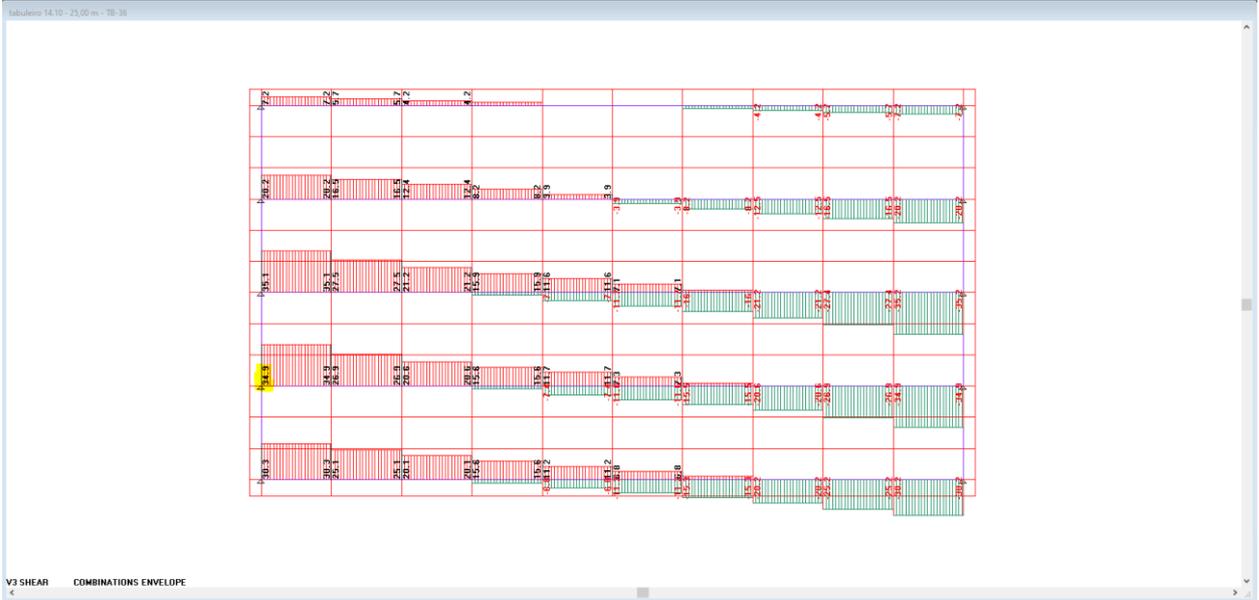
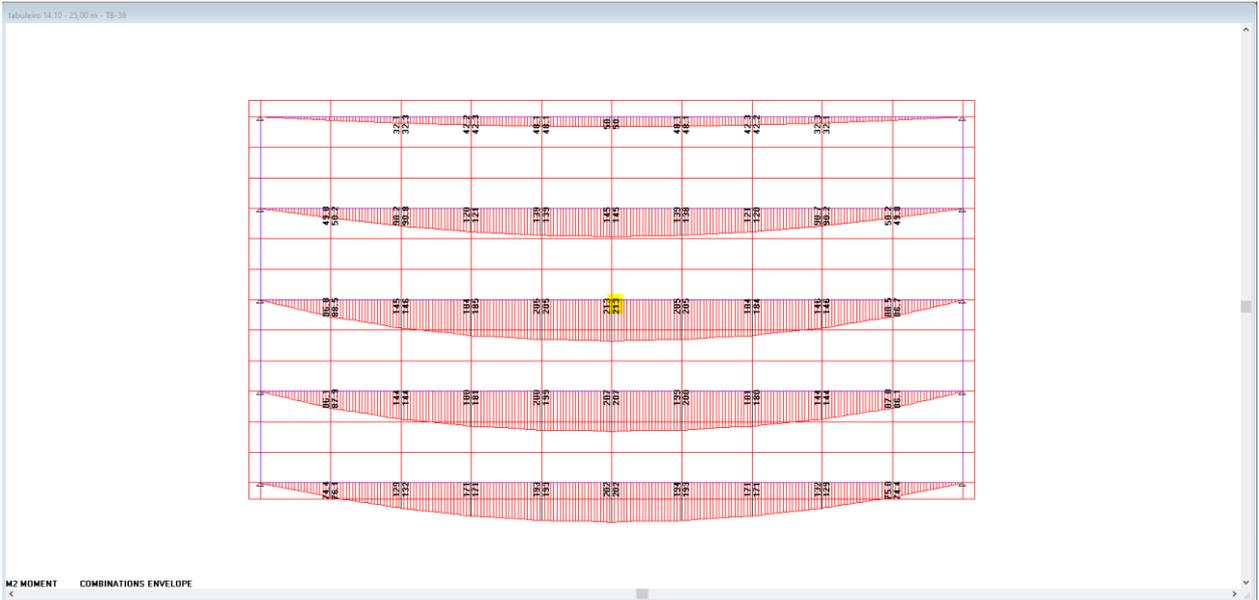


### NOTA TÉCNICA



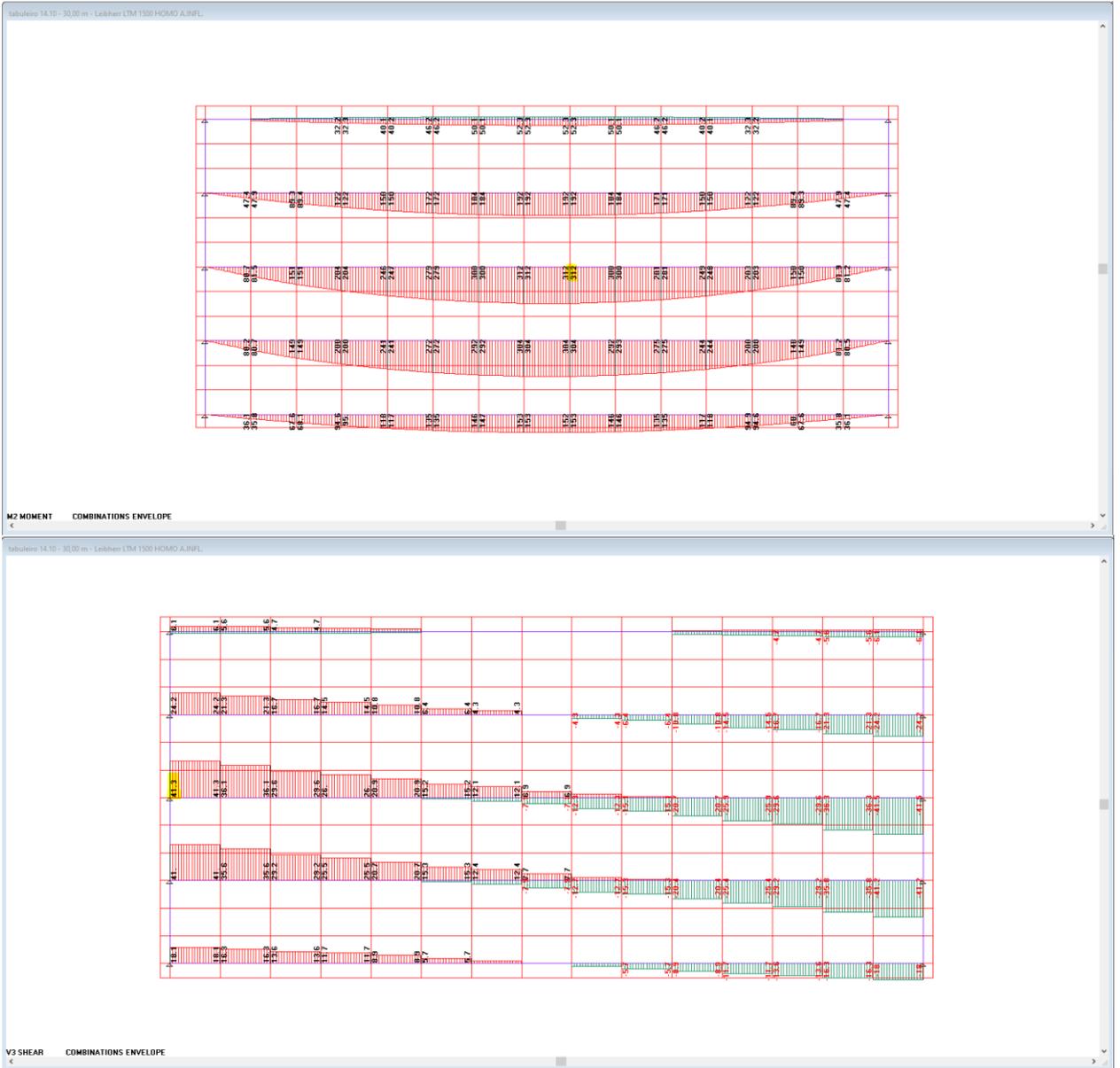


### NOTA TÉCNICA



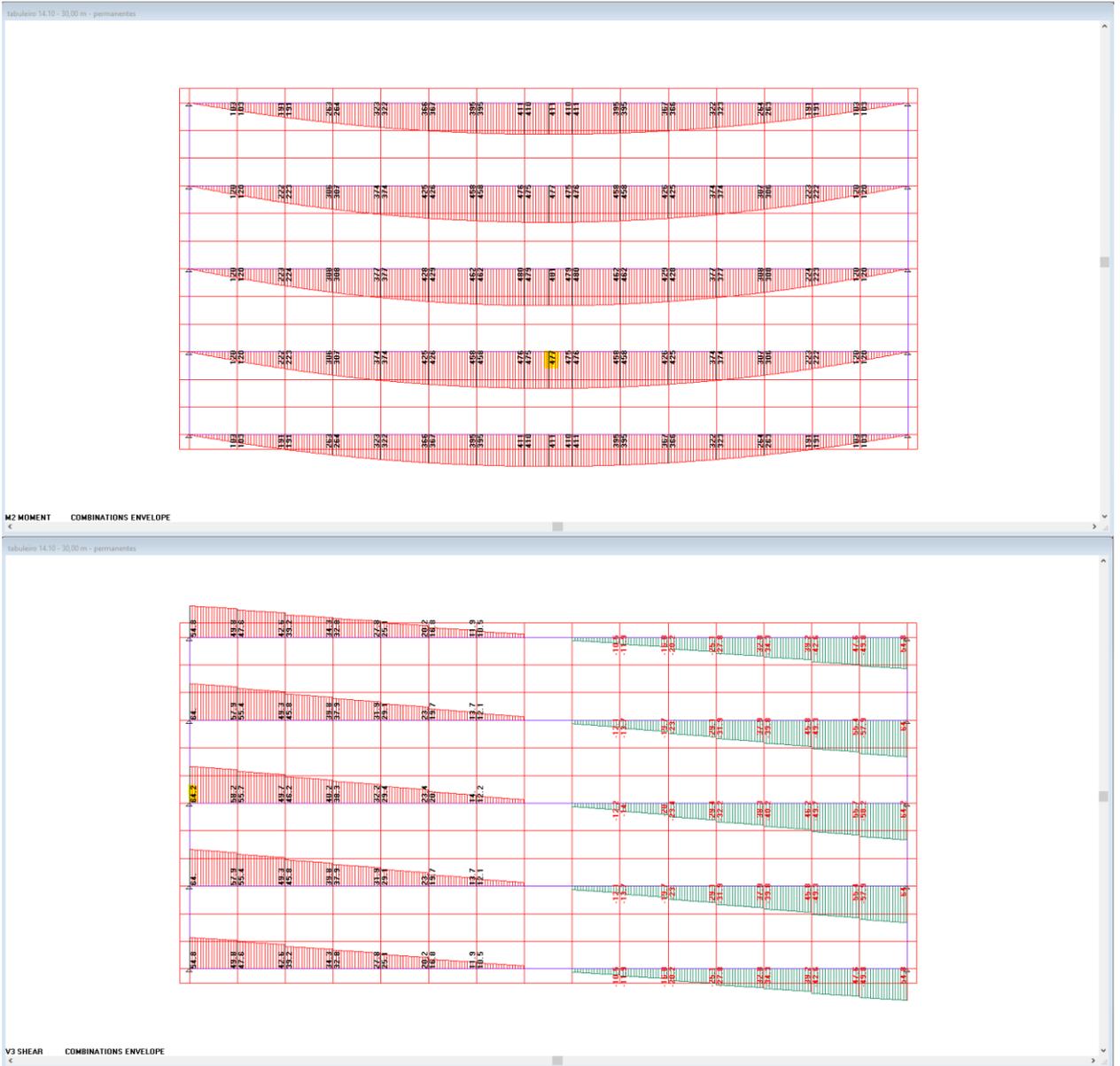


### NOTA TÉCNICA



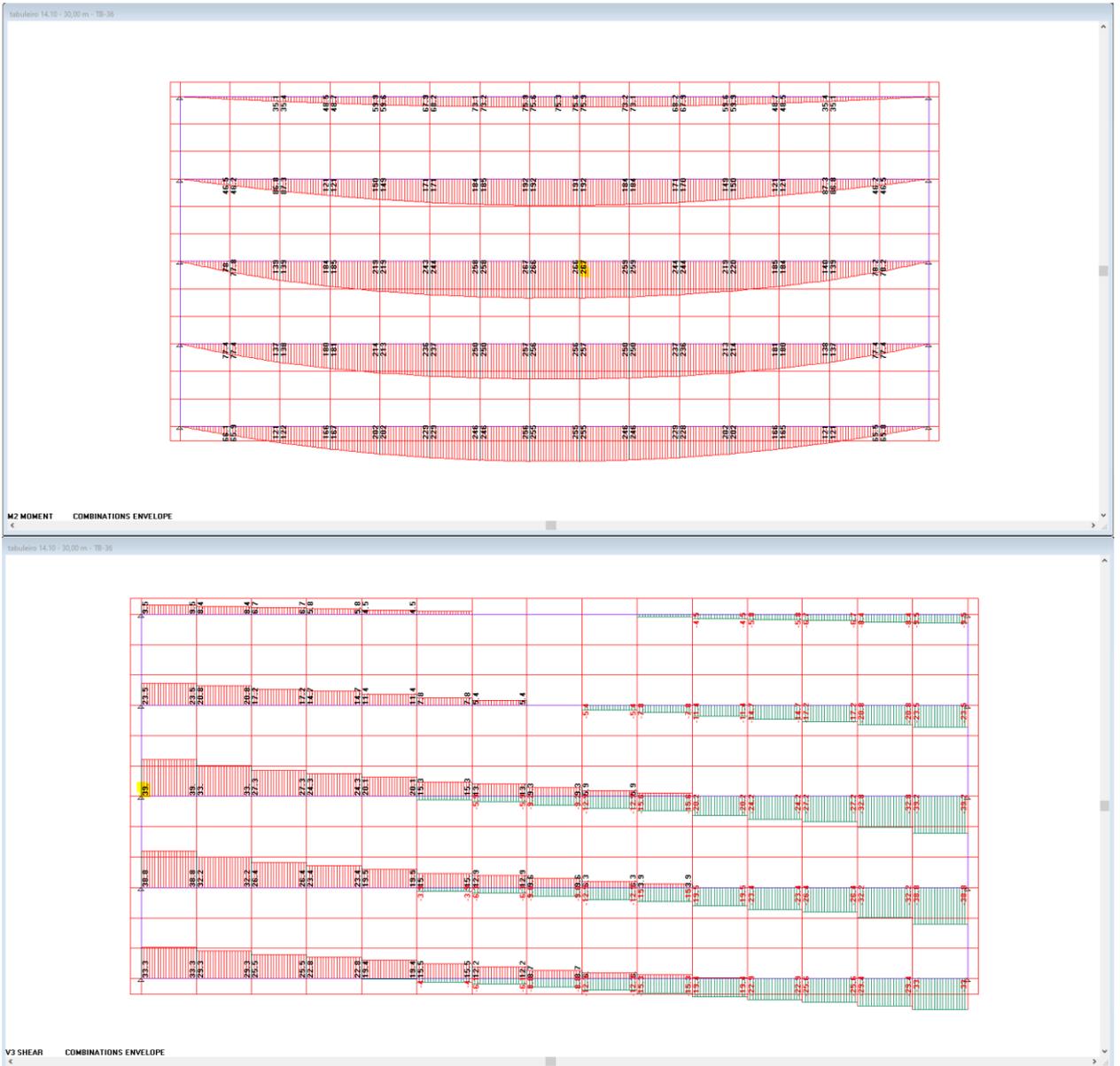


### NOTA TÉCNICA



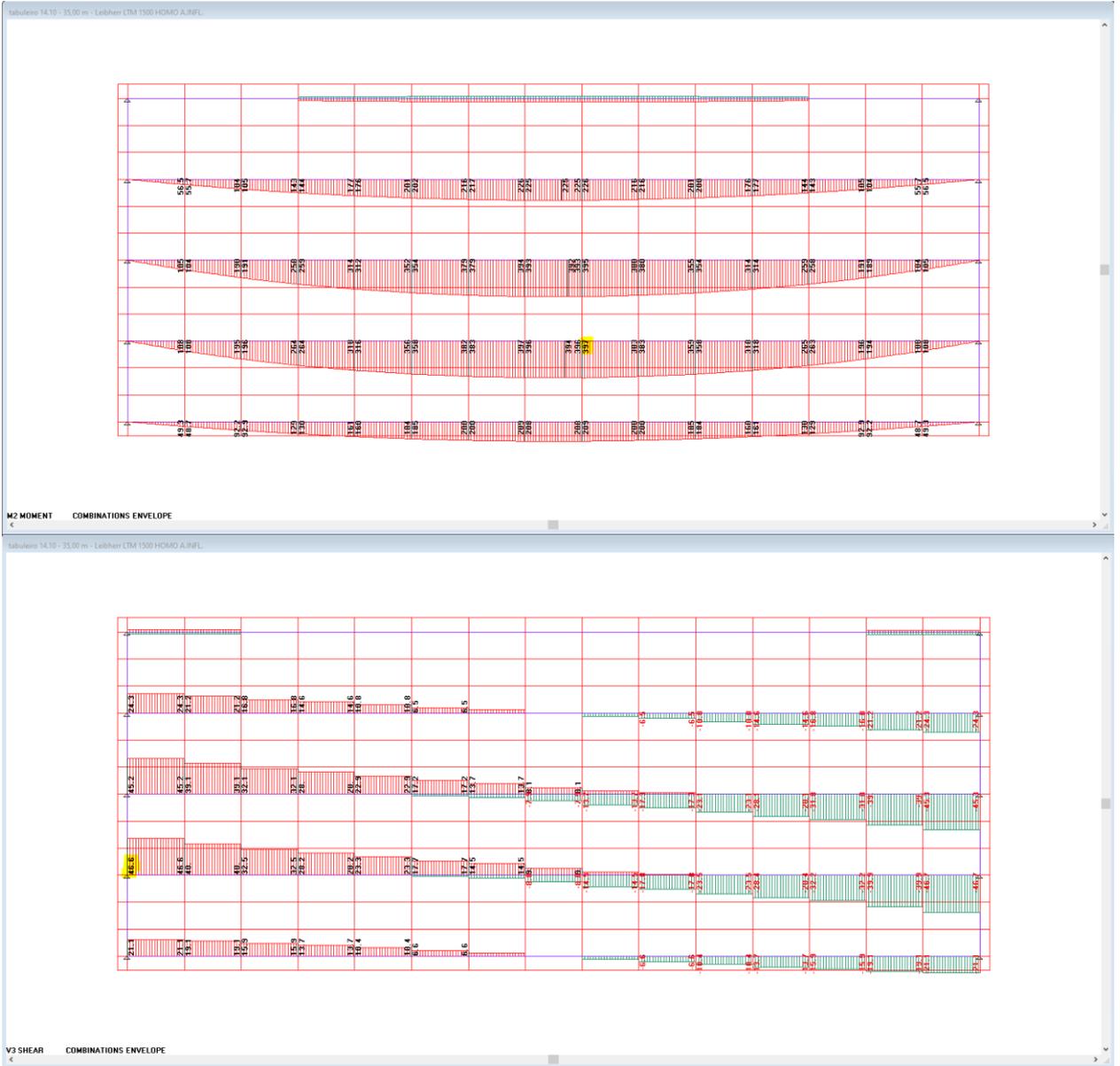


### NOTA TÉCNICA



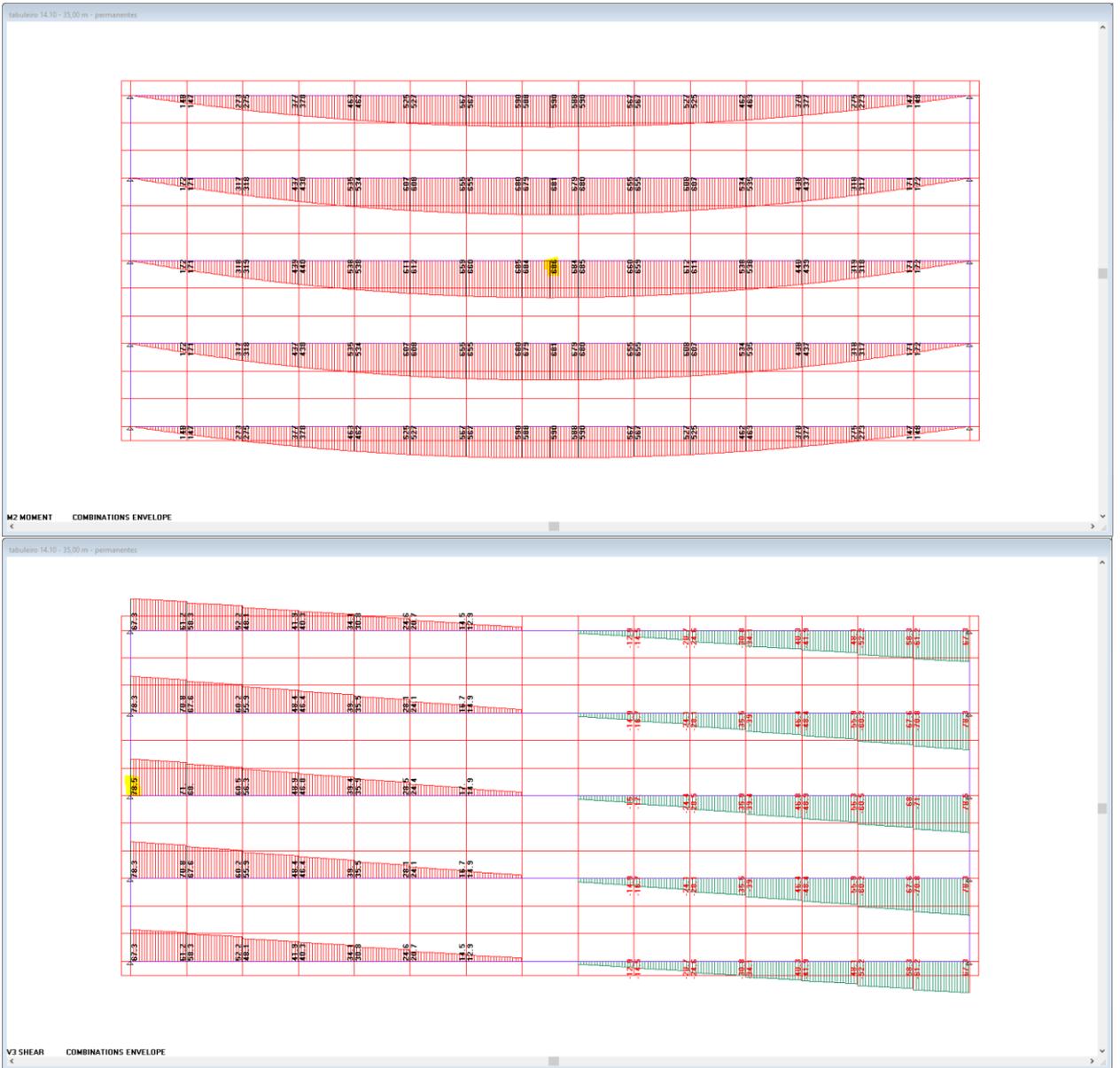


### NOTA TÉCNICA



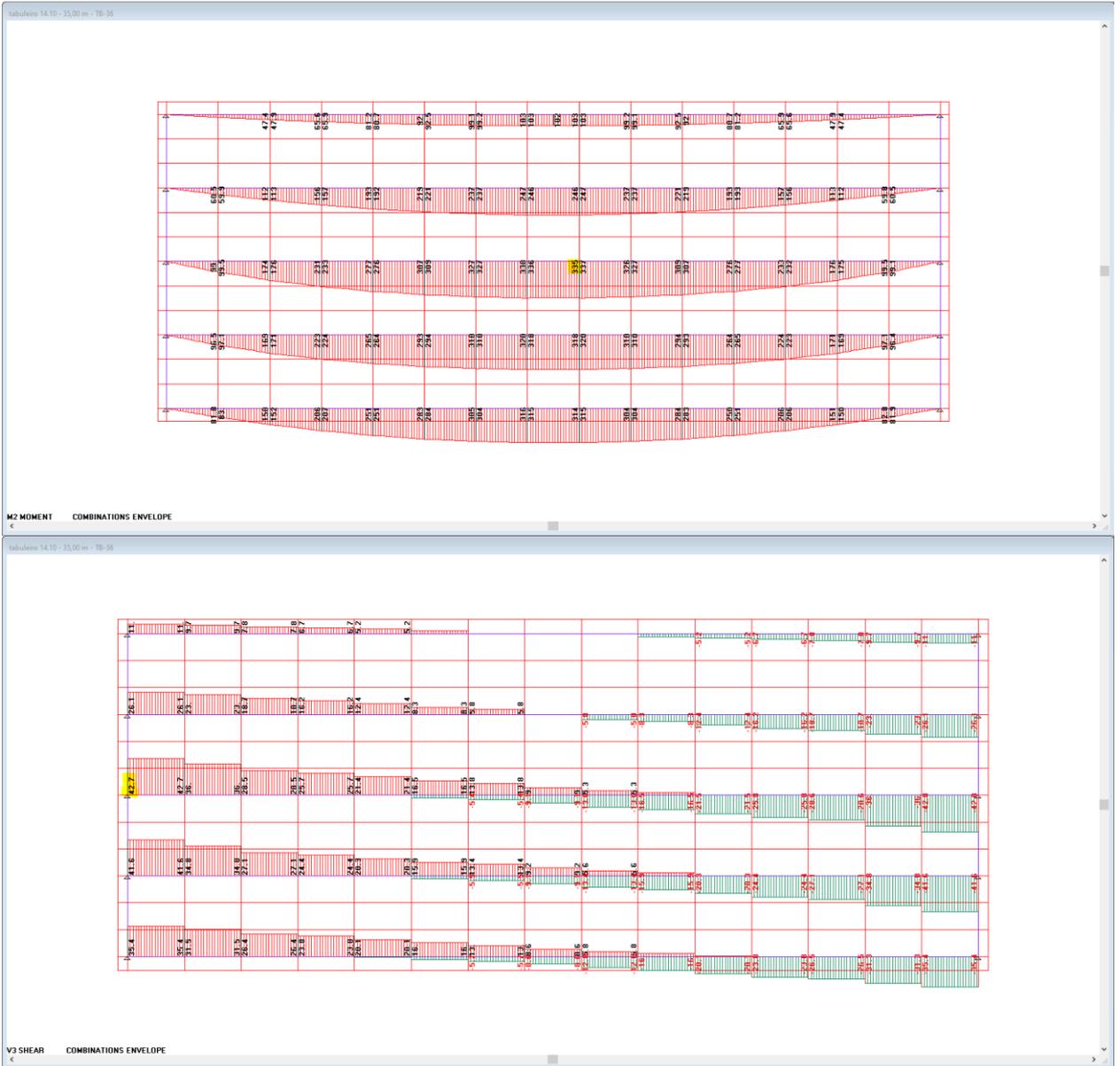


### NOTA TÉCNICA



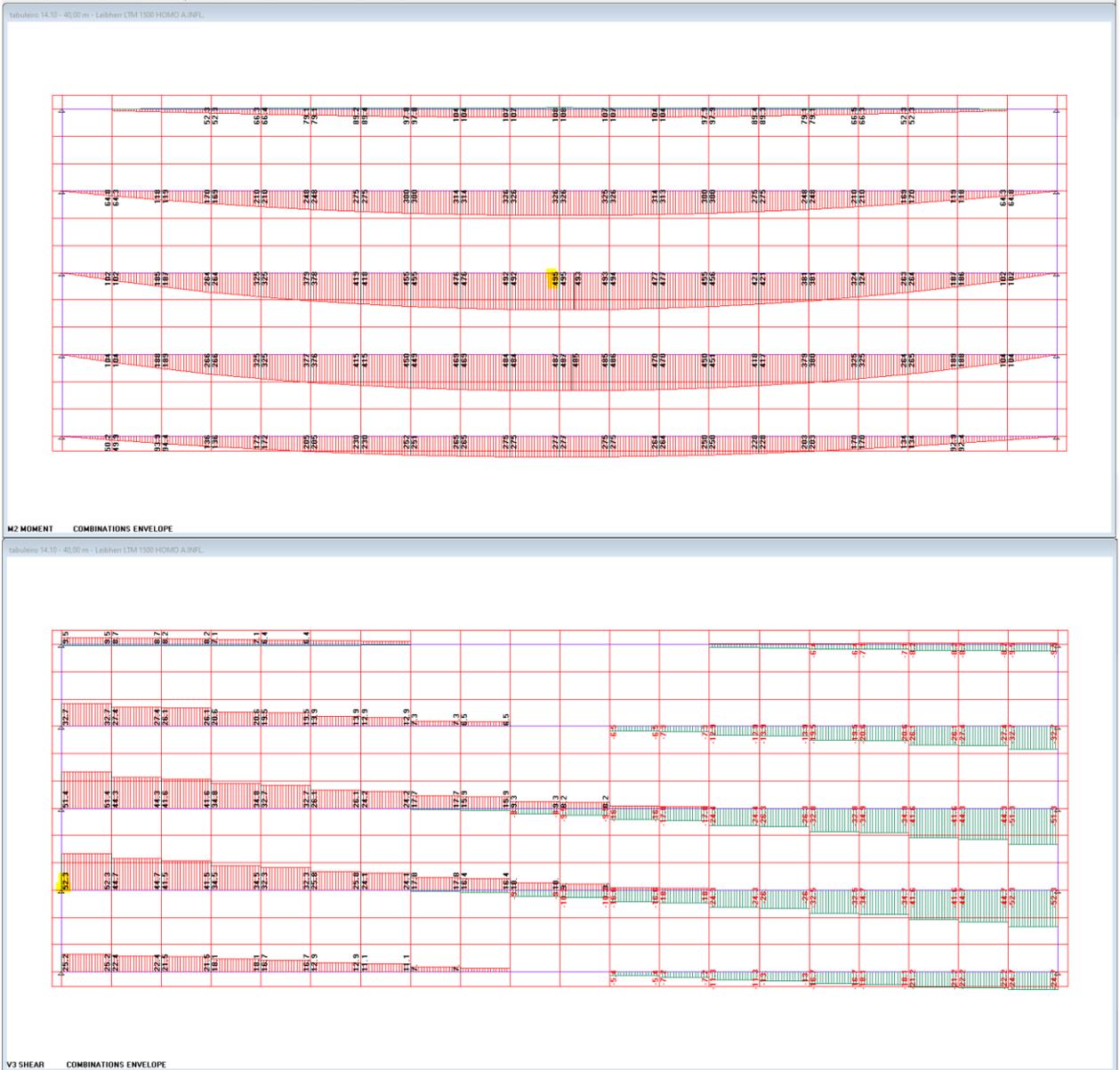


### NOTA TÉCNICA



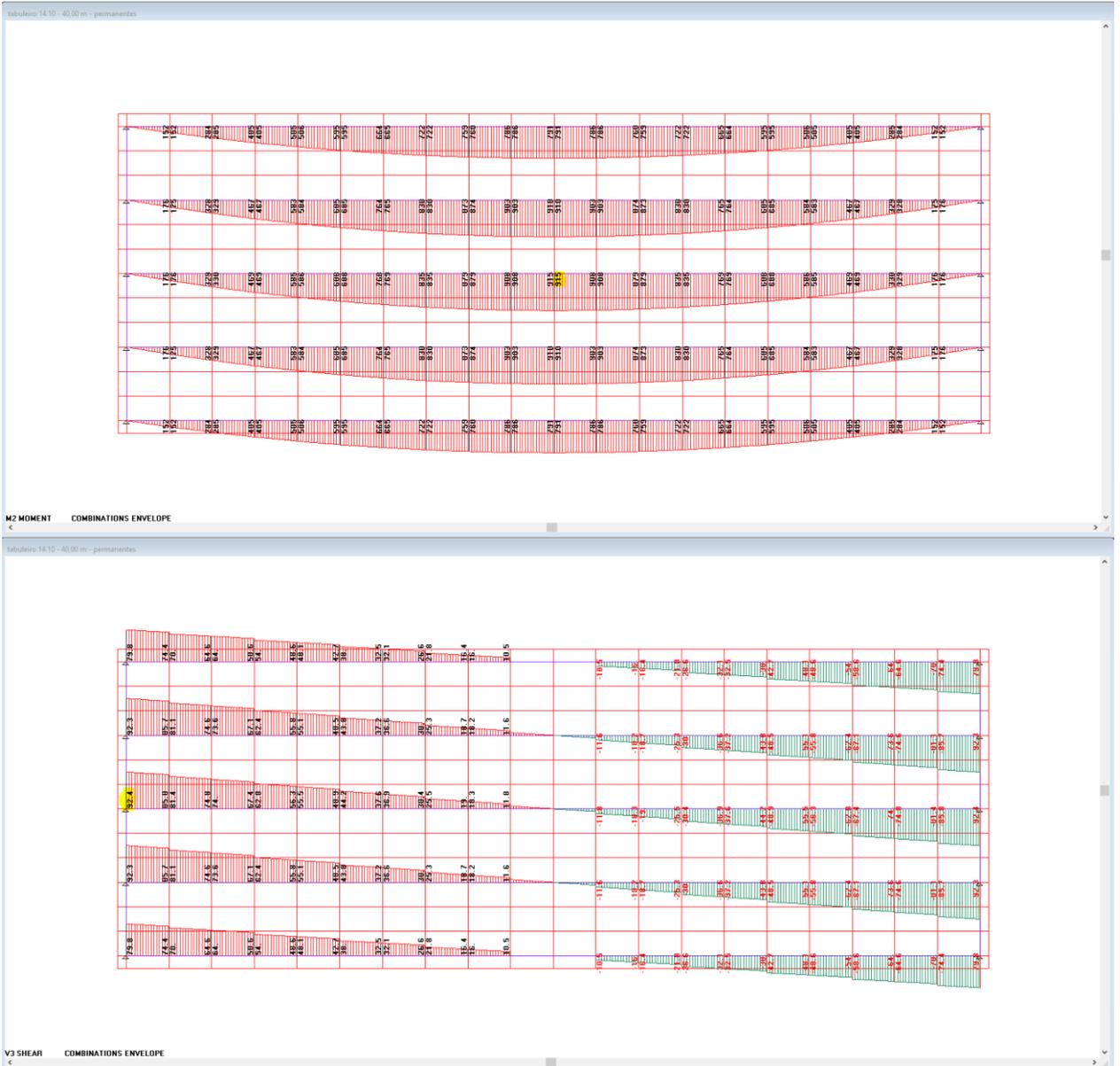


### NOTA TÉCNICA



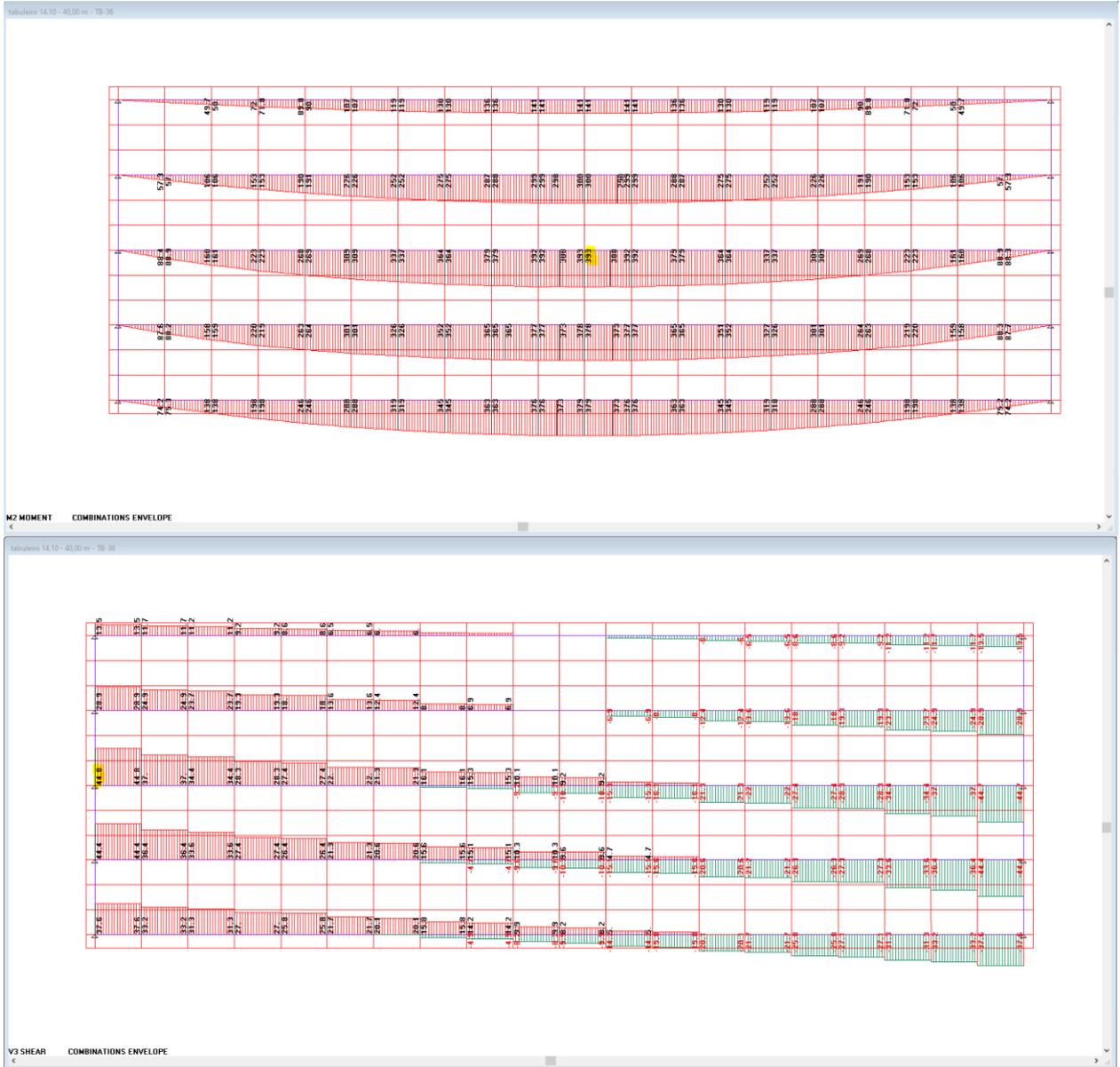


### NOTA TÉCNICA





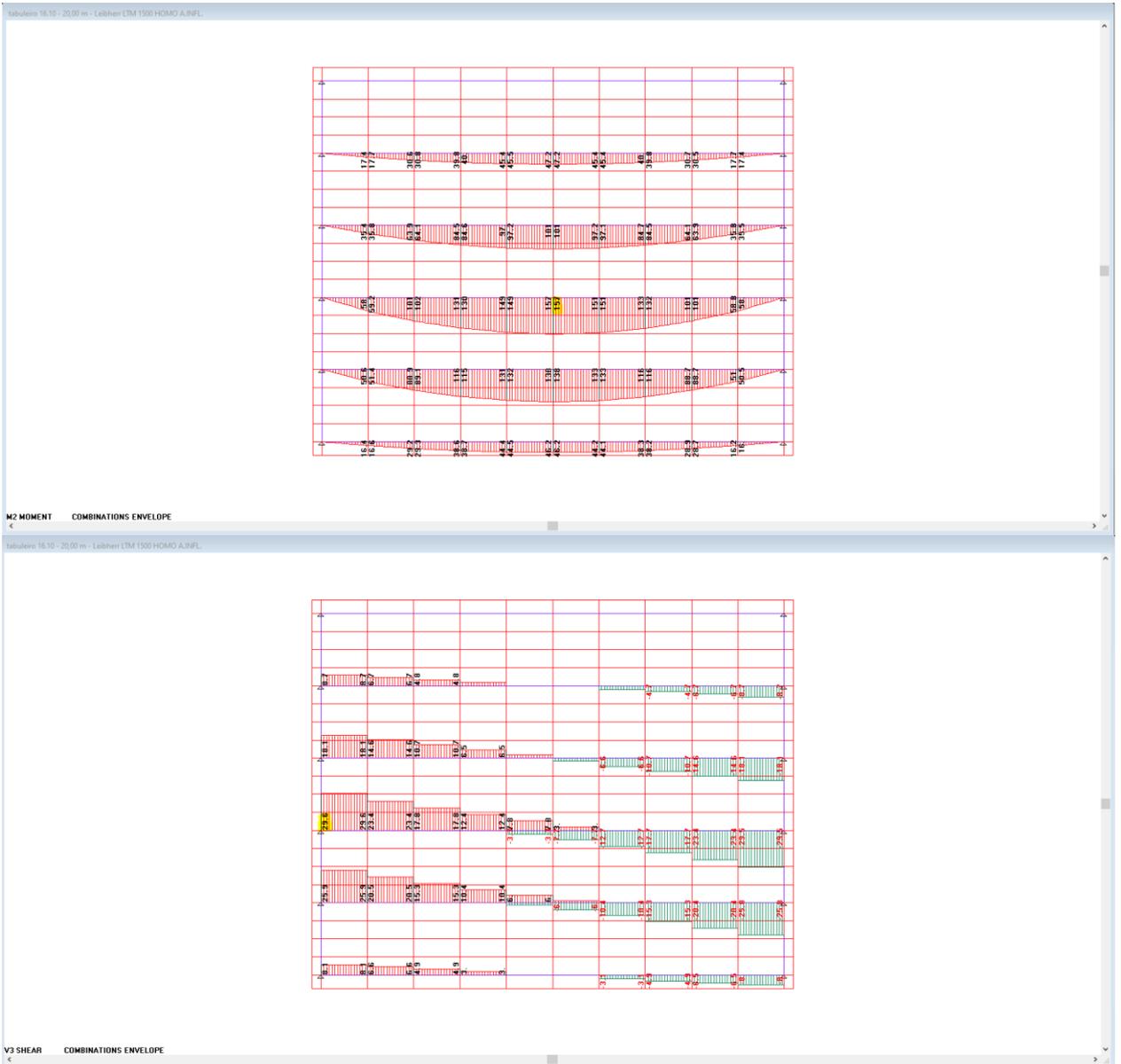
### NOTA TÉCNICA





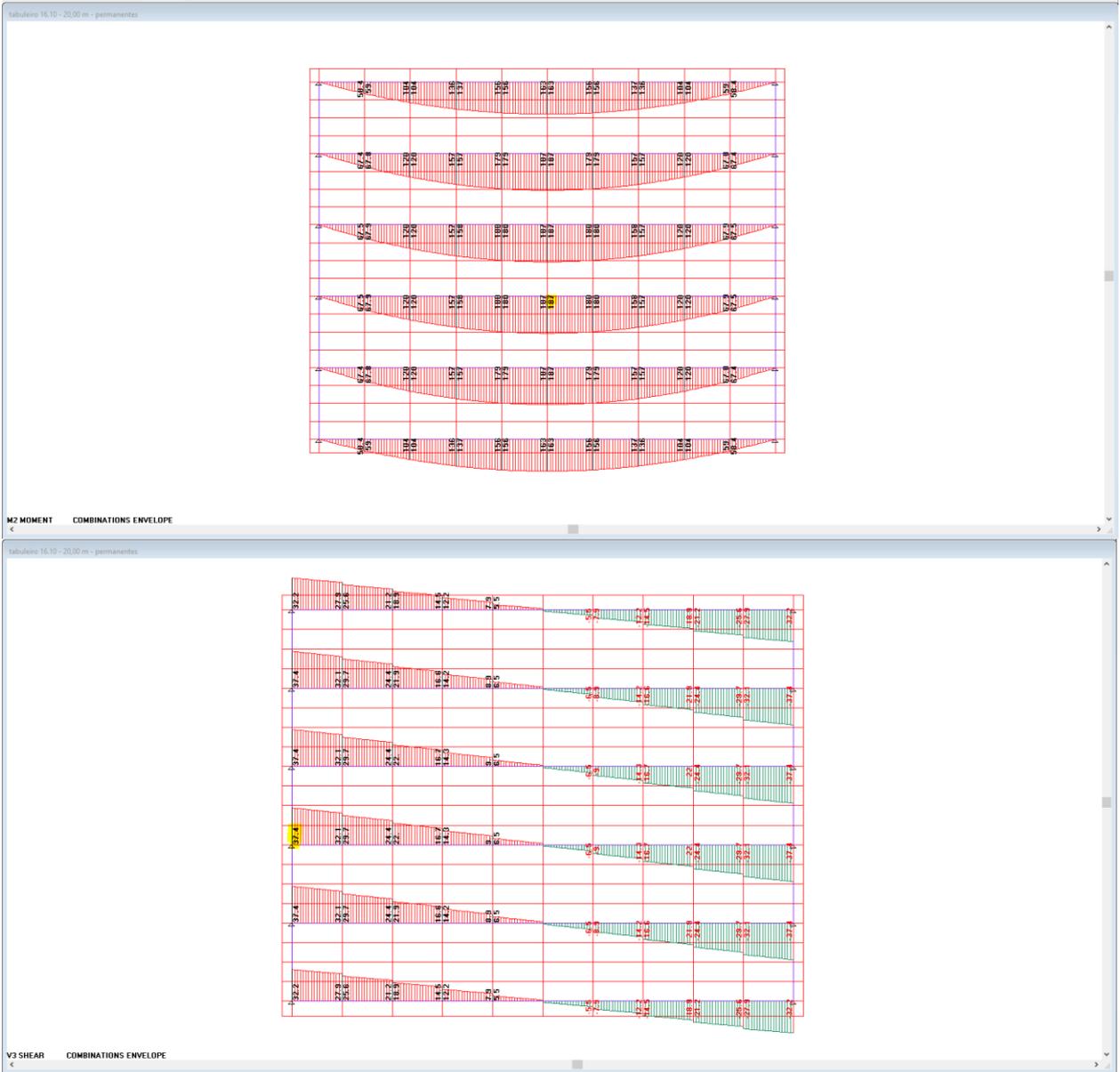
### NOTA TÉCNICA

#### 4.6.4. Tabuleiro 16,10 m



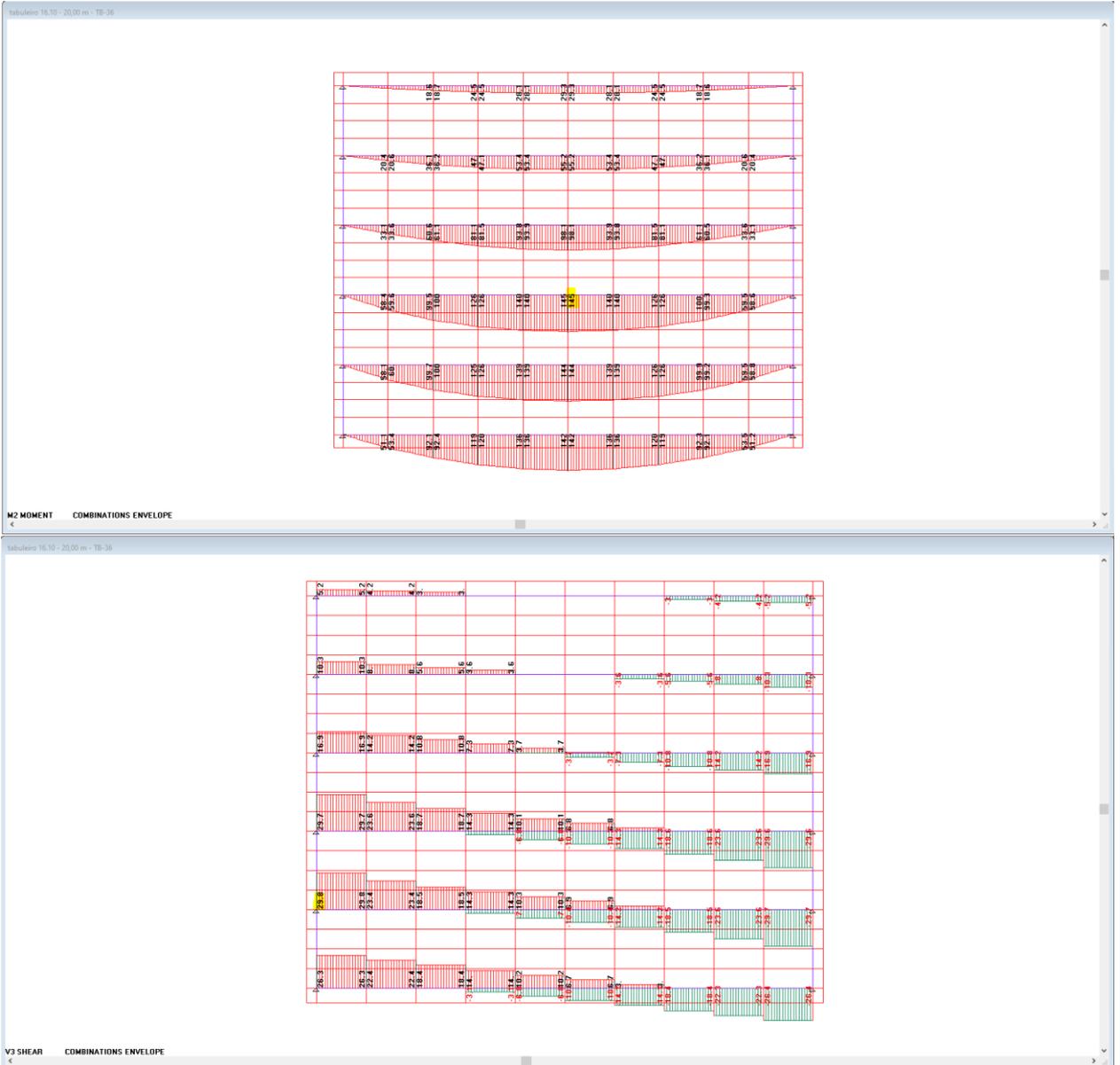


### NOTA TÉCNICA



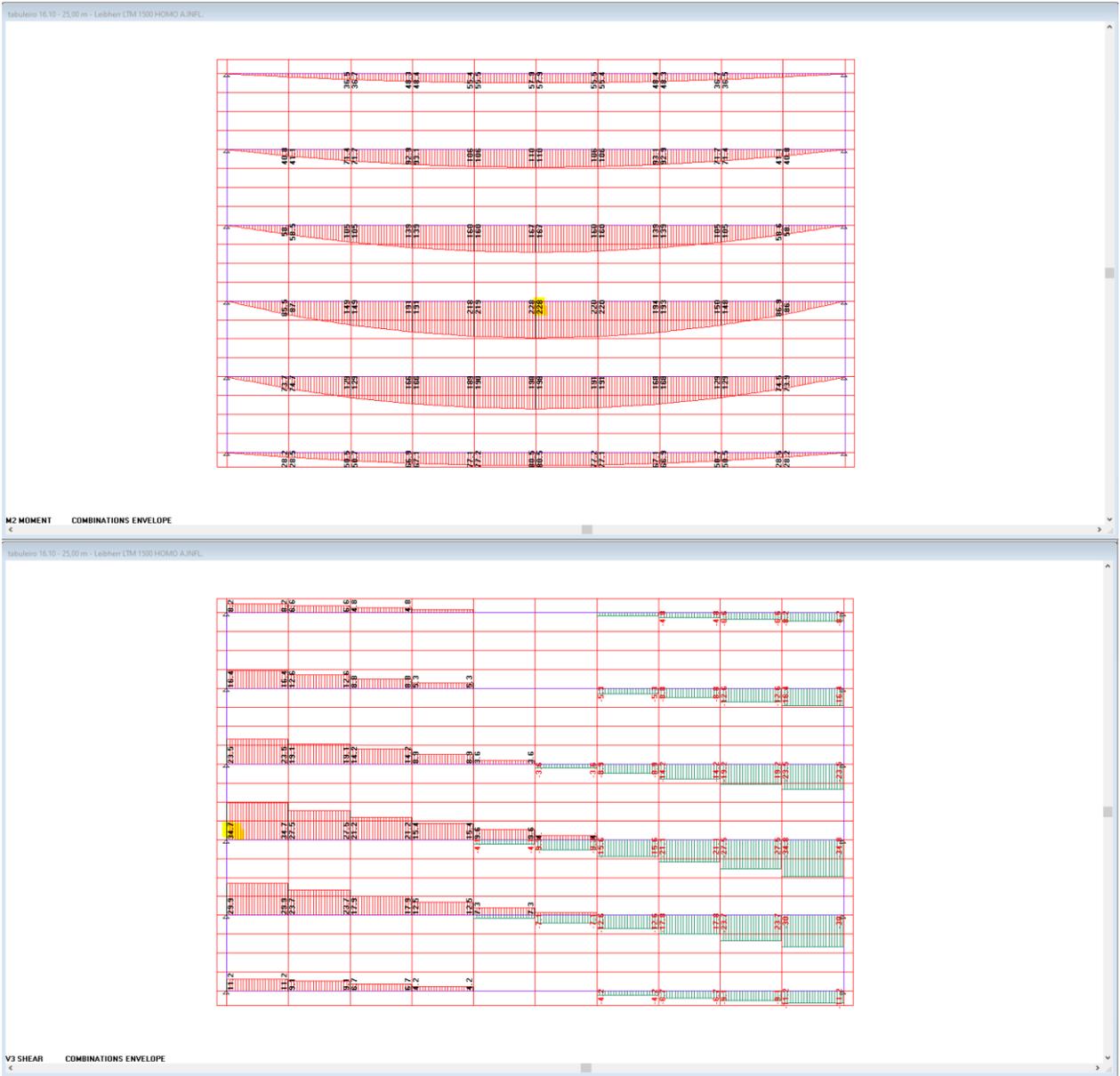


### NOTA TÉCNICA



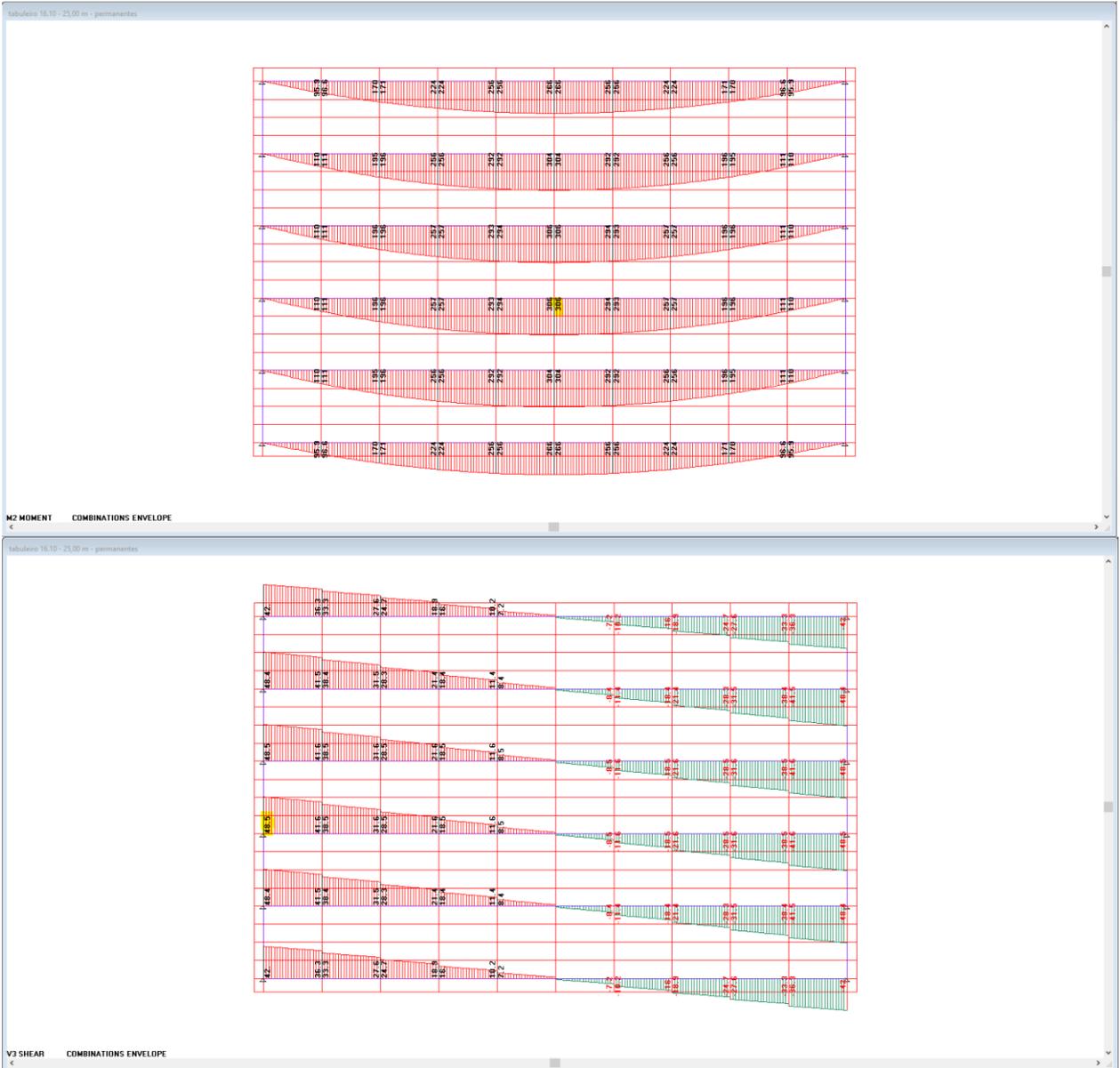


### NOTA TÉCNICA



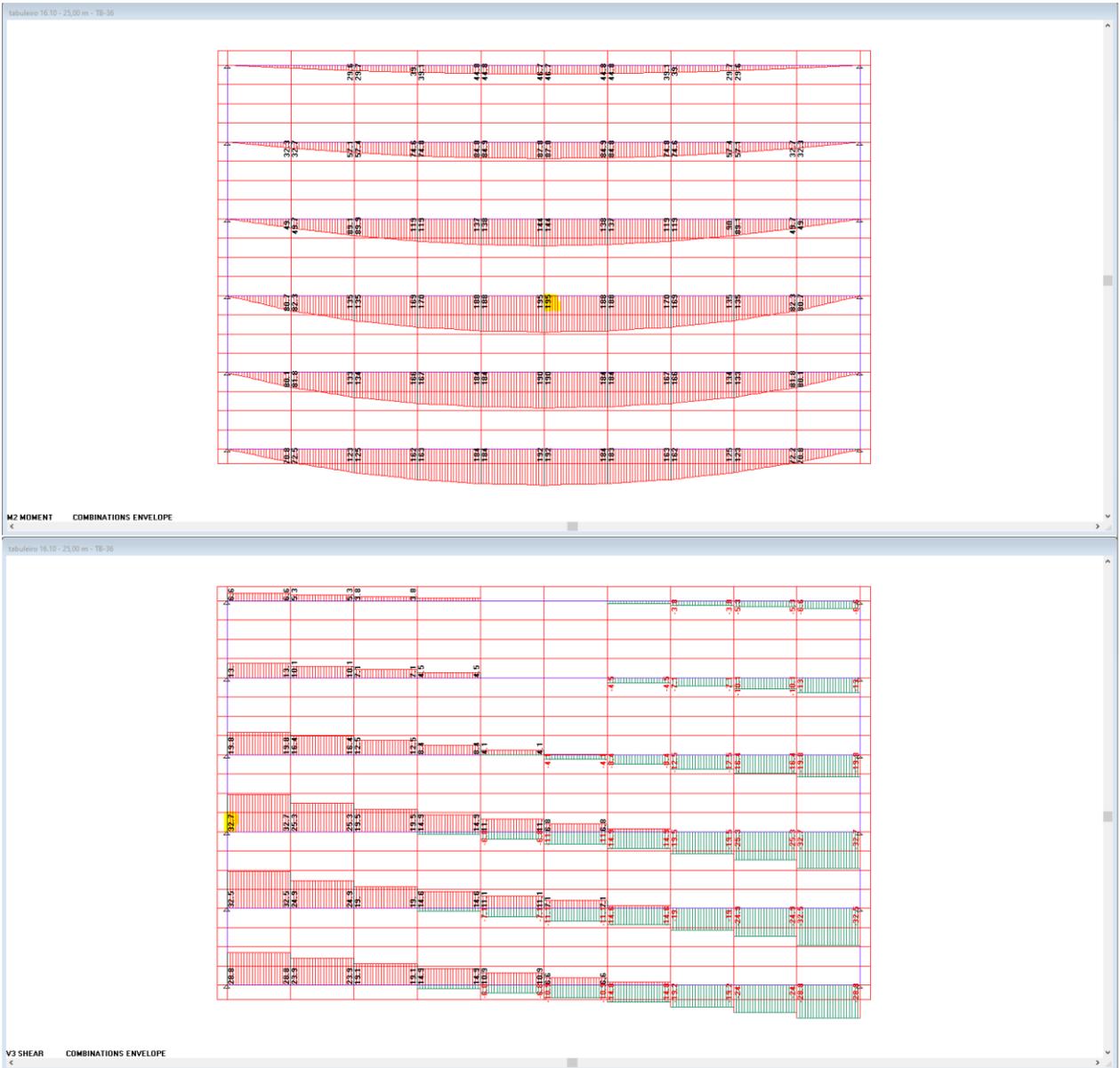


### NOTA TÉCNICA



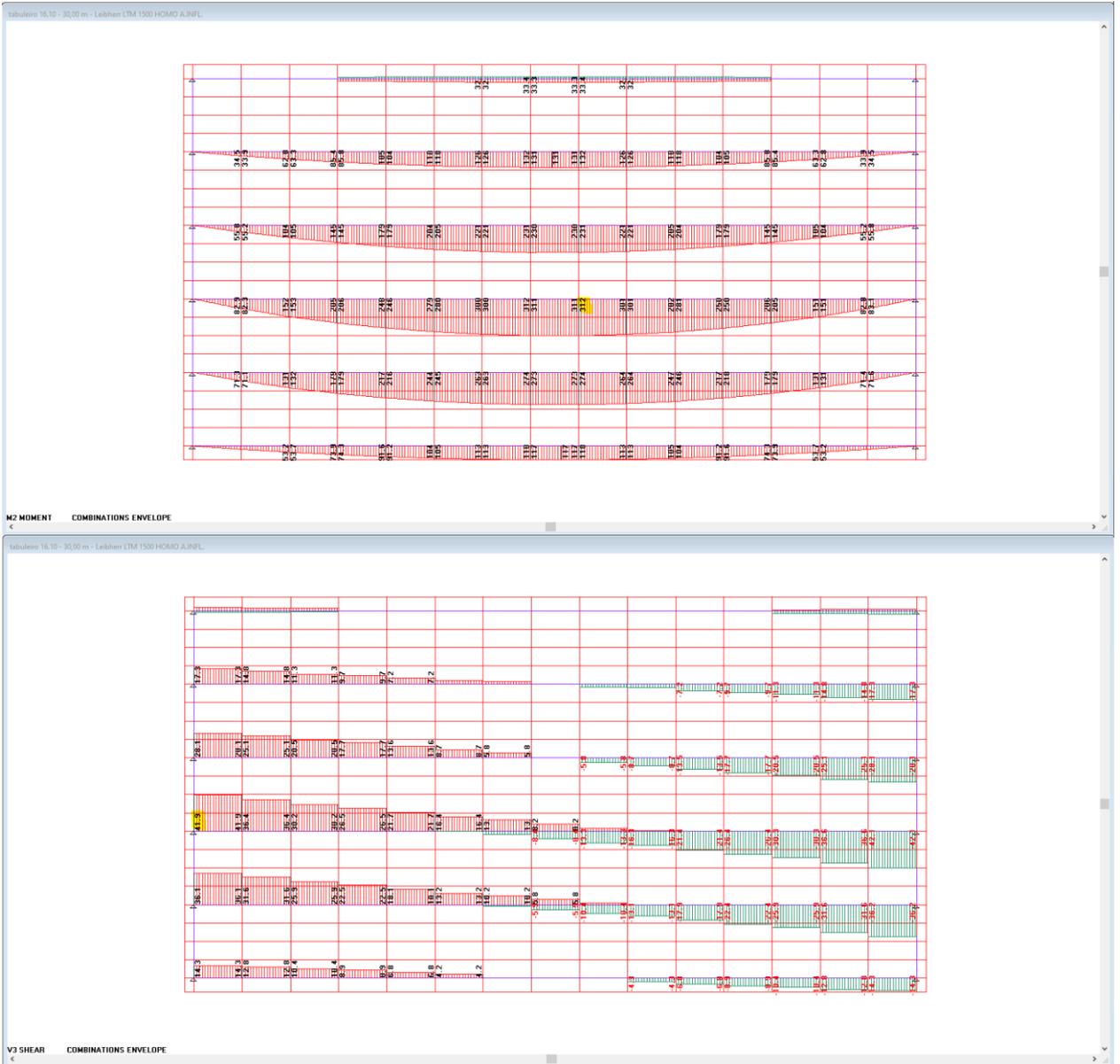


### NOTA TÉCNICA



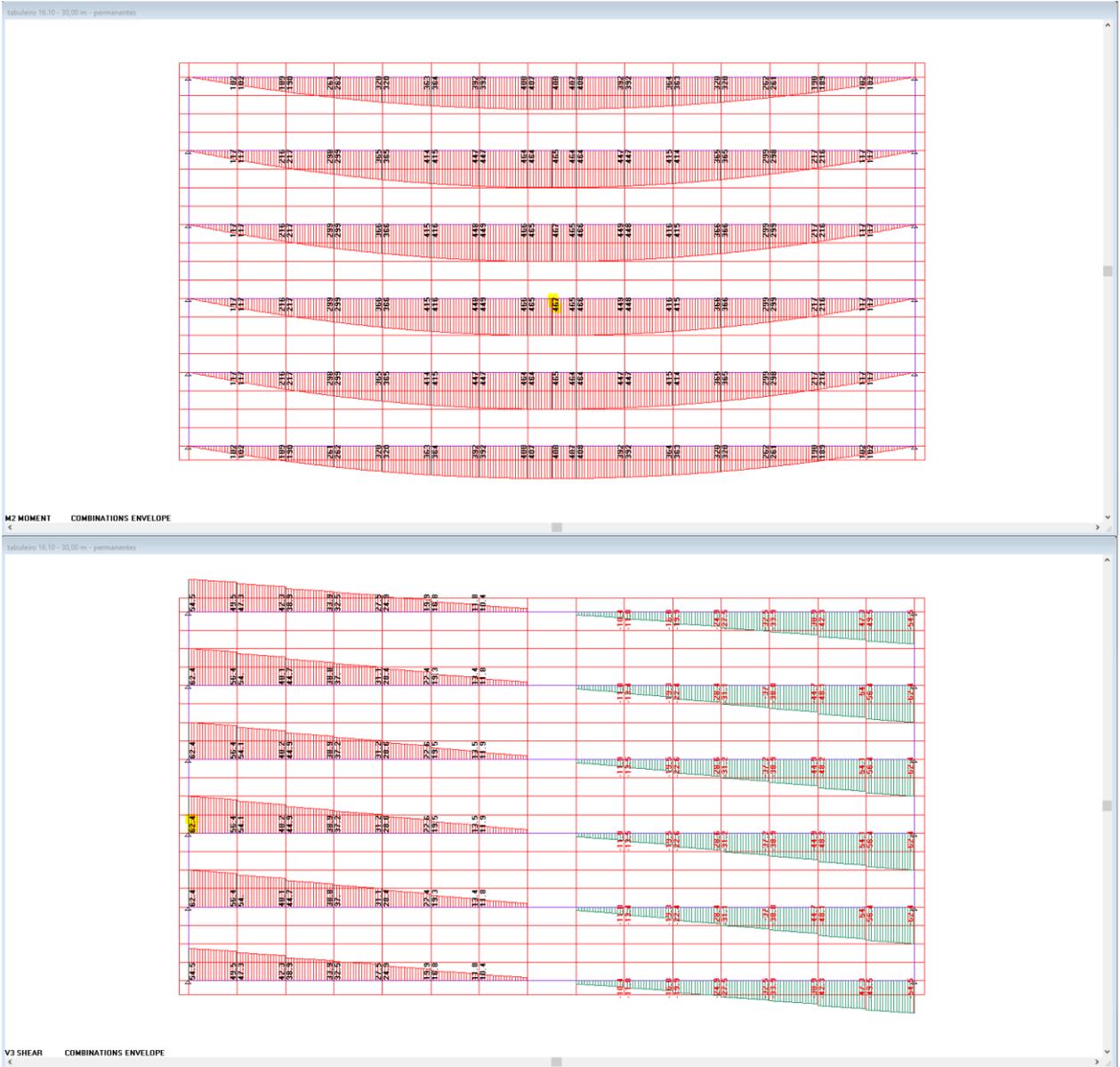


### NOTA TÉCNICA



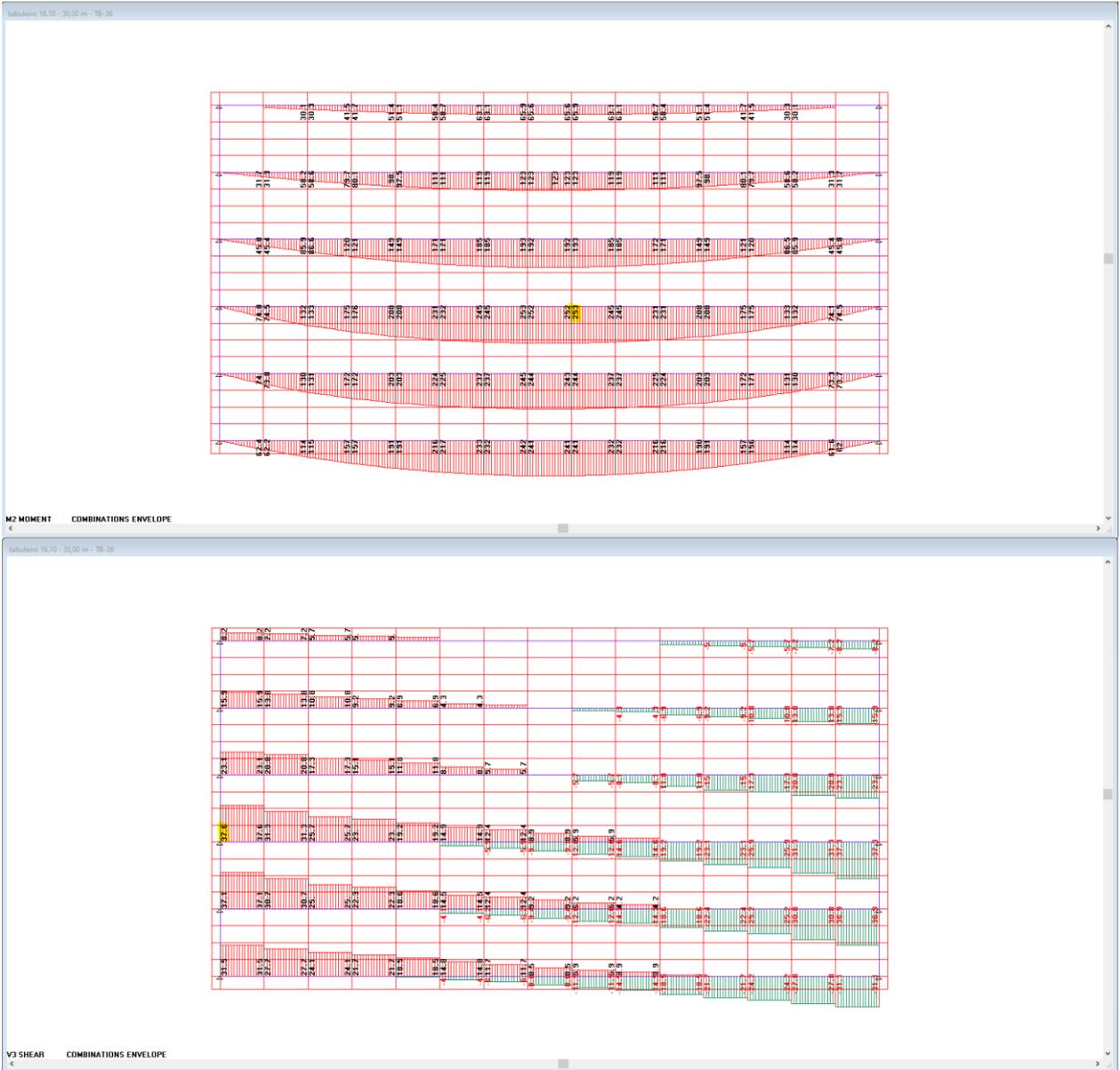


### NOTA TÉCNICA



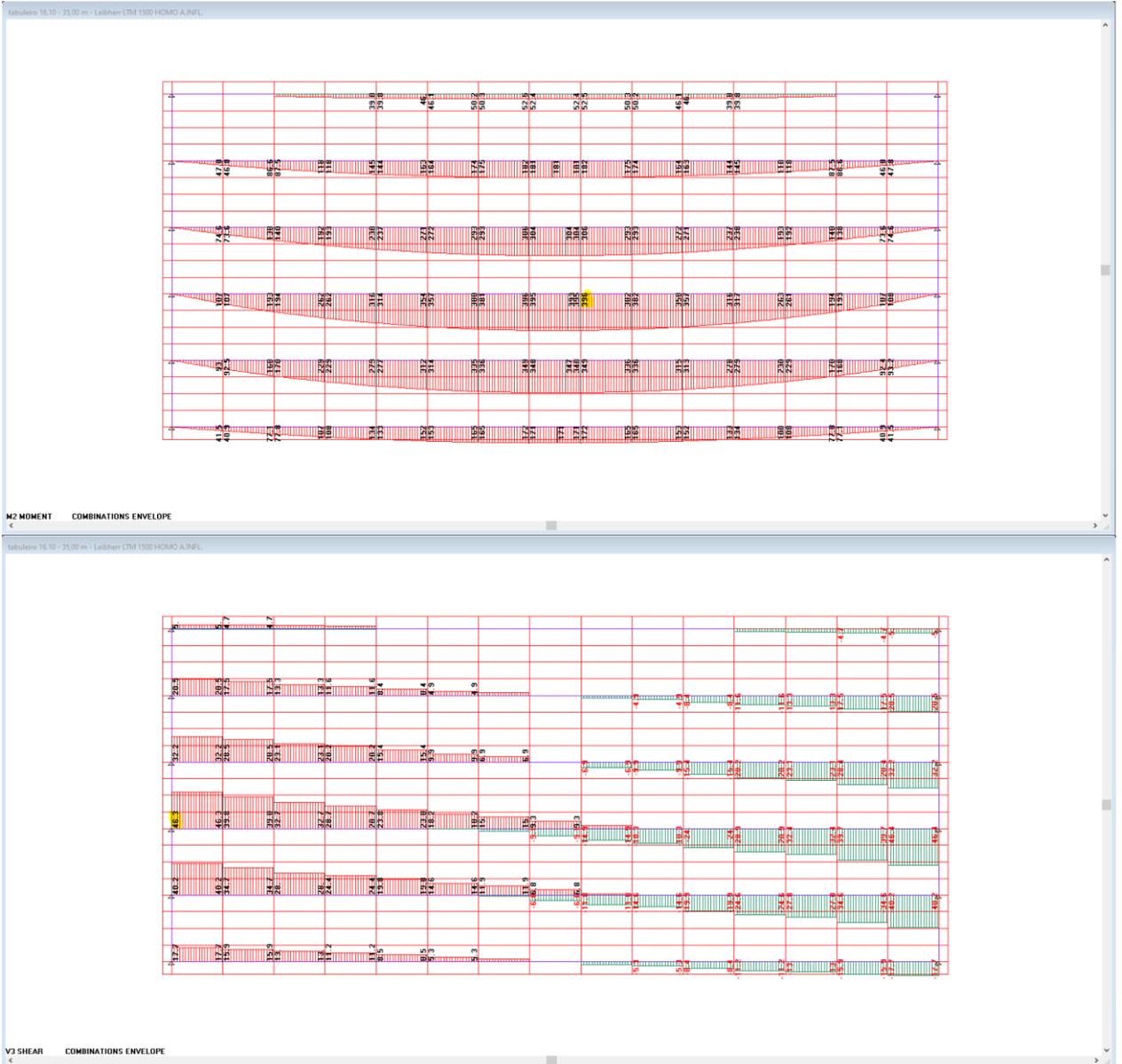


### NOTA TÉCNICA



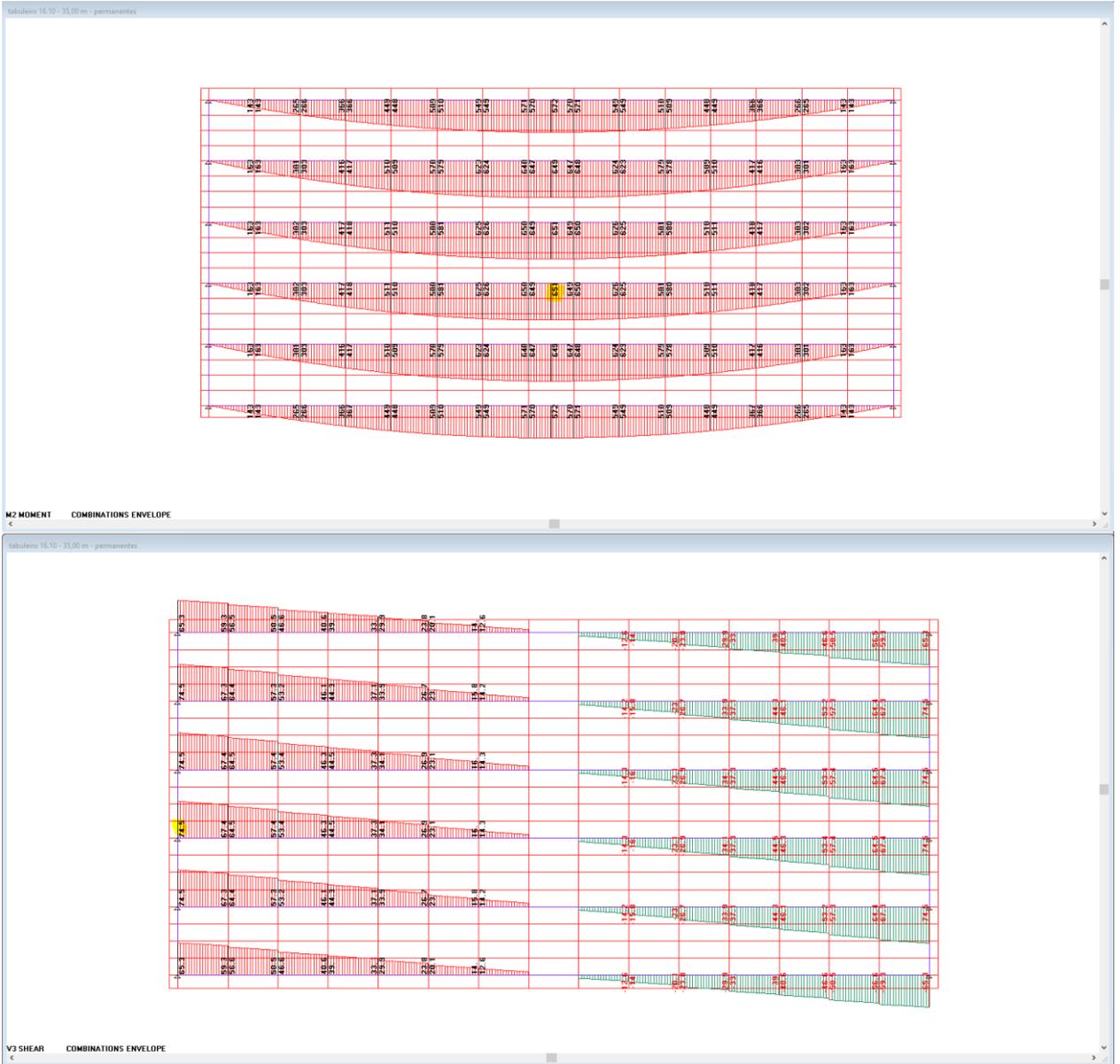


### NOTA TÉCNICA



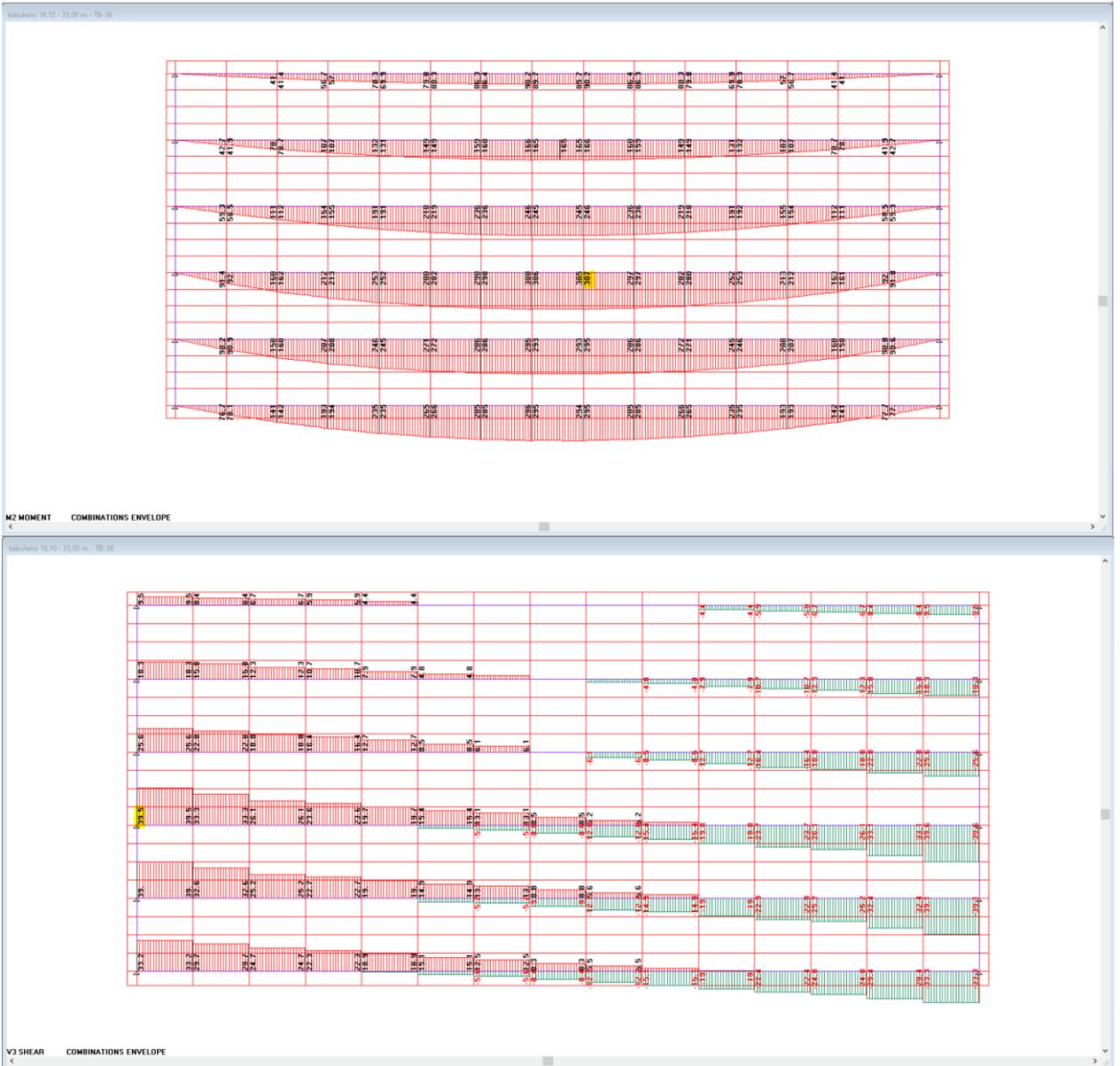


### NOTA TÉCNICA



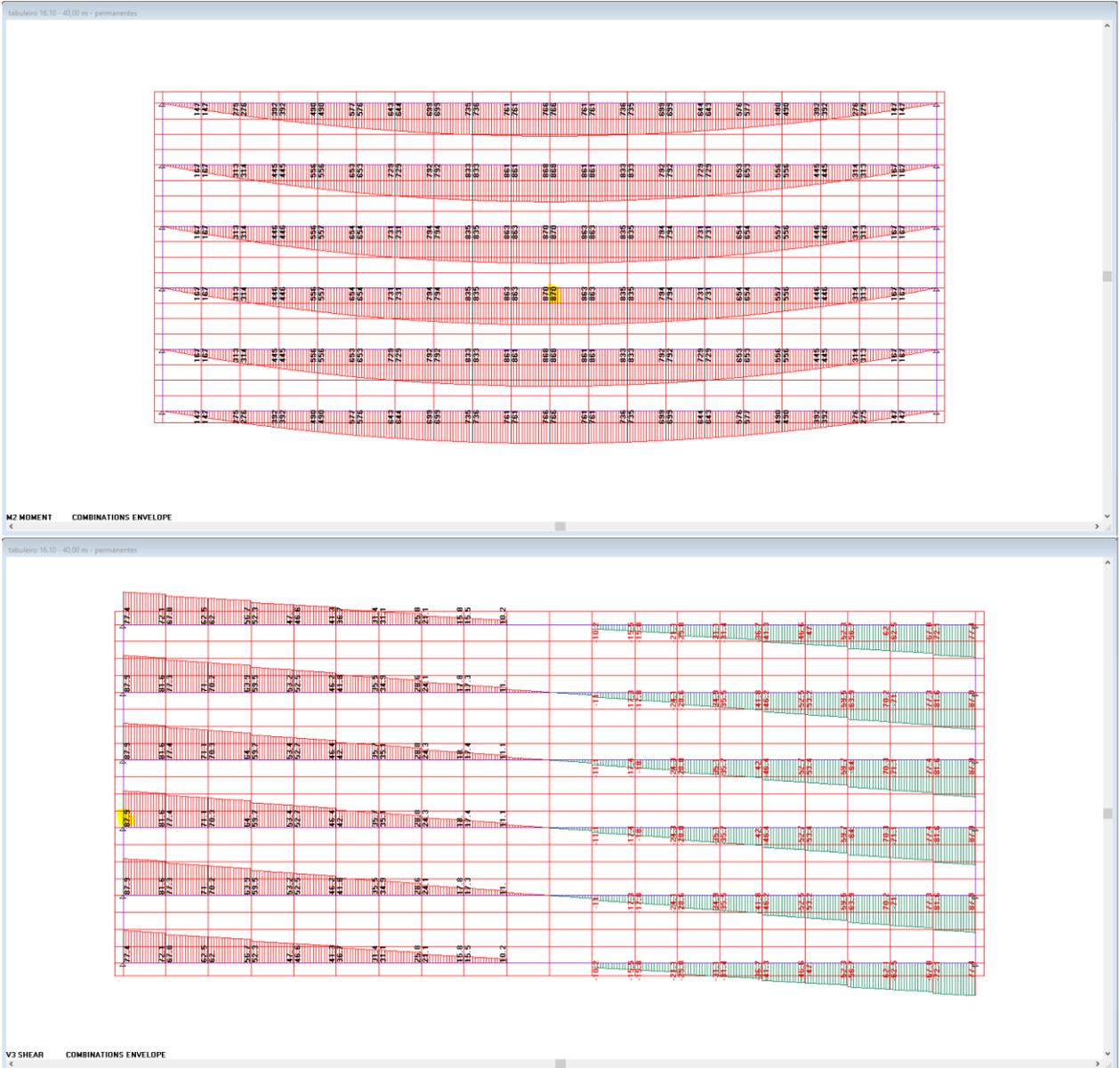


### NOTA TÉCNICA



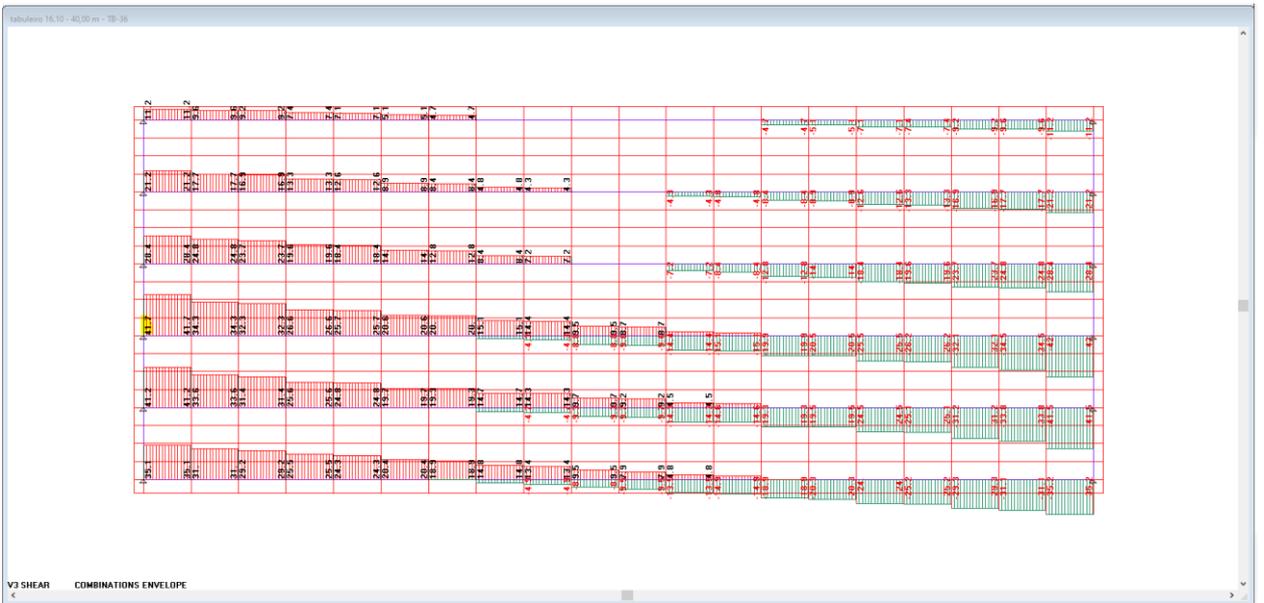
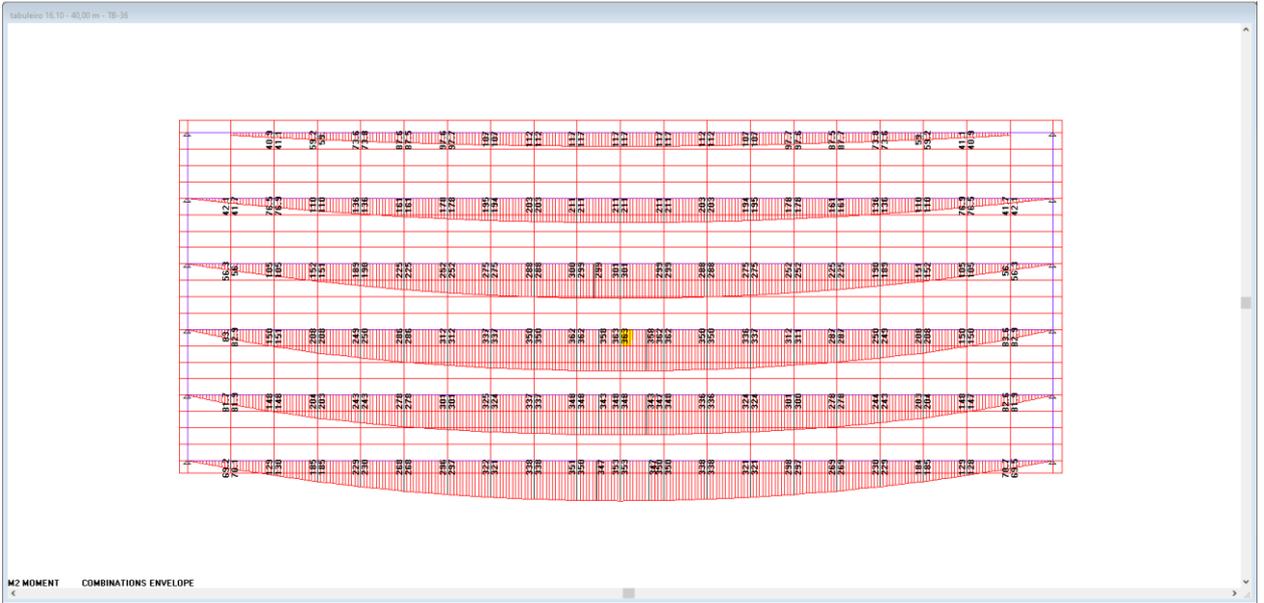


### NOTA TÉCNICA





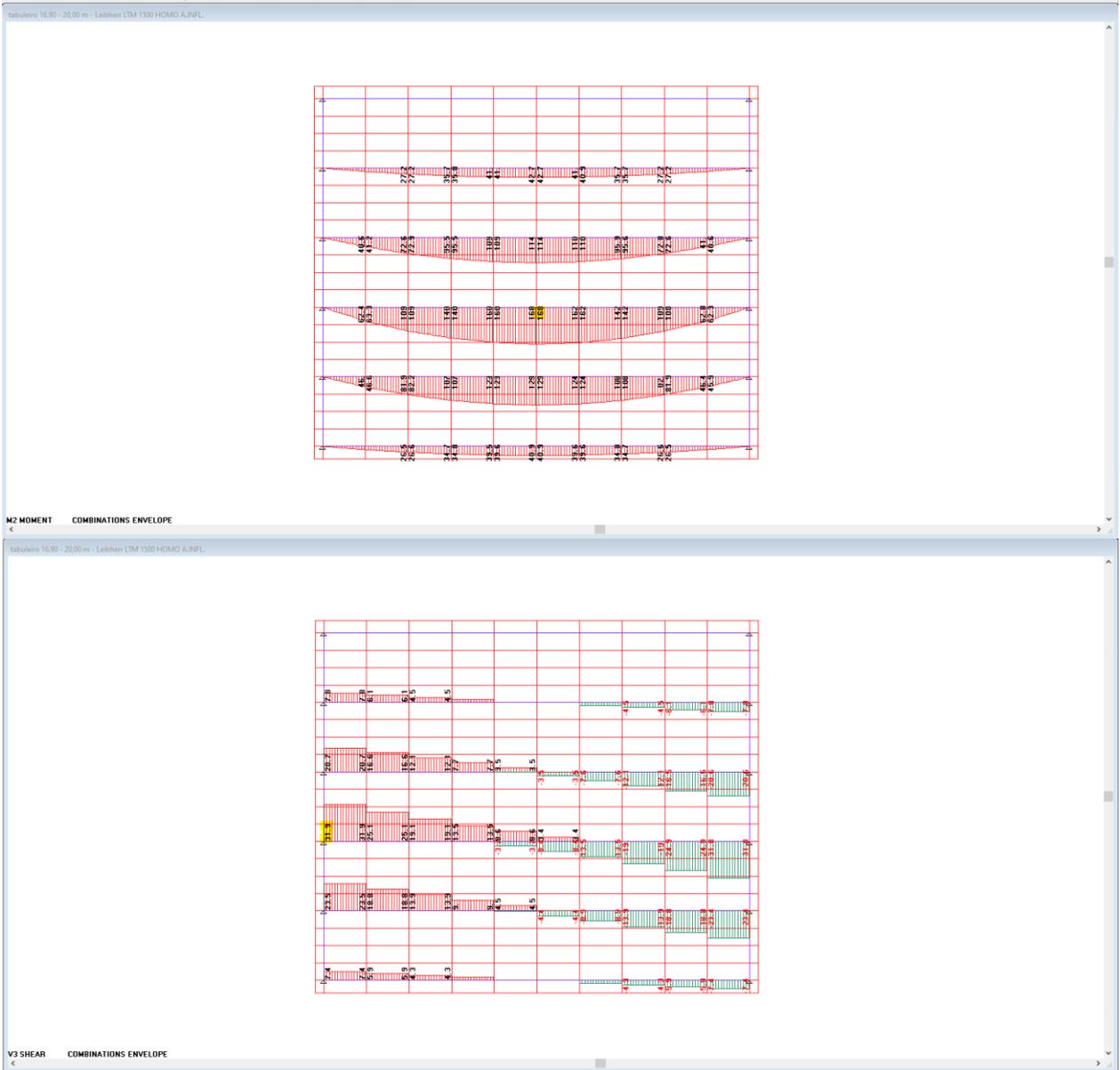
### NOTA TÉCNICA





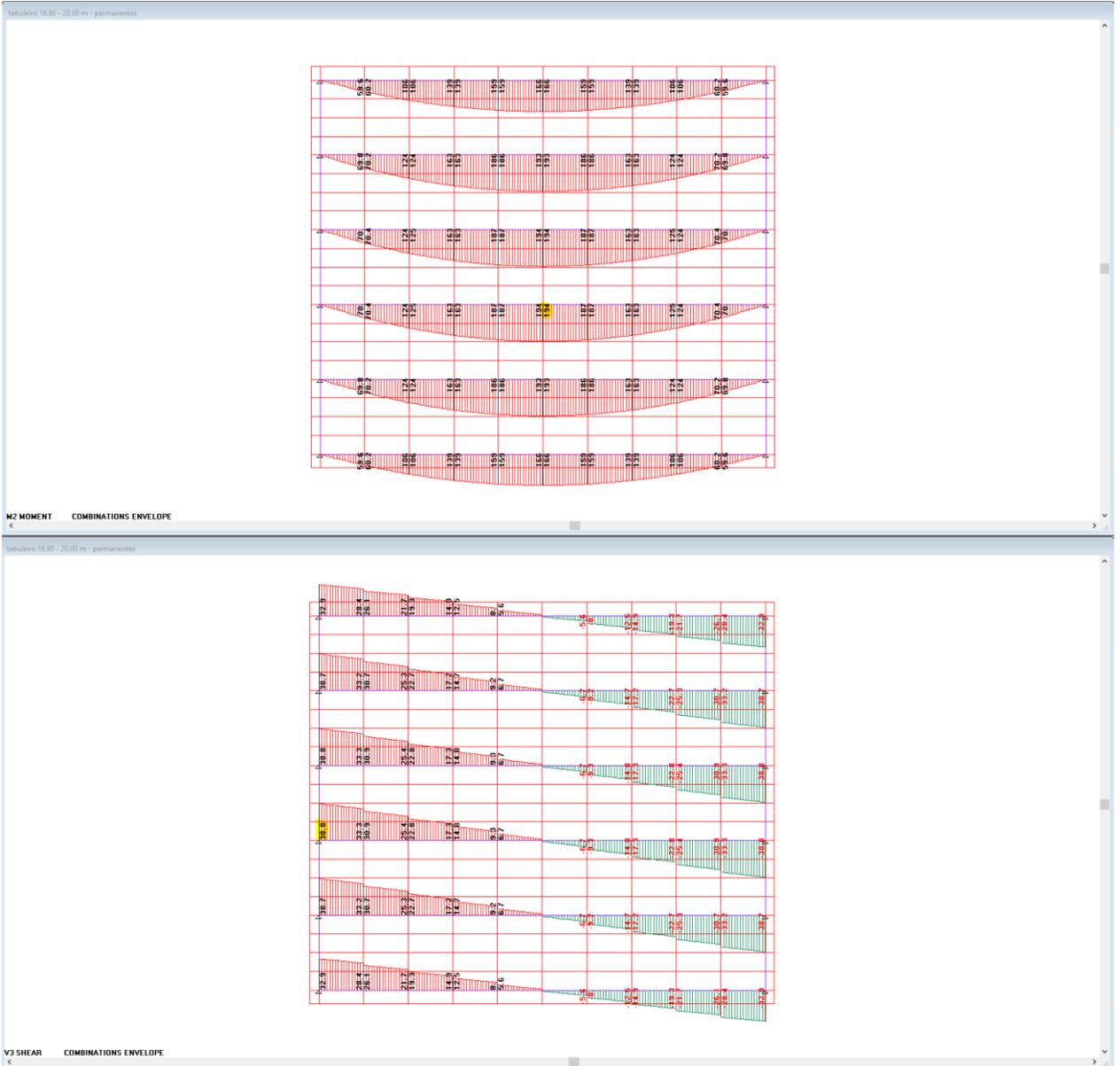
### NOTA TÉCNICA

#### 4.6.5. Tabuleiro 16,90 m



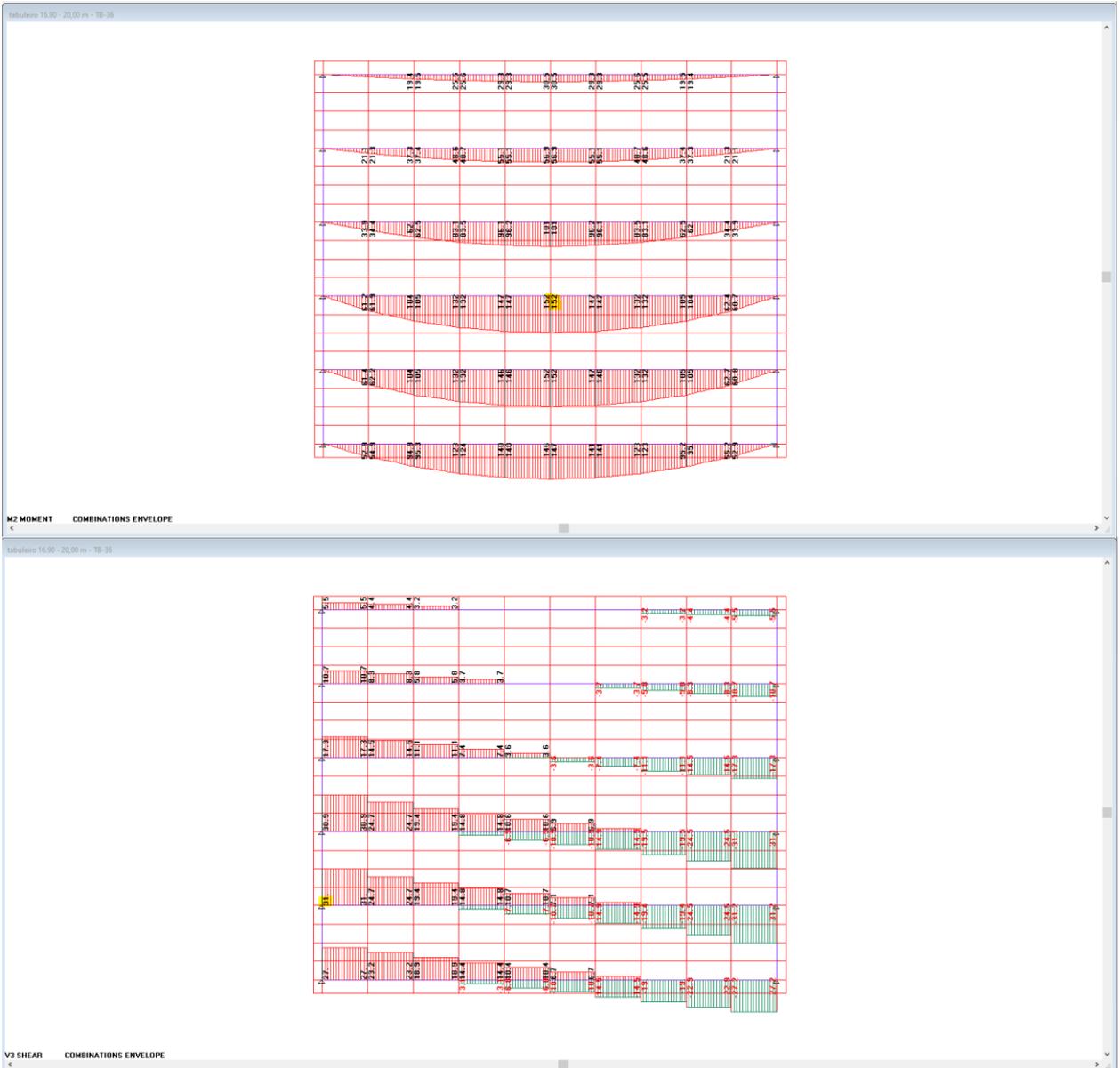


### NOTA TÉCNICA



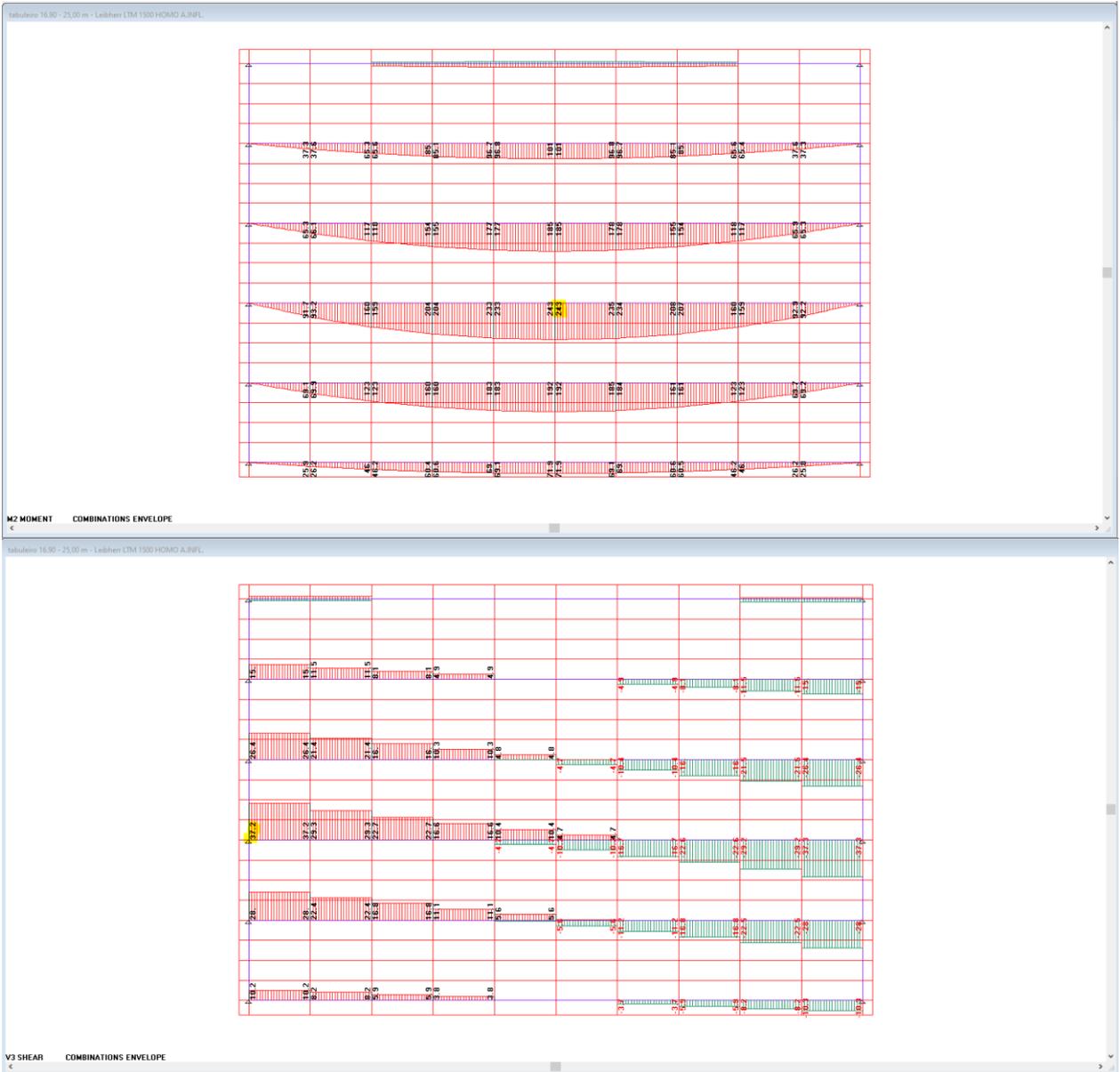


### NOTA TÉCNICA



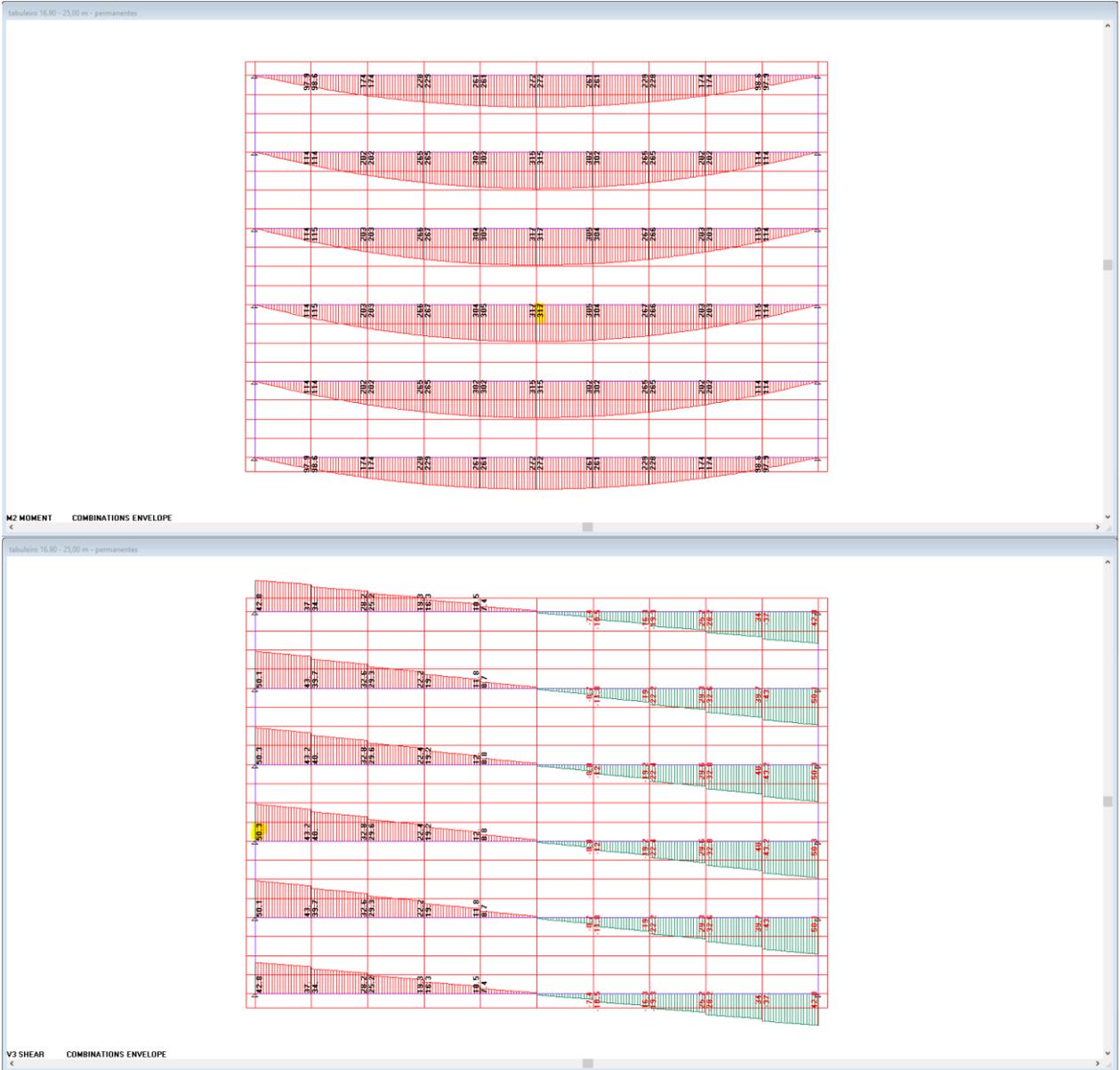


### NOTA TÉCNICA



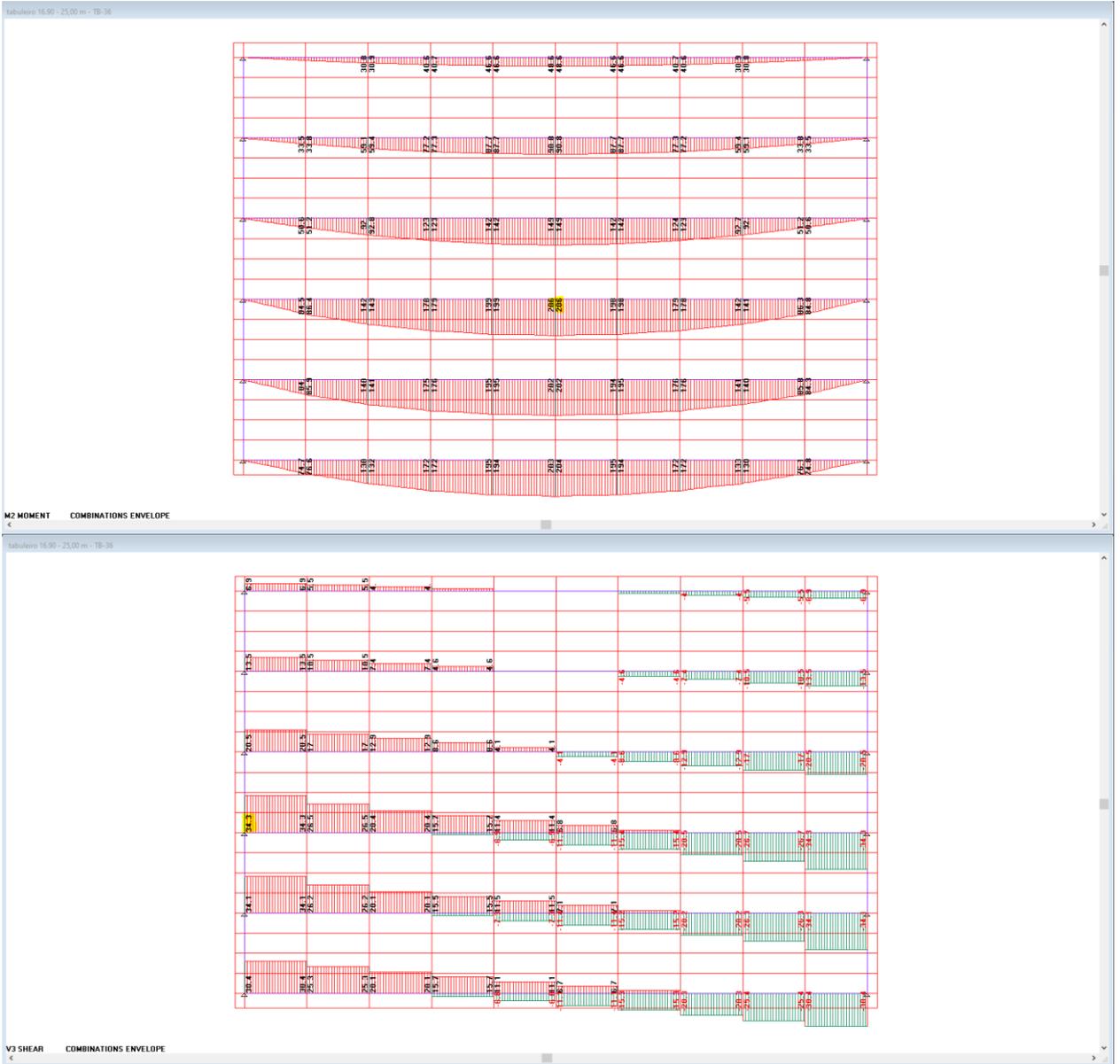


### NOTA TÉCNICA



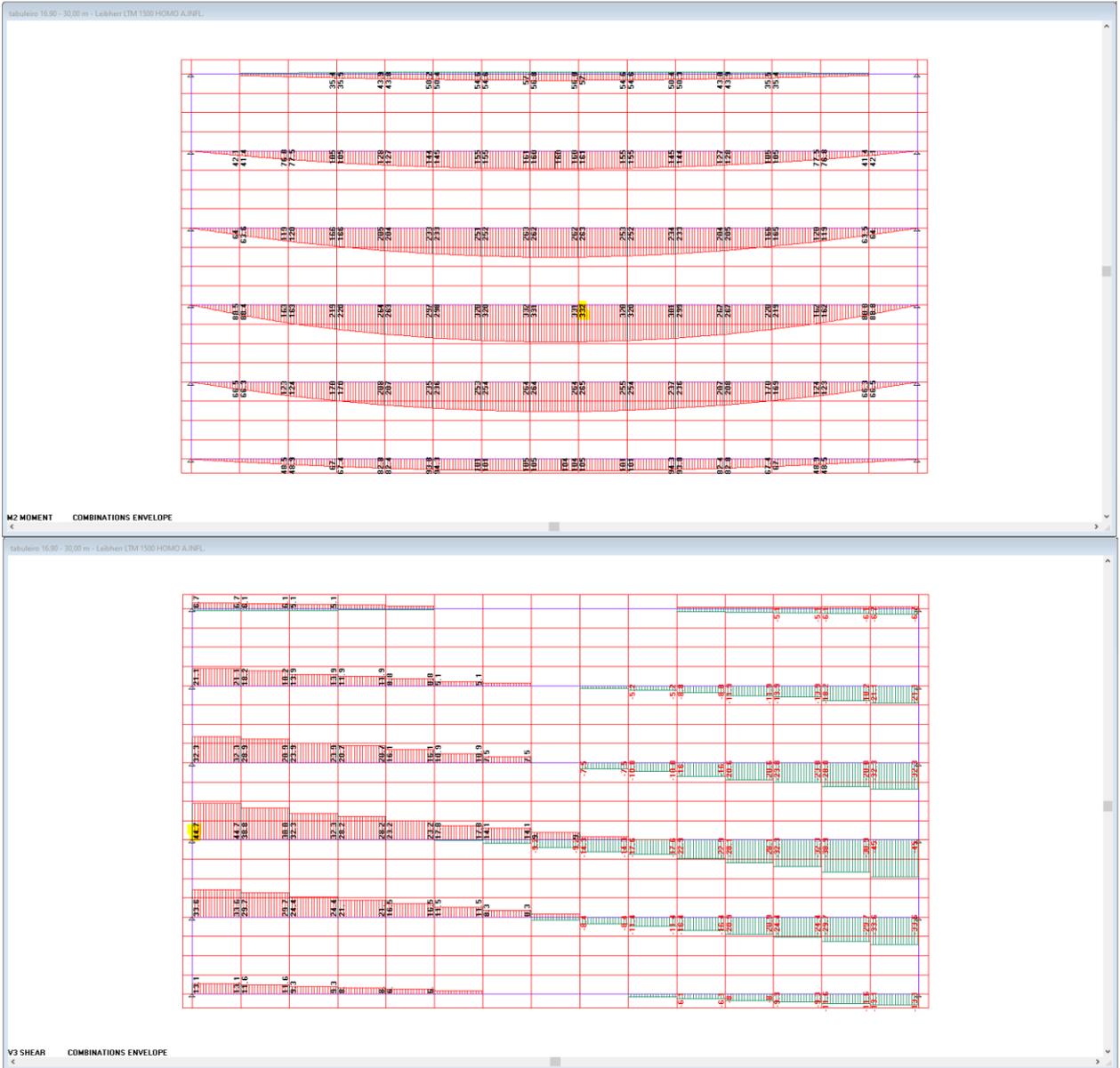


### NOTA TÉCNICA



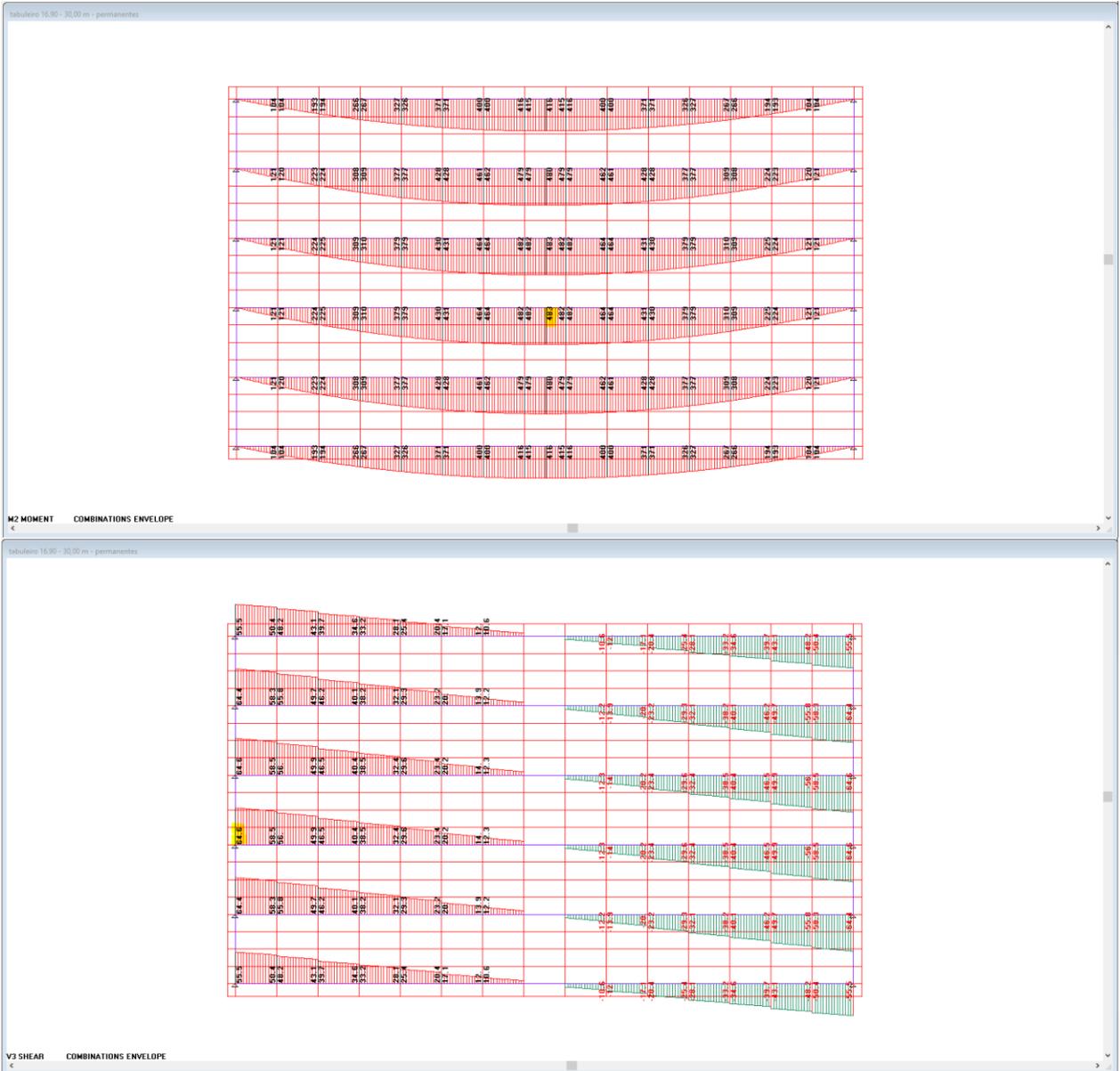


### NOTA TÉCNICA



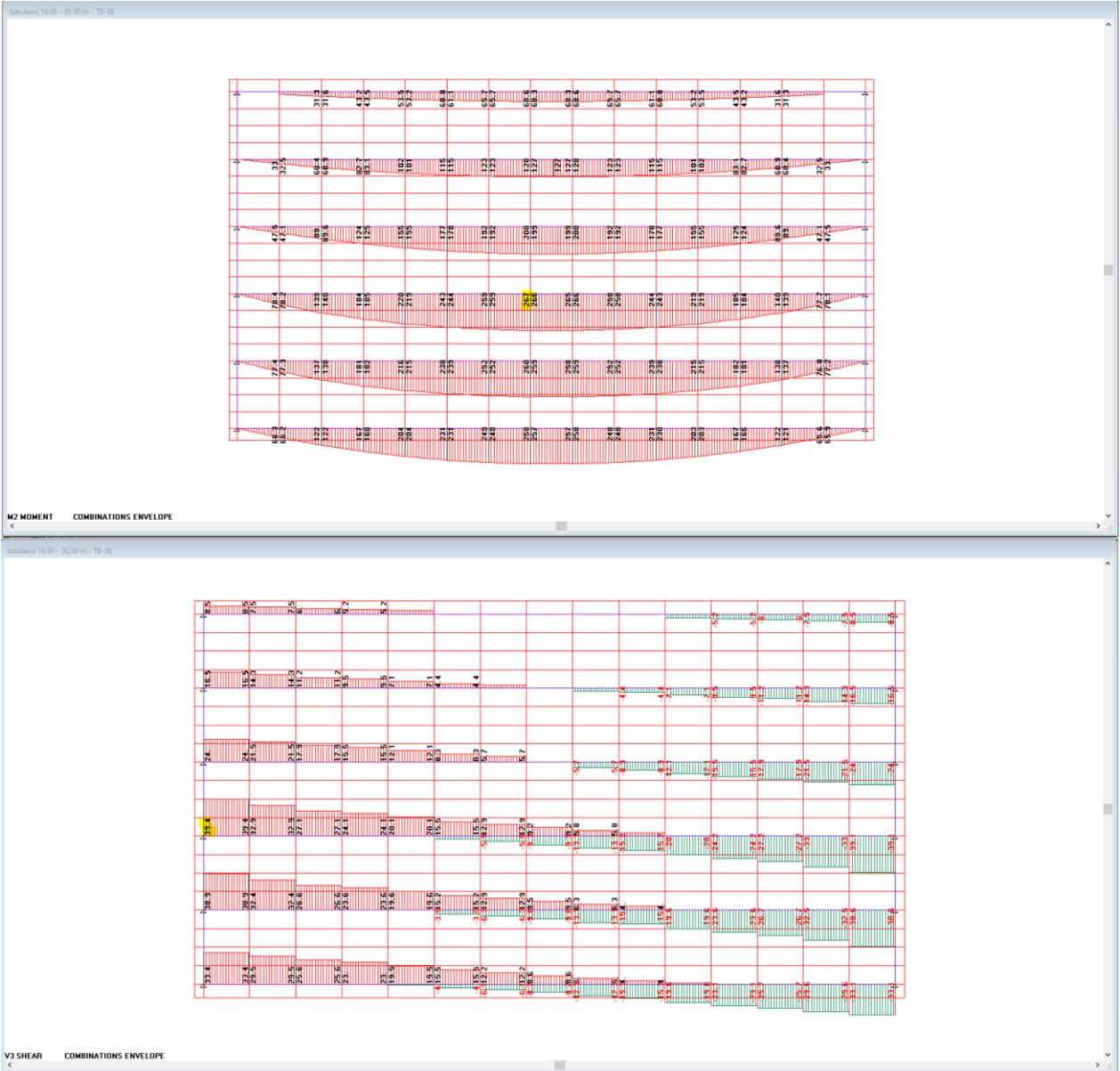


### NOTA TÉCNICA



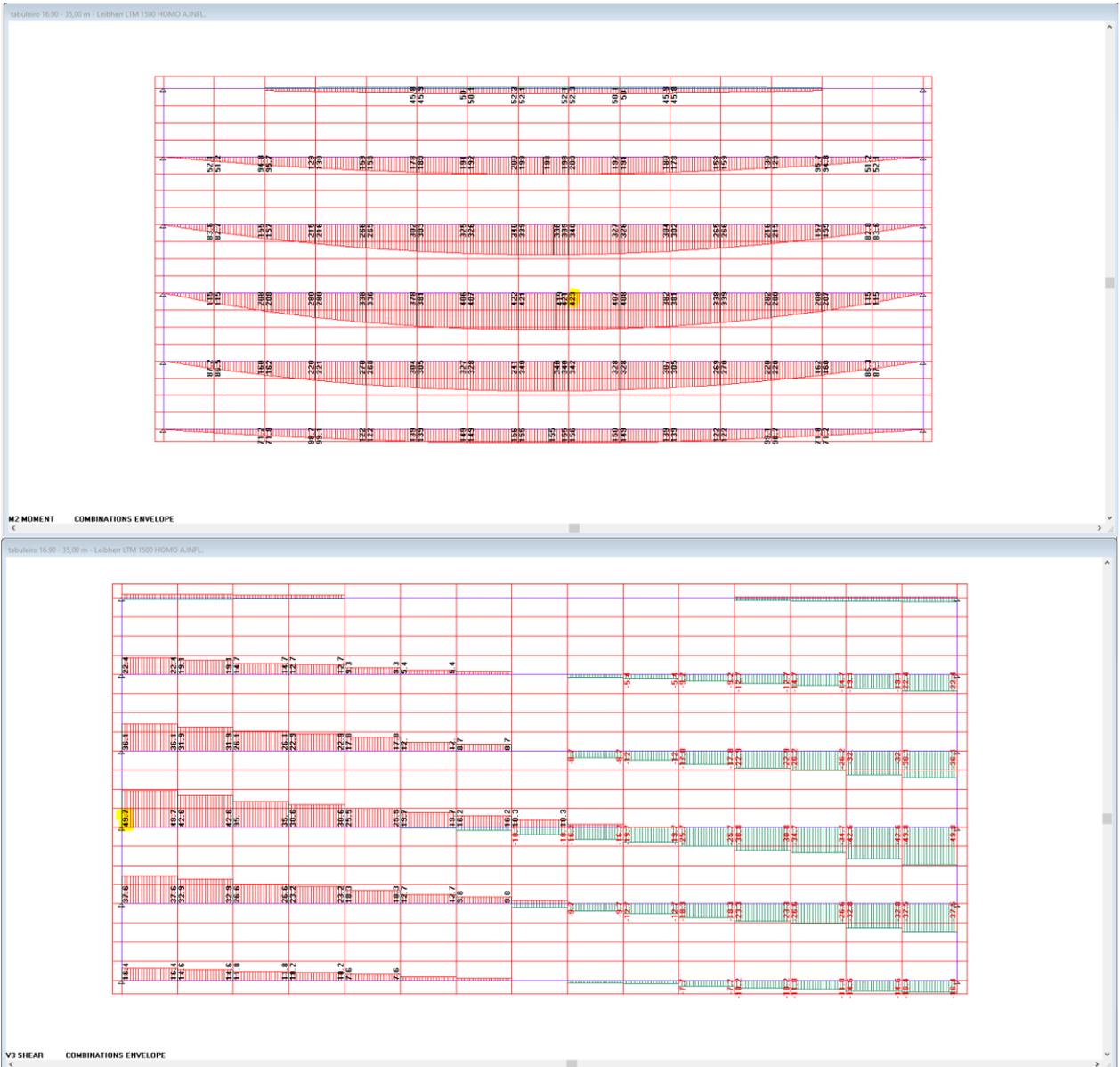


### NOTA TÉCNICA



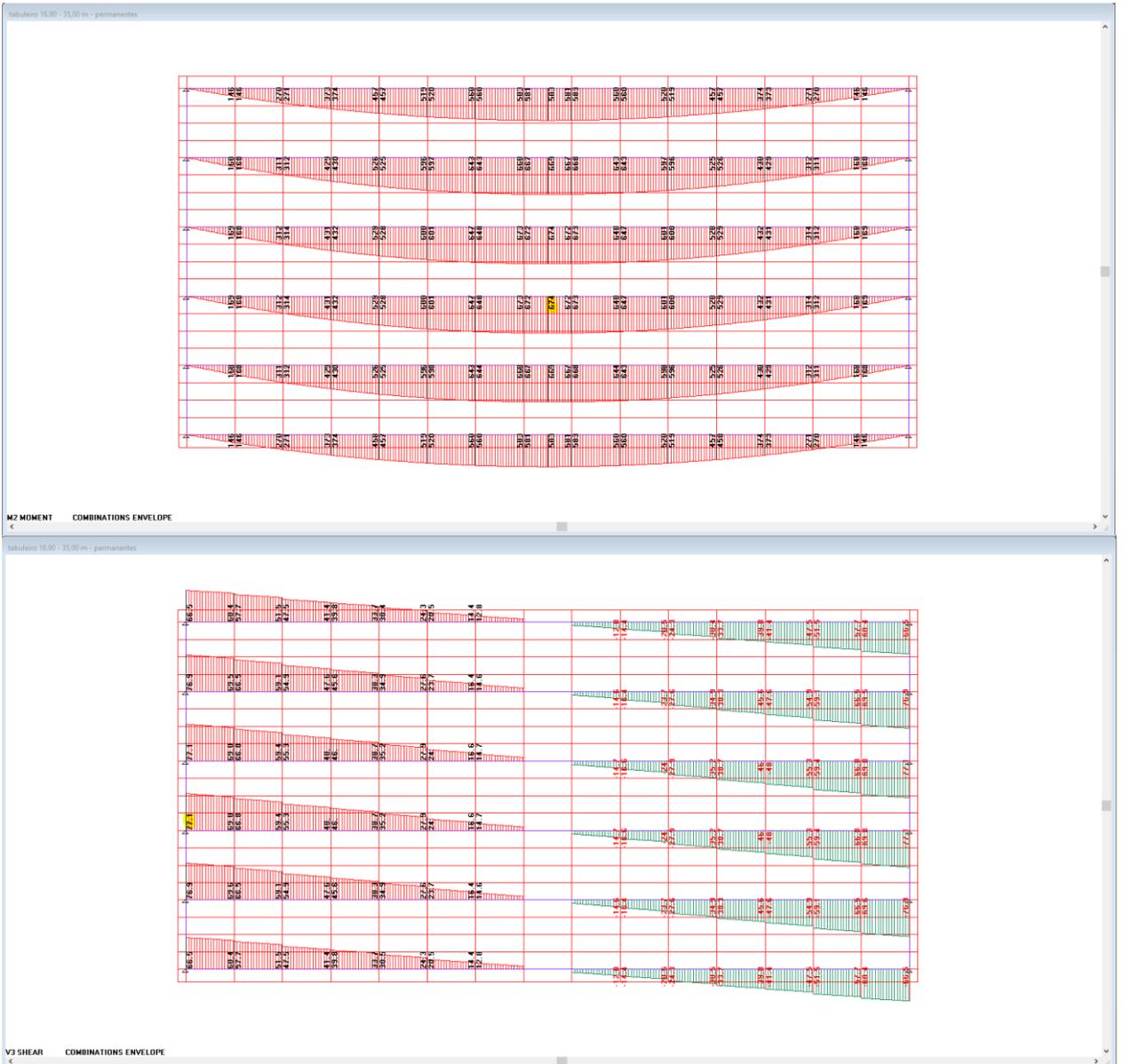


### NOTA TÉCNICA



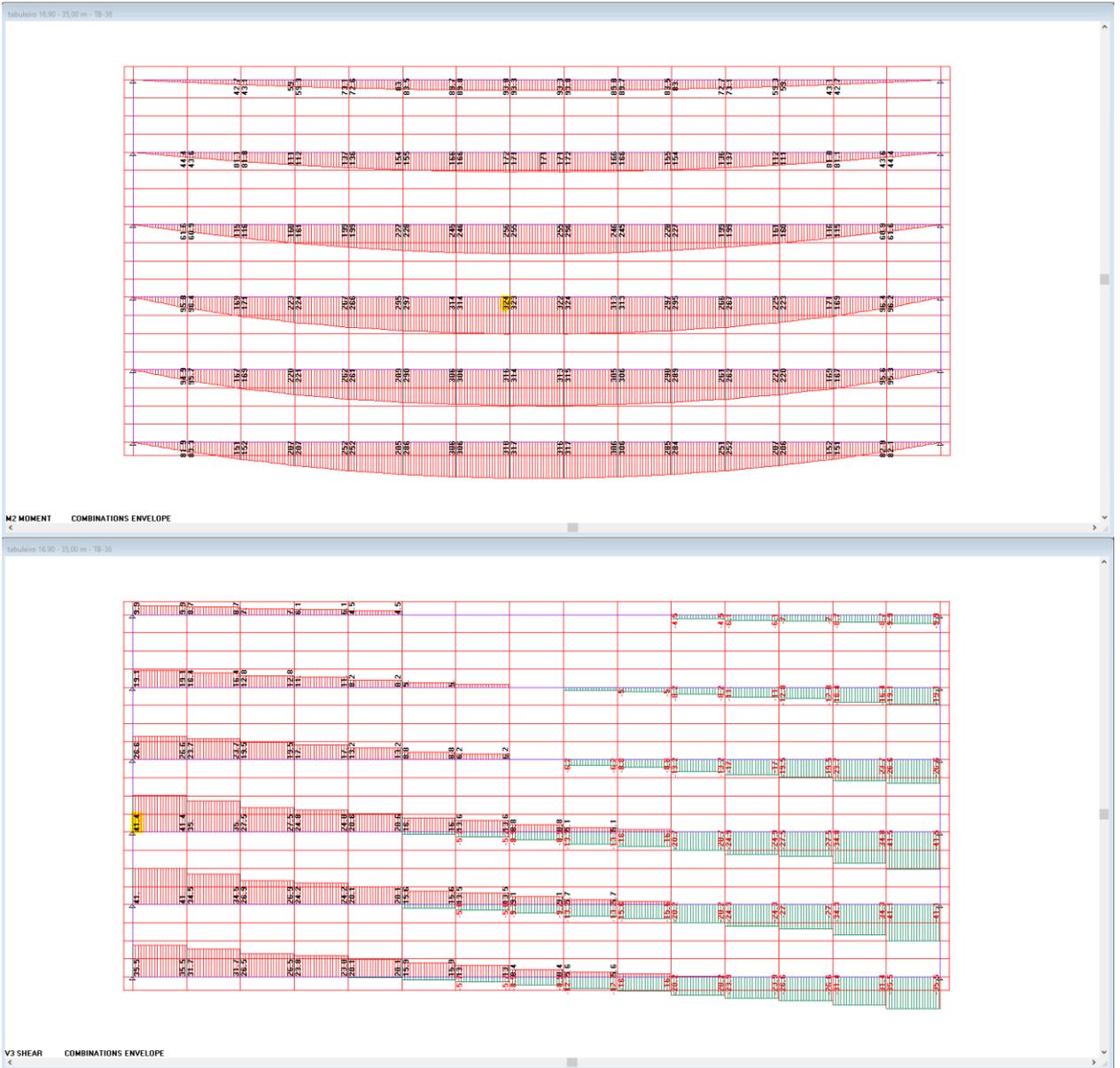


### NOTA TÉCNICA



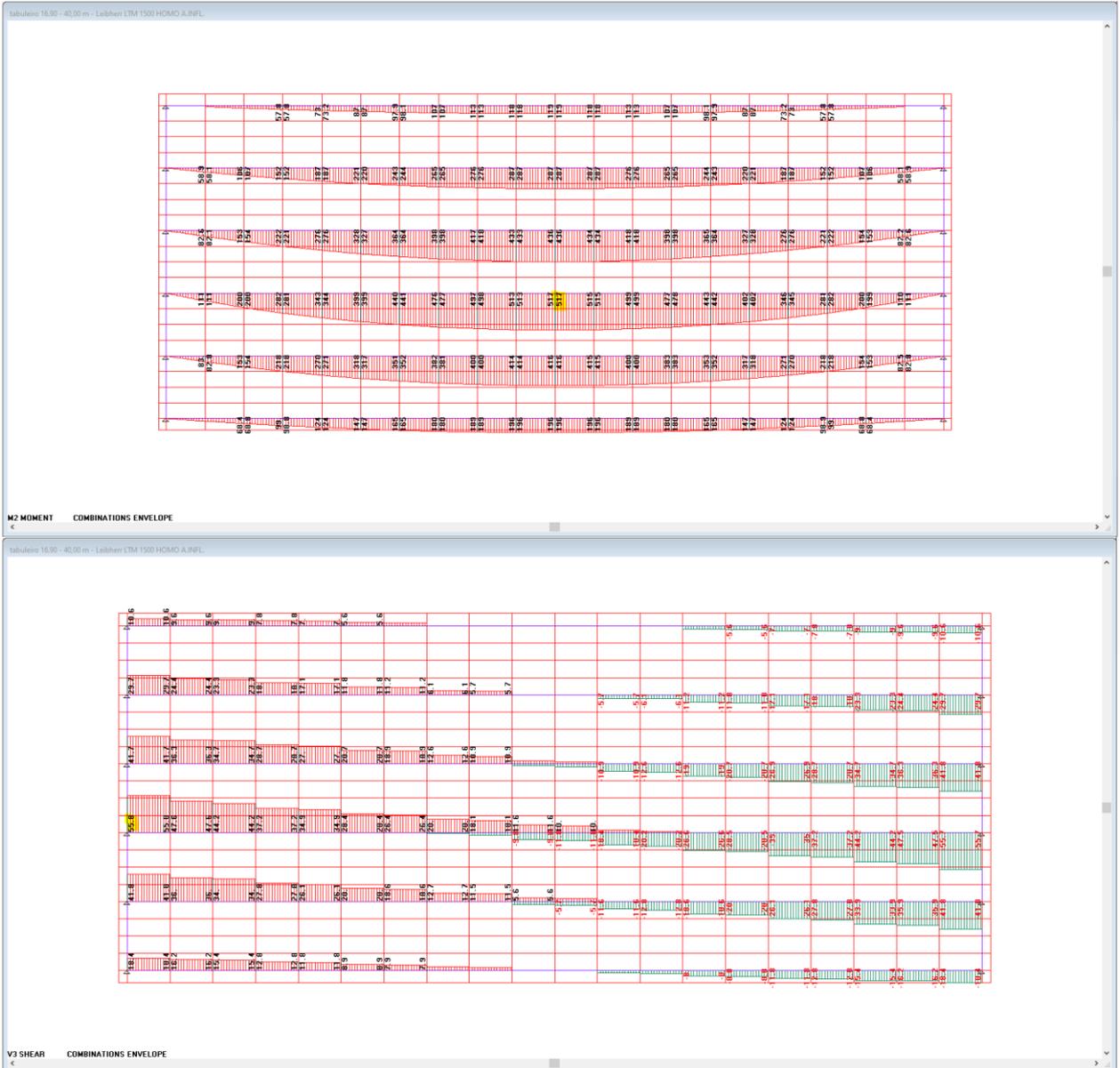


### NOTA TÉCNICA



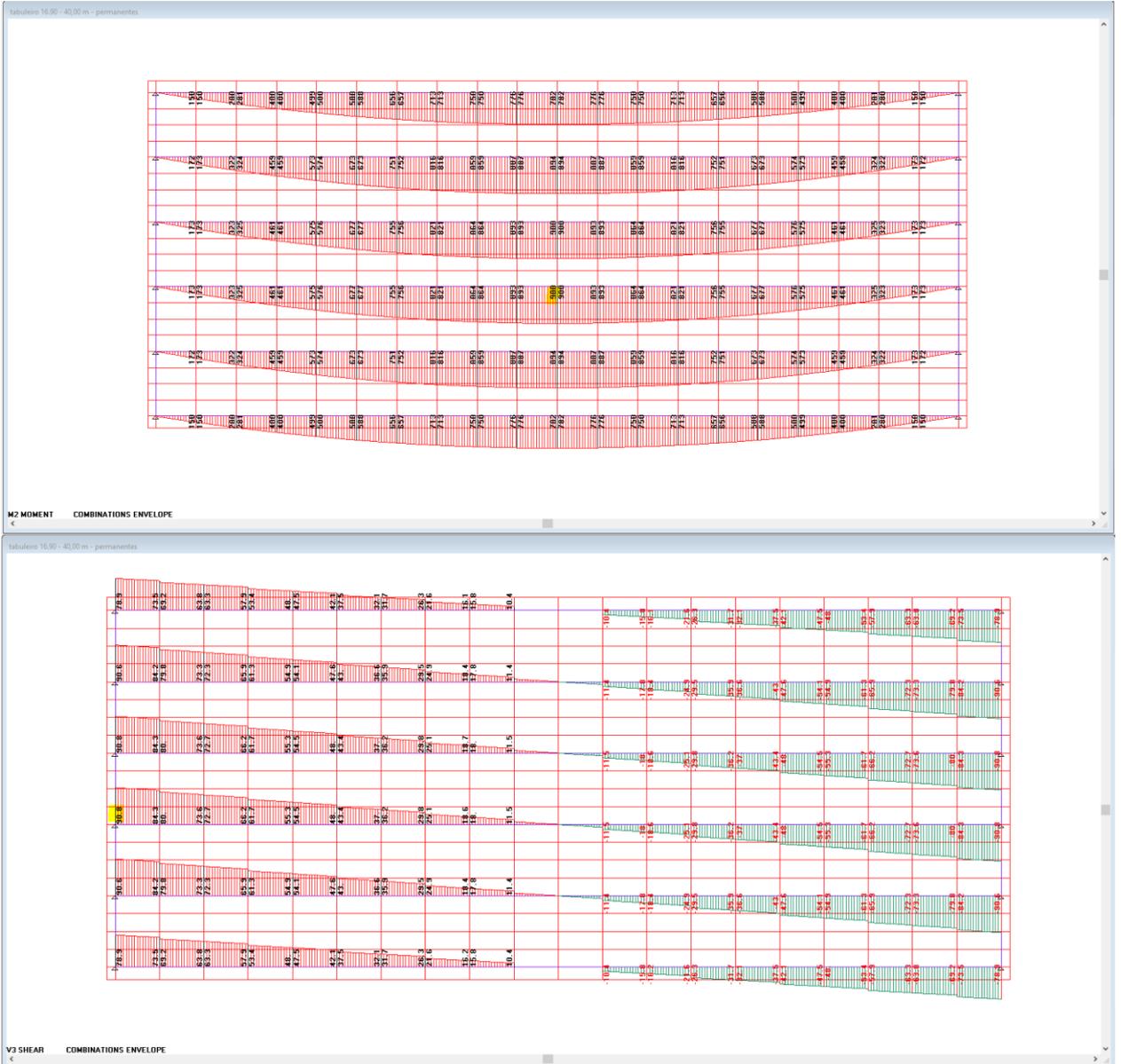


### NOTA TÉCNICA



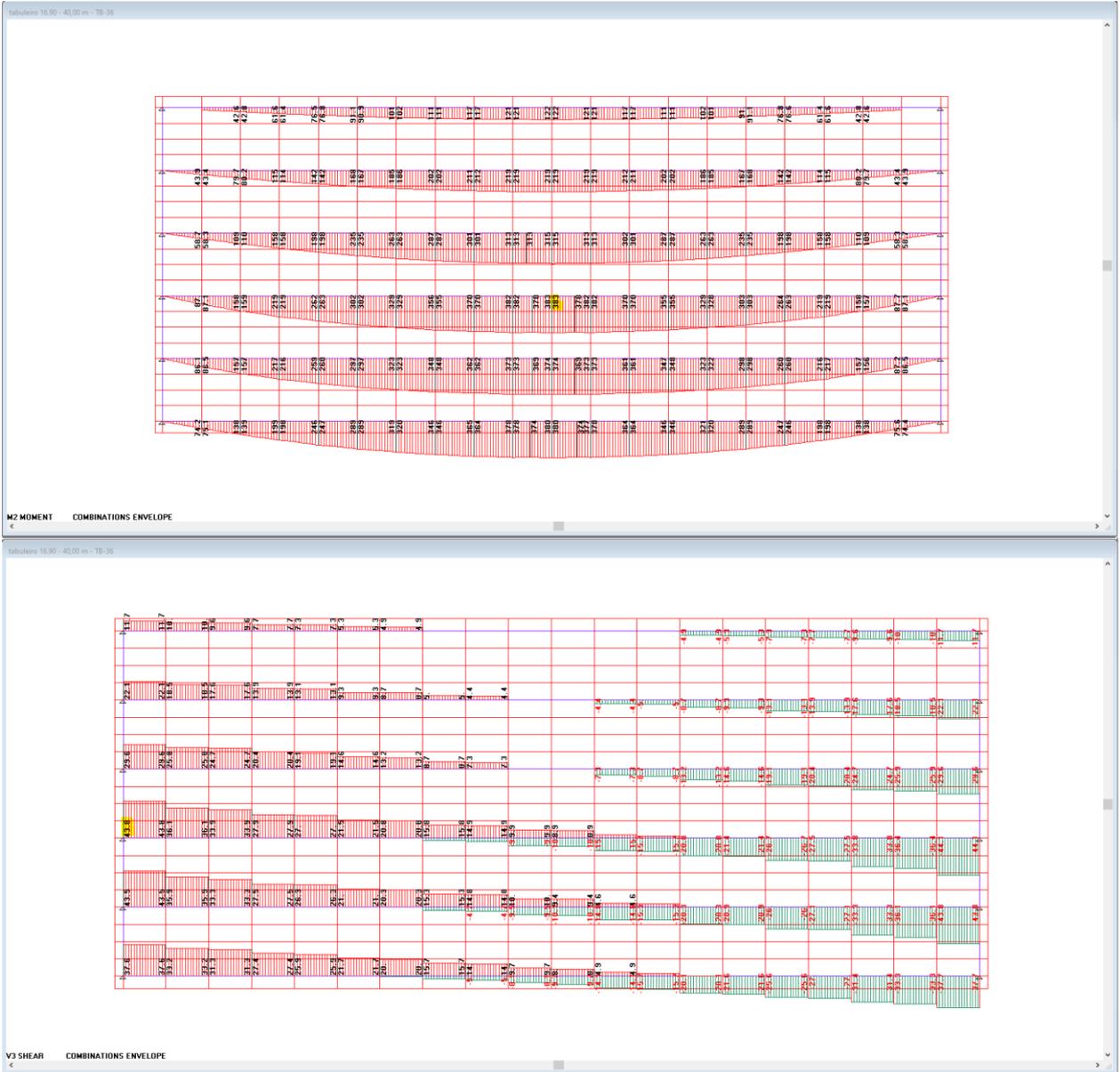


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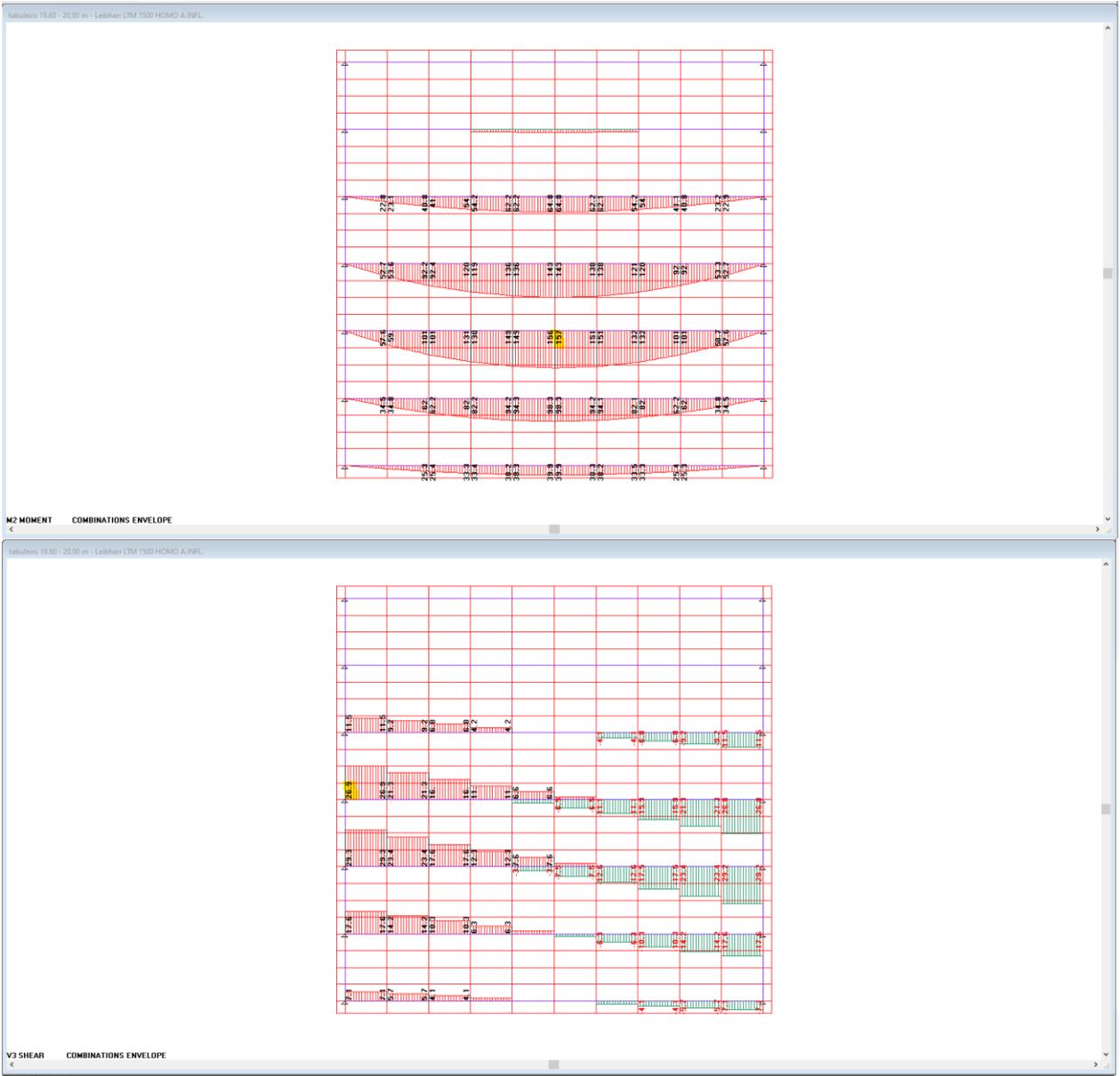
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### NOTA TÉCNICA

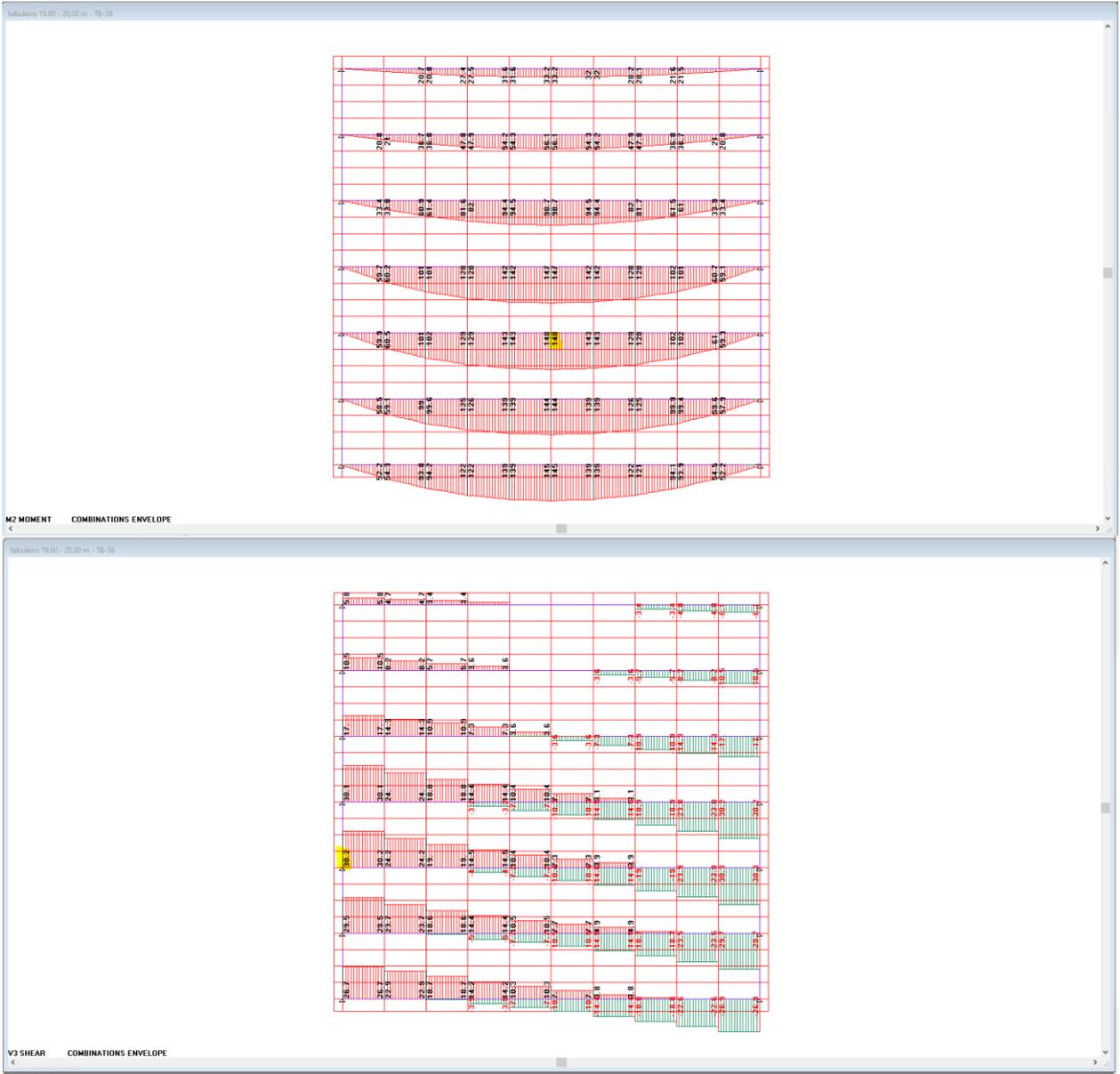
#### 4.6.6. Tabuleiro 19,60 m





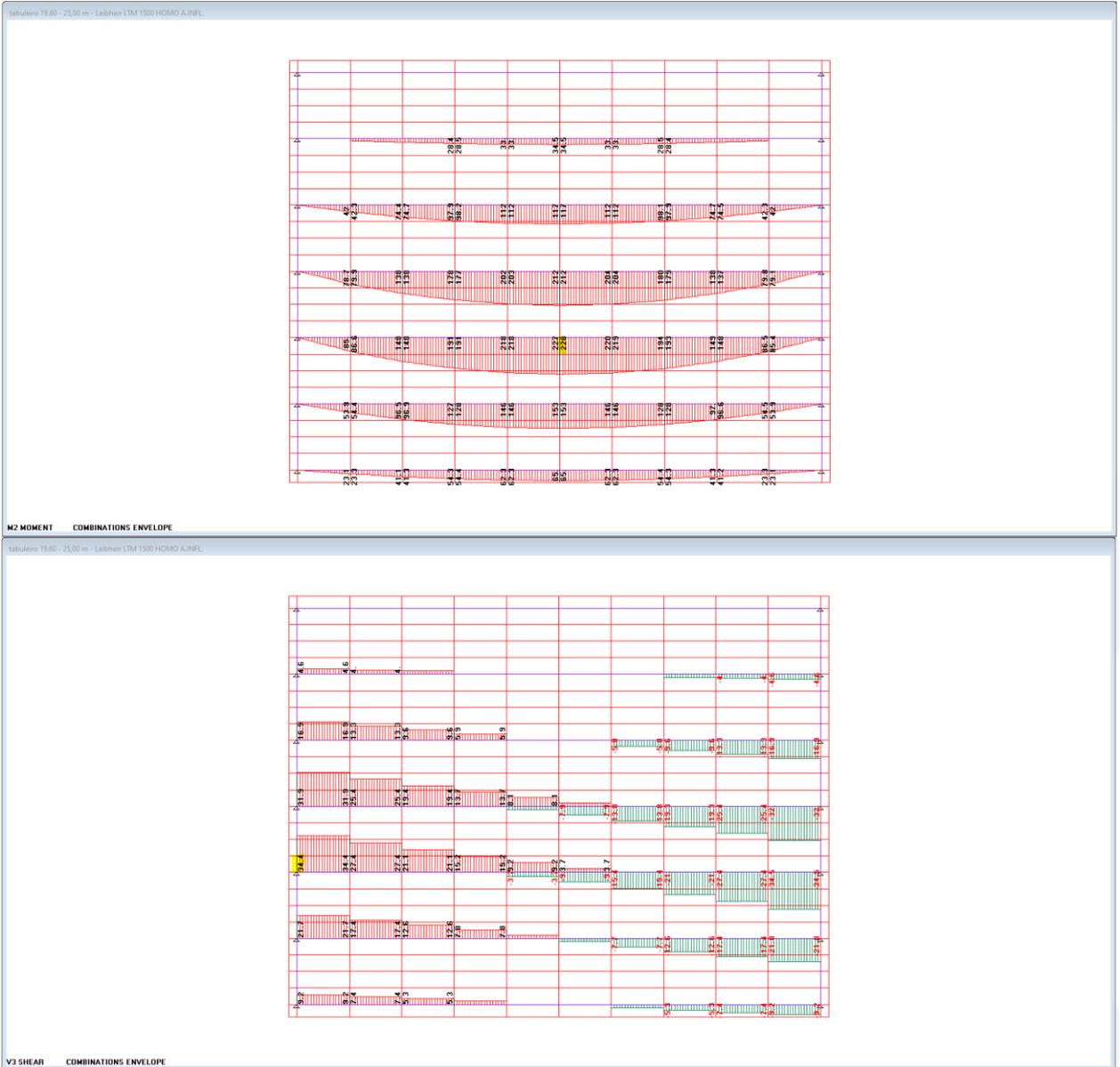


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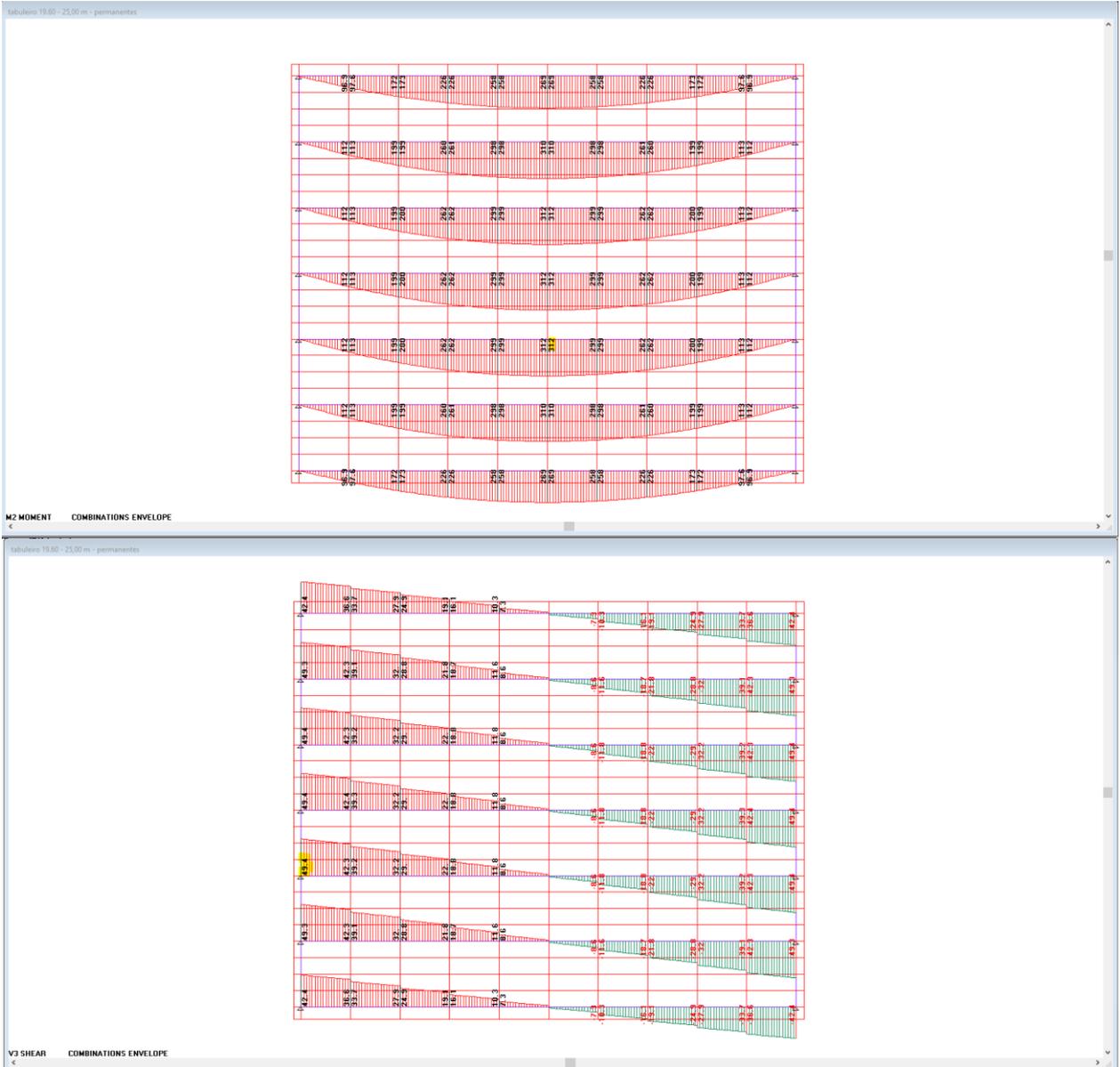


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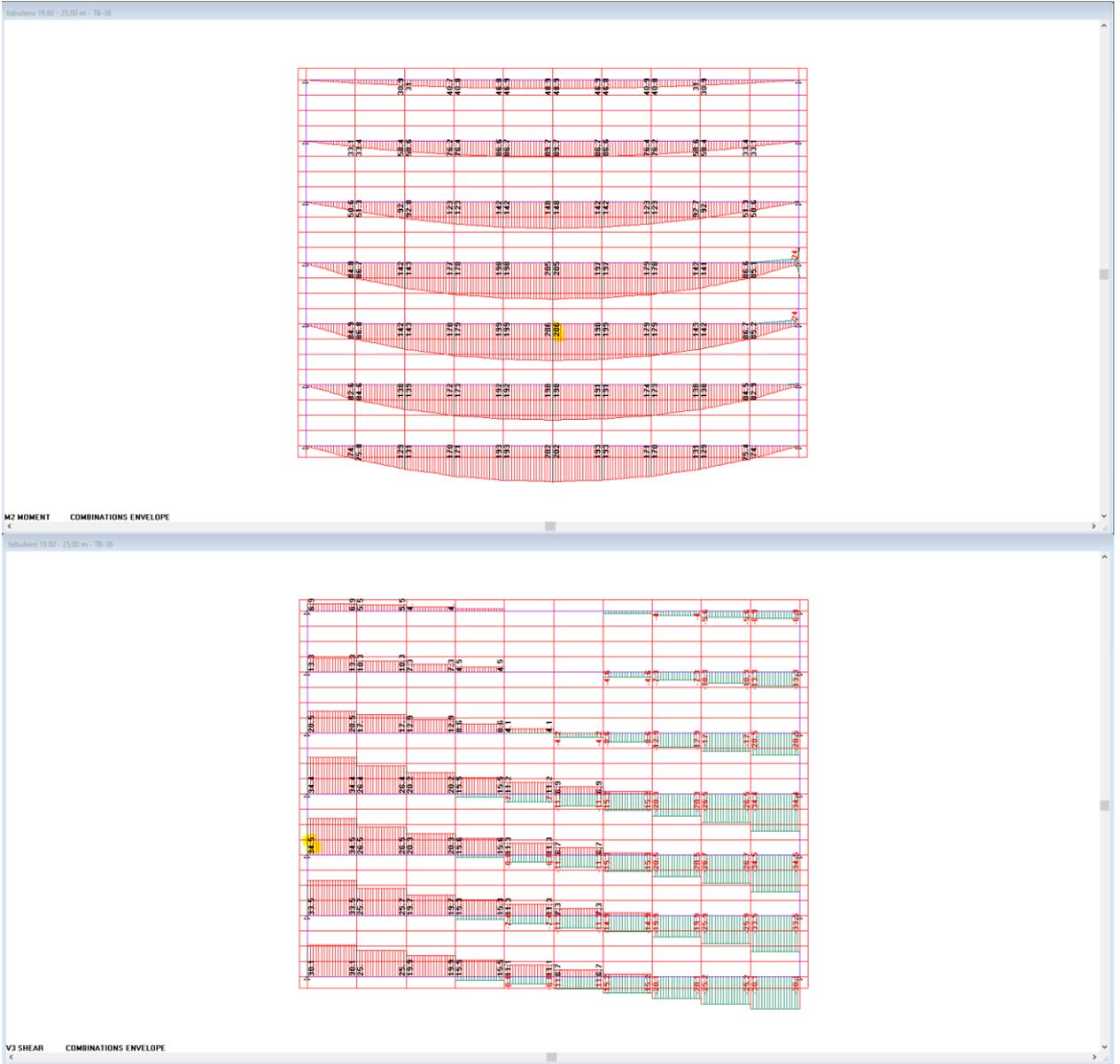


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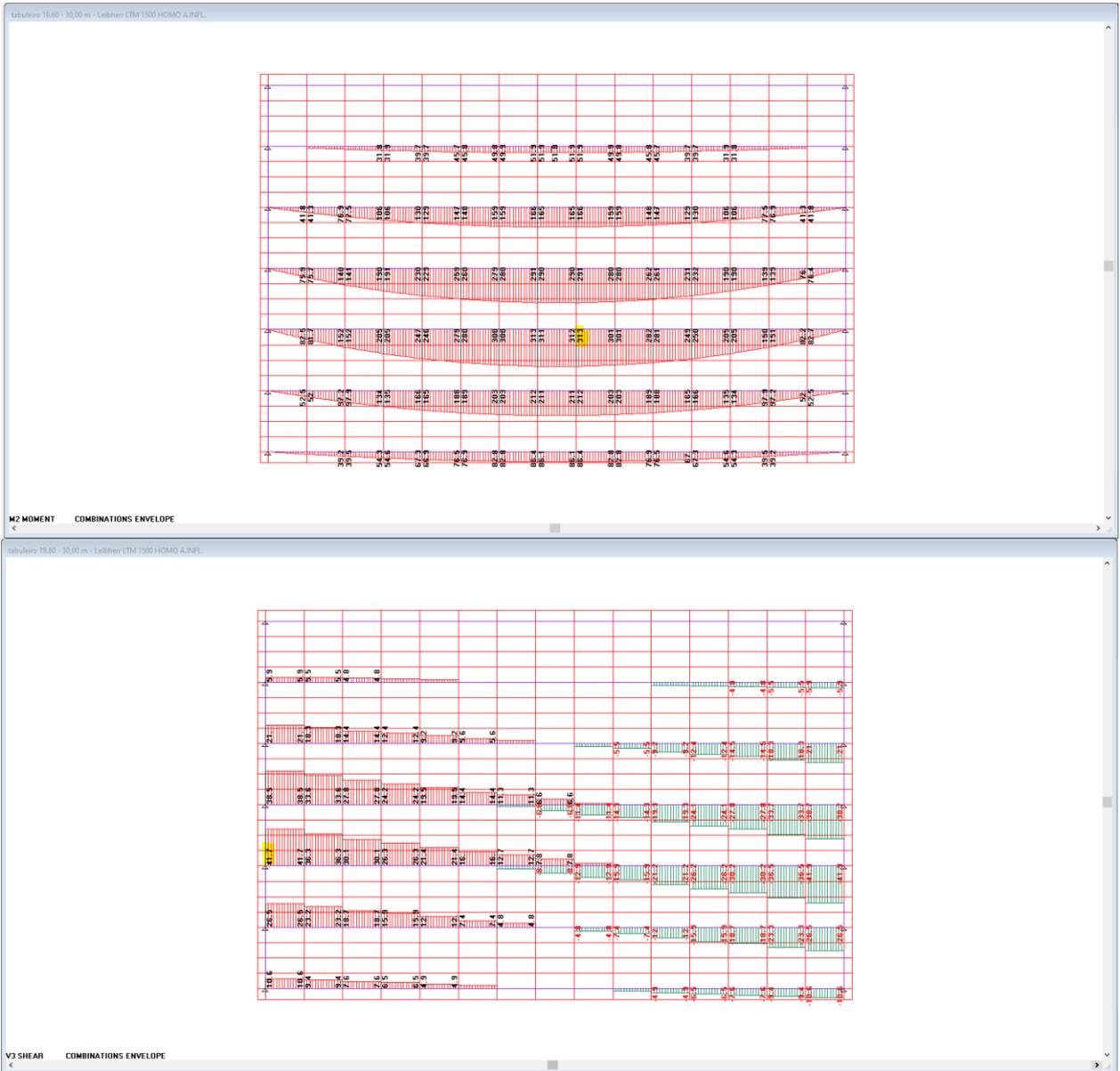


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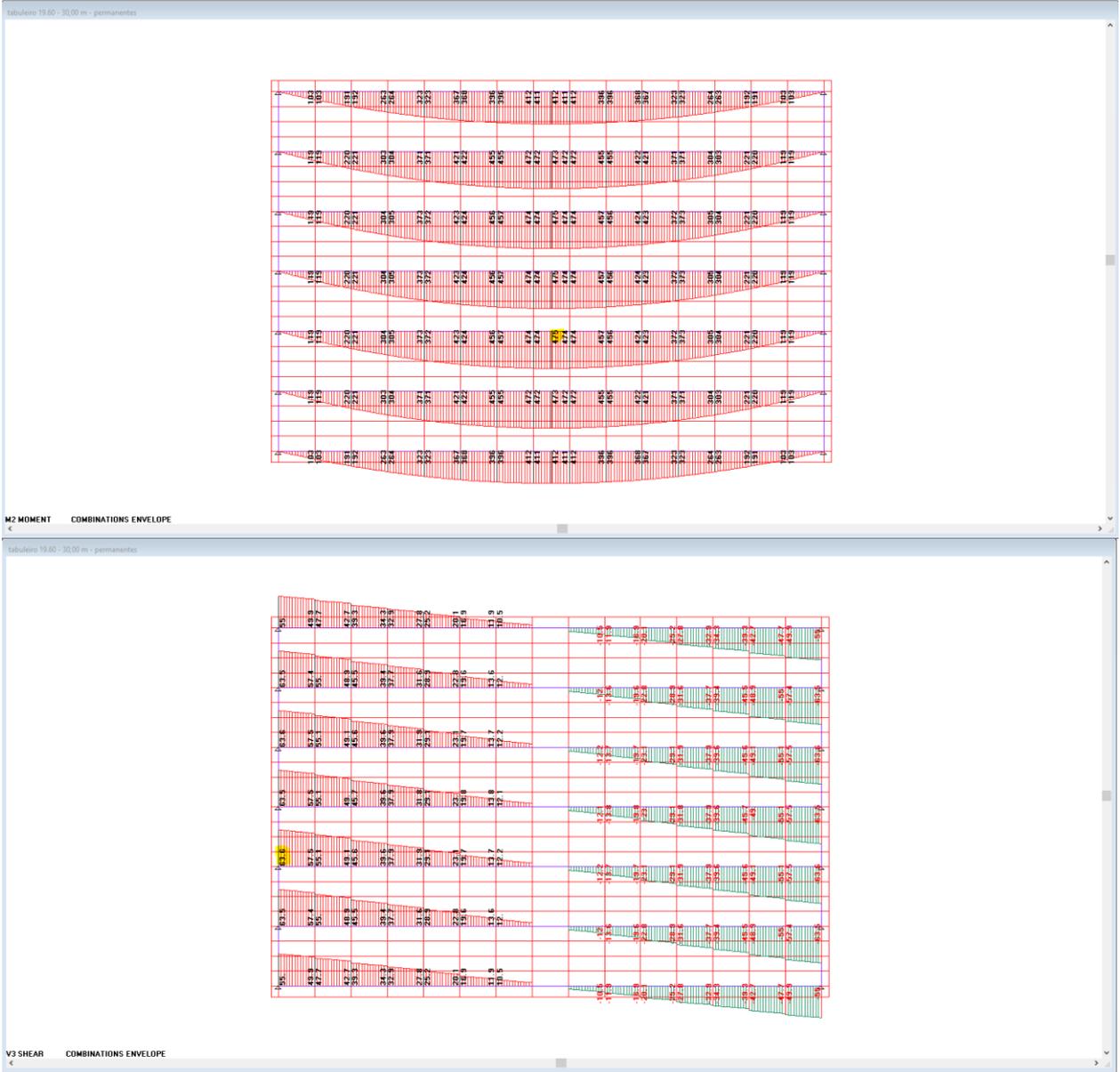


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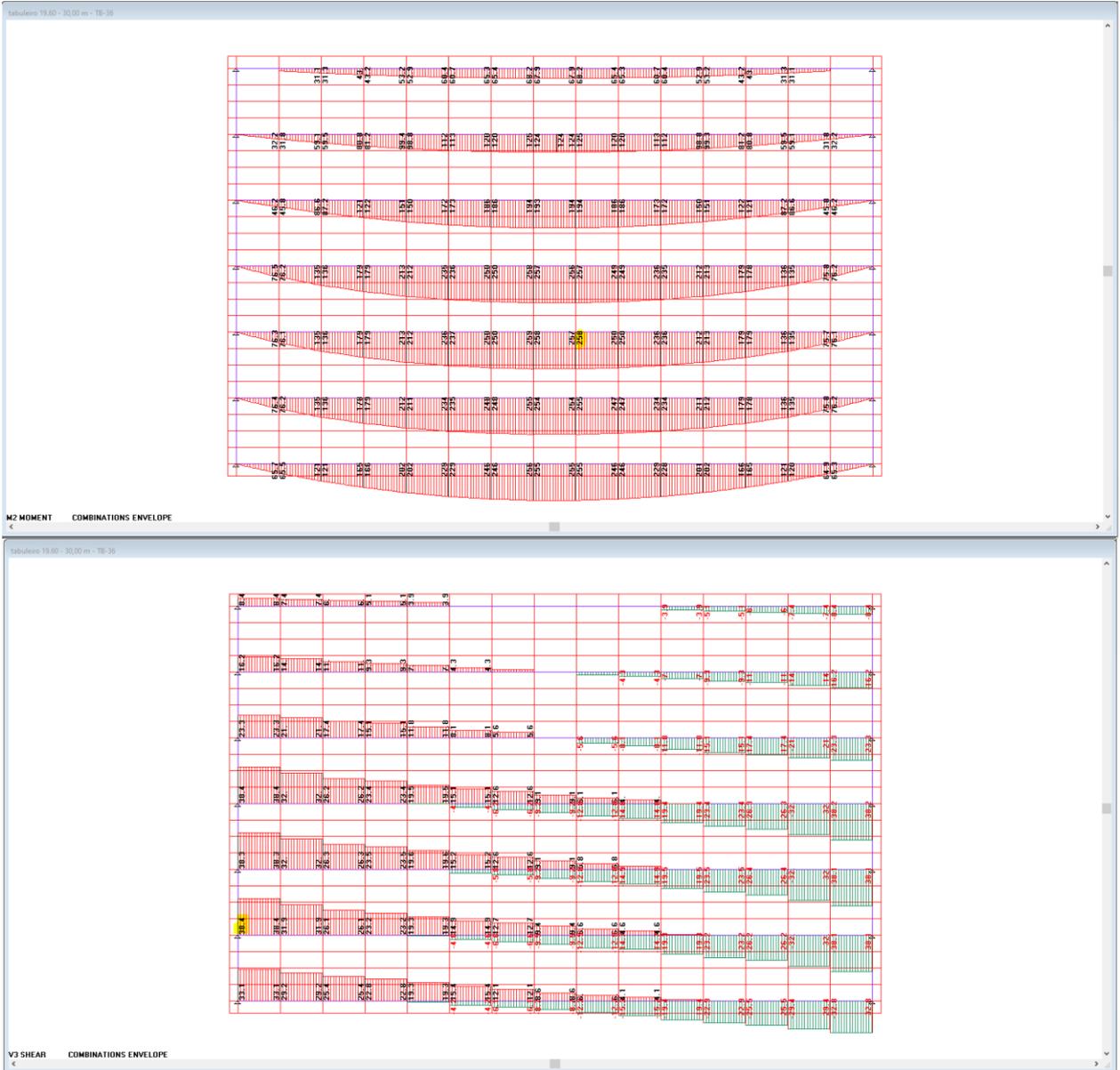


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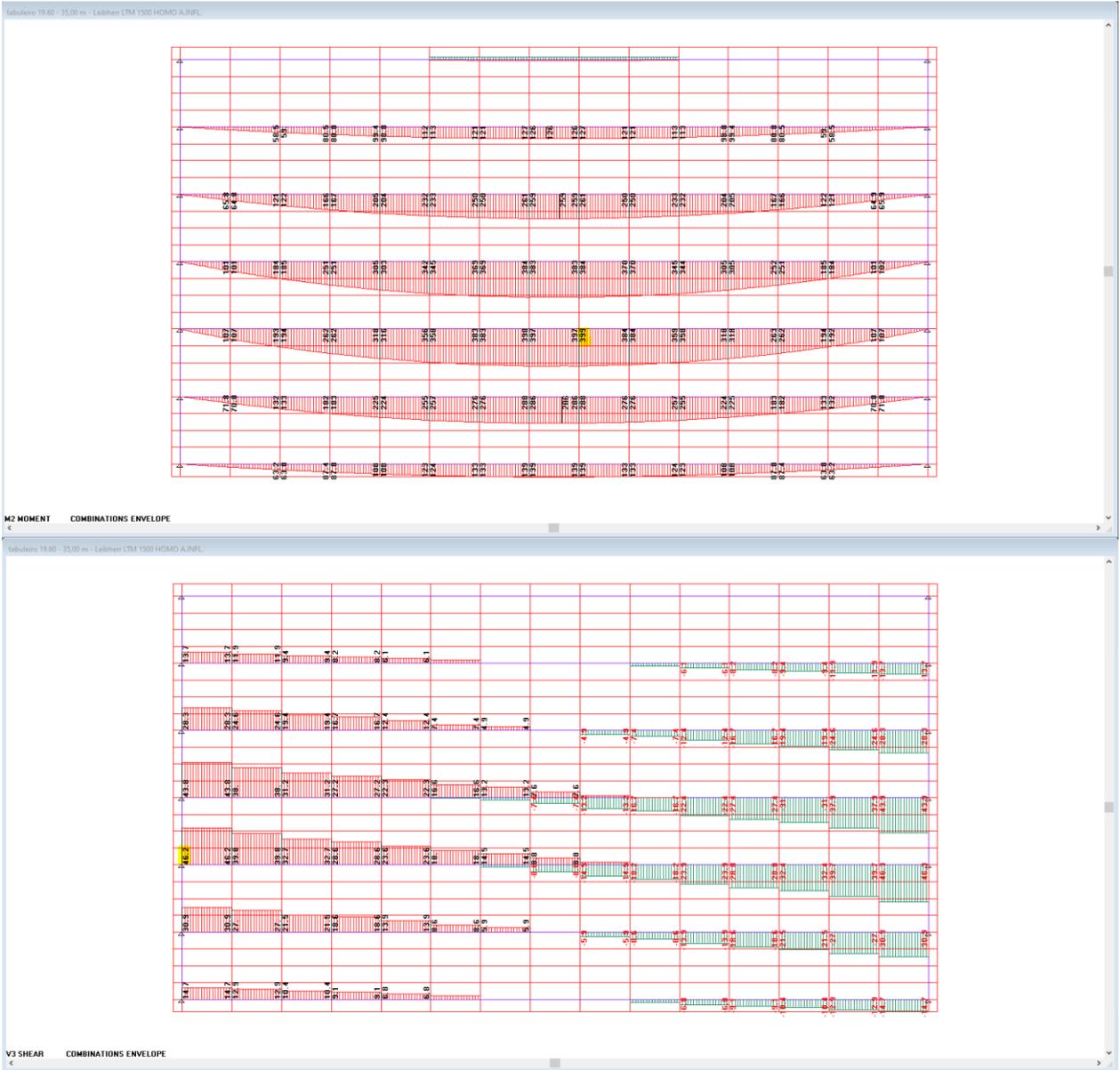


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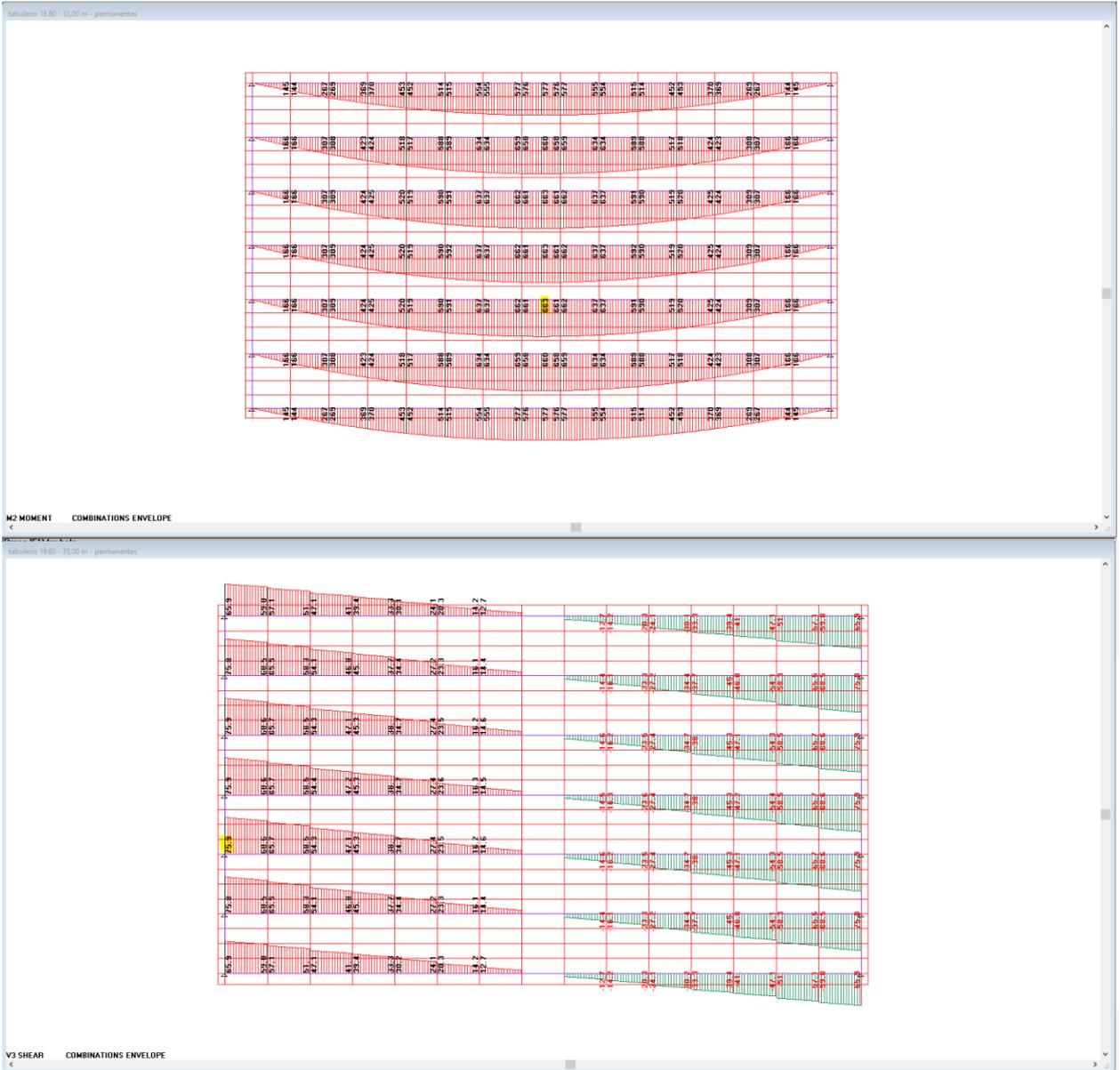


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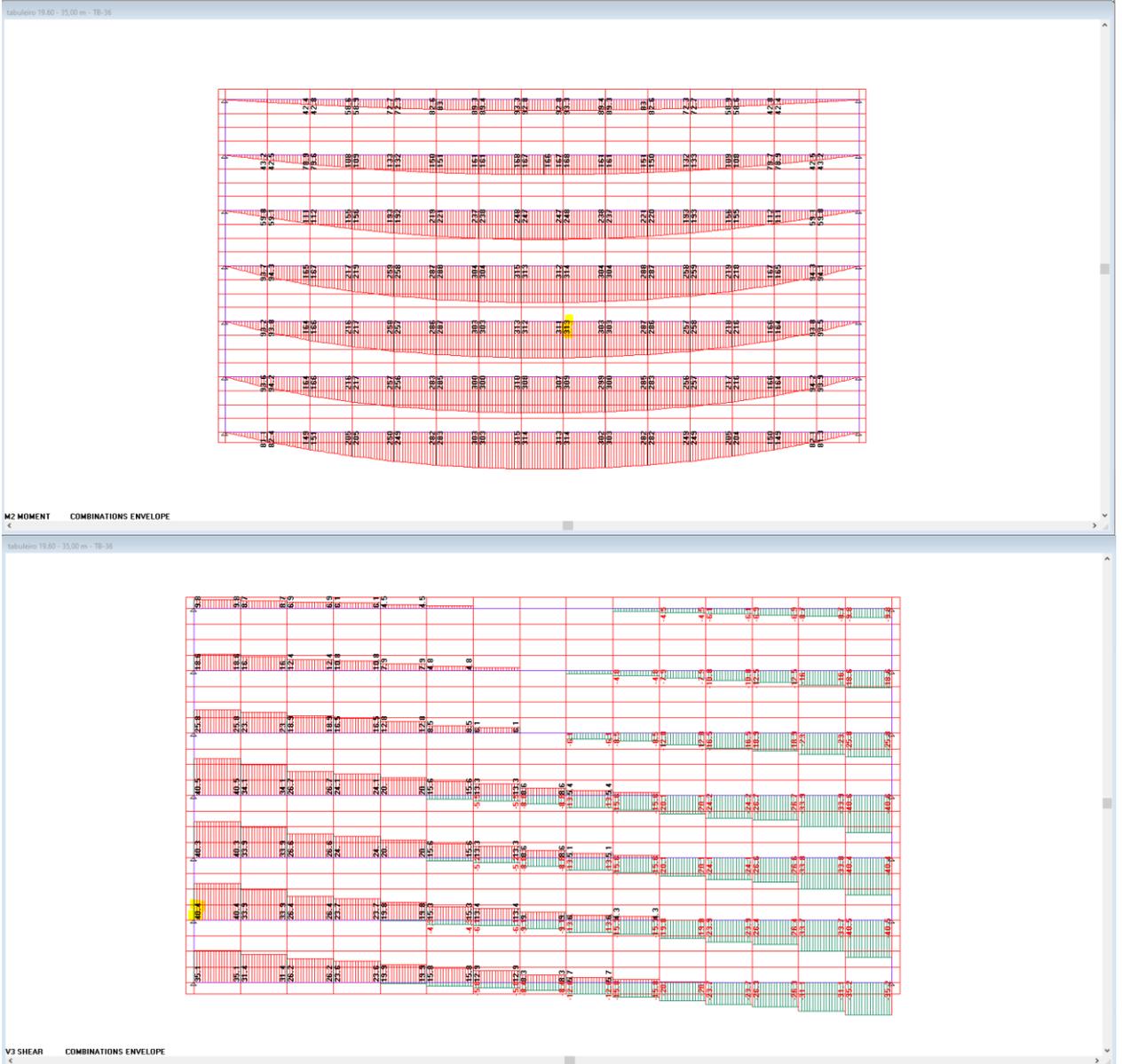


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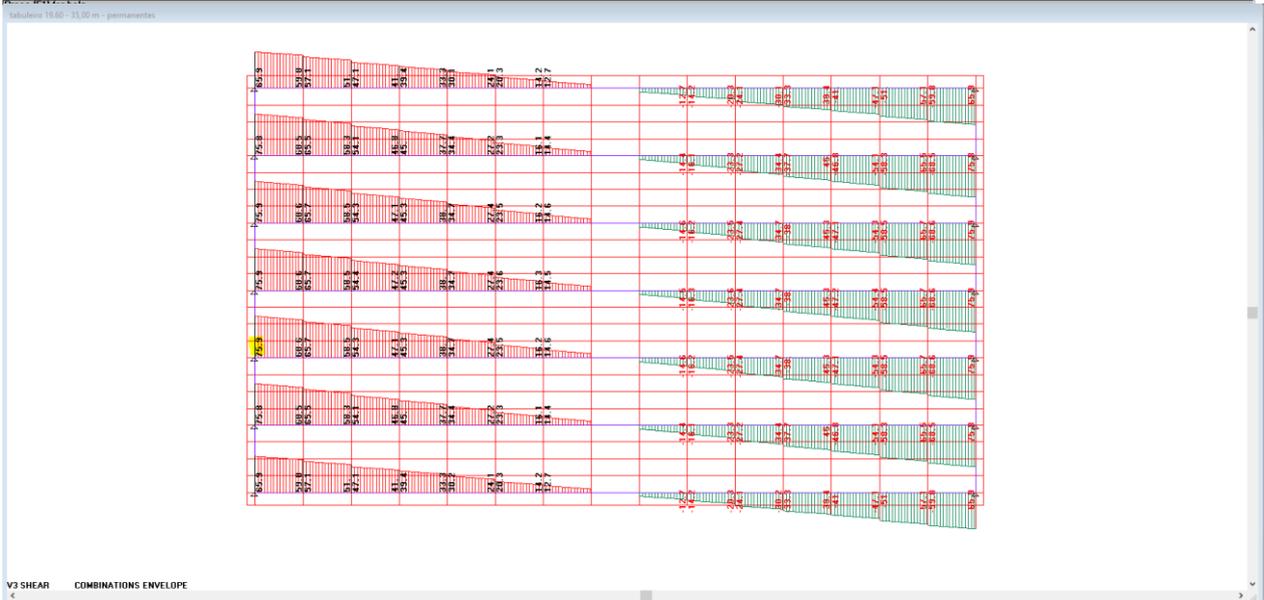
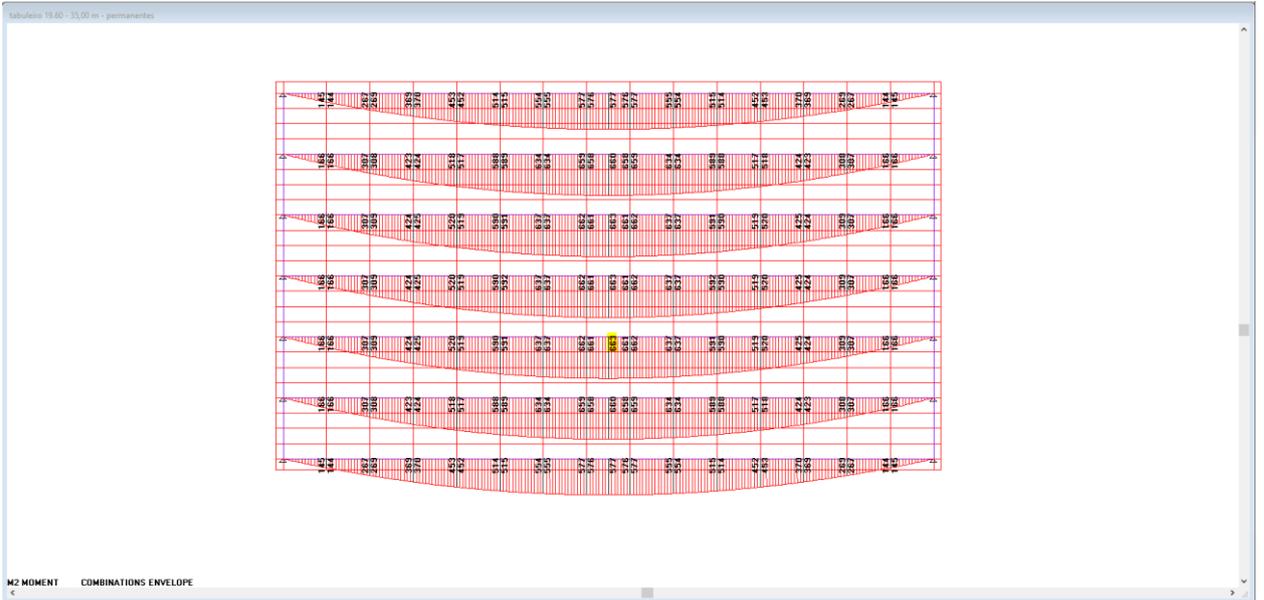


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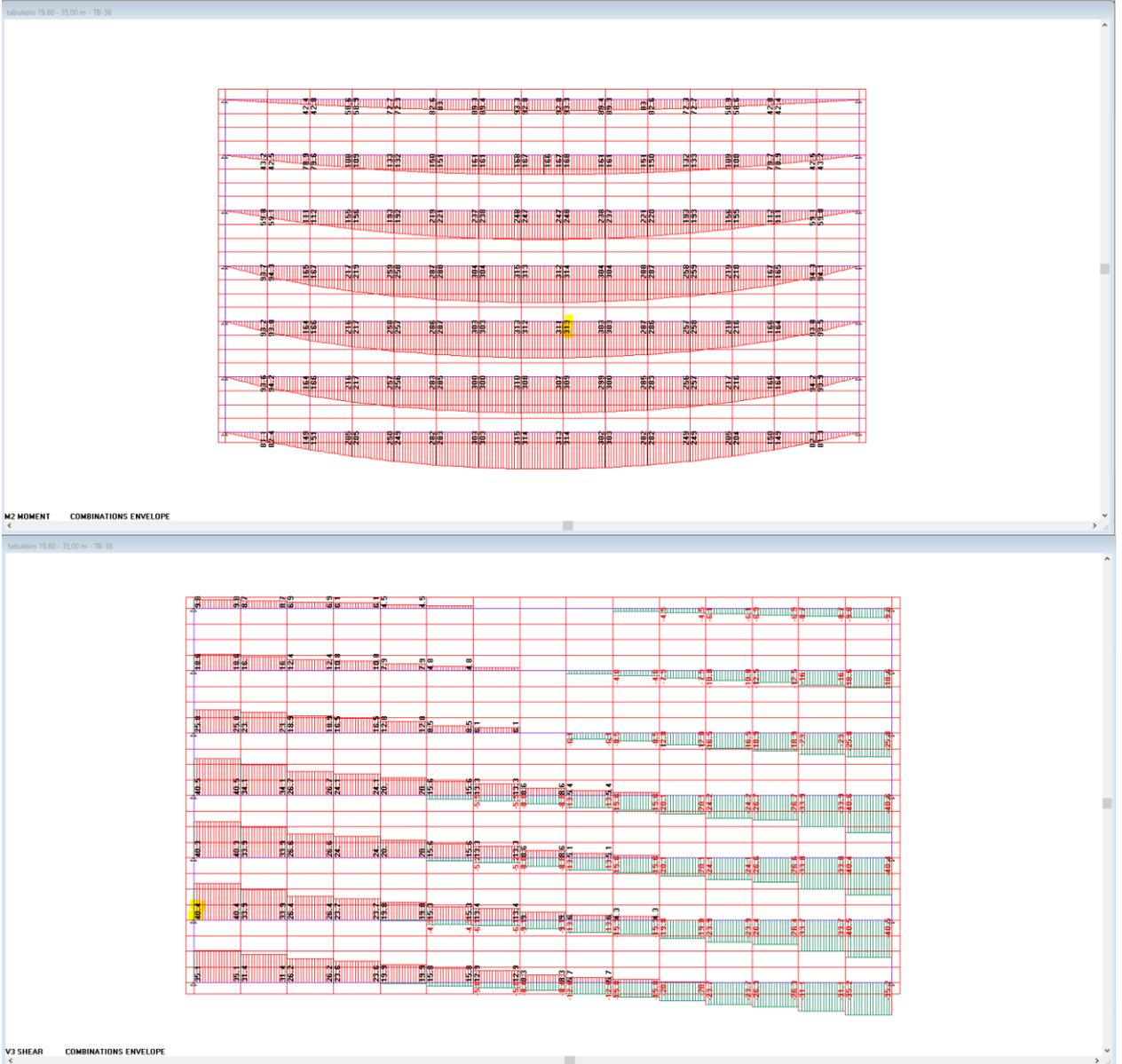


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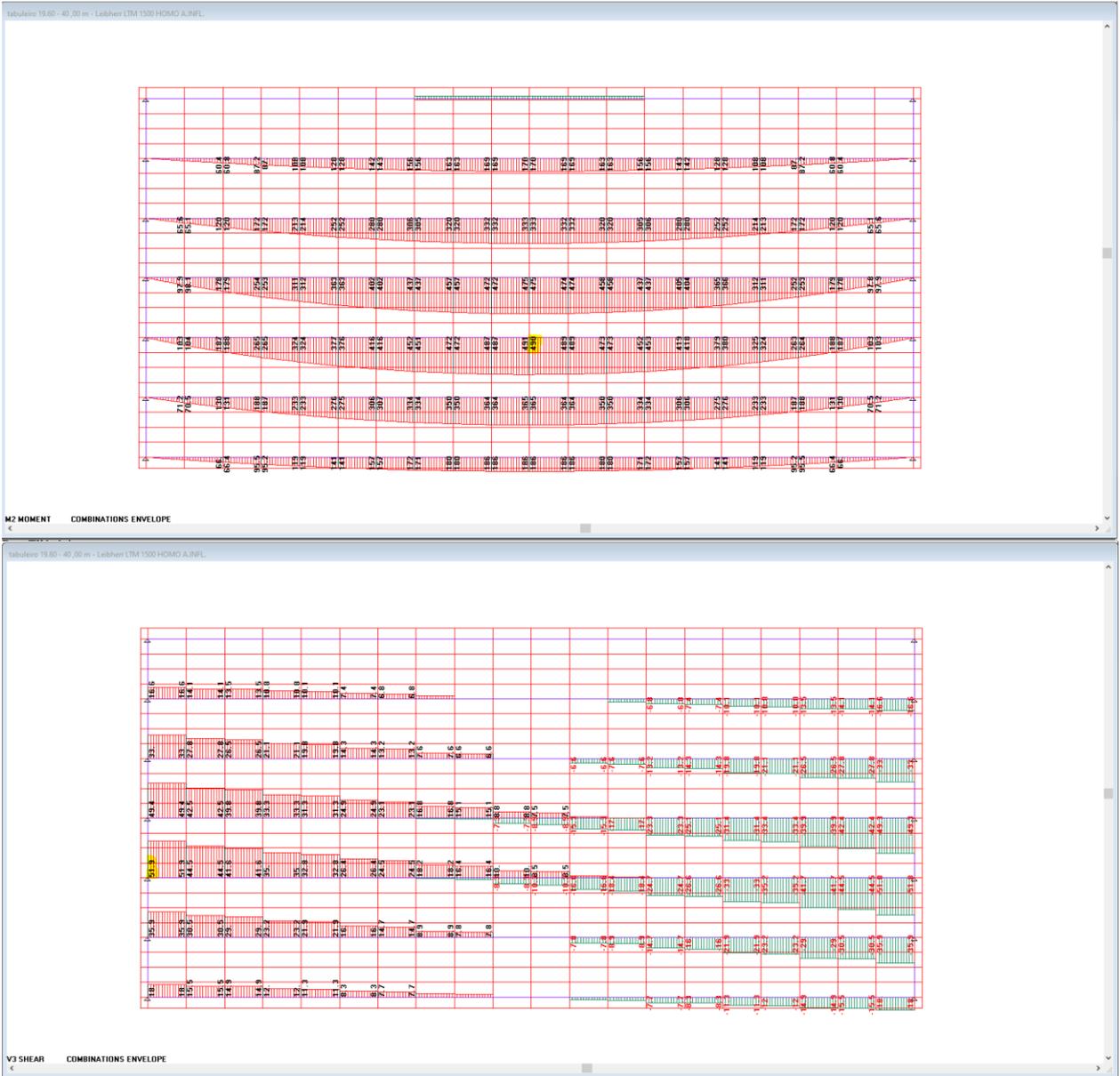


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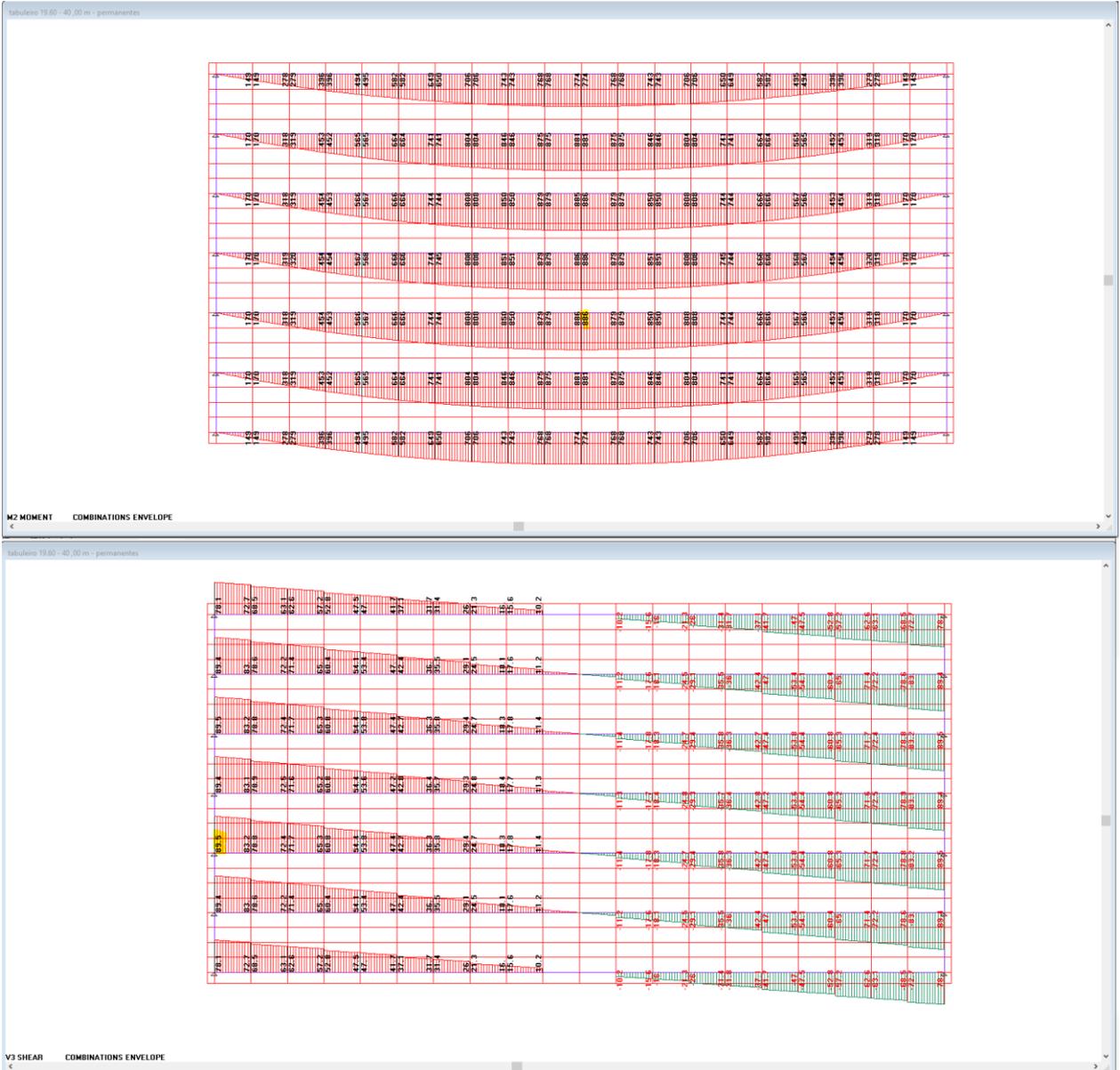


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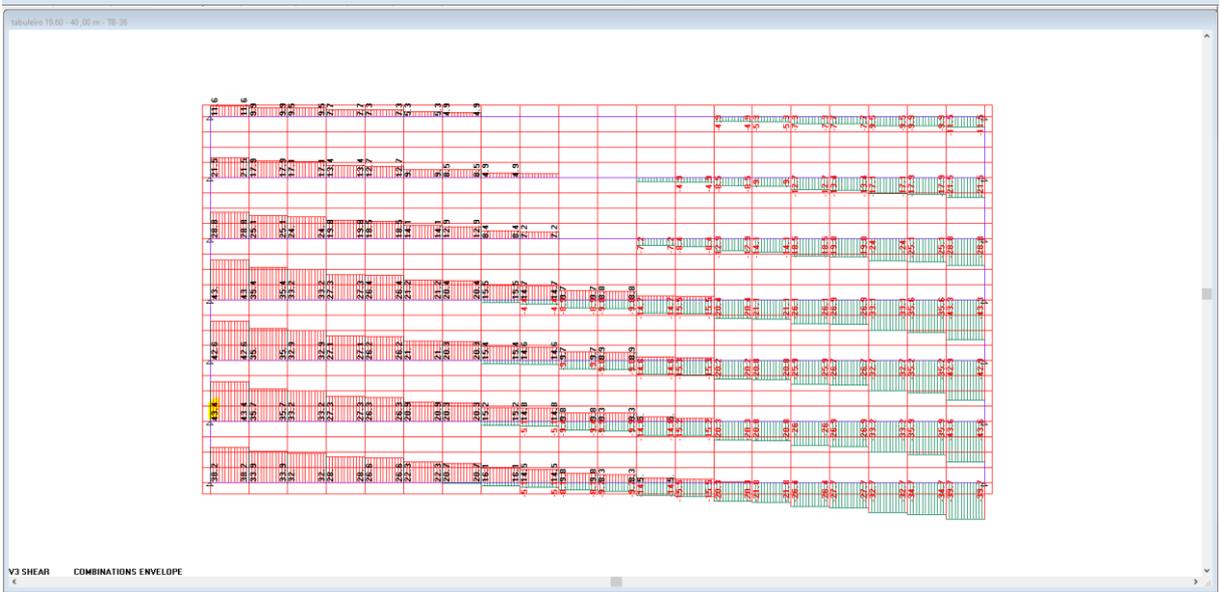
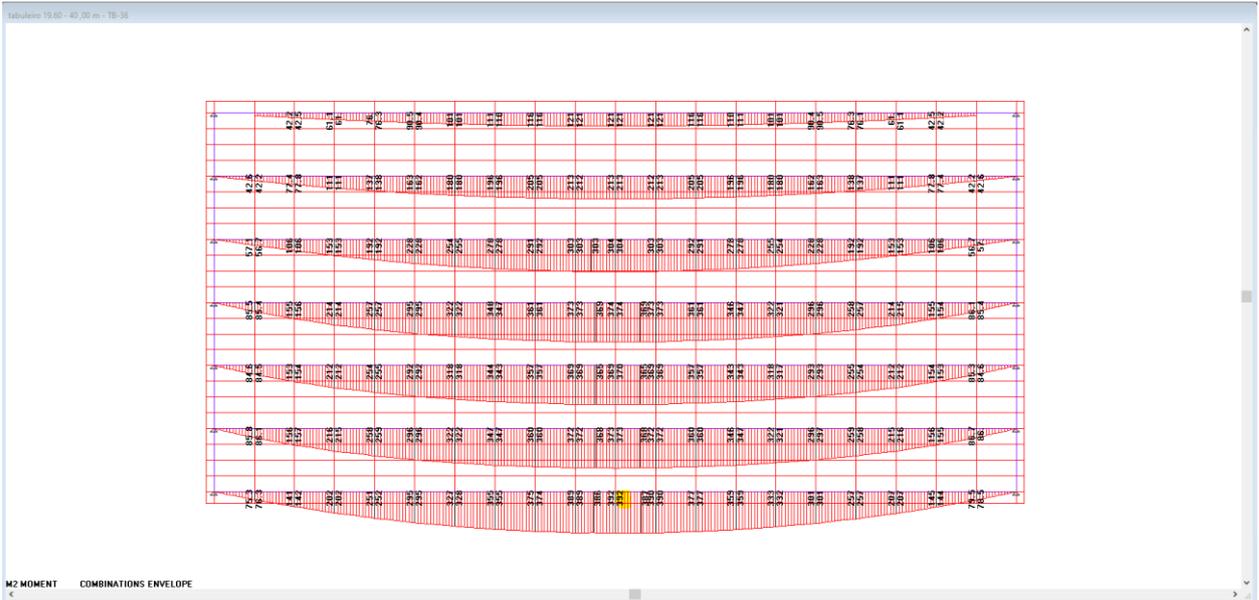


### NOTA TÉCNICA





### NOTA TÉCNICA





## NOTA TÉCNICA

### 4.7. Resultados

#### 4.7.1. Cálculo do CS (Coeficiente de Segurança)

Com base nos momentos e cortantes máximos obtidos para cada largura e comprimento de tabuleiro é possível calcular o Coeficiente de Segurança (CS), isto a partir da comparação dos esforços de cálculo de projeto com os esforços provocados pela passagem do guindaste.

A fórmula adotada para o coeficiente de segurança foi baseada no formulário definido na portaria SUP/DER-138-20/12/2021, que aprova norma para concessão de autorização especial de trânsito ao veículo ou combinação de veículos utilizados no transporte de carga indivisível e veículos especiais nas rodovias estaduais.

A carga especial passa centrada e sozinha sobre a obra, com velocidade controlada e neste caso o objetivo é que a liberação do guindaste ocorra de forma que ele trafegue junto com trânsito.

Segue o formulário para liberação exclusiva de cargas especiais adotado pelo DER/SP:

$$FS = \frac{1,40 \times S_g + 1,68 \times \varphi \times S_q}{1,2 \times S_g + 1,30 \times S_e}$$

O peso próprio da obra no numerador da fração e no denominador multiplicados por quantis diferentes levam o coeficiente de segurança a resultados mais favoráveis, condizentes com a passagem da carga especial centrada, controlada e isolada sobre a obra.

O guindaste não é considerado carga especial, já que trafega junto ao tráfego usual da rodovia, por isso o critério do coeficiente de segurança deve ser o mesmo adotado para as Combinações de Veículos de Carga (CVC), onde a comparação para obtenção do coeficiente é feita entre os esforços acidentais de cálculo e os esforços acidentais provocadas pelo CVC.

Desta forma, a comparação entre os esforços acidentais fica semelhante a fórmula acima suprimindo-se a parcela das cargas permanentes  $\frac{1,40 \times S_g}{1,20 \times S_g}$ , resultando em:

$$CS = \frac{1,20 \times 1,40 \times \varphi_{TB} \times S_{Q-TB}}{CIV \times CNF \times 1,10 \times S_{Q-GUIN_{96-8}}}$$

$$CS = \frac{1,68 \times \varphi_{TB} \times S_{Q-TB}}{CIV \times CNF \times 1,10 \times S_{Q-GUIN_{96-8}}}$$



## NOTA TÉCNICA

Em que,

**1,20:** Coeficiente adotado a partir do estudo "Análise estrutural de pontes utilizadas por veículos de carga especial", apresentado na XXXII Jornada Sul-americana de Engenharia Estrutural de Campinas.

O coeficiente 1,2 permite ampliar as solicitações de carga dos TB-24 e TB-36 de modo que o cálculo da armadura da época seja equivalente à armadura calculada para o TB-45.

O coeficiente 1,20 é utilizado no estudo do IPT feito para os CVCs na comparação dos esforços.

**1,40:** Este é o coeficiente padrão utilizado na época para majoração dos esforços (Mq).

**1,10:** Utilizado para cargas truncadas, conforme norma, onde o valor é mais preciso e a majoração não precisa ser tão alta.

**$\varphi_{TB}$  e CIV:**

Para o TB-24  $\rightarrow \varphi_{TB} = 1,30$  (coeficiente de impacto constante);

Para o TB-36  $\rightarrow \varphi_{TB} = 1,4 - 0,007 \times L_{v\tilde{a}o}$  ou  $\varphi_{TB} = 1,4 - 0,007 \times 2 \times L_{bal}$ ;

Para o Guindaste  $\rightarrow CIV = 1 + 1,06 \times \left(\frac{20}{50+L_{v\tilde{a}o}}\right)$  ou  $CIV = 1 + 1,06 \times \left(\frac{20}{50+L_{bal}}\right)$ .

Os coeficientes de impacto das normas TB-36 e TB-24 foram multiplicados pelos coeficientes de impacto adotados em suas respectivas épocas ( $\varphi_{TB}$ ), para que os resultados estejam de acordo com a capacidade de suporte das pontes.

Em contrapartida, os esforços do guindaste foram multiplicados pelo coeficiente de impacto da norma atual TB-45 (CIV), com o intuito de verificar se, com as considerações atuais, uma ponte mais antiga seria capaz de suportar essas cargas.

**CNF:** Cálculo de Número de Faixas. Neste estudo, consideramos o número de faixas igual a 2, isto a favor da segurança.

$$CNF = 1 - 0,05 \times (N - 2) > 0,9$$



## NOTA TÉCNICA

Na segunda linha do quadro temos o CIV x CNF que equivale ao CIV puro, conforme norma NBR-7188 (1984) para efeito de comparação.

	Liv	5	8	10	20	30	40	50	60	80	100	120	140	160	180	200
	<b>NBR - 7188 (1984)</b>	1,37	1,34	1,33	1,26	1,19	1,12	1,05	1	1	1	1	1	1	1	1
	<b>CIV</b>	<b>1,35</b>	<b>1,35</b>	<b>1,35</b>	<b>1,3</b>	<b>1,27</b>	<b>1,24</b>	<b>1,21</b>	<b>1,19</b>	<b>1,16</b>	<b>1,14</b>	<b>1,12</b>	<b>1,11</b>	<b>1,1</b>	<b>1,09</b>	<b>1,08</b>
n	CIV/NBR	0,99	1	1,02	1,03	1,06	1,1	1,15	1,19	1,16	1,14	1,12	1,11	1,1	1,09	1,08
1	CIV x CNF	1,42	1,42	1,42	1,42	1,33	1,3	1,27	1,25	1,22	1,2	1,18	1,17	1,16	1,15	1,14
2	CIV x CNF	1,35	1,35	1,35	1,35	1,27	1,24	1,21	1,19	1,16	1,14	1,12	1,11	1,1	1,09	1,08
3	CIV x CNF	1,28	1,28	1,29	1,29	1,2	1,7	1,15	1,13	1,1	1,08	1,07	1,06	1,05	1,04	1,03
4	CIV x CNF	1,28	1,28	1,29	1,29	1,2	1,17	1,15	1,13	1,1	1,08	1,07	1,06	1,05	1,04	1,03

Coeficiente de impacto aplicado nos modelos de cálculo.

O coeficiente de impacto aplicado na modelagem 2D foi aplicado diretamente no carregamento do STRAP, portanto os esforços do processamento já trazem embutido os coeficientes de impacto.

Já para os esforços provocados pelo guindaste, os esforços obtidos no processamento são puros e sem impacto, para exemplificar este processo:

Tabuleiro de 11,20 x 20,00 m:

$$\varphi = 1,0 + 1,06 \times \left( \frac{20}{20 + 50} \right)$$

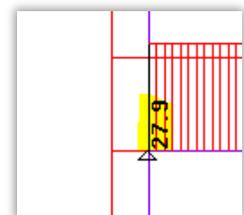
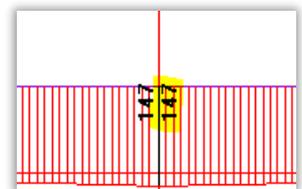
$$\varphi = 1,30$$

$$Mq = 1,30 \times 147$$

$$Mq = 191,10 \text{ ton/m}$$

$$Vq = 1,30 \times 27,9$$

$$Vq = 36,27 \text{ ton/m}$$



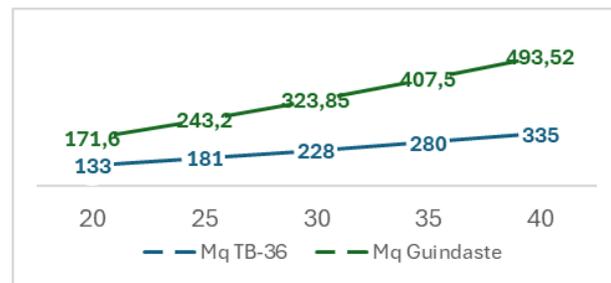
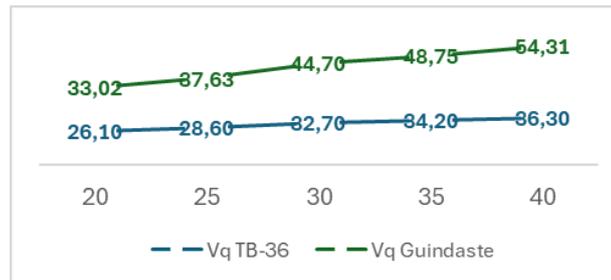
Com todos os dados coletados, segue abaixo os quadros de resumo de carga e a aplicação da fórmula para cada largura de tabuleiro.



### NOTA TÉCNICA

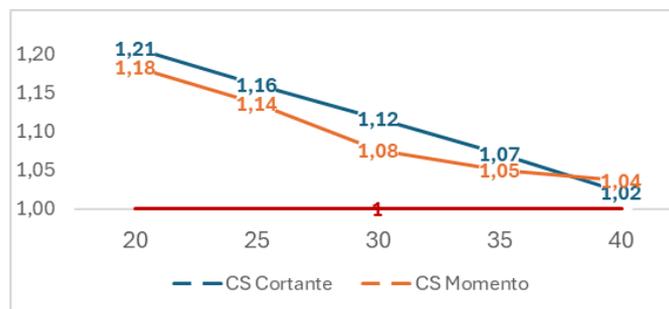
TABULEIROS		TB-36		GUINDASTE	
LARG (m)	COMP (m)	MOMENTO Mq (txm)	CORTANTE Vq (t)	MOMENTO Mq (txm)	CORTANTE Vq (t)
11,20 x	20	133	26,10	171,6	33,02
	25	181	28,60	243,2	37,63
	30	228	32,70	323,85	44,70
	35	280	34,20	407,5	48,75
	40	335	36,30	493,52	54,31

#### Consolidação e validação dos valores:



#### Cálculo do CS:

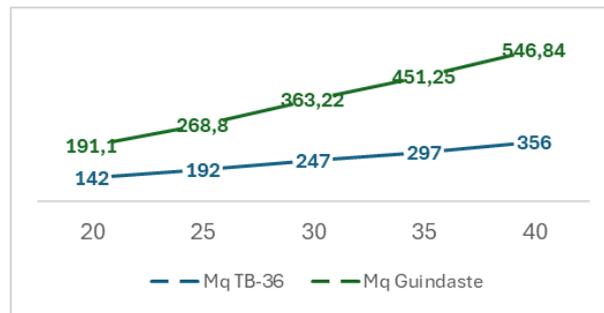
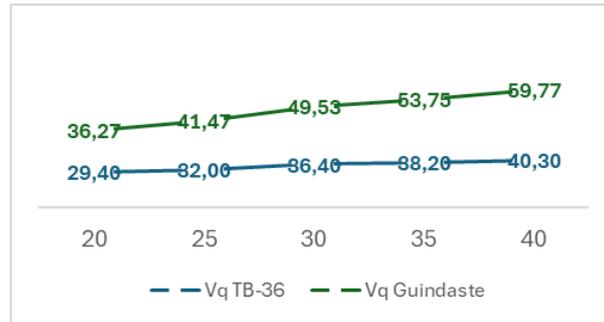
LARG (m)	COMP (m)	MOMENTO	CORTANTE
11,20 x	20	1,18	1,21
	25	1,14	1,16
	30	1,08	1,12
	35	1,05	1,07
	40	1,04	1,02



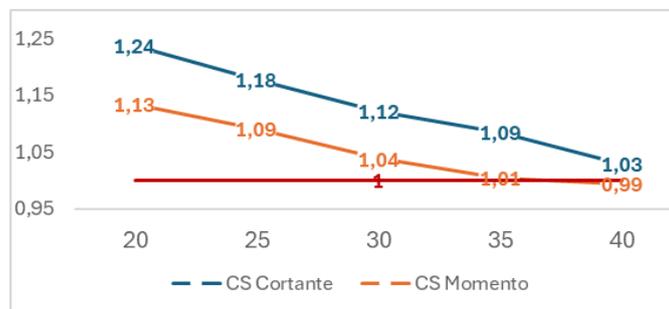


NOTA TÉCNICA

LARG (m)	TABULEIROS COMP (m)	TB-36		GUINDASTE	
		MOMENTO Mq (txm)	CORTANTE Vq (t)	MOMENTO Mq (txm)	CORTANTE Vq (t)
12,60 x	20	142	29,40	191,1	36,27
	25	192	32,00	268,8	41,47
	30	247	36,40	363,22	49,53
	35	297	38,20	451,25	53,75
	40	356	40,30	546,84	59,77



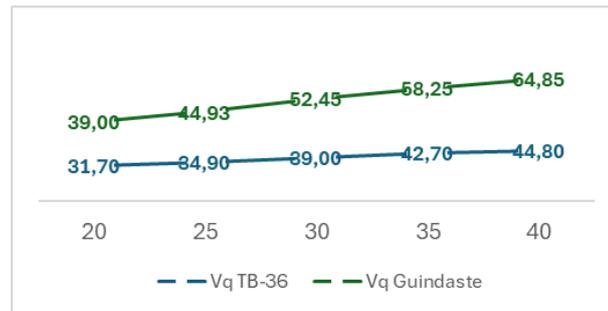
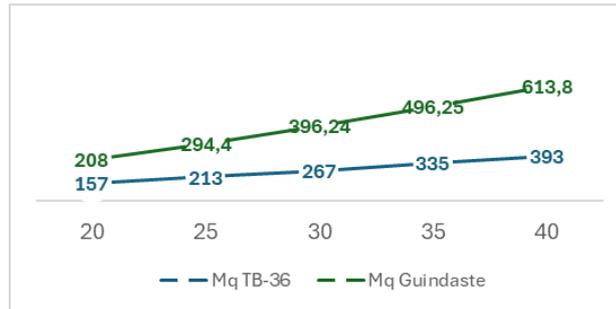
LARG (m)	COMP (m)	MOMENTO	CORTANTE
12,60 x	20	1,13	1,24
	25	1,09	1,18
	30	1,04	1,12
	35	1,01	1,09
	40	0,99	1,03



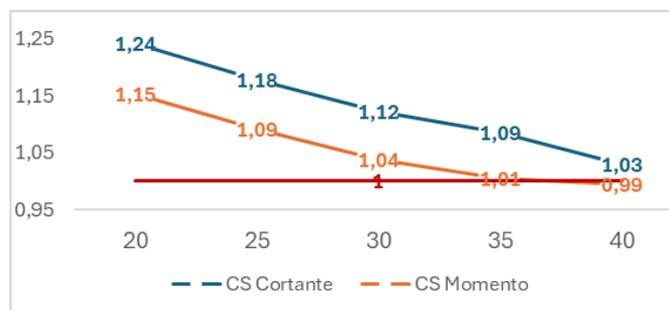


NOTA TÉCNICA

LARG (m)	TABULEIROS COMP (m)	TB-36		GUINDASTE	
		MOMENTO Mq (txm)	CORTANTE Vq (t)	MOMENTO Mq (txm)	CORTANTE Vq (t)
14,10 x	20	157	31,70	208	39,00
	25	213	34,90	294,4	44,93
	30	267	39,00	396,24	52,45
	35	335	42,70	496,25	58,25
	40	393	44,80	613,8	64,85



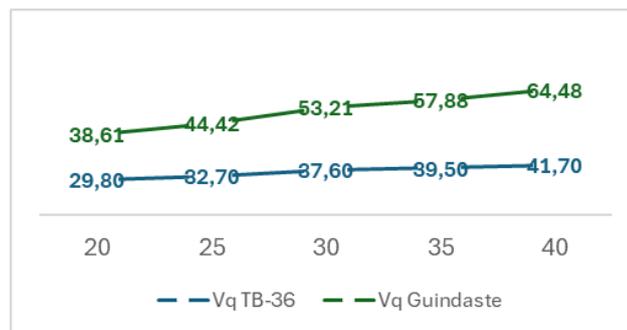
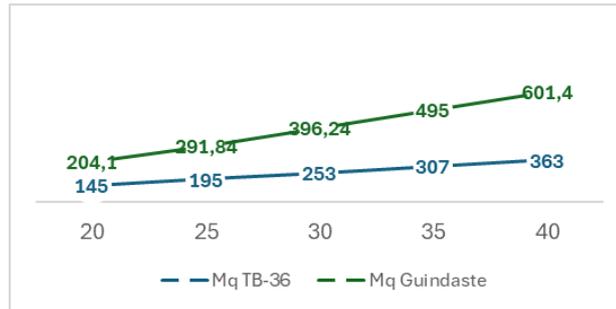
LARG (m)	COMP (m)	MOMENTO	CORTANTE
14,10 x	20	1,15	1,24
	25	1,09	1,18
	30	1,04	1,12
	35	1,01	1,09
	40	0,99	1,03



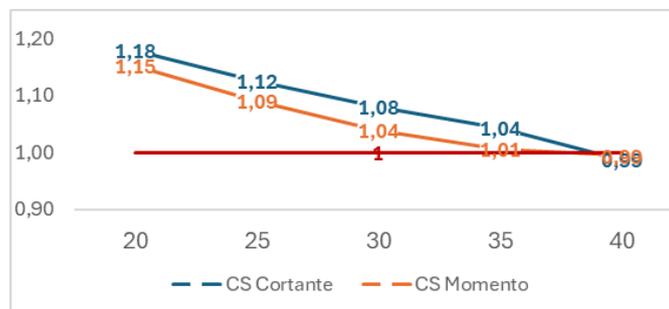


NOTA TÉCNICA

TABULEIROS		TB-36		GUINDASTE	
LARG (m)	COMP (m)	MOMENTO Mq (txm)	CORTANTE Vq (t)	MOMENTO Mq (txm)	CORTANTE Vq (t)
16,10 x	20	145	29,80	204,1	38,61
	25	195	32,70	291,84	44,42
	30	253	37,60	396,24	53,21
	35	307	39,50	495	57,88
	40	363	41,70	601,4	64,48



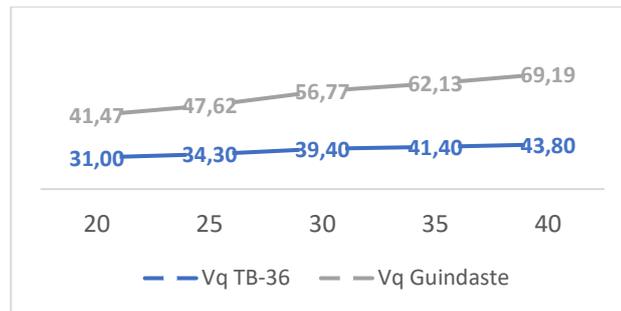
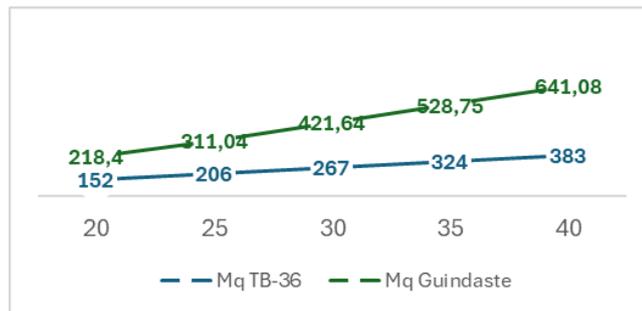
LARG (m)	COMP (m)	MOMENTO	CORTANTE
16,10 x	20	1,09	1,18
	25	1,02	1,12
	30	0,98	1,08
	35	0,95	1,04
	40	0,92	0,99



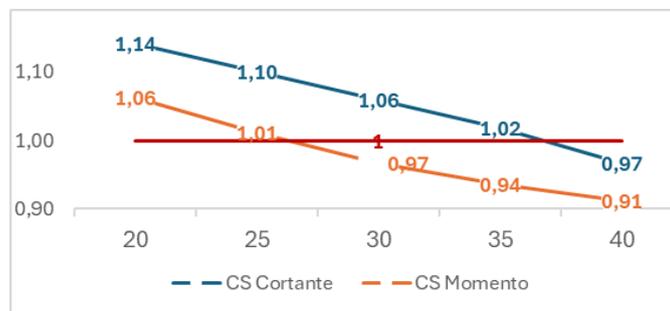


### NOTA TÉCNICA

TABULEIROS		TB-36		GUINDASTE	
LARG (m)	COMP (m)	MOMENTO Mq (txm)	CORTANTE Vq (t)	MOMENTO Mq (txm)	CORTANTE Vq (t)
16,90 x	20	152	31,00	218,4	41,47
	25	206	34,30	311,04	47,62
	30	267	39,40	421,64	56,77
	35	324	41,40	528,75	62,13
	40	383	43,80	641,08	69,19



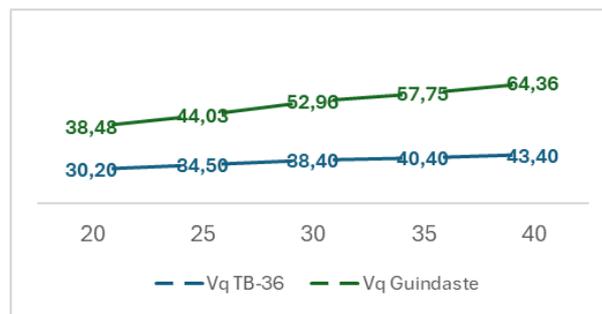
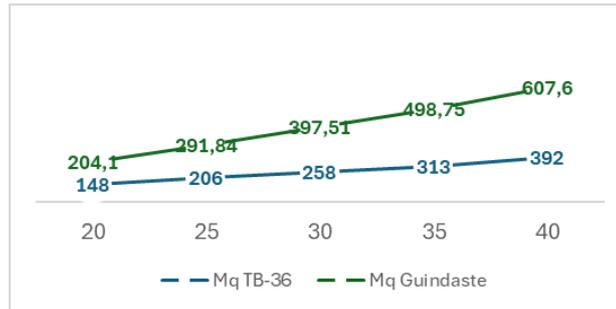
LARG (m)	COMP (m)	COEFICIENTE DE SEGURANÇA	
		MOMENTO	CORTANTE
16,90 x	20	1,06	1,14
	25	1,01	1,10
	30	0,97	1,06
	35	0,94	1,02
	40	0,91	0,97



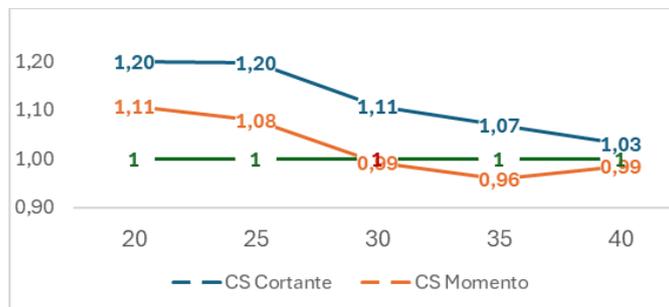


NOTA TÉCNICA

TABULEIROS		TB-36		GUINDASTE	
LARG (m)	COMP (m)	MOMENTO Mq (txm)	CORTANTE Vq (t)	MOMENTO Mq (txm)	CORTANTE Vq (t)
19,60 x	20	148	30,20	204,1	38,48
	25	206	34,50	291,84	44,03
	30	258	38,40	397,51	52,96
	35	313	40,40	498,75	57,75
	40	392	43,40	607,6	64,36



LARG (m)	COMP (m)	MOMENTO	CORTANTE
19,60 x	20	1,11	1,20
	25	1,08	1,20
	30	0,99	1,11
	35	0,96	1,07
	40	0,99	1,03





NOTA TÉCNICA

4.7.2. Cálculo da área de aço – armadura cortante

Também foi realizada a comparação entre a armadura de cortante suficiente para passar o guindaste com a que foi calculada para o TB-36. Para o TB-36, utilizamos a seguinte planilha:

CÁLCULO DO AÇO - NBR 1980 - 1984		
<p><b>Cálculo de <math>\tau_{wd}</math></b></p> $\tau_{wd} = \frac{1,4 \times V_{m\acute{a}x}}{bw \times d}$ <p> <math>V_g =</math> <input type="text"/> ton  <math>V_q =</math> <input type="text"/> ton  <math>V_{m\acute{a}x} =</math> <input type="text" value="0,00"/> ton </p> <p> <math>bw =</math> <input type="text"/> cm  <math>h =</math> <input type="text"/> cm  <math>d =</math> <input type="text" value="0,00"/> cm </p> <p> <math>f_{ck} =</math> <input type="text"/> kgf/cm<sup>2</sup>  <math>f_{cd} =</math> <input type="text" value="0,00"/> kgf/cm<sup>2</sup>  <math>\tau_{wd} =</math> <input type="text"/> kgf/cm<sup>2</sup> </p> <p> <math>\tau_{wd\acute{u}ltimo} = 0,25 \times f_{cd} \leq 45 \frac{kgf}{cm^2}</math> </p> <p> <math>\tau_{wd\acute{u}ltimo} =</math> <input type="text" value="0,00"/> <input type="text" value="OK"/> </p> <p> <math>\tau_{wd\acute{u}ltimo} =</math> <input type="text" value="0,00"/> </p>	<p><b>VERIFICAÇÃO:</b></p> $\tau_{wd} \leq \tau_{wd\acute{u}ltimo}$ <p style="text-align: right;"><b>NÃO OK</b></p> <p><b>Cálculo de <math>\tau_d</math></b></p> $\tau_d = 1,15 \times \tau_{wd} - \tau_c$ $\tau_c = \varphi_1 \times \sqrt{f_{ck}}$ <p><i>*consideramos o mínimo, que está sempre a favor do concreto</i></p> $\varphi_1 = \frac{0,24kgf}{cm^2} \text{ para } \rho_1 \leq 0,001$ <p> <math>\varphi_1 =</math> <input type="text" value="0,24"/> kg/cm<sup>2</sup> </p> <p> <math>\tau_c =</math> <input type="text" value="0,00"/> kg/cm<sup>2</sup>  <math>\tau_d =</math> <input type="text"/> kg/cm<sup>2</sup> </p>	<p><b>Cálculo de <math>\rho_t</math></b></p> $\rho_t = \frac{\tau_d}{f_{yd}}$ <p> <math>f_{yk} =</math> <input type="text"/> kgf/cm<sup>2</sup>  <math>f_{yd} =</math> <input type="text" value="0,00"/> kg/cm<sup>2</sup>  <math>\rho_t =</math> <input type="text"/> </p> <p><b>Cálculo de <math>A_{te}</math></b></p> $A_{te} = \rho_t \times bw \times d$ <p> <math>A_{te} =</math> <input type="text"/> cm<sup>2</sup>/m </p>

E seguindo os critérios atuais, utilizamos a planilha abaixo para o guindaste:

CÁLCULO DO AÇO - NBR 6118	
<b>FÓRMULAS:</b>	
$V_{sd} = 1,35 \times V_g + 1,50 \times V_p$	
$V_{sd} \leq V_{Rd2} = 0,27 \times \left(1 - \frac{f_{ck}}{250}\right) \times f_{cd} \times bw \times d - f_{ck} \text{ em Mpa}$	
$\tau_{wd} = \frac{0,126 \times f_{ck}^{2/3}}{\gamma_c}$	
$\tau_{wd} = \frac{V_{sd}}{bw \times d}$	
$A_{sw} = \frac{(\tau_{wd} - \tau_c) \times 100 \times bw}{0,9 \times f_{yd}} \left(\frac{cm^2}{m}\right)$	
$f_{ck} =$ <input type="text"/> Mpa $bw =$ <input type="text"/> cm $h =$ <input type="text"/> cm $d =$ <input type="text" value="0,00"/> cm $V_{sd} =$ <input type="text"/> ton	$V_{Liebherrd} = 1,20 \times V_g + 1,10 \times V_q$
$V_{Rd2} =$ <input type="text" value="0,00"/> ton/cm <sup>2</sup> <b>NÃO OK</b> $\tau_{wd} =$ <input type="text"/> kgf/cm <sup>2</sup> $\tau_c =$ <input type="text" value="0,00"/> kgf/cm <sup>2</sup> $A_{sw} =$ <input type="text" value="cm2/m"/>	



### NOTA TÉCNICA

Para utilizar a planilha de dimensionamento do aço necessário para a cortante, para o guindaste, foi adotado o valor de  $V_{sd}$  com a seguinte formulação:

$$V_d = 1,20 \times V_g + 1,1 \times V_q$$

Em que,

**Carga permanente ( $V_g$ ):** Considera-se um fator de 1,20, assumindo que a obra está íntegra e classificada como nível 3 ou maior de acordo com a norma de vistoria NBR 9452. Uma vez a obra íntegra, podemos adotar o coeficiente = 1,20, baseado no estudo: “Safety of Existing Bridges” que em função do estado de conservação da obra adota um coeficiente menor que o atual = 1,35 preconizado na norma atual para esforços de dimensionamento.

**Carga acidental ( $V_q$ ):** Utiliza-se um fator de 1,10, uma vez que o peso do guindaste é uma carga bem definida, ou seja, seu peso ao trafegar pelas rodovias é conhecido.

O valor de  $V_{sd}$  para o TB-36, foi obtido conforme a fórmula da NB 1/78:

$$V_d = 1,40 \times V_g + 1,40 \times V_q$$

Todos os resultados, para todos os tabuleiros, podem ser vistos nas tabelas abaixo:

$V_d = 1,40 \times V_g + 1,40 \times V_q$										
TB-36										
TABULEIROS	20		25		30		35		40	
	$V_g$	$V_q$	$V_g$	$V_q$	$V_g$	$V_q$	$V_g$	$V_q$	$V_g$	$V_q$
11,2	33,30	26,10	43,40	28,60	56,20	32,70	67,40	34,20	79,70	36,30
5 longarinas $V_{sd} =$	83,16		100,80		124,46		142,24		162,40	
$Asw \text{ (cm}^2\text{/m)} =$	19,39		24,06		29,20		33,63		38,68	

$V_d = 1,20 \times V_g + 1,1 \times V_q$										
LIEBHERR										
TABULEIROS	20		25		30		35		40	
	$V_g$	$V_q$	$V_g$	$V_q$	$V_g$	$V_q$	$V_g$	$V_q$	$V_g$	$V_q$
11,2	33,30	33,02	43,4	37,632	56,2	44,70	67,4	48,75	79,7	54,312
5 longarinas $V_{sd} =$	76,28		93,48		116,61		134,51		155,38	
$Asw \text{ (cm}^2\text{/m)} =$	13,18		16,67		14,26		15,47		16,89	

$$V_{d\text{Liebherr}} < V_{d\text{TB-36}}$$

VERIFICAÇÃO	RESISTE	RESISTE	RESISTE	RESISTE	RESISTE
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### NOTA TÉCNICA

$V_d = 1,40 \times V_g + 1,40 \times V_q$ TB-36										
TABULEIROS	20		25		30		35		40	
	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq
12,6	36,40	29,40	47,10	32,00	60,80	36,40	72,40	38,20	85,80	40,30
5 longarinas										
Vsd =		92,12		110,74		136,08		154,84		176,54
Asw (cm <sup>2</sup> /m) =		21,76		26,69		32,28		36,96		42,42

$V_d = 1,20 \times V_g + 1,1 \times V_q$ LIEBHERR										
TABULEIROS	20		25		30		35		40	
	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq
12,6	36,40	36,27	47,1	41,472	60,80	49,53	72,40	53,75	85,80	59,77
5 longarinas										
Vsd =		83,58		102,14		127,44		146,01		168,70
Asw =		14,66		18,42		15,80		16,99		18,56

$$V_{dLieberherr} < V_{dTB-36}$$

VERIFICAÇÃO	RESISTE	RESISTE	RESISTE	RESISTE	RESISTE
-------------	---------	---------	---------	---------	---------

$V_d = 1,40 \times V_g + 1,40 \times V_q$ TB-36										
TABULEIROS	20		25		30		35		40	
	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq
14,1	39,60	31,70	51,30	34,90	64,20	39,00	78,50	42,70	92,40	44,80
5 longarinas										
Vsd =		99,82		120,68		144,48		169,68		192,08
Asw (cm <sup>2</sup> /m) =		23,80		29,42		34,50		40,88		46,32

$V_d = 1,20 \times V_g + 1,1 \times V_q$ LIEBHERR										
TABULEIROS	20		25		30		35		40	
	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq
14,1	39,60	39,00	51,3	44,928	64,20	52,45	78,50	58,25	92,40	64,85
5 longarinas										
Vsd =		90,42		110,98		134,74		158,28		182,22
Asw (cm <sup>2</sup> /m) =		16,05		20,21		16,84		18,61		20,09

$$V_{dLieberherr} < V_{dTB-36}$$

VERIFICAÇÃO	RESISTE	RESISTE	RESISTE	RESISTE	RESISTE
-------------	---------	---------	---------	---------	---------



NOTA TÉCNICA

$V_d = 1,40 \times V_g + 1,40 \times V_q$										
TB-36										
TABULEIROS	20		25		30		35		40	
	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq
16,1	37,40	29,80	48,50	32,70	62,40	37,60	74,50	39,50	87,90	41,70
6 longarinas										
Vsd =	94,08		113,68		140,00		159,60		181,44	
Asw (cm <sup>2</sup> /m) =	22,28		27,34		33,83		39,40		43,72	

$V_d = 1,20 \times V_g + 1,1 \times V_q$										
LIEBHERR										
TABULEIROS	20		25		30		35		40	
	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq
16,1	37,40	38,61	48,5	44,416	62,40	53,21	74,50	57,88	87,90	64,48
6 longarinas										
Vsd =	87,35		107,06		133,41		153,06		176,41	
Asw =	15,31		19,42		16,65		17,92		19,48	

$V_{dLieberherr} < V_{dTB-36}$

VERIFICAÇÃO	RESISTE	RESISTE	RESISTE	RESISTE	RESISTE
-------------	---------	---------	---------	---------	---------

$V_d = 1,40 \times V_g + 1,40 \times V_q$										
TB-36										
TABULEIROS	20		25		30		35		40	
	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq
16,9	38,80	31,00	50,30	34,30	64,60	39,40	77,10	41,40	90,80	43,80
6 longarinas										
Vsd =	97,72		118,44		145,60		165,90		188,44	
Asw (cm <sup>2</sup> /m) =	22,95		28,59		34,79		39,88		45,35	

$V_d = 1,20 \times V_g + 1,1 \times V_q$										
LIEBHERR										
TABULEIROS	20		25		30		35		40	
	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq
16,9	38,80	41,47	50,3	47,616	64,60	56,77	77,10	62,13	90,80	69,19
6 longarinas										
Vsd =	92,18		112,74		139,97		160,86		185,07	
Asw =	16,29		20,57		17,58		18,95		20,55	

$V_{dLieberherr} < V_{dTB-36}$

VERIFICAÇÃO	RESISTE	RESISTE	RESISTE	RESISTE	RESISTE
-------------	---------	---------	---------	---------	---------



### NOTA TÉCNICA

$V_d = 1,40 \times V_g + 1,40 \times V_q$										
TB-36										
TABULEIROS	20		25		30		35		40	
	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq
19,6	38,10	30,20	49,40	34,50	63,60	38,40	75,90	40,40	89,50	43,40
7 longarinas										
Vsd =		95,62		117,46		142,80		162,82		186,06
Asw (cm <sup>2</sup> /m) =		22,69		28,34		34,04		39,07		44,94

$V_d = 1,20 \times V_g + 1,1 \times V_q$										
LIEBHERR										
TABULEIROS	20		25		30		35		40	
	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq	Vg	Vq
19,6	38,10	38,48	49,4	44,032	63,60	52,96	75,90	57,75	89,50	64,36
7 longarinas										
Vsd =		88,05		107,72		134,57		154,61		178,19
Asw =		15,45		19,55		16,81		18,13		19,70

$$V_{dLiebherr} < V_{dTB-36}$$

VERIFICAÇÃO	RESISTE	RESISTE	RESISTE	RESISTE	RESISTE
-------------	---------	---------	---------	---------	---------

#### 4.7.3. Considerações para o TB-36

Concluimos que o guindaste trafega sobre obras TB-36 com o coeficiente de segurança maior que 1. A análise do TB-45 não é necessária, visto que a capacidade de suporte é maior que a do TB-36.



## NOTA TÉCNICA

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### 5. DESENVOLVIMENTO: TB-24 (1943 A 1950)

#### 5.1. Introdução

Utilizamos a mesma fórmula de CS para o TB-24, que possui o processo de cálculo diferente para dois períodos – 1943 a 1950 e 1950 a 1960.

Para ambos, optamos por realizar o estudo a partir da Classe I, que são estradas tronco-federais, as mais robustas e importantes. Para estruturas Classe II e III, que são pontes localizadas em rodovias secundárias é necessário um estudo caso a caso.

As pontes rodoviárias são agrupadas em três classes:

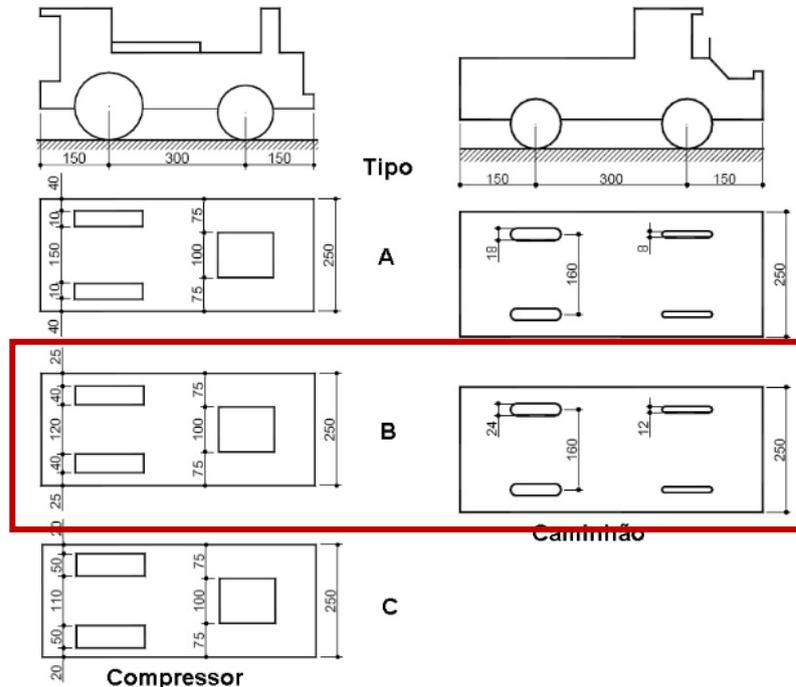
- Classe I: Pontes situadas em estradas-tronco federais e estaduais ou nas estradas de ligação principais entre esses troncos.
- Classe II: Pontes situadas em estradas de ligação secundárias, mas que podem prever a passagem de veículos pesados.
- Classe III: Pontes situadas em estradas de ligação secundárias não incluídas na Classe II.

Para o estudo do primeiro período (1943 a 1950), a norma exige a verificação dos esforços com a passagem do rolo compressor tipo B mais próximo do acostamento em conjunto com um caminhão do tipo B.



## NOTA TÉCNICA

Figura 1 - Compressor e caminhão utilizado no trem-tipo segundo NB6/43 (ABNT, 1943)



O trem-tipo para pontes da **Classe I** compõe-se de multidão com  $g_o = 450$   $\text{kgf/m}^2$ , de um compressor **Tipo B** e de tantos caminhões **tipo B** quantas forem as faixas de tráfego, menos uma, e dispostos como no caso do item 2.2.2. A resistência da estrutura deve ainda ser verificada para um compressor Tipo C (Tabela 1), colocado como no caso do item 2.2.2.

**FONTE:** "Evolução dos trem-tipos de projeto de cargas rodoviárias das normas brasileiras", elaborado pelo Prof. Paulo de Sá Pereira Cavalcanti.

Para a verificação, foi adotado homogeneização das cargas do rolo compressor e do caminhão:

- Área do veículo:  $2,5 \times 6 = 15 \text{ m}^2$
- Alívio:  $0,45 \times 15 = 6,75$  toneladas

Exemplo de Cálculo para o Compressor tipo B:

- Peso total: 16 toneladas
- Peso da roda dianteira: 7 toneladas
- Peso da roda traseira: 4,5 toneladas
- Peso homogeneizado:  $16 - 6,75 = 9,25$  toneladas



## NOTA TÉCNICA

Aplicando uma regra de três:

- Eixo Dianteiro (ED):
  - 7 tf (peso de cada roda) - 16 tf (peso total do veículo)
  - $x - 9,25$  tf (peso homogeneizado)
  - $x = 4,05$  tf
- Eixo Traseiro (ET):
  - 4,5 tf - 16 tf
  - $x - 9,25$  tf
  - $x = 2,60$  tf

O mesmo critério foi adotado para a homogeneização do caminhão

Desenhamos as seções transversais mais comuns de três tabuleiros utilizados na época do estudo e realizamos o cálculo a partir da LI (Linha de Influência).

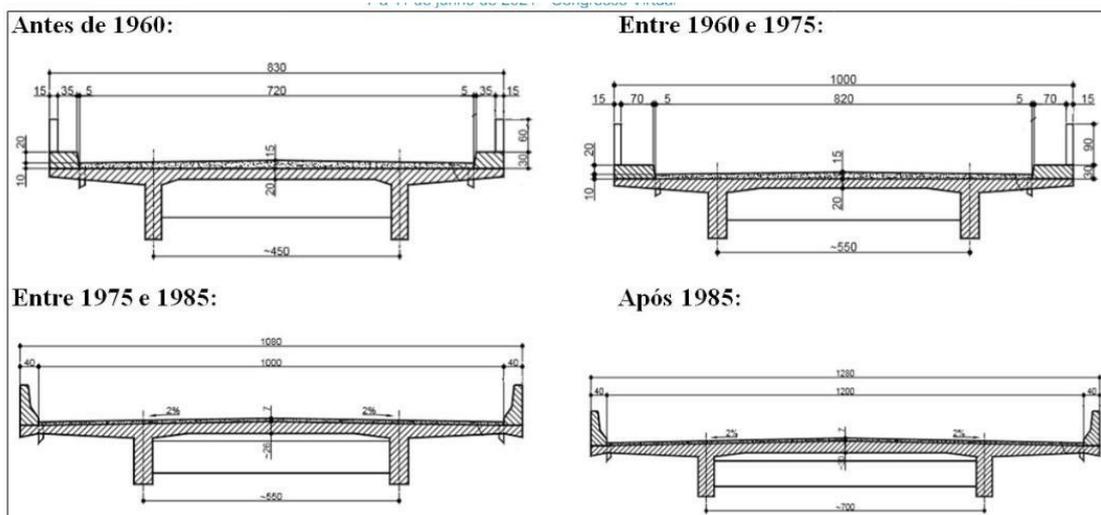
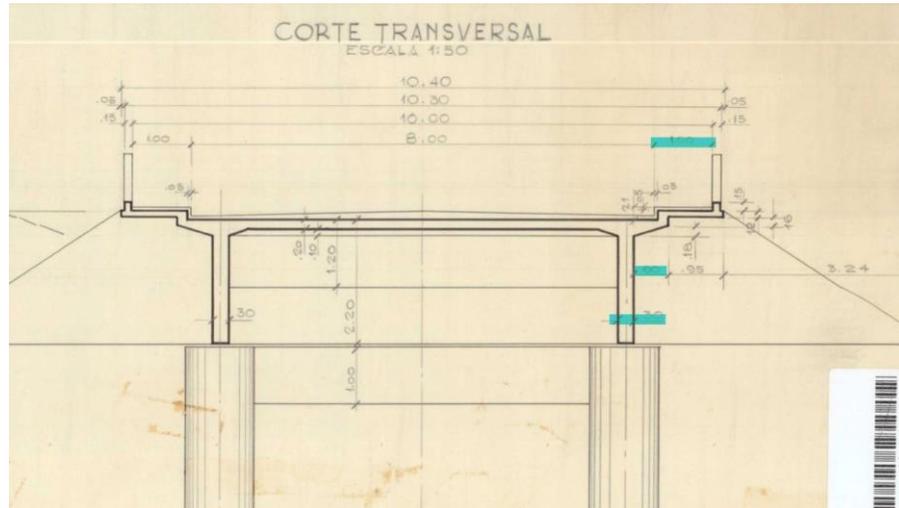


Figura 3 – Correspondência das seções transversais tipo com a época de construção (adaptado de MANUAL 709 (BRASIL, 2004).

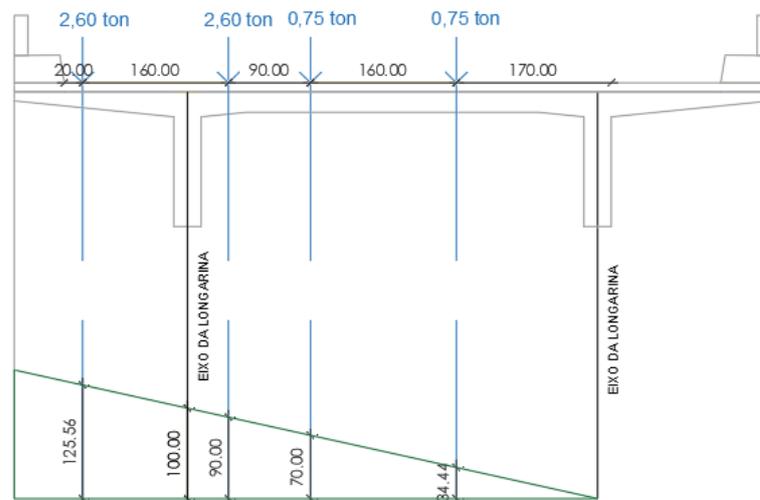
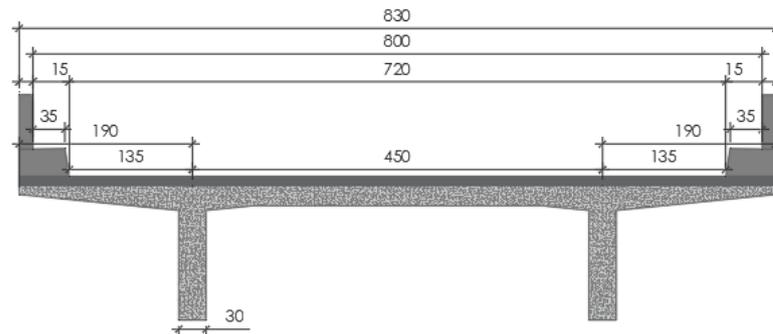


## NOTA TÉCNICA



### 5.2. Linhas de influência de reação de apoio – Rolo compressor + caminhão

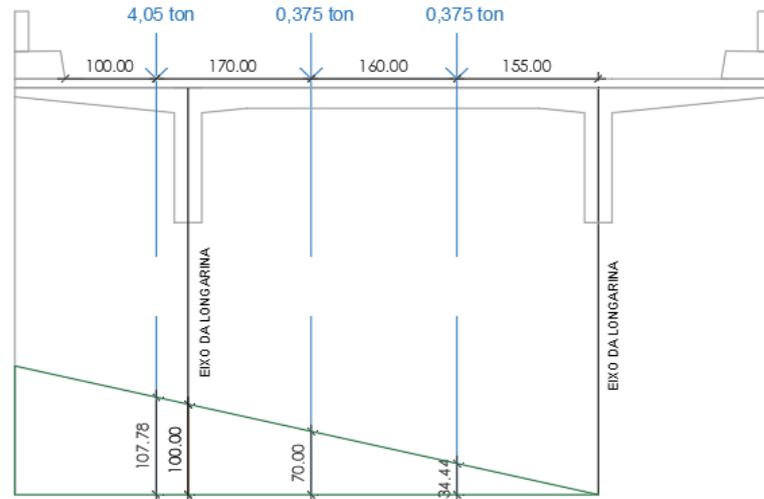
#### 5.2.1. Tabuleiro 8,30 m



$$\text{RODAS TRASEIRAS} = 2,60 \times (1,2556 + 0,9000) + 0,75 \times (0,7000 + 0,3444) = 6,39 \text{ ton}$$



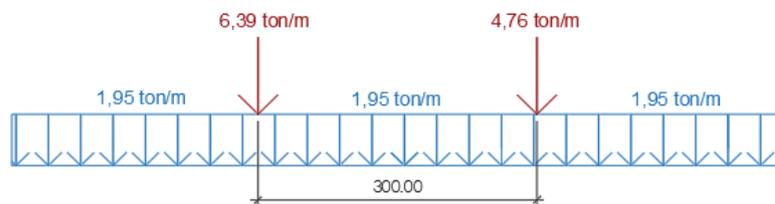
### NOTA TÉCNICA



$$\text{RODAS DIANTEIRAS} = (4,05 \times 1,0778) + 0,375 \times (0,7000 + 0,3444) = 4,76 \text{ ton}$$



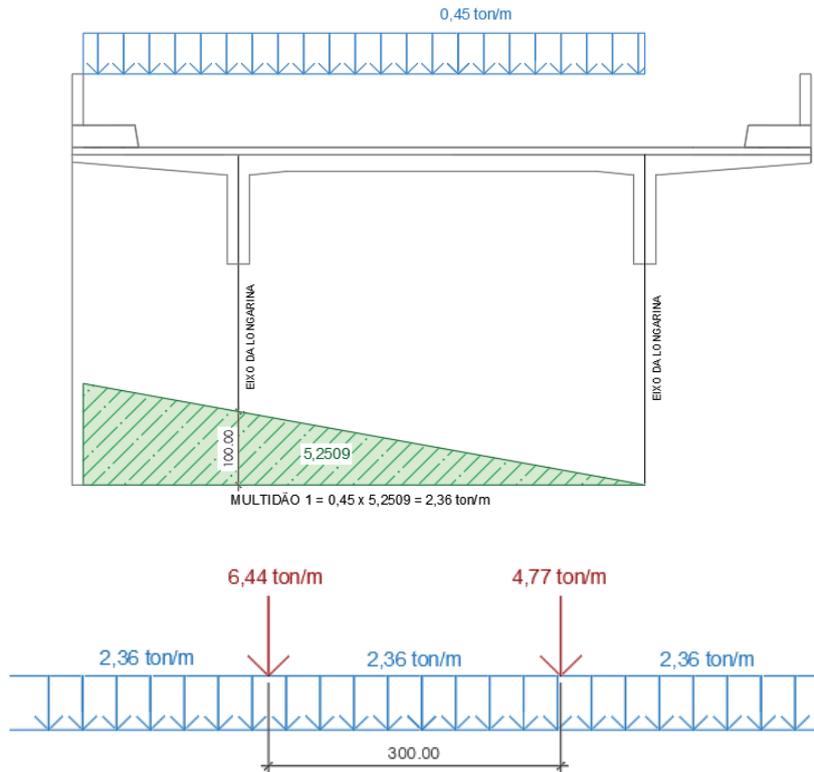
$$\text{MULTIDÃO 1} = 0,45 \times 4,3403 = 1,95 \text{ ton/m}$$



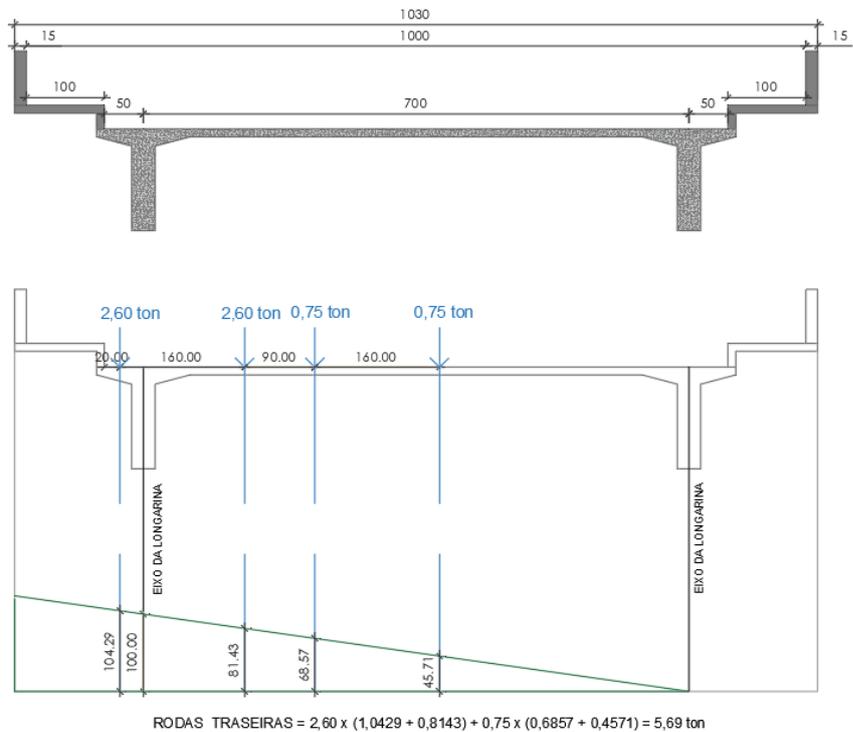




### NOTA TÉCNICA

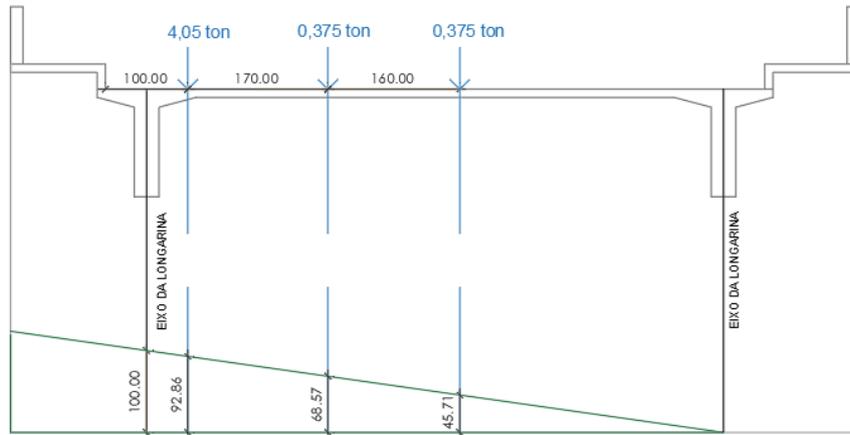


### 5.2.3. Tabuleiro 10,30 m

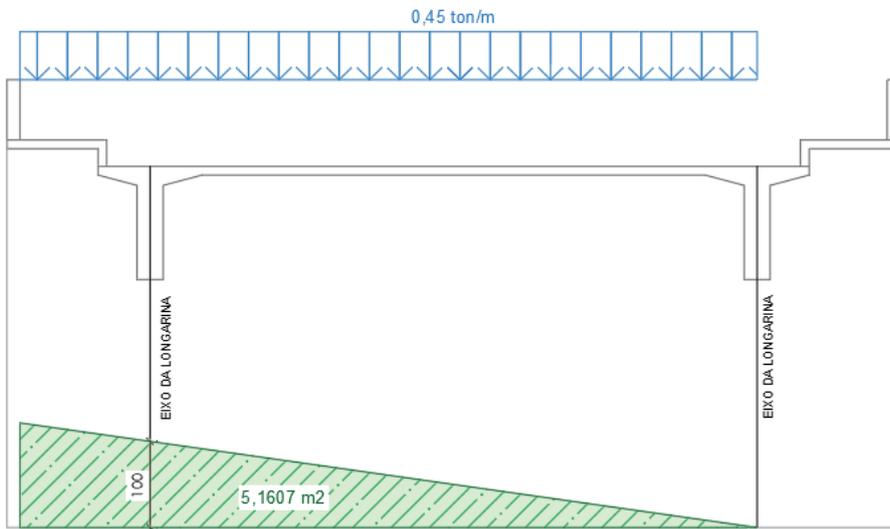




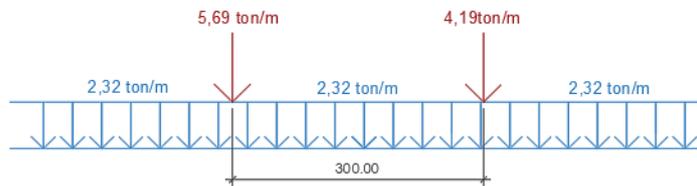
### NOTA TÉCNICA



$$\text{RODAS DIANTEIRAS} = 4,05 \times 0,9286 + 0,375 \times (0,6857 + 0,4571) = 4,19 \text{ ton}$$



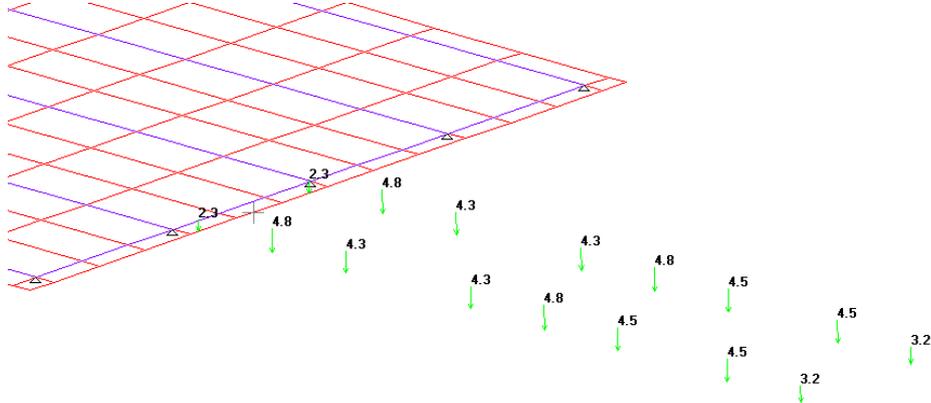
$$\text{MULTIDÃO 1} = 0,45 \times 5,1607 = 2,32 \text{ ton/m}$$





NOTA TÉCNICA

**GUINDASTE LEIBHERR HOMOGENIZADO - LTM1500-C-HOAlpu**



**LTM1500-C-HOAlpu**

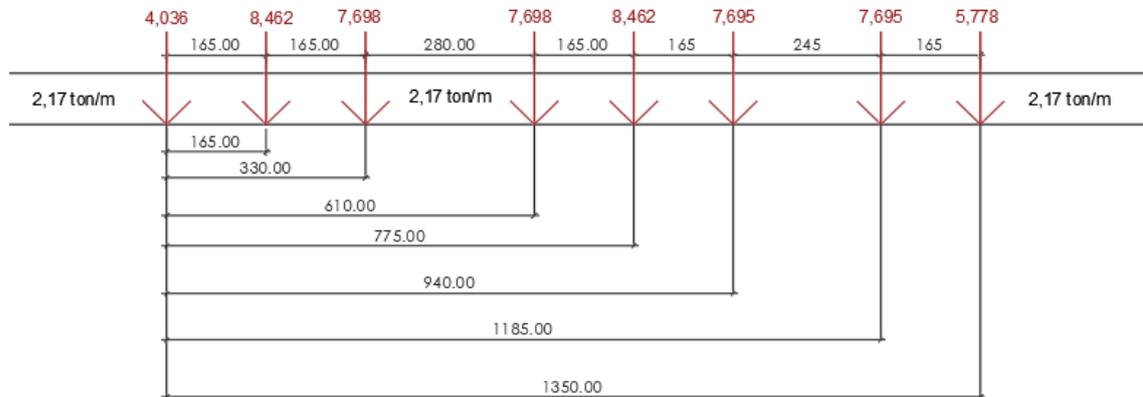
- CONC -2.27 C 0.00 1.305
- CONC -2.27 C 0.00 -1.305
- CONC -4.76 C 1.65 1.305
- CONC -4.76 C 1.65 -1.305
- CONC -4.33 C 3.30 1.305
- CONC -4.33 C 3.30 -1.305
- CONC -4.33 C 6.10 1.305
- CONC -4.33 C 6.10 -1.305
- CONC -4.76 C 7.75 1.305
- CONC -4.76 C 7.75 -1.305
- CONC -4.48 C 9.40 1.305
- CONC -4.48 C 9.40 -1.305
- CONC -4.48 C 11.85 1.305
- CONC -4.48 C 11.85 -1.305
- CONC -3.25 C 13.50 1.305
- CONC -3.25 C 13.50 -1.305





## NOTA TÉCNICA

MULTIDÃO =  $0,5 \times 4,3403 = 2,17 \text{ ton/m}$



$$\text{EIXO 1} = 2,27 \times (1,1778 + 0,6000) = 4,036 \text{ ton}$$

$$\text{EIXO 2} = 4,76 \times (1,1778 + 0,6000) = 8,462 \text{ ton}$$

$$\text{EIXO 3} = 4,33 \times (1,1778 + 0,6000) = 7,698 \text{ ton}$$

$$\text{EIXO 4} = 4,33 \times (1,1778 + 0,6000) = 7,698 \text{ ton}$$

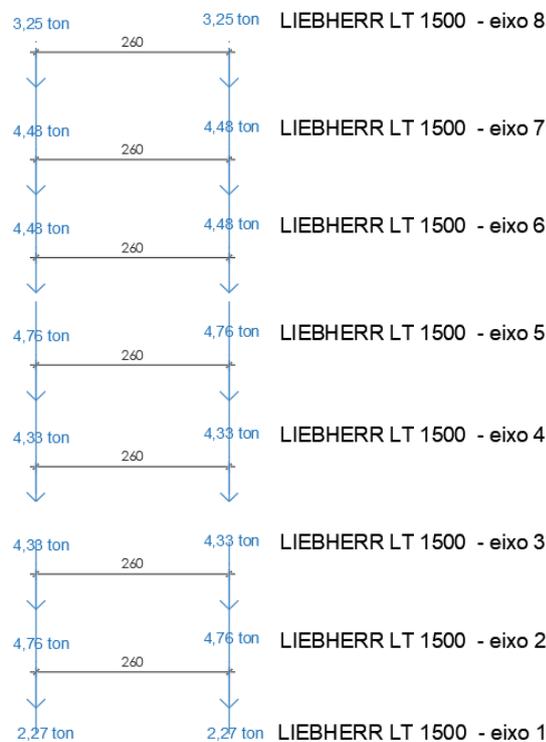
$$\text{EIXO 5} = 4,76 \times (1,1778 + 0,6000) = 8,462 \text{ ton}$$

$$\text{EIXO 6} = 4,48 \times (1,1778 + 0,6000) = 7,965 \text{ ton}$$

$$\text{EIXO 7} = 4,48 \times (1,1778 + 0,6000) = 7,965 \text{ ton}$$

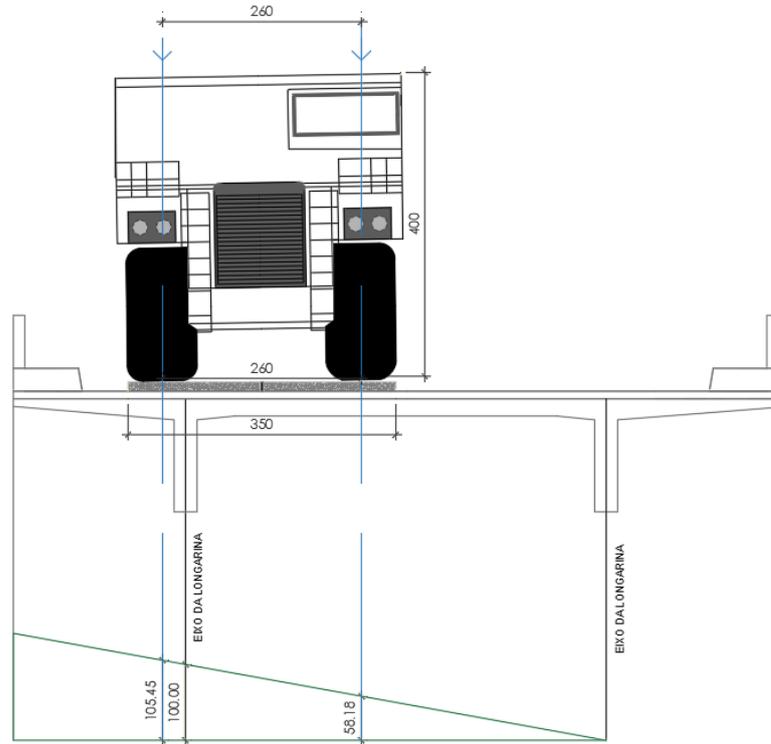
$$\text{EIXO 8} = 3,25 \times (1,1778 + 0,6000) = 5,778 \text{ ton}$$

### 5.3.2. Tabuleiro 10,00 m

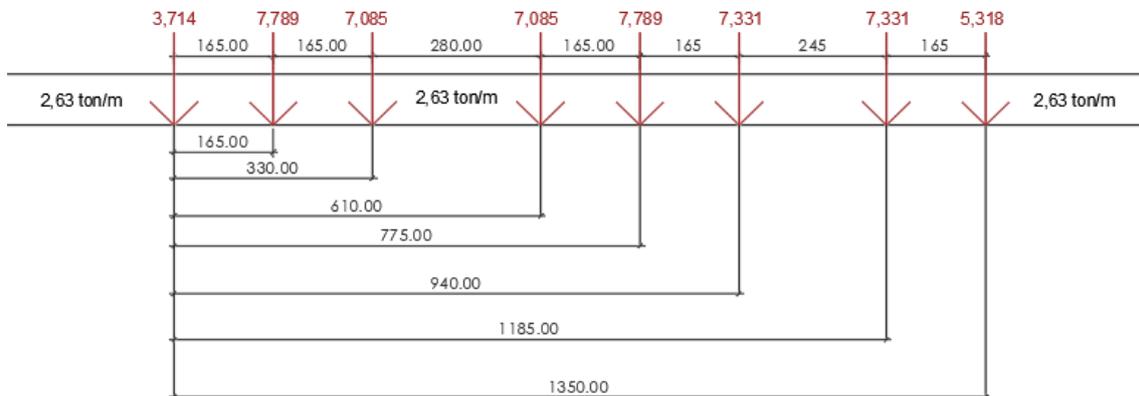




### NOTA TÉCNICA



$$\text{MULTIDÃO} = 0,5 \times 5,2509 = 2,63 \text{ ton/m}$$



$$\text{EIXO 1} = 2,27 \times (1,0545 + 0,5818) = 3,714 \text{ ton}$$

$$\text{EIXO 2} = 4,76 \times (1,0545 + 0,5818) = 7,789 \text{ ton}$$

$$\text{EIXO 3} = 4,33 \times (1,0545 + 0,5818) = 7,085 \text{ ton}$$

$$\text{EIXO 4} = 4,33 \times (1,0545 + 0,5818) = 7,085 \text{ ton}$$

$$\text{EIXO 5} = 4,76 \times (1,0545 + 0,5818) = 7,789 \text{ ton}$$

$$\text{EIXO 6} = 4,48 \times (1,0545 + 0,5818) = 7,331 \text{ ton}$$

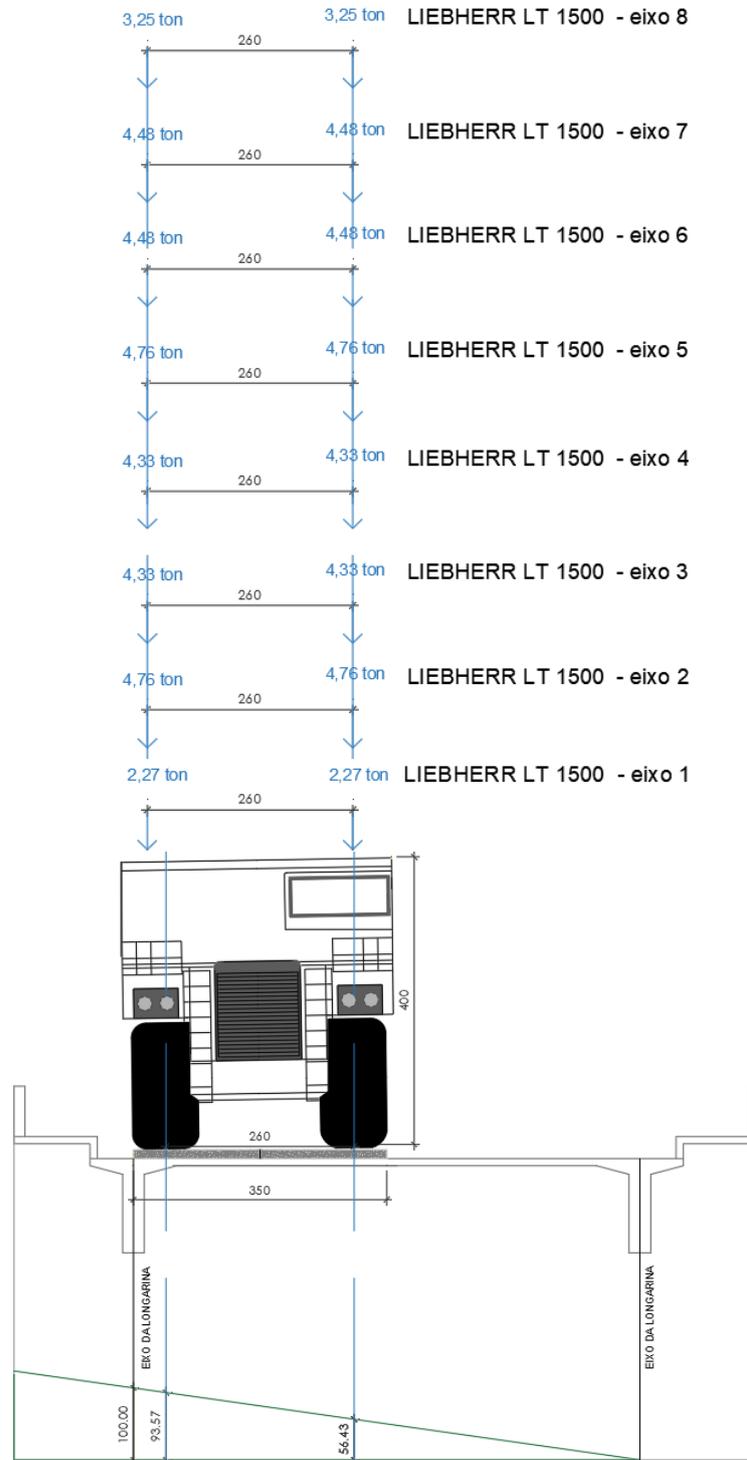
$$\text{EIXO 7} = 4,48 \times (1,0545 + 0,5818) = 7,331 \text{ ton}$$

$$\text{EIXO 8} = 3,25 \times (1,0545 + 0,5818) = 5,318 \text{ ton}$$



NOTA TÉCNICA

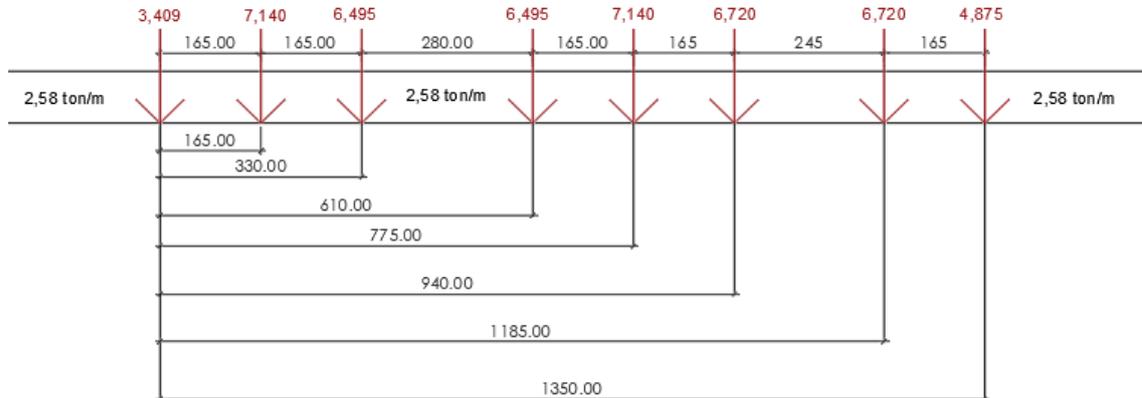
5.3.3. Tabuleiro 10,30 m



MULTIDÃO =  $0,5 \times 5,1607 = 2,58 \text{ ton/m}$



### NOTA TÉCNICA



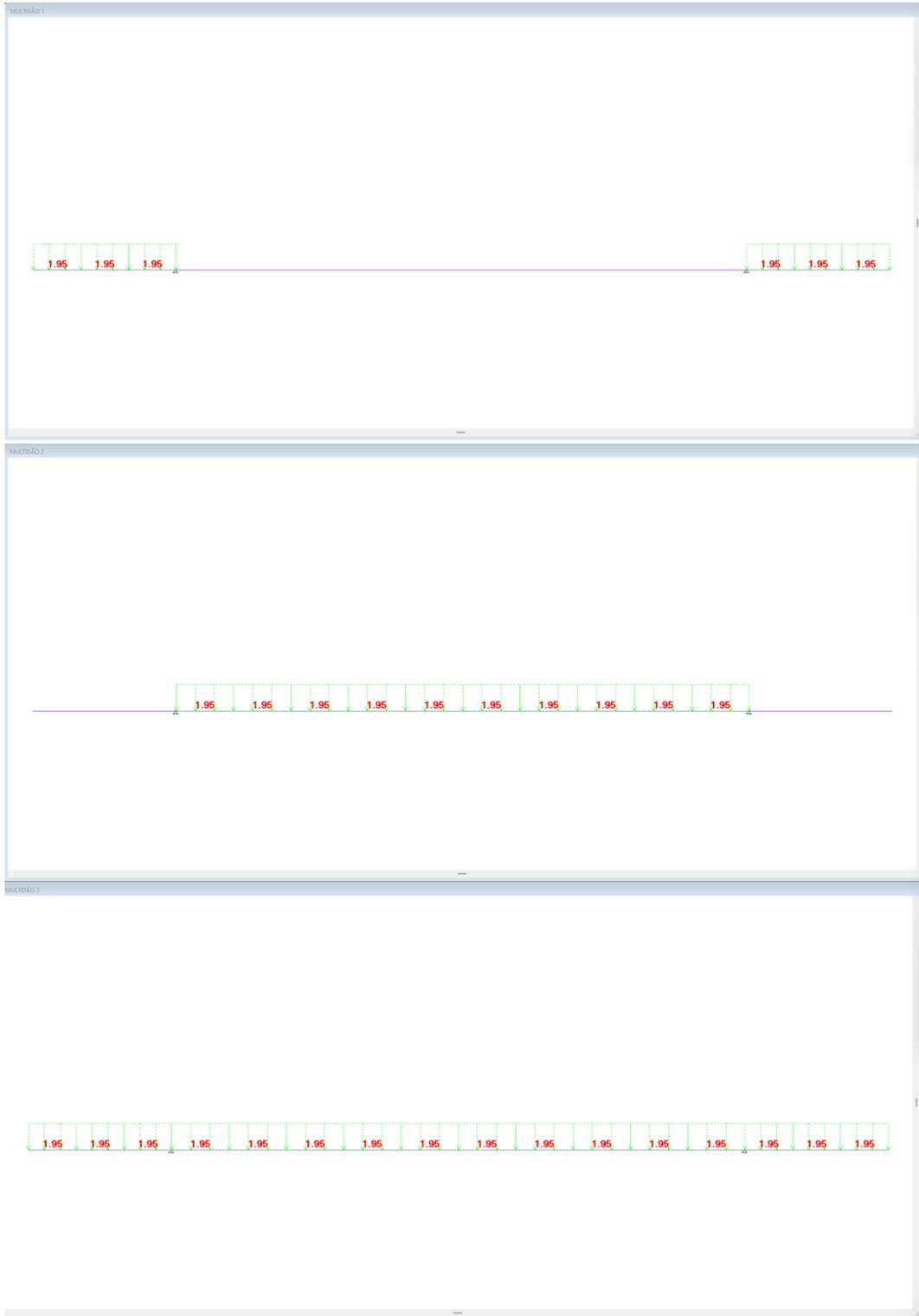
EIXO 1 = $2,27 \times (0,9357 + 0,5643) = 3,405$ ton	EIXO 5 = $4,76 \times (0,9357 + 0,5643) = 7,140$ ton
EIXO 2 = $4,76 \times (0,9357 + 0,5643) = 7,140$ ton	EIXO 6 = $4,48 \times (0,9357 + 0,5643) = 6,720$ ton
EIXO 3 = $4,33 \times (0,9357 + 0,5643) = 6,495$ ton	EIXO 7 = $4,48 \times (0,9357 + 0,5643) = 6,720$ ton
EIXO 4 = $4,33 \times (0,9357 + 0,5643) = 6,495$ ton	EIXO 8 = $3,25 \times (0,9357 + 0,5643) = 4,875$ ton



NOTA TÉCNICA

### 5.4. Cargas acidentais (TB-24 e Guindaste) – Momentos e cortantes

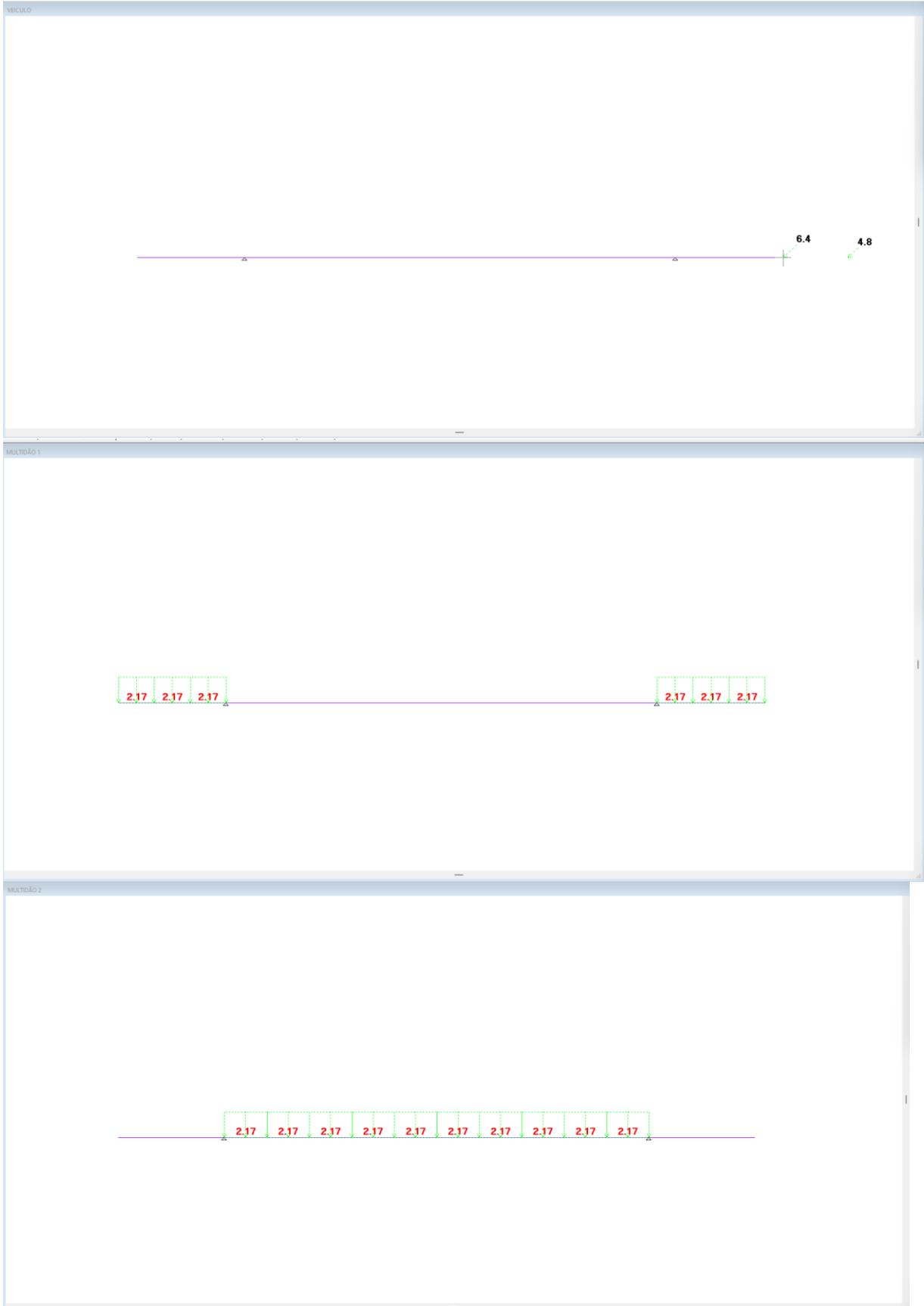
#### 5.4.1. Tabuleiro 8,30 m





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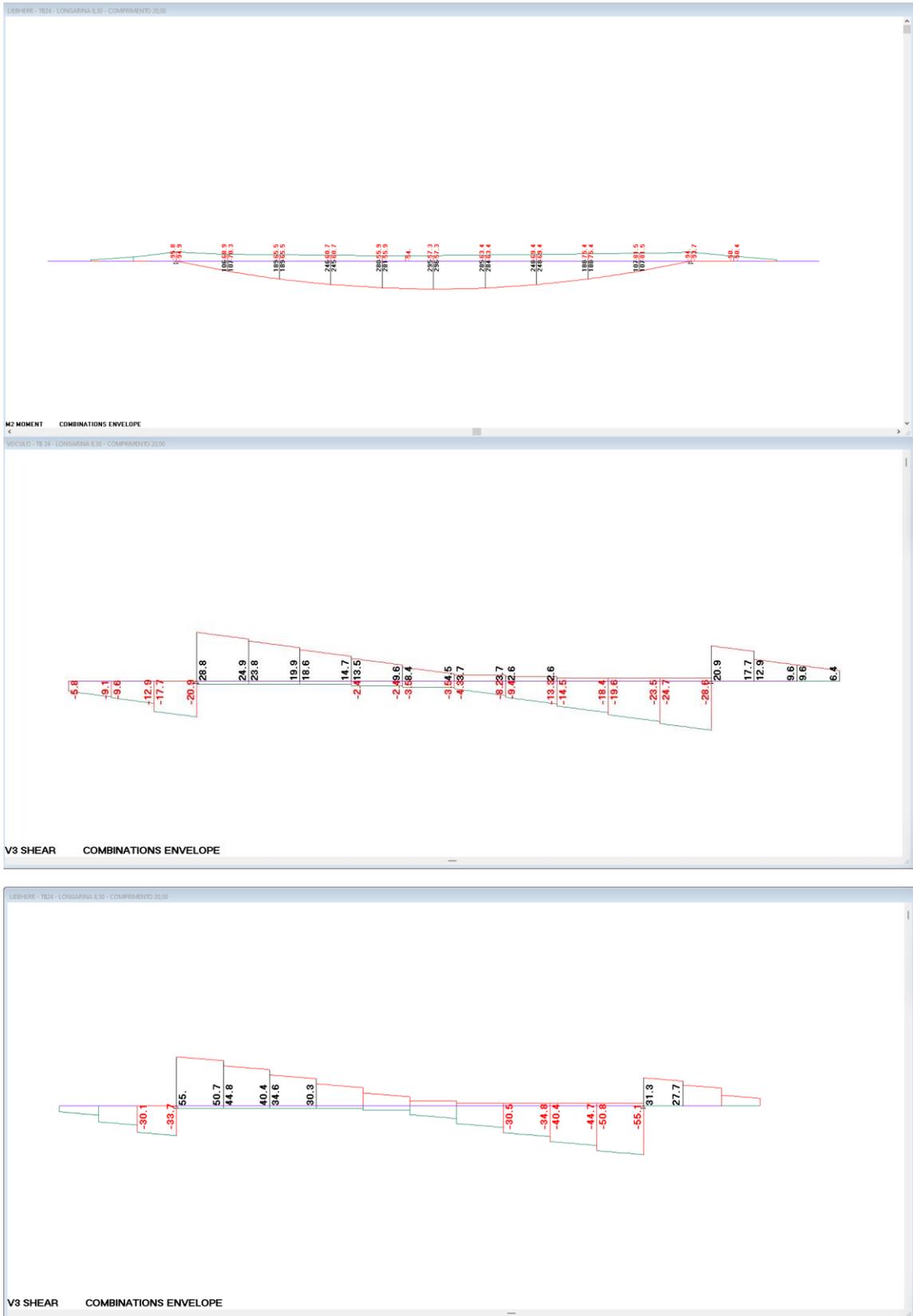
### NOTA TÉCNICA





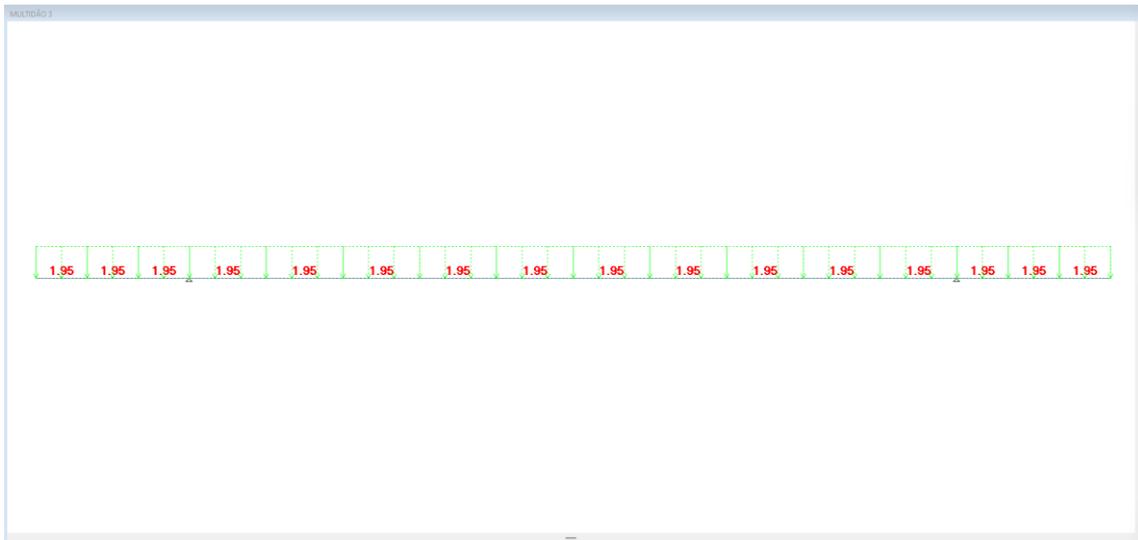
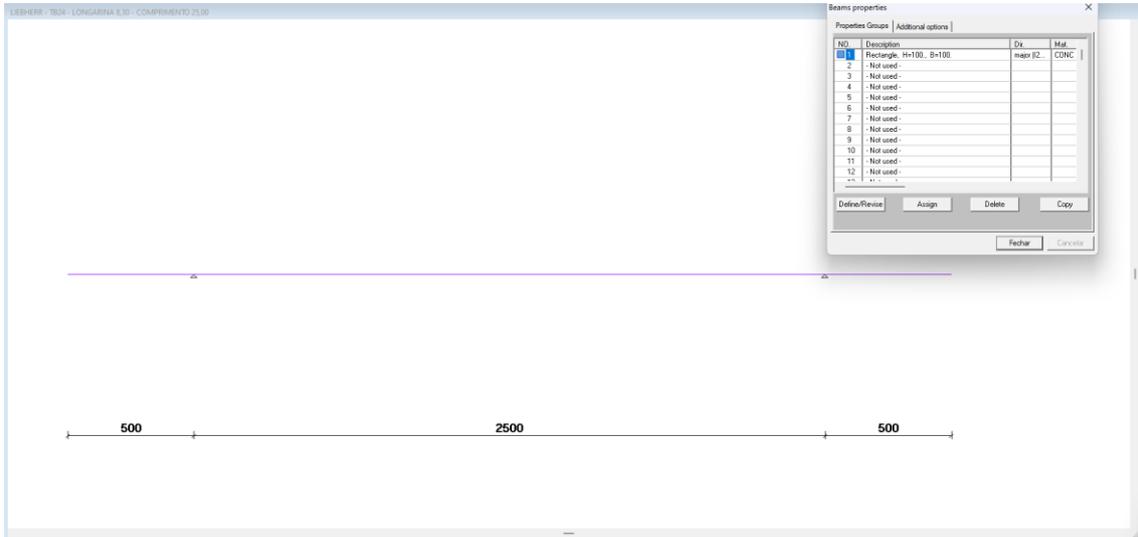


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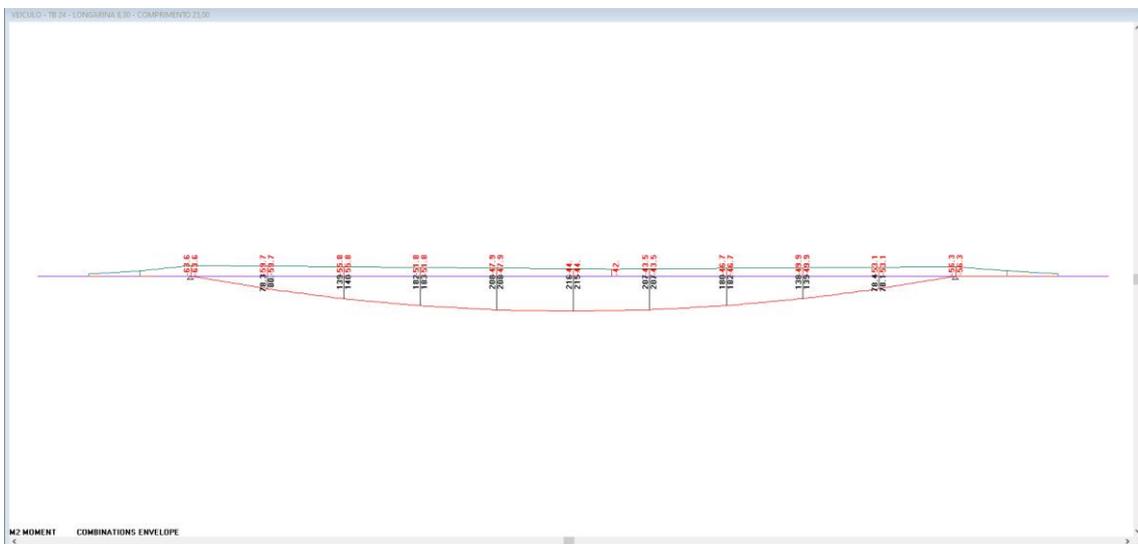
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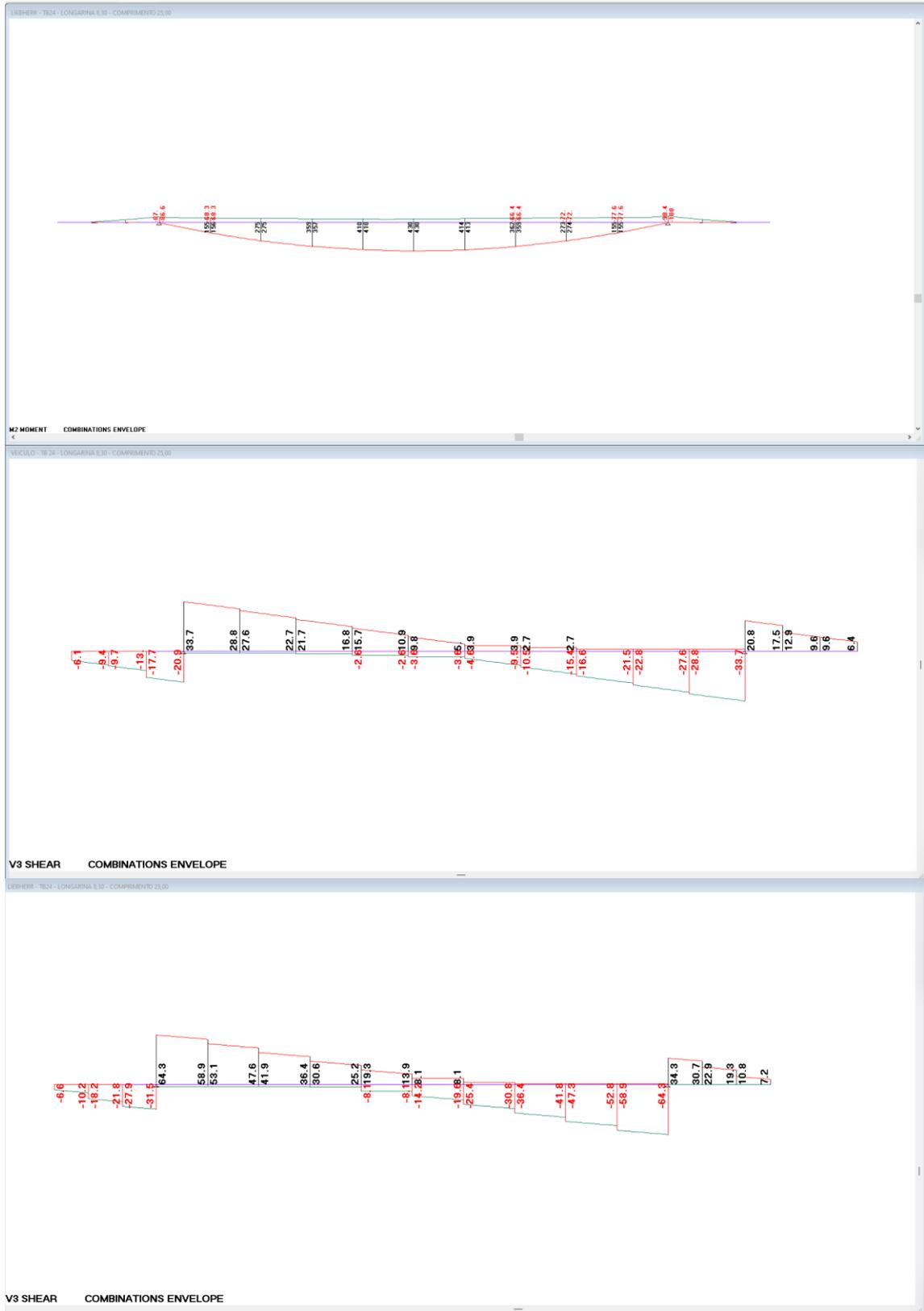
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### NOTA TÉCNICA



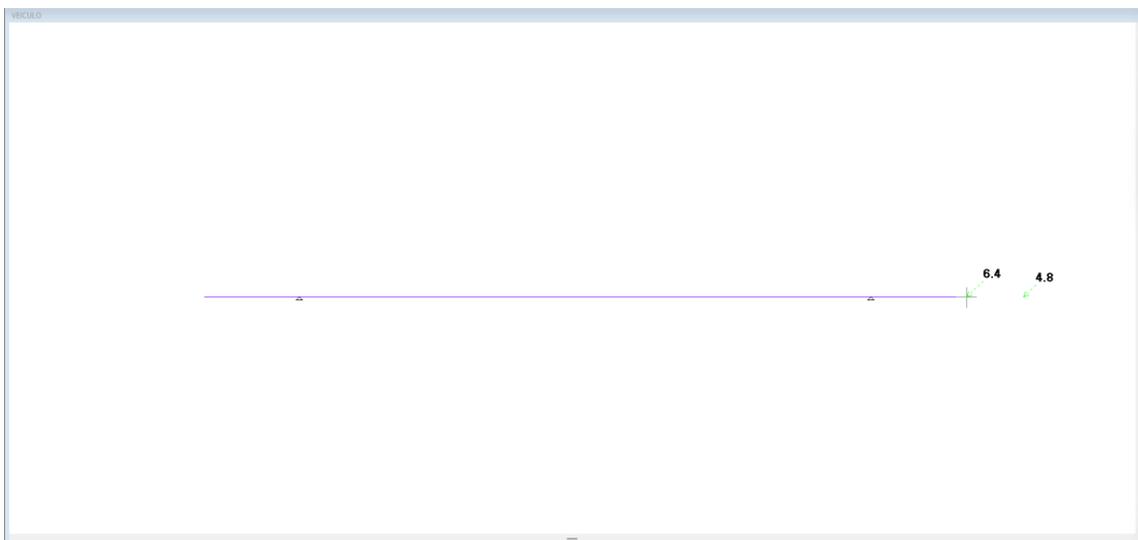


### NOTA TÉCNICA





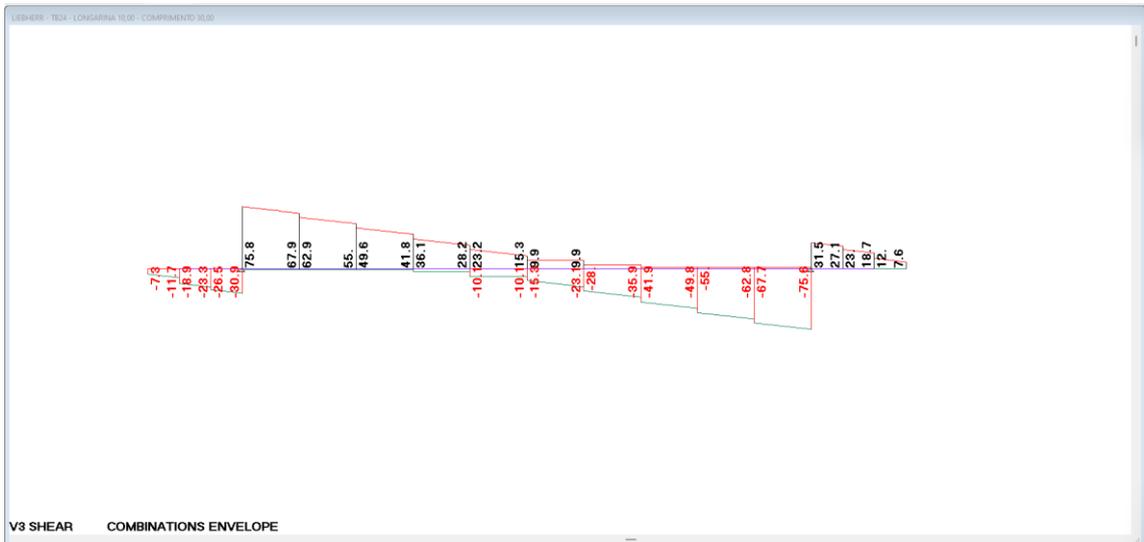
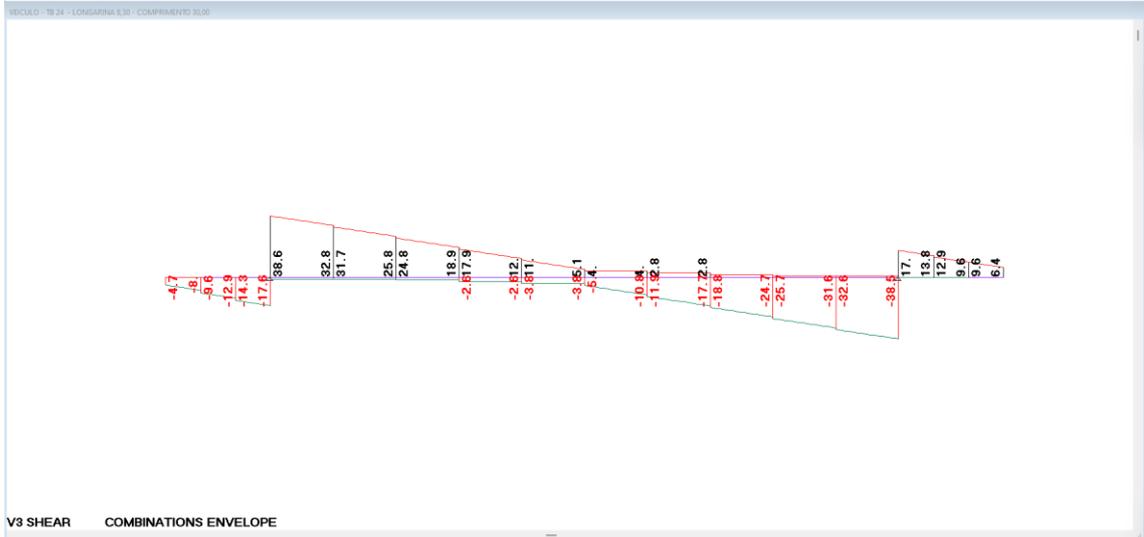
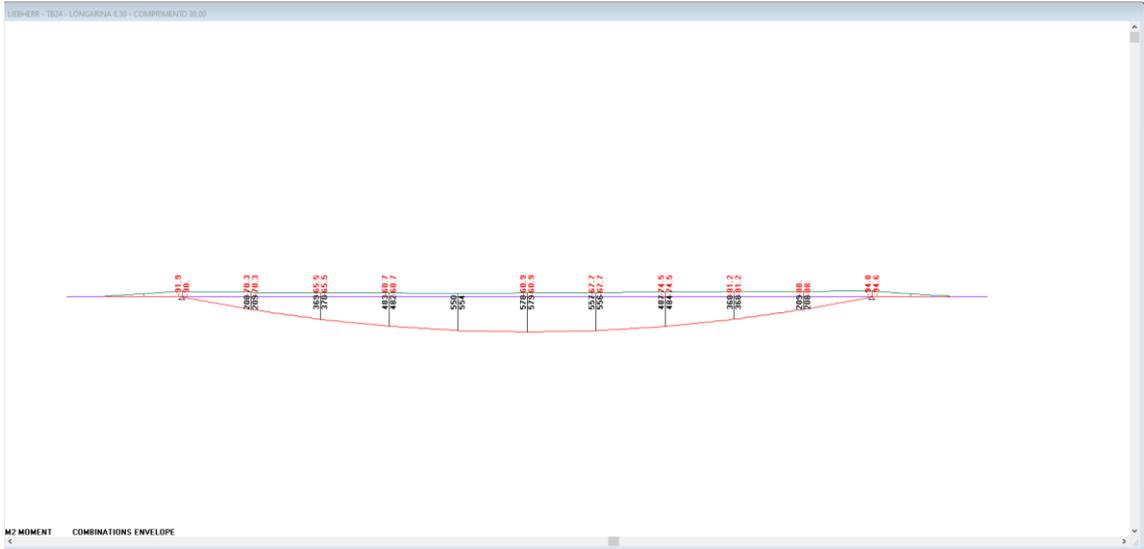
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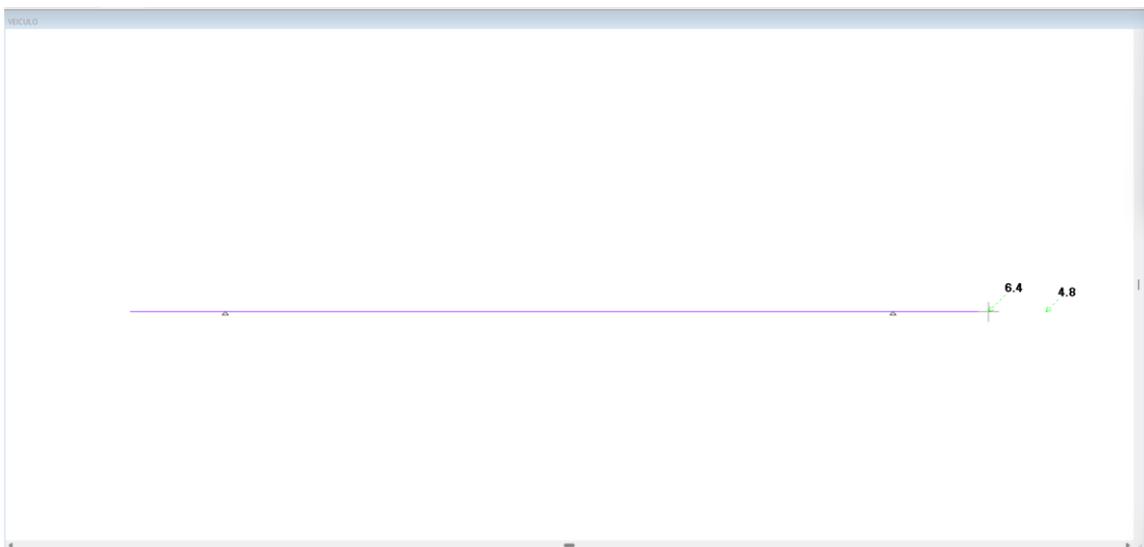
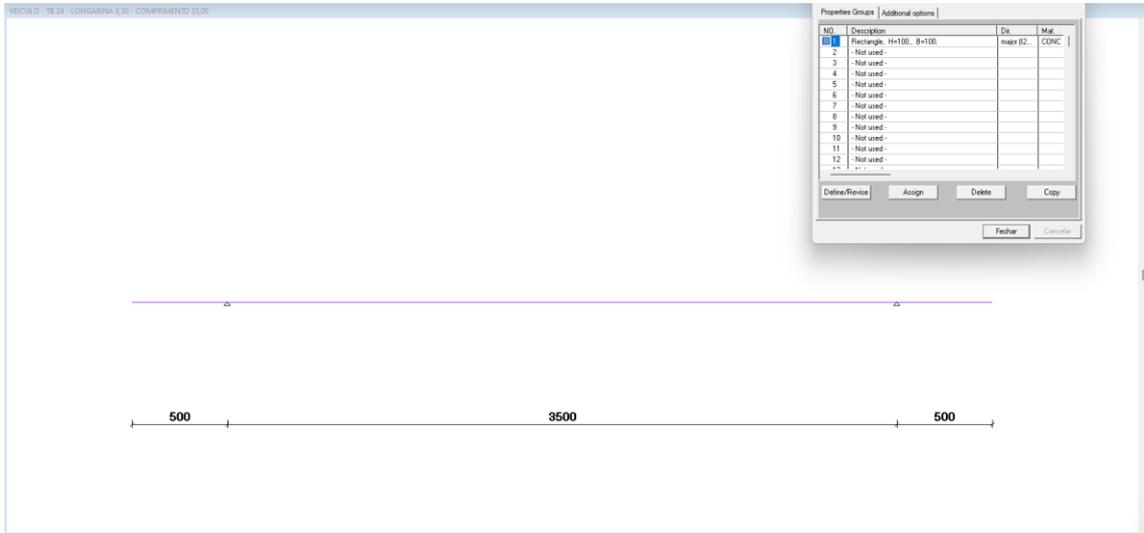


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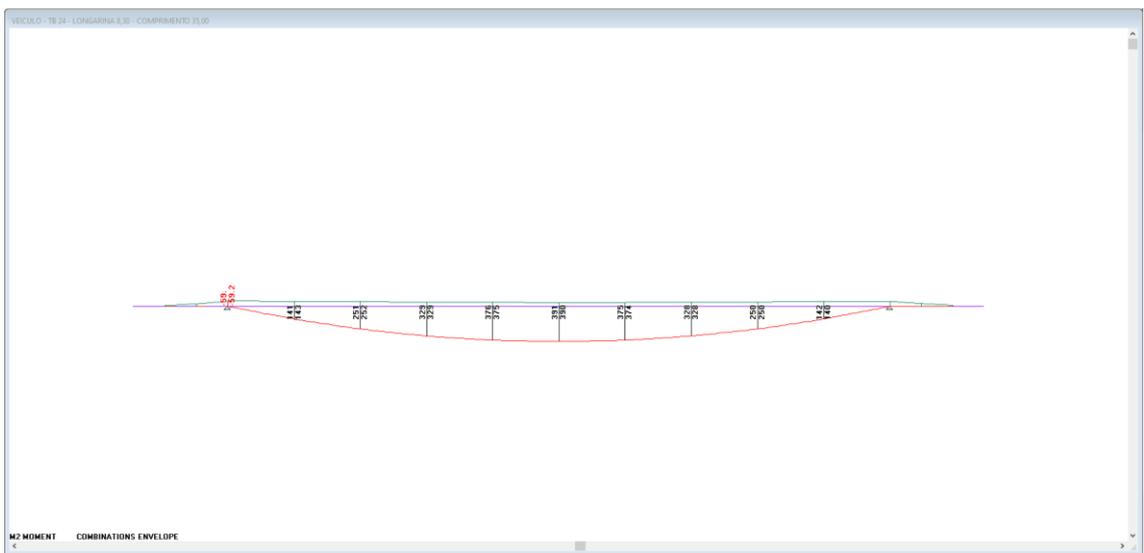
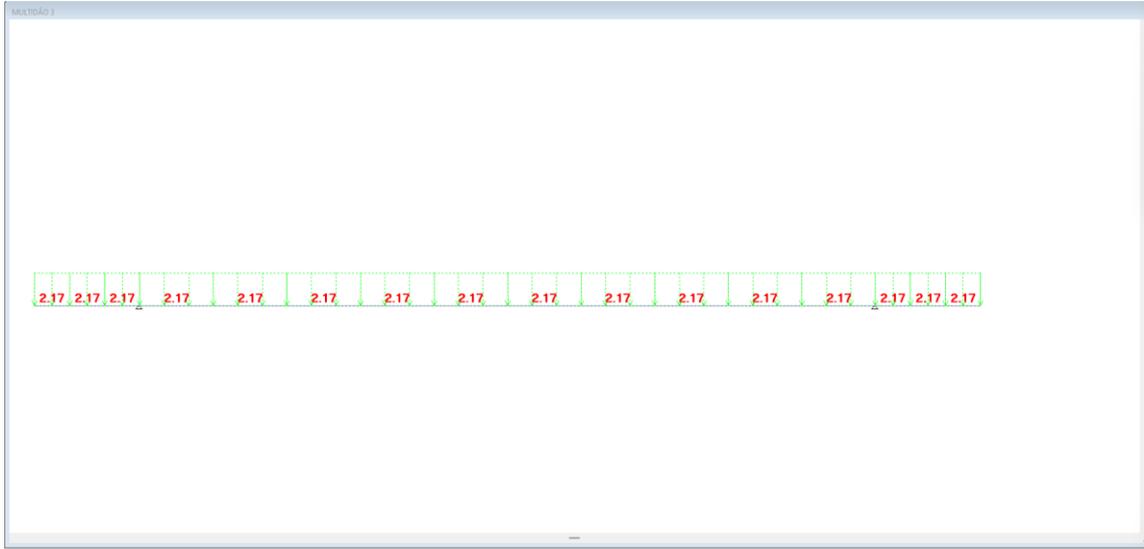
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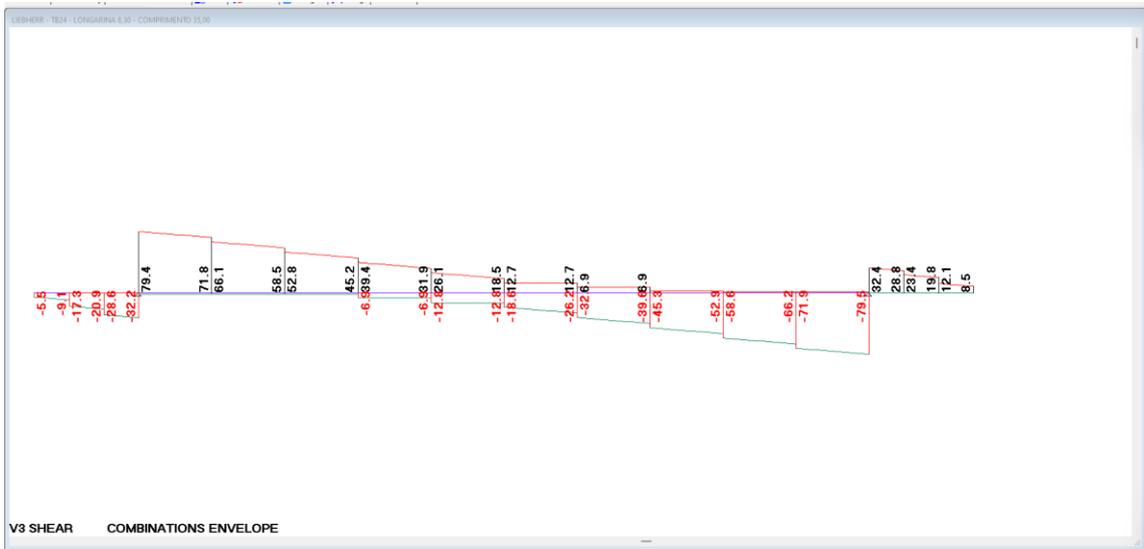
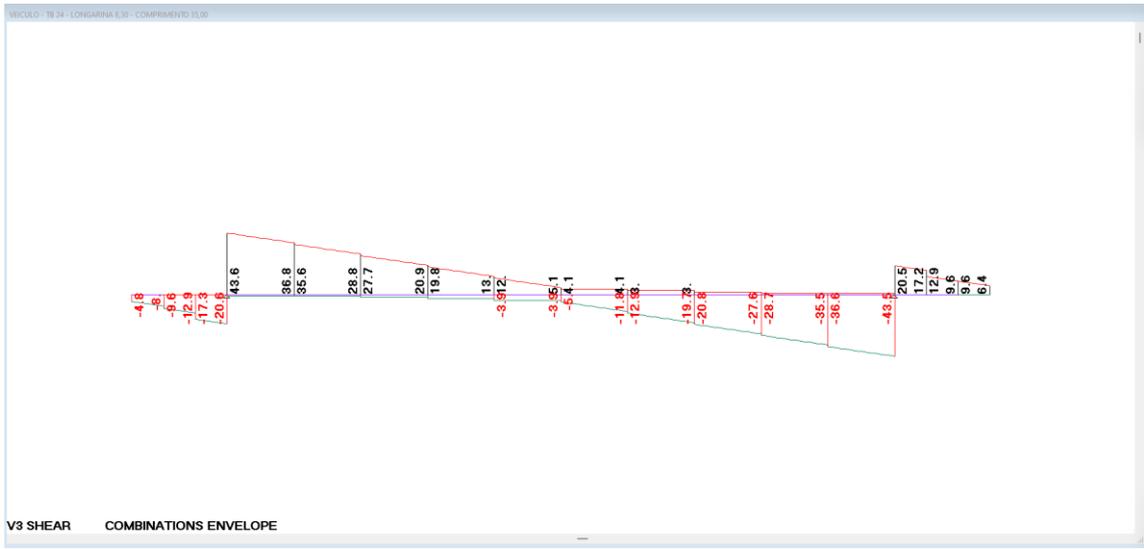
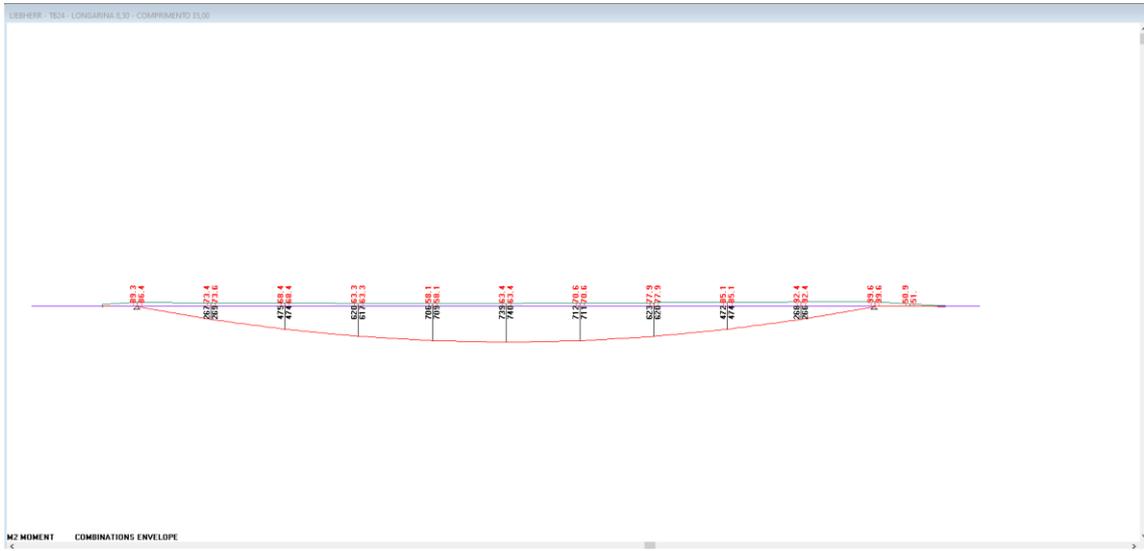
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### NOTA TÉCNICA





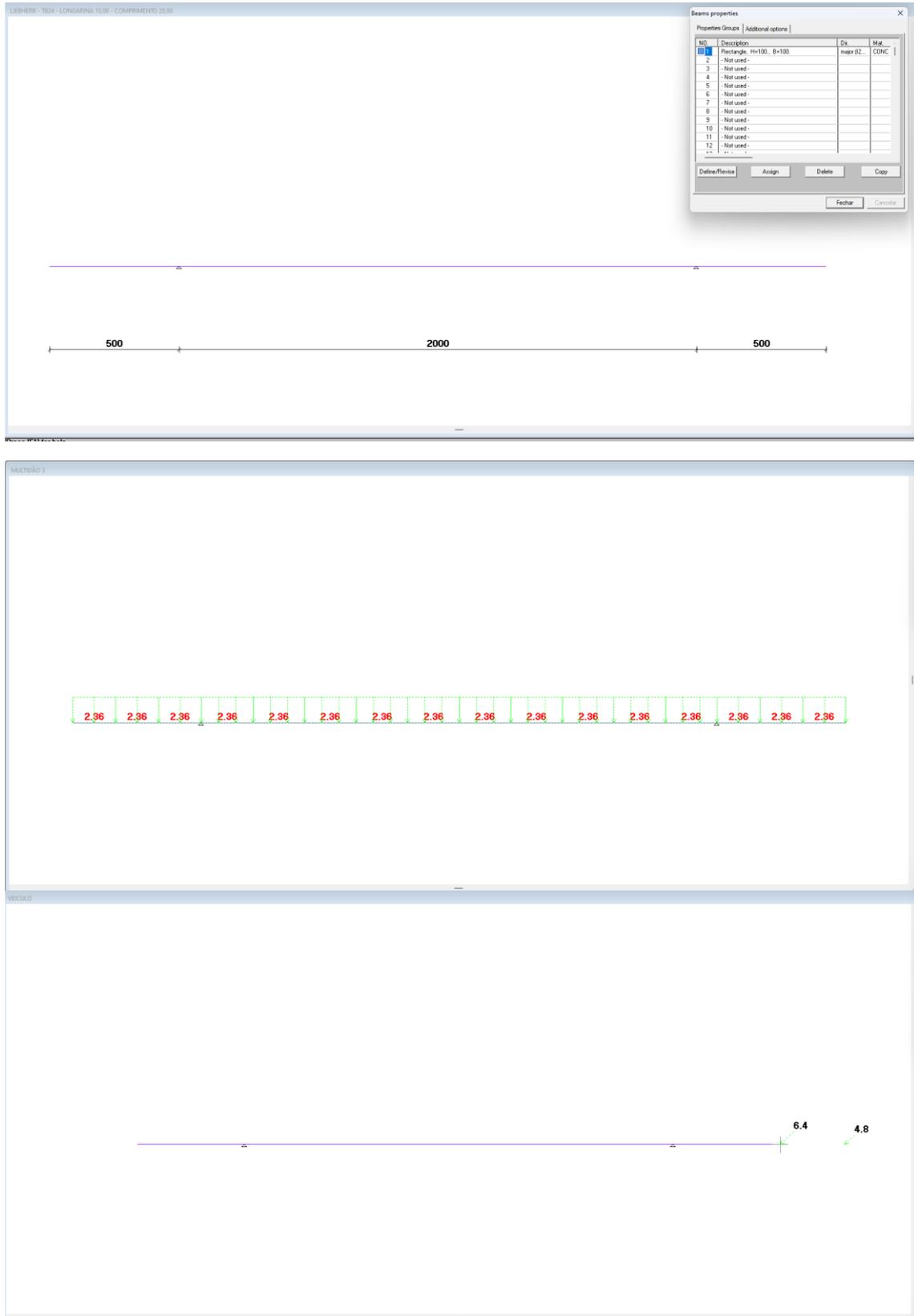
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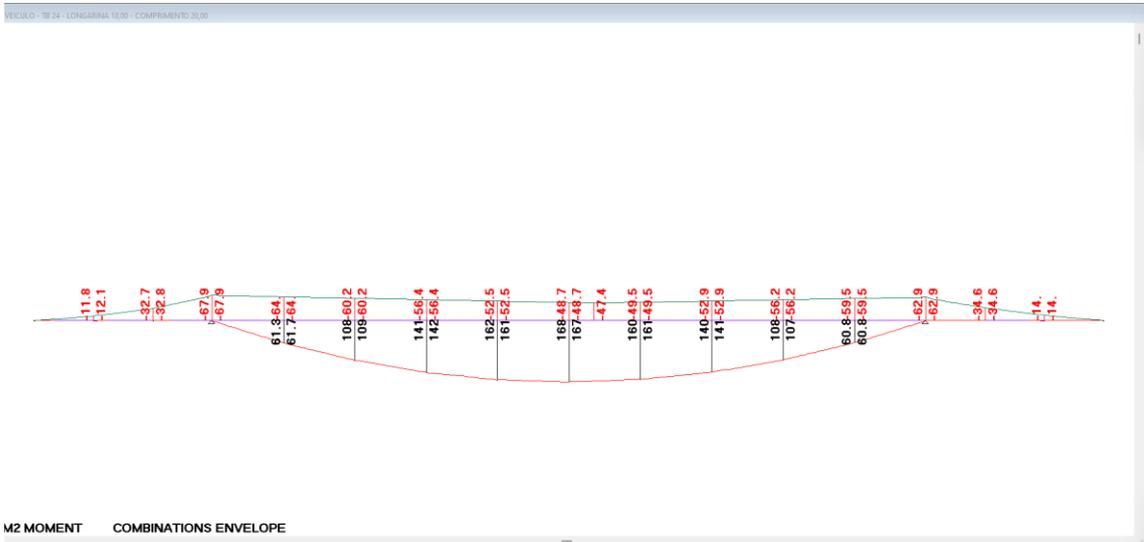
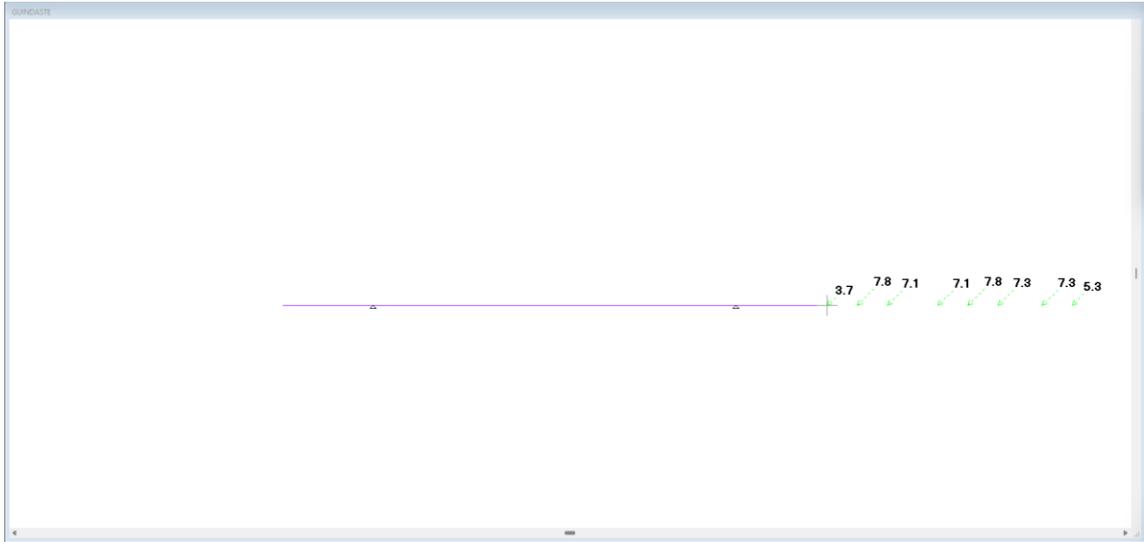
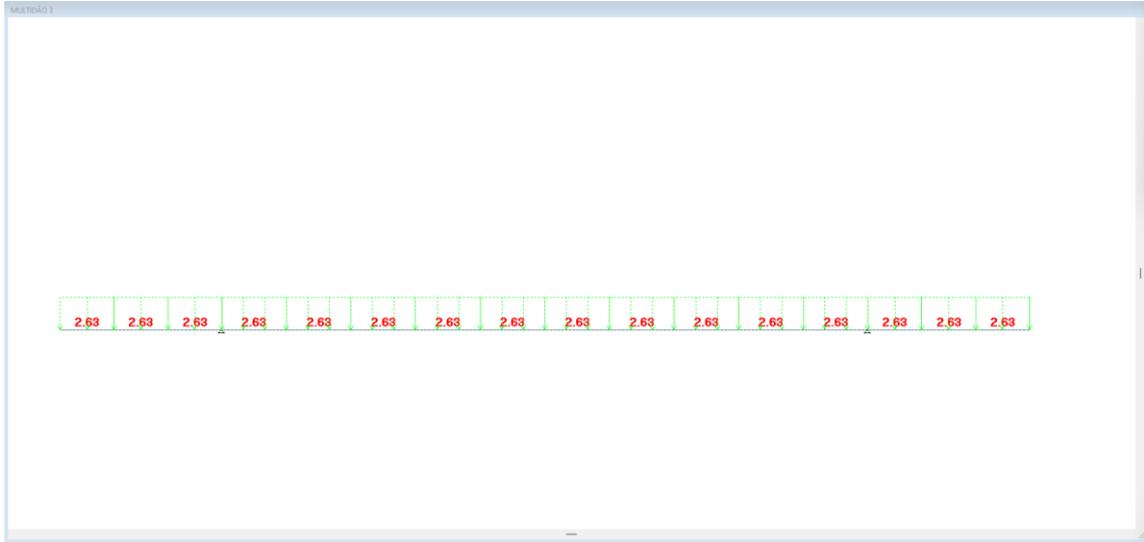
### NOTA TÉCNICA

#### 5.4.2. Tabuleiro 10,00 m



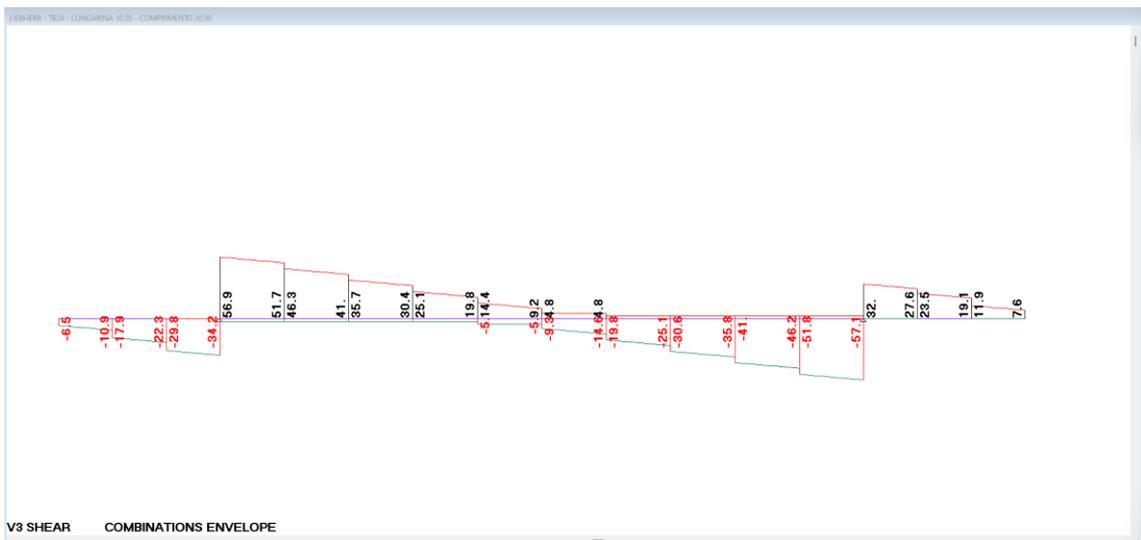
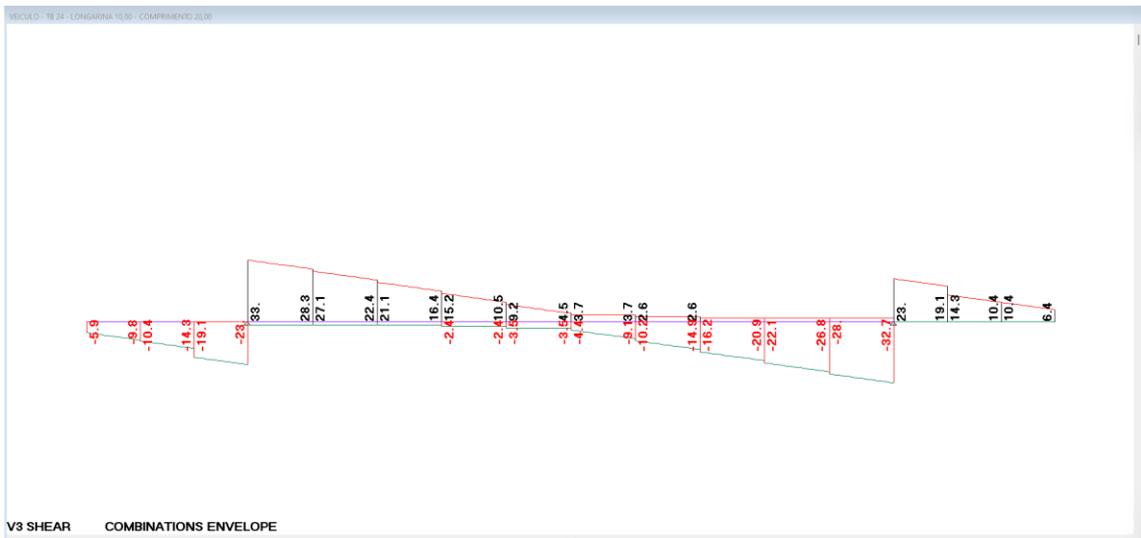
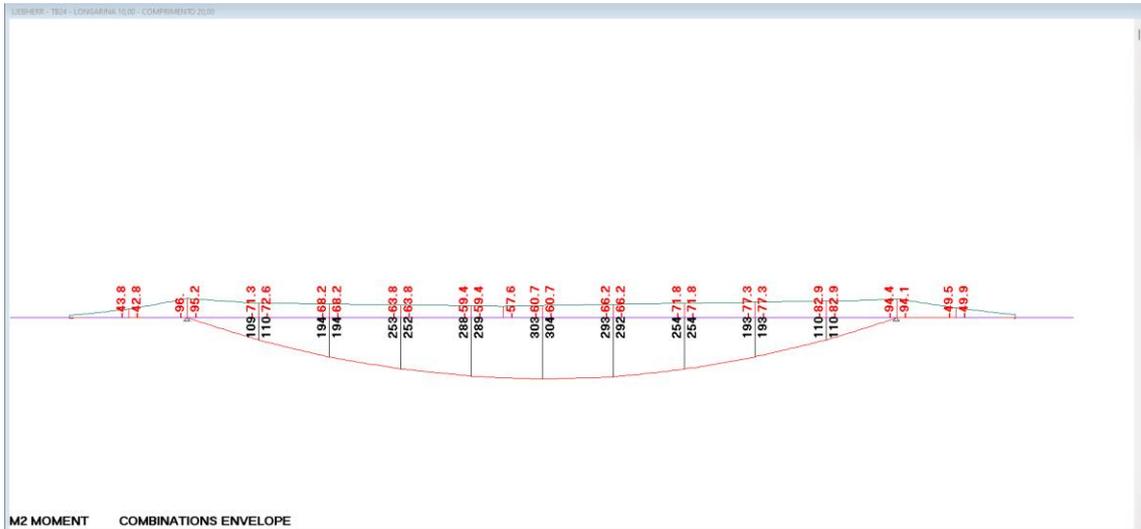


### NOTA TÉCNICA



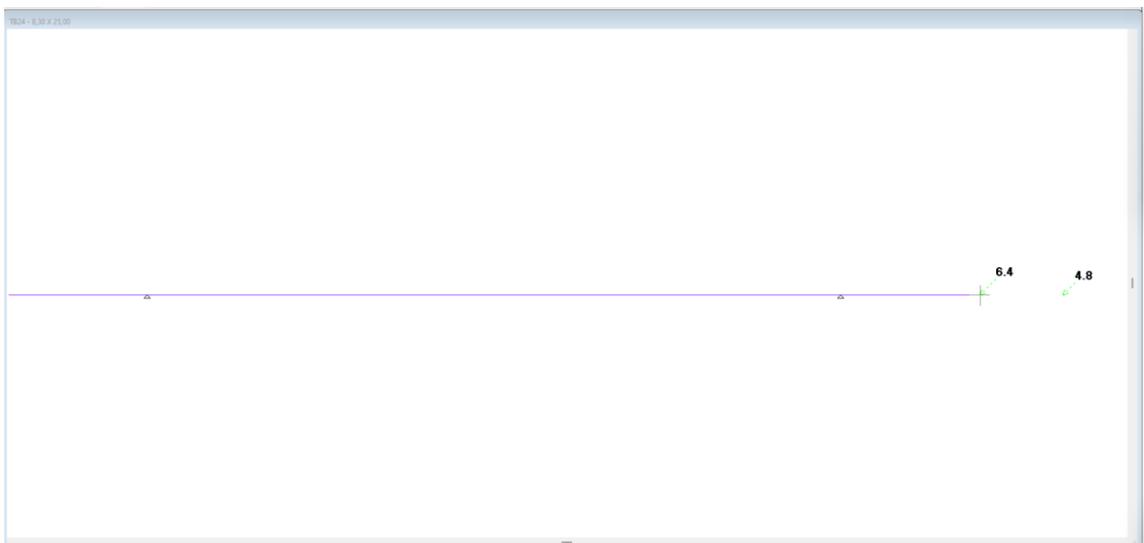


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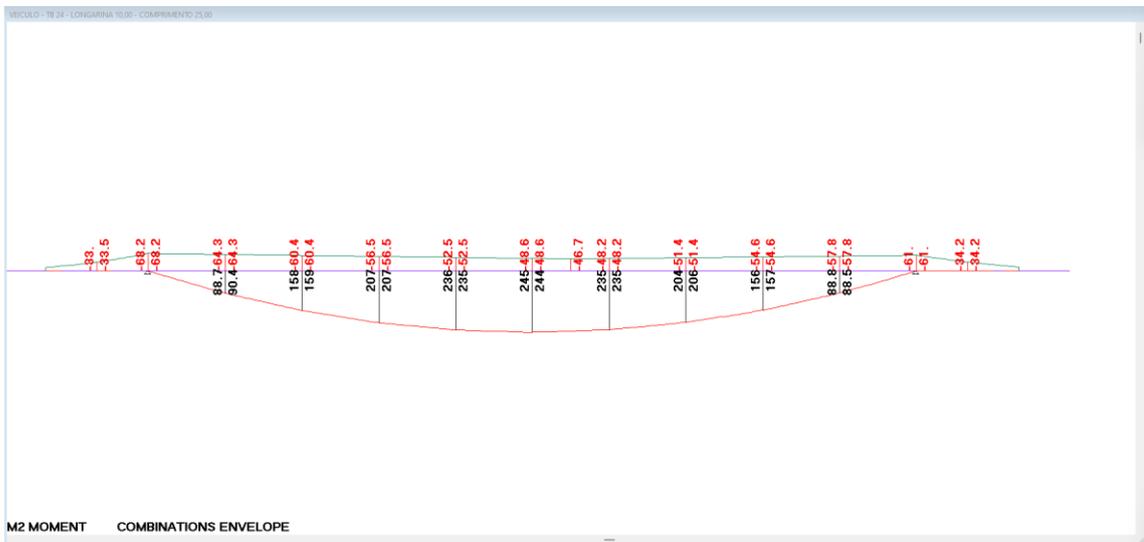
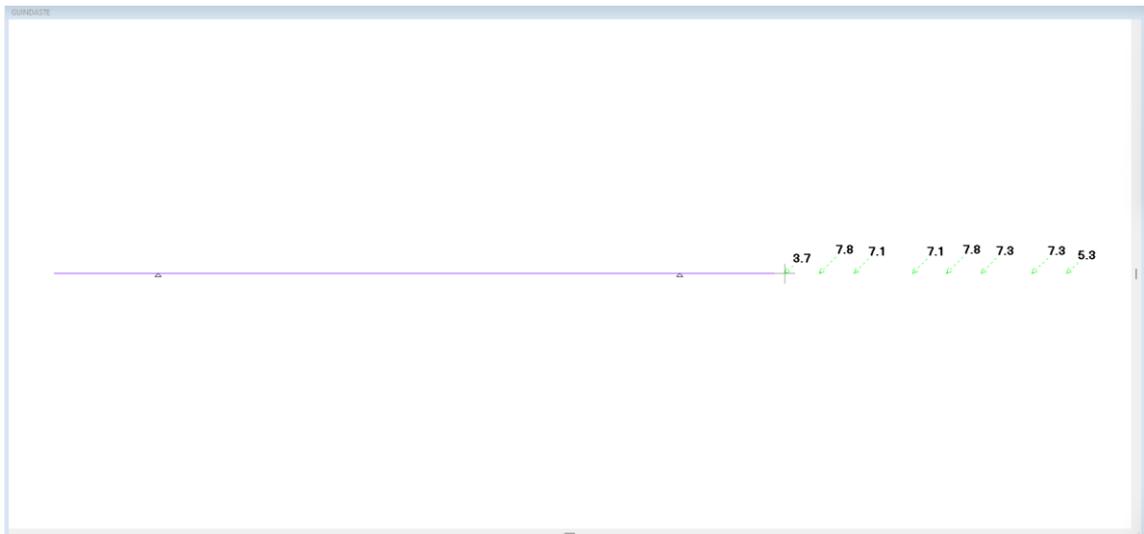
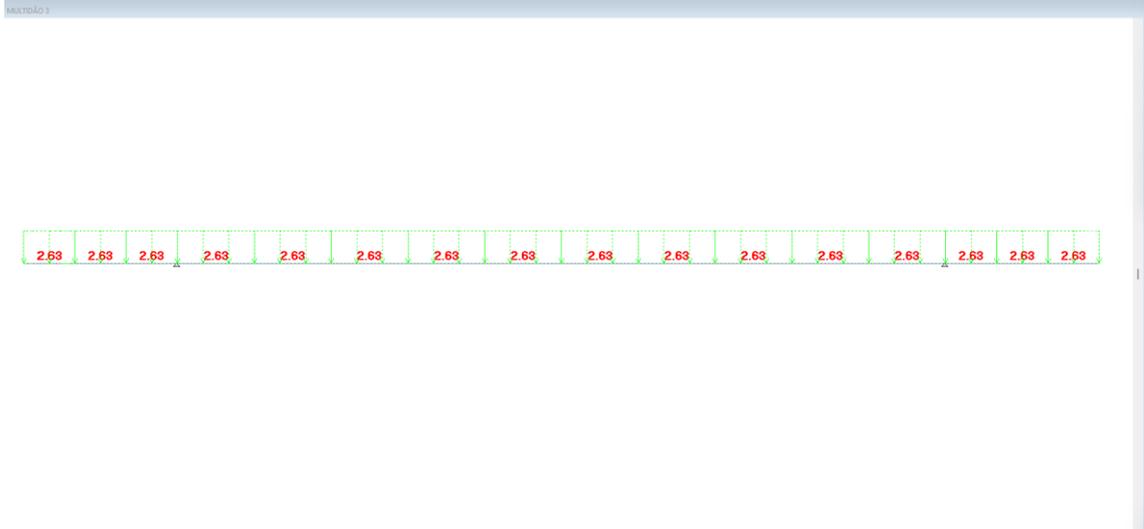


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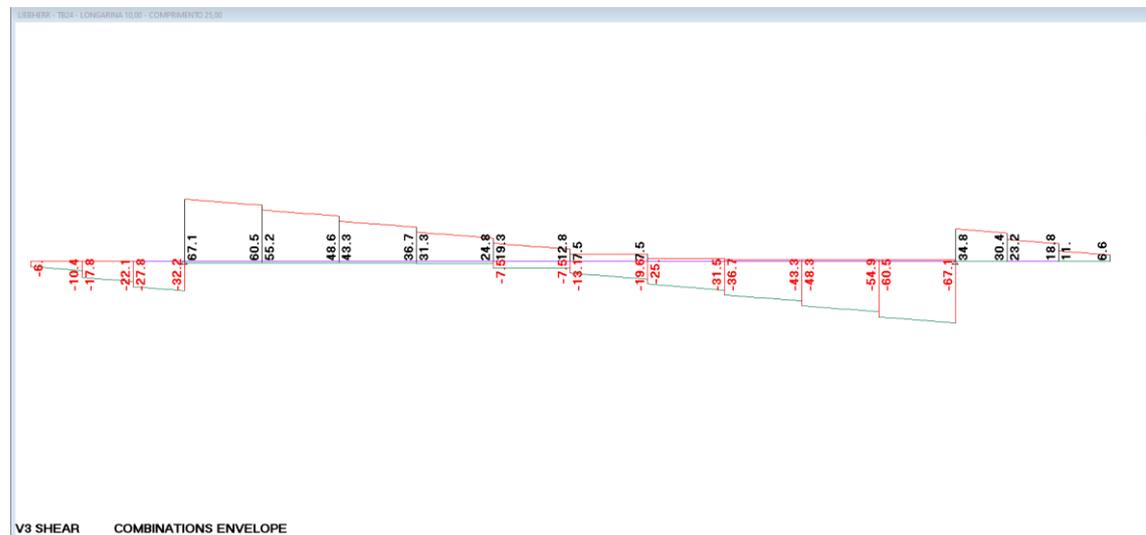
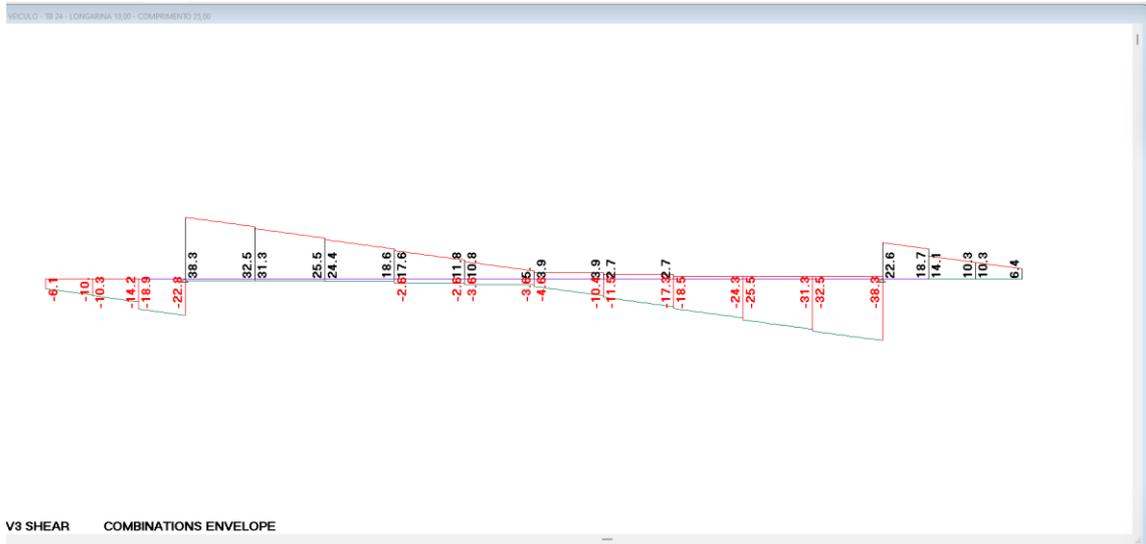
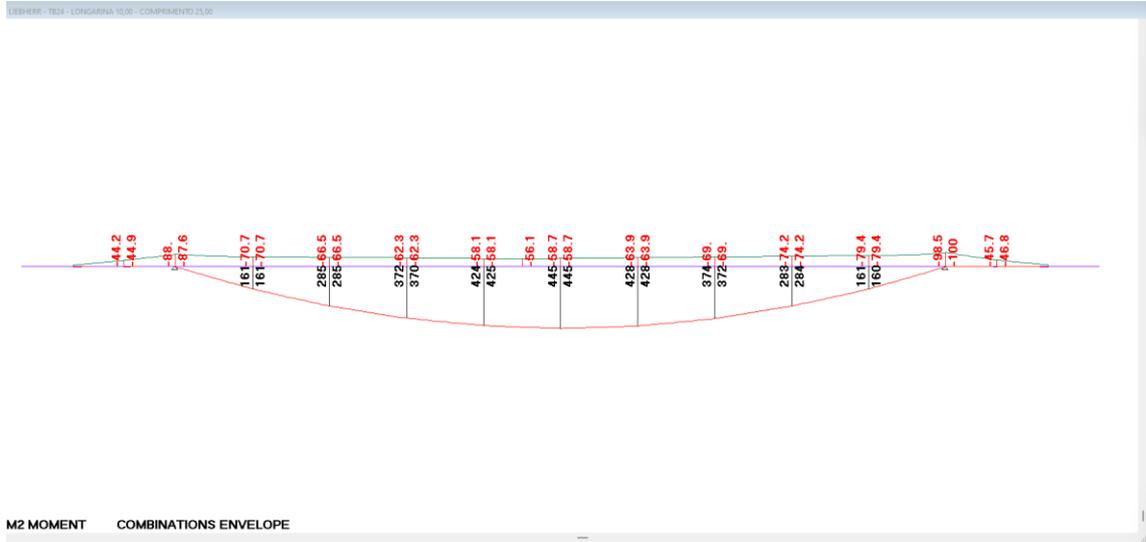


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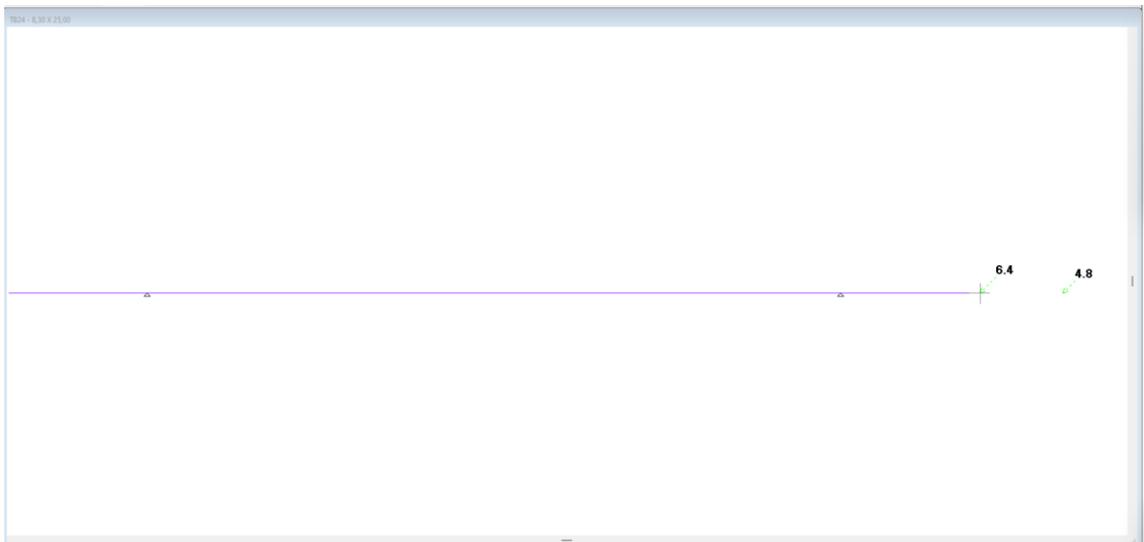
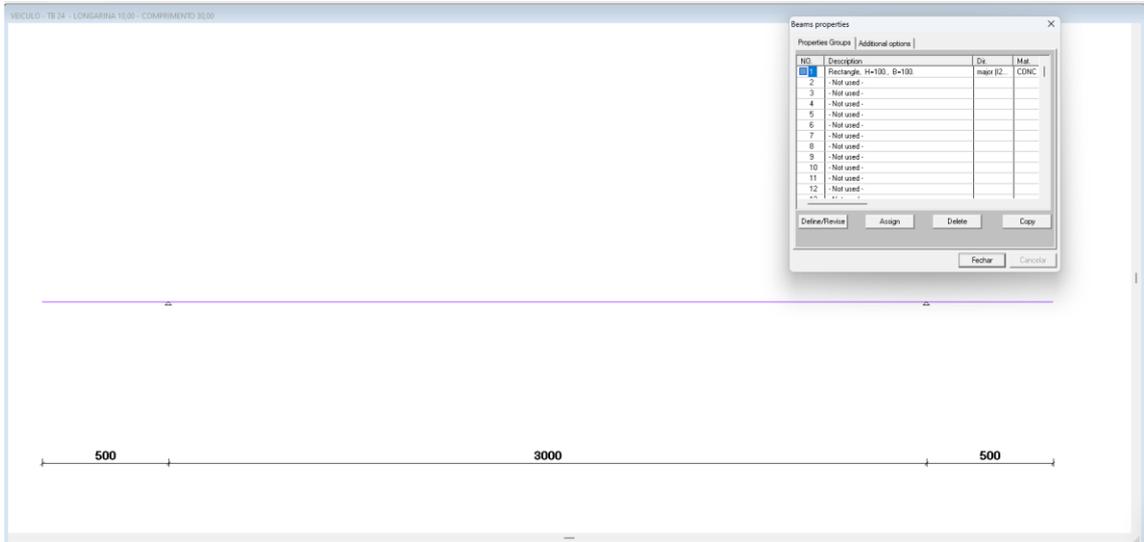


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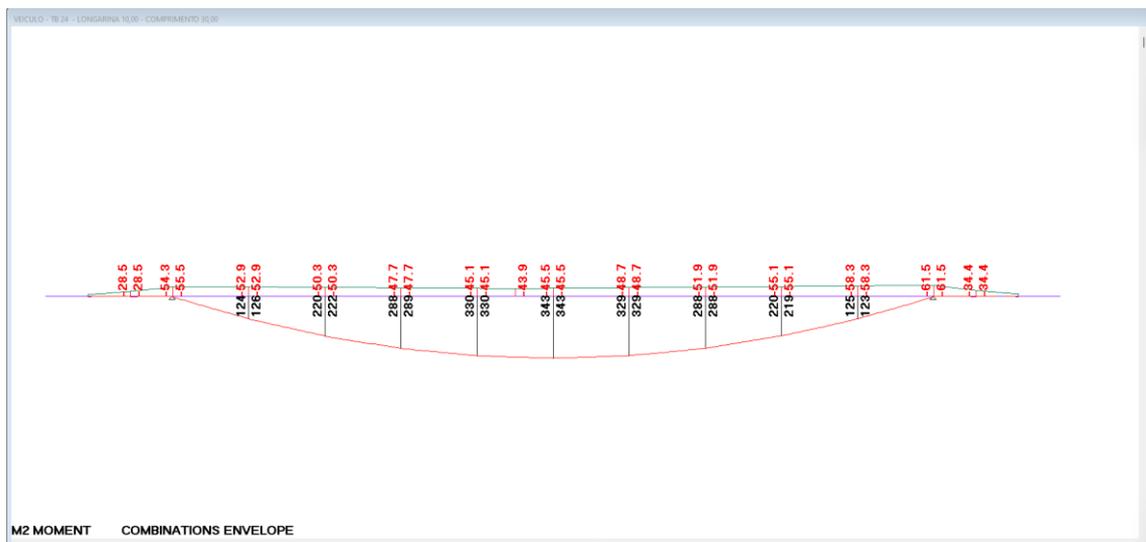
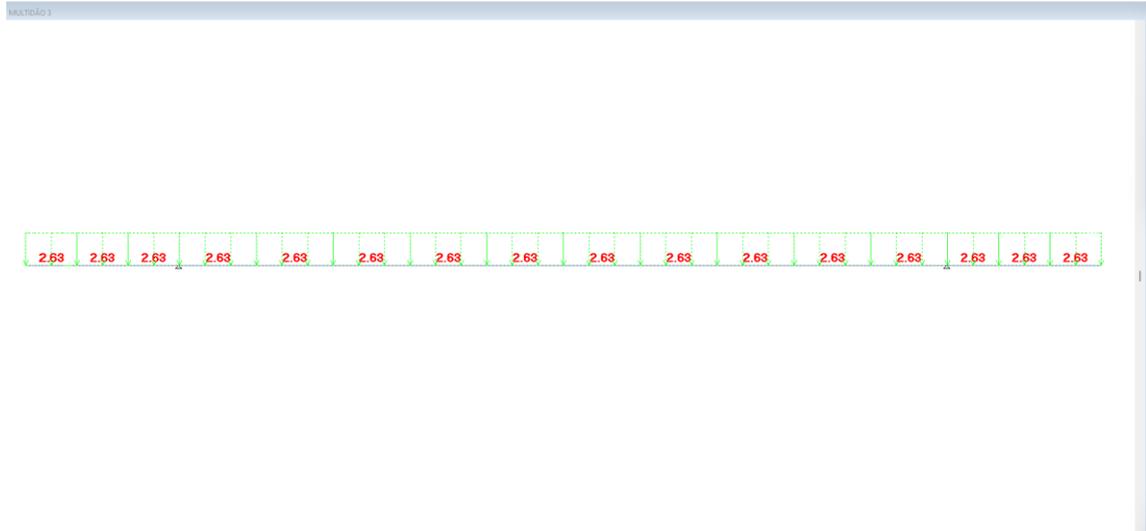
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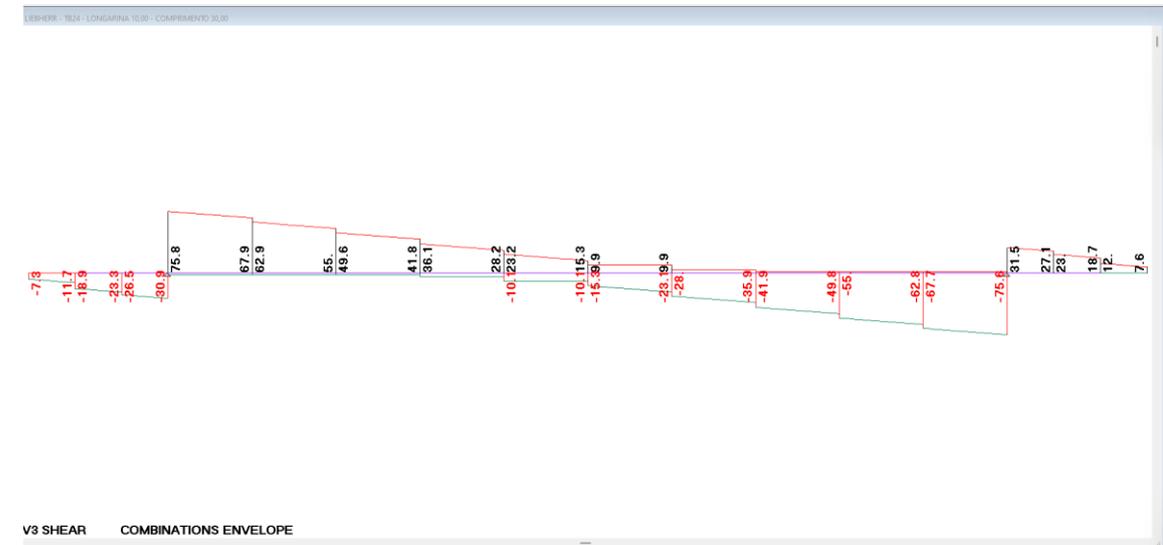
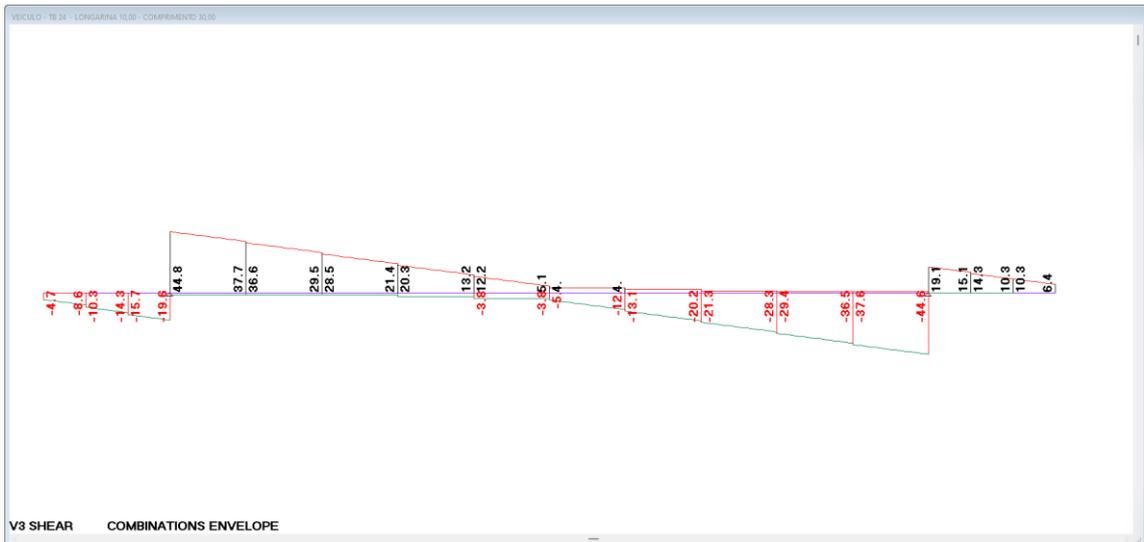
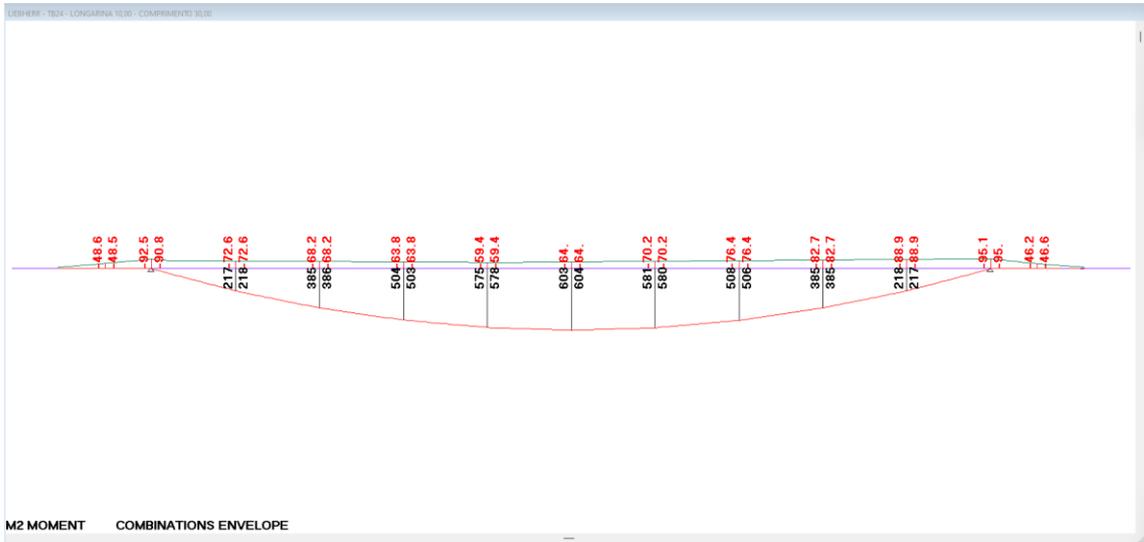
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### NOTA TÉCNICA



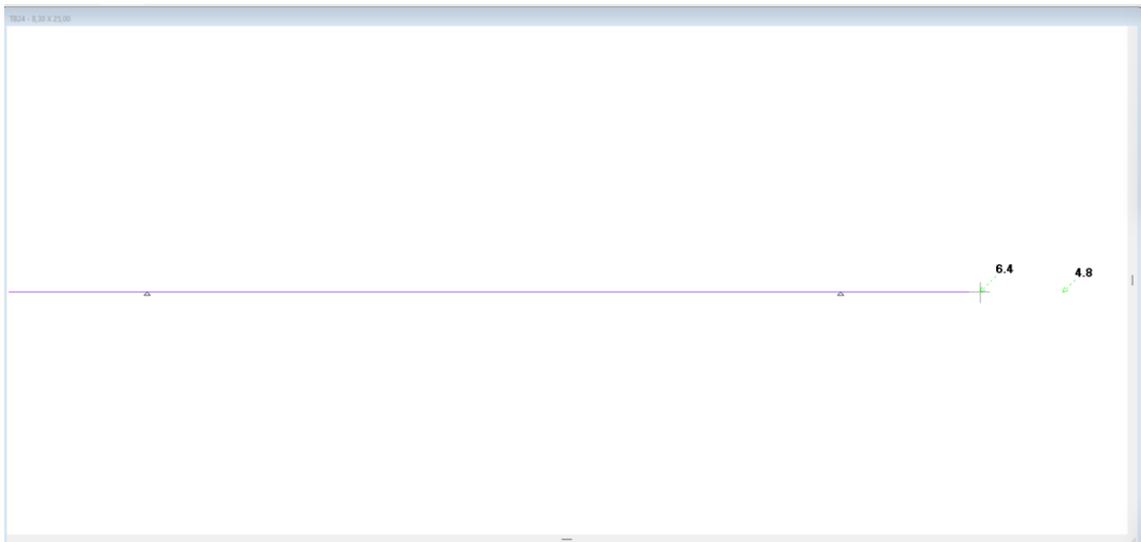
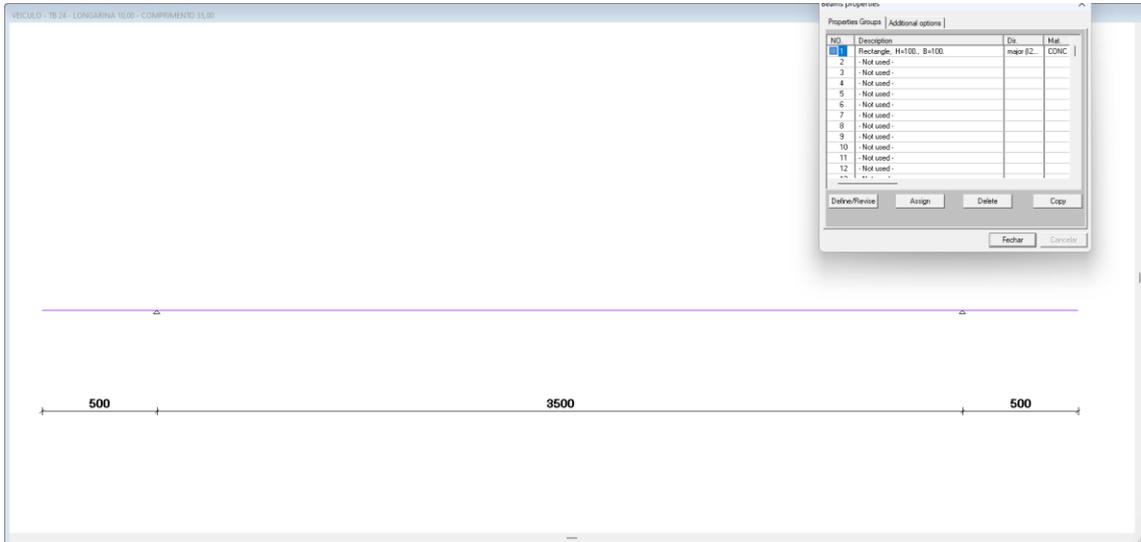


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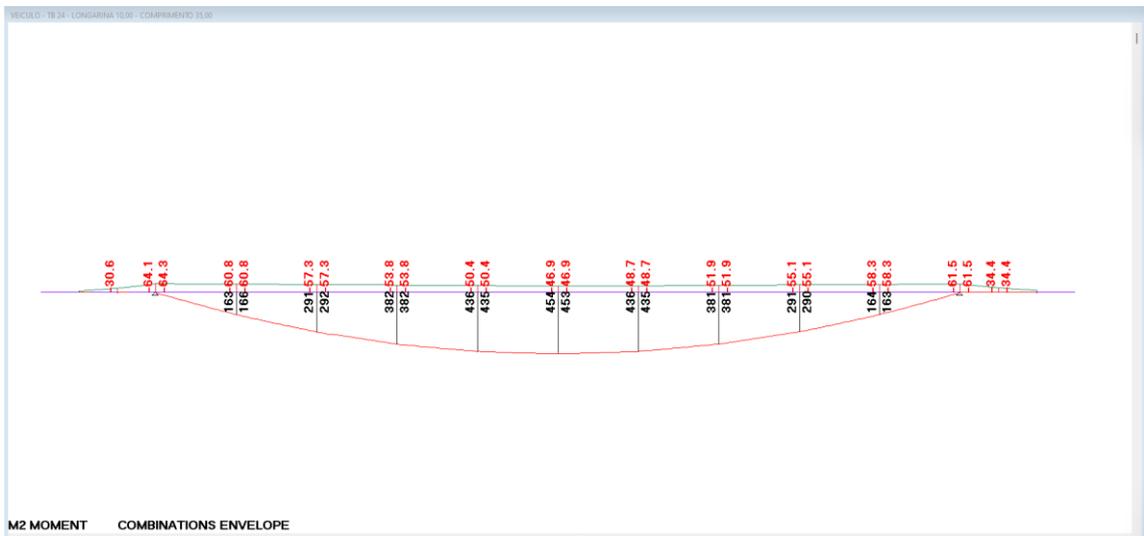
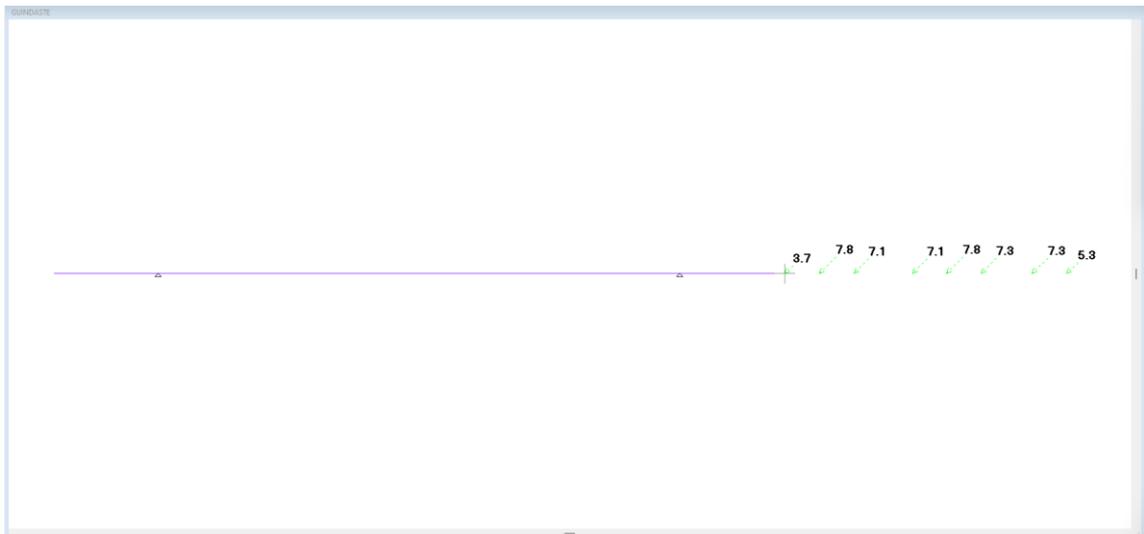
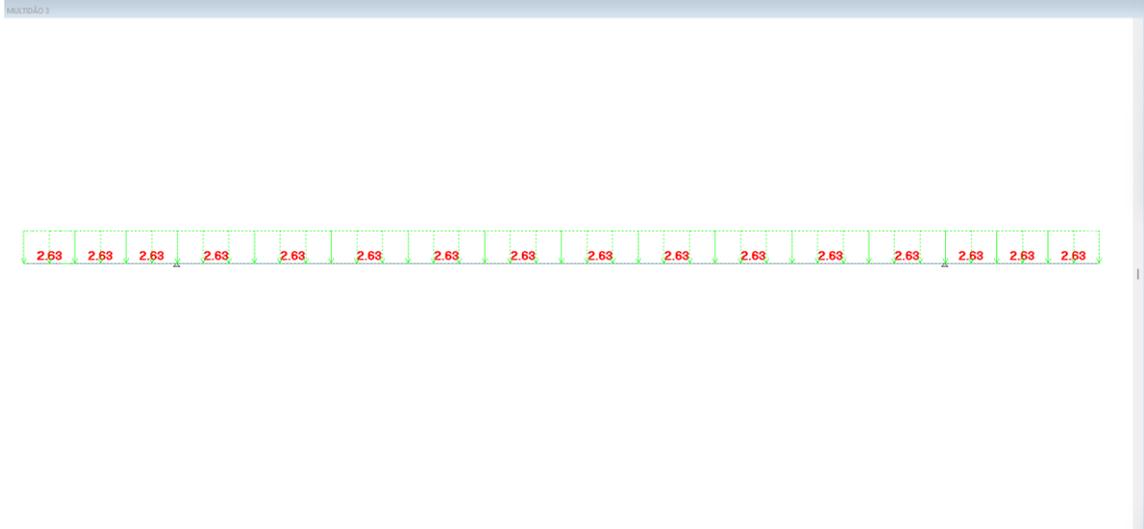


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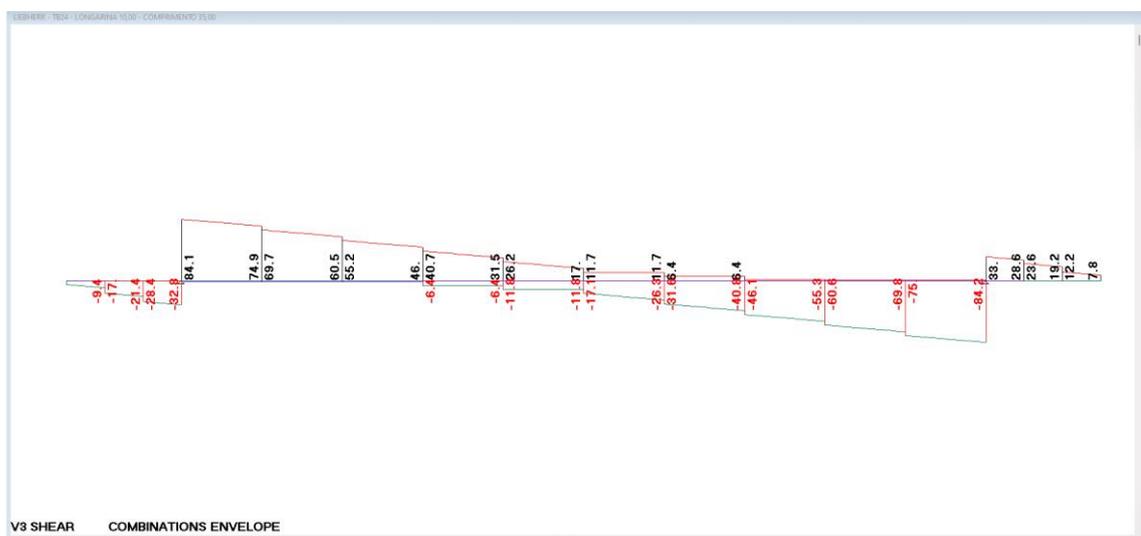
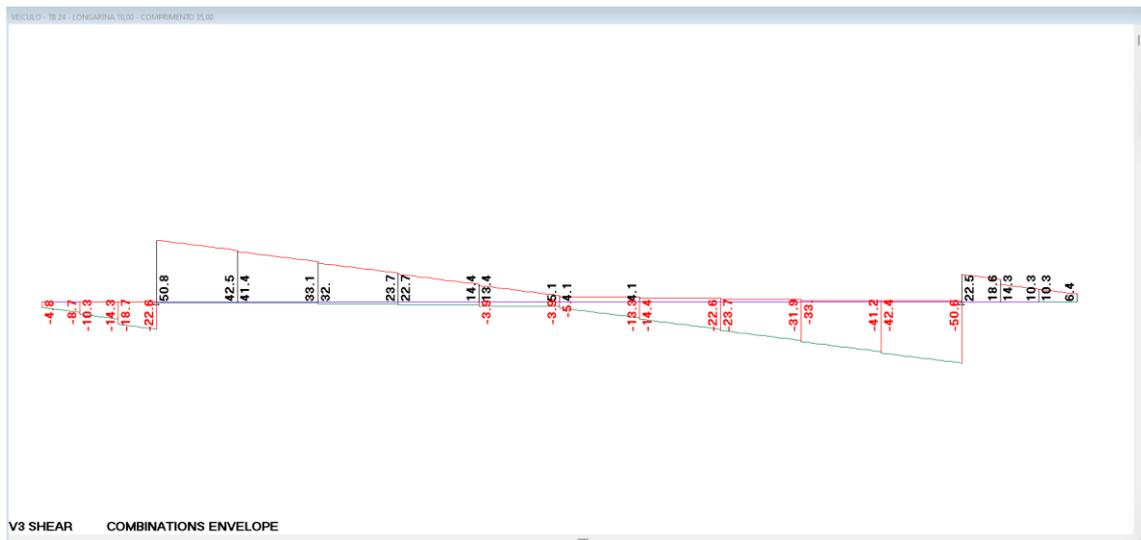
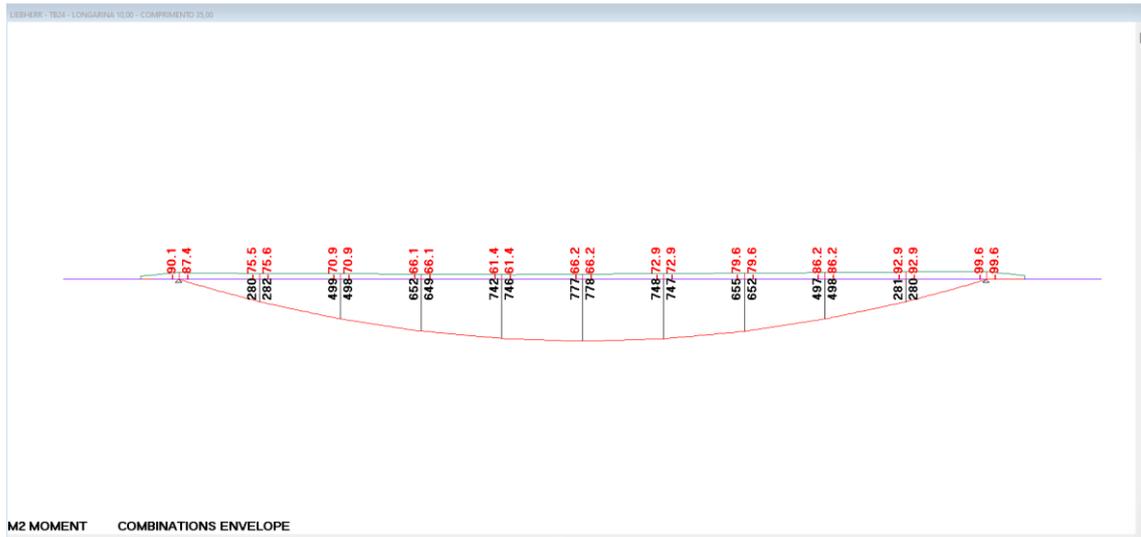


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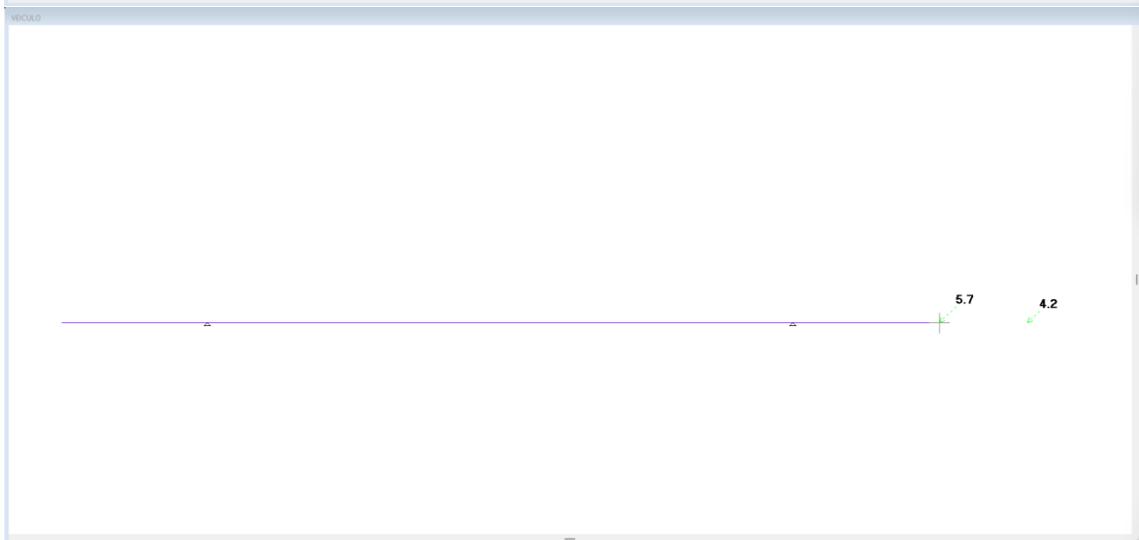
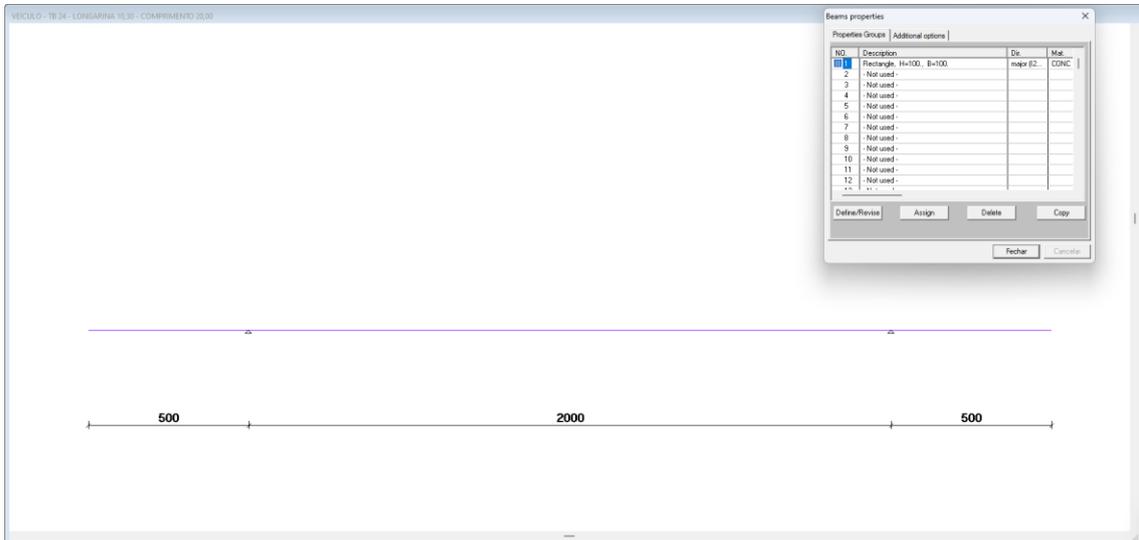
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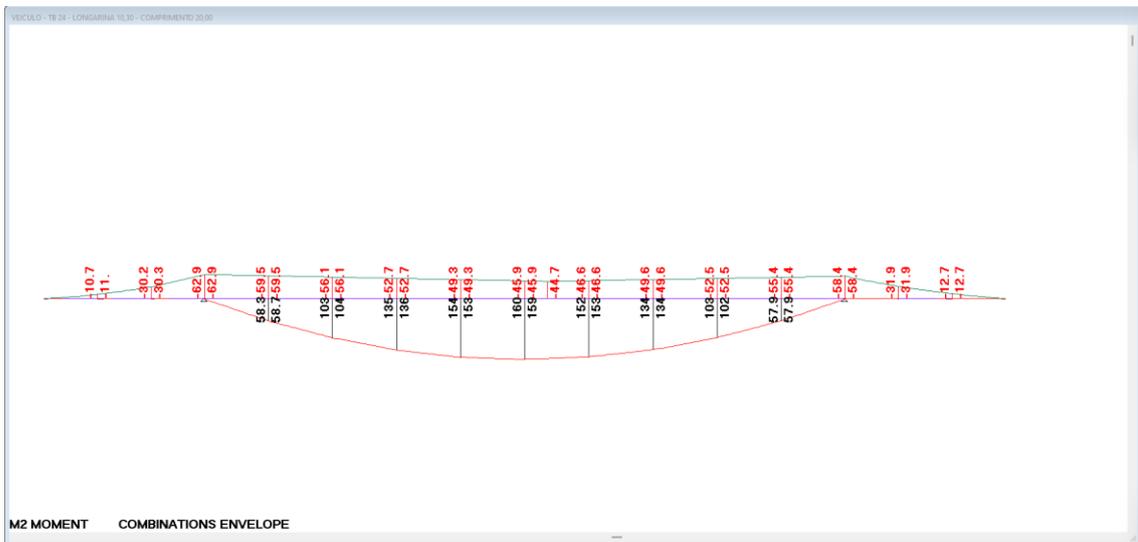
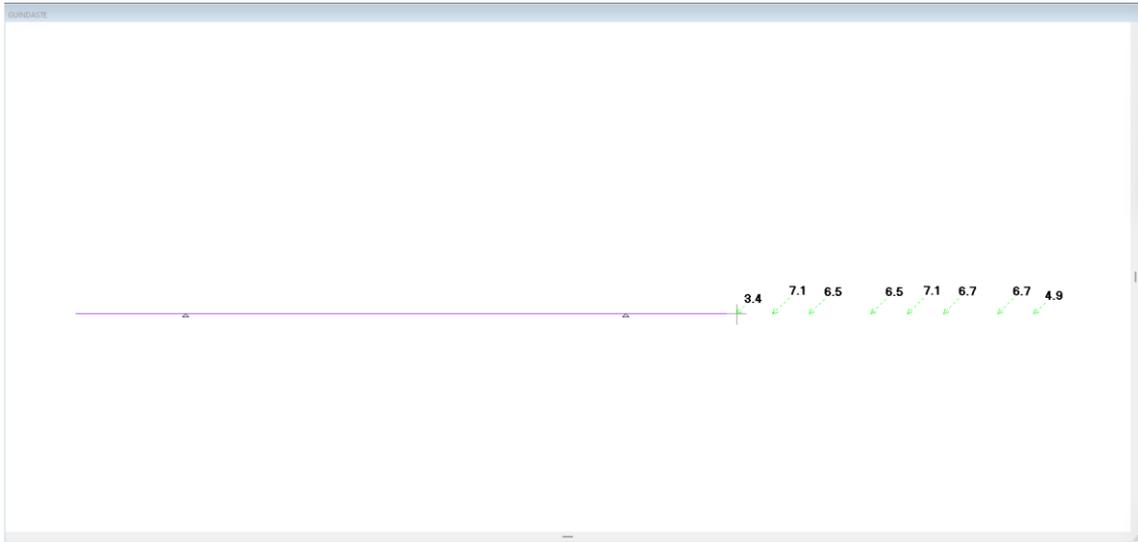
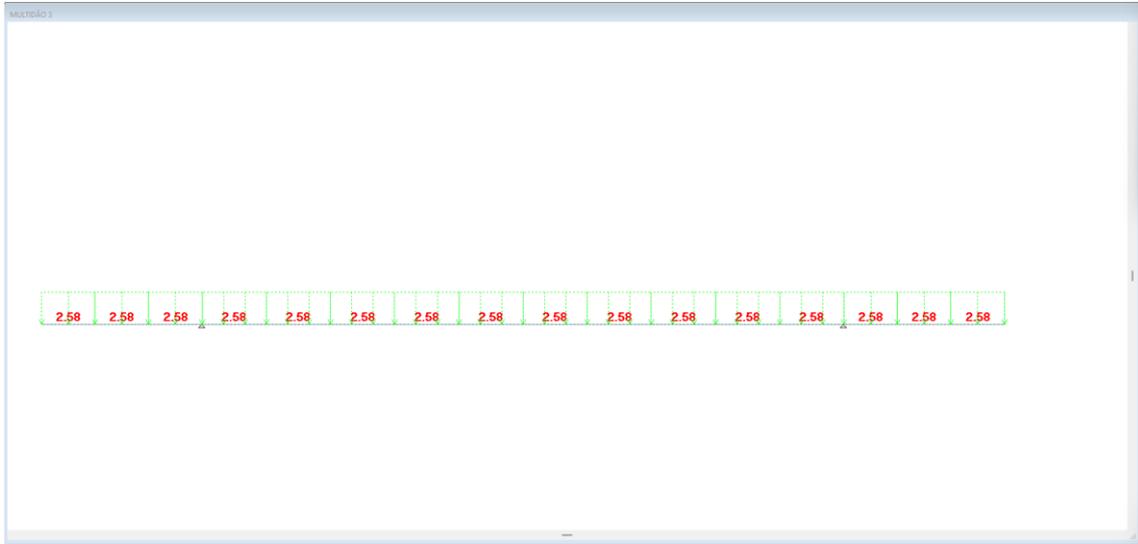
### NOTA TÉCNICA

#### 5.4.3. Tabuleiro 10,30 m



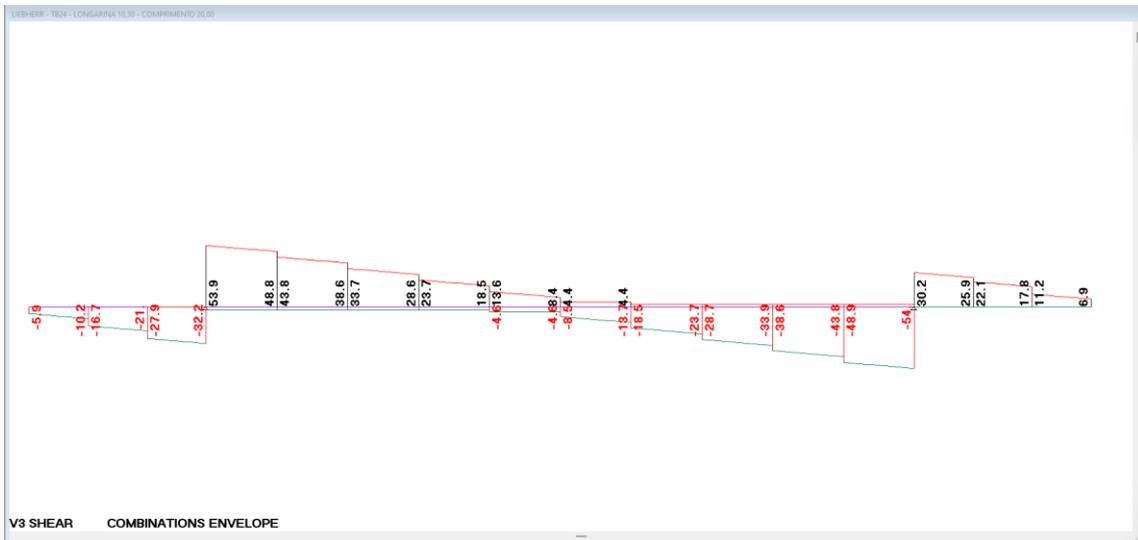
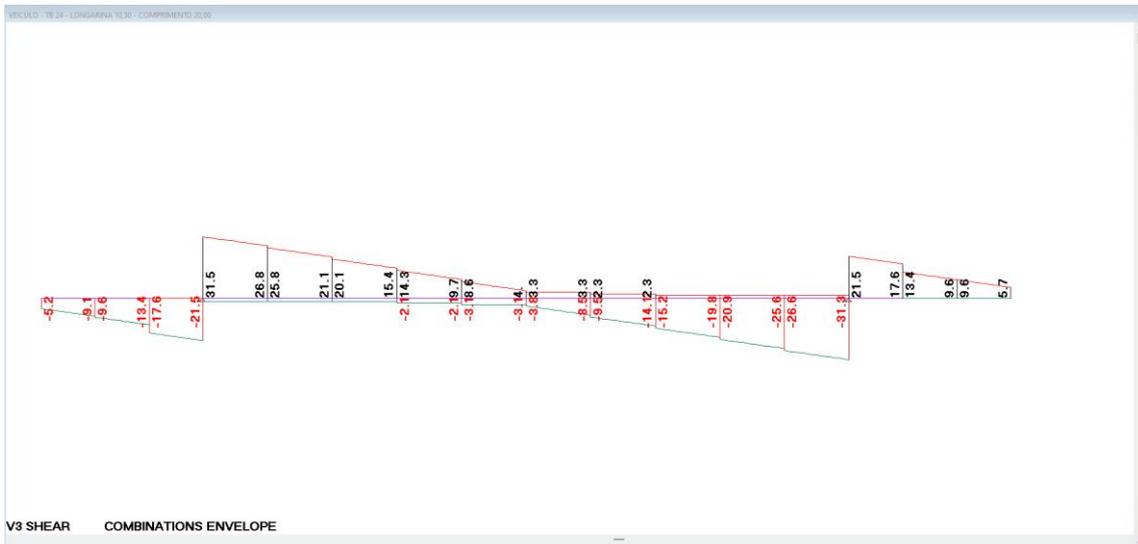
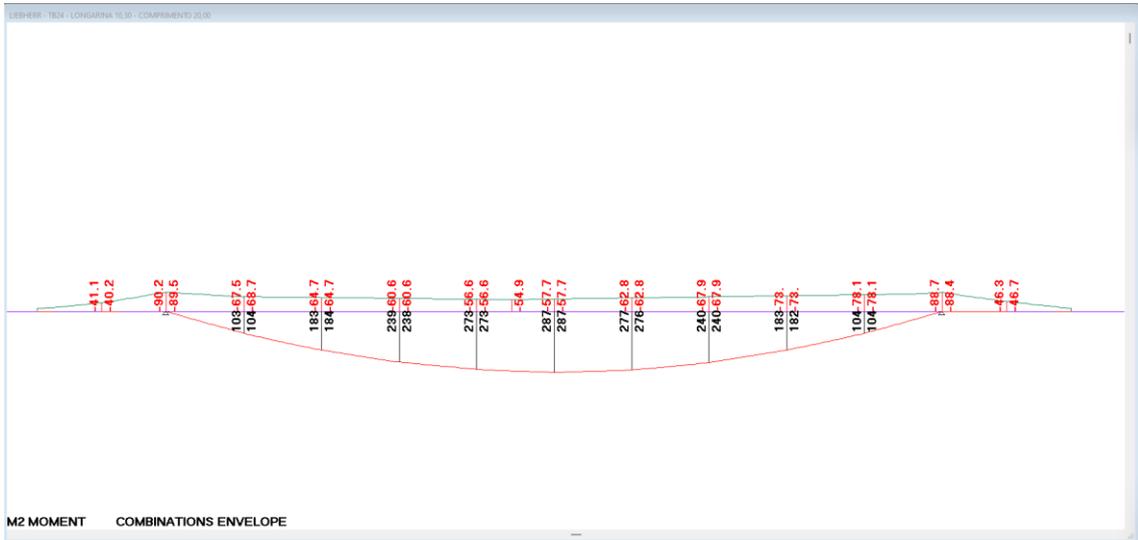


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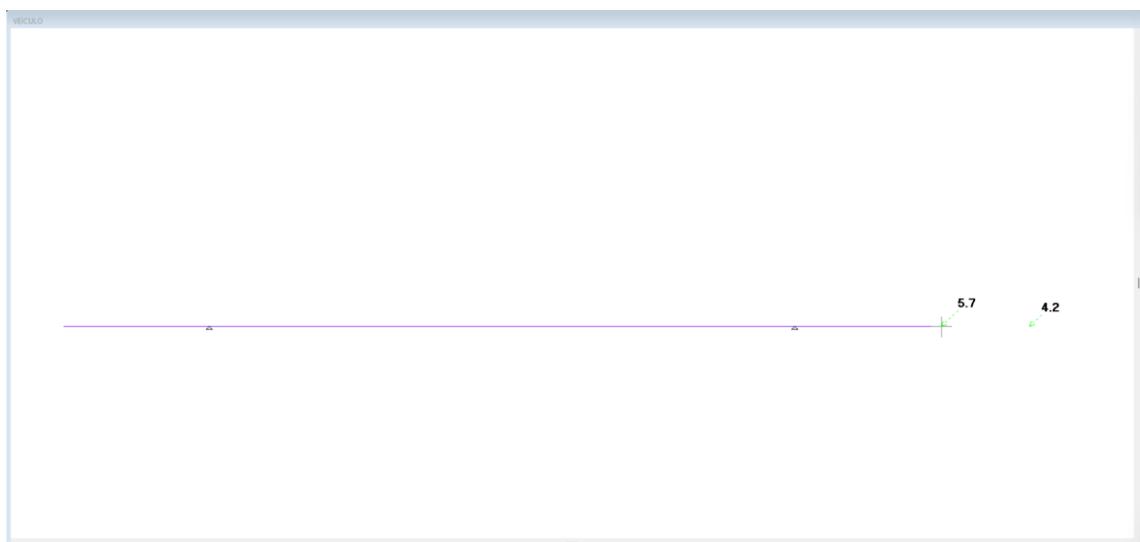
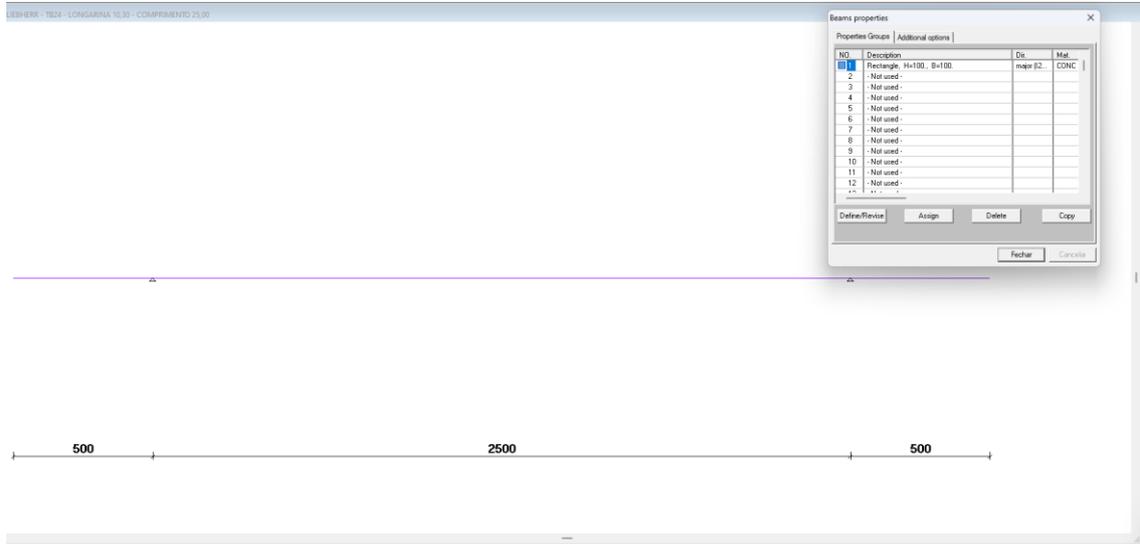


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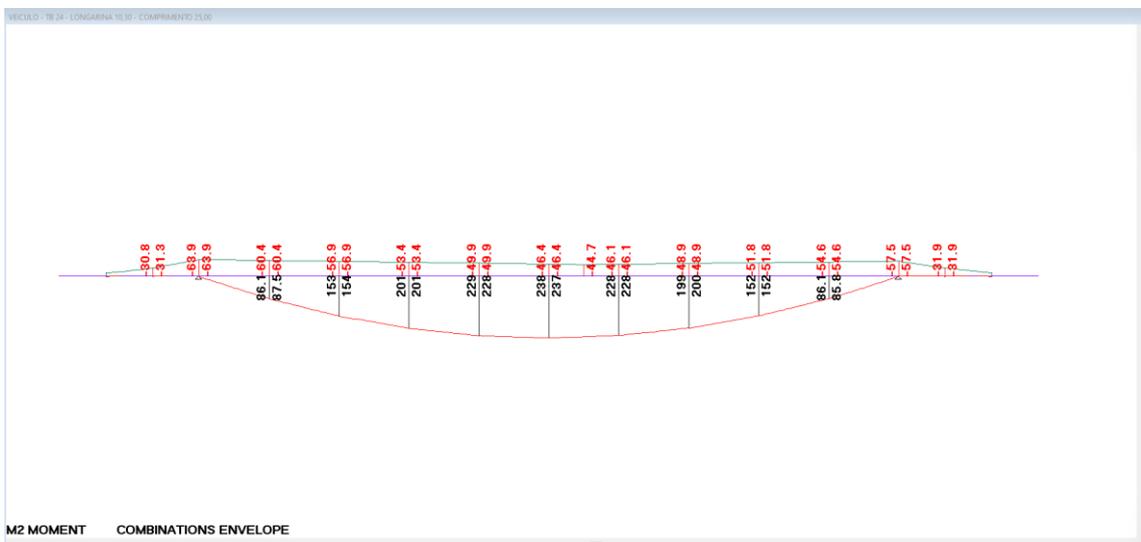


### NOTA TÉCNICA



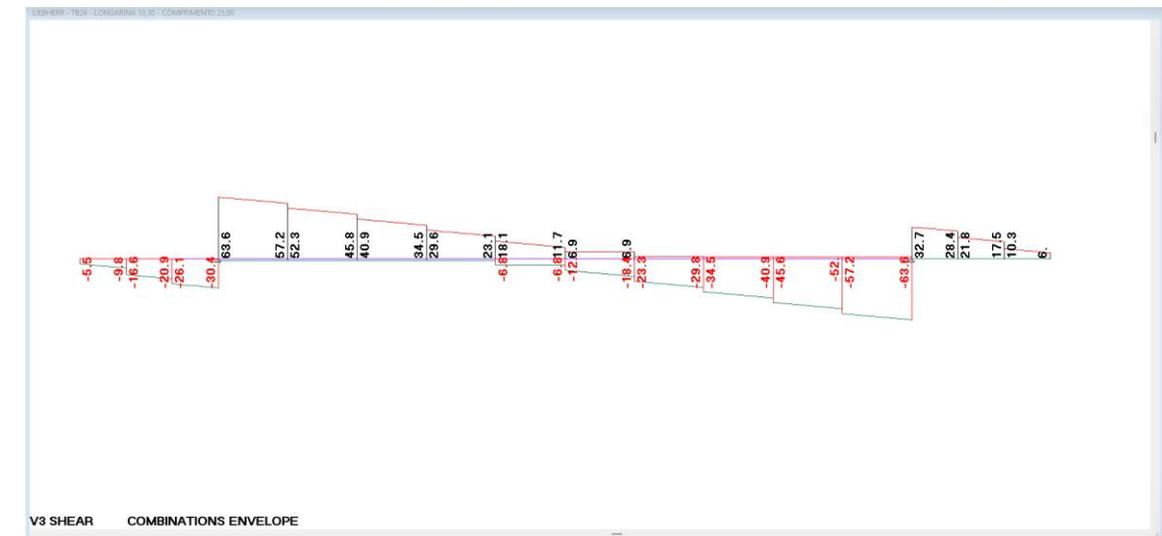
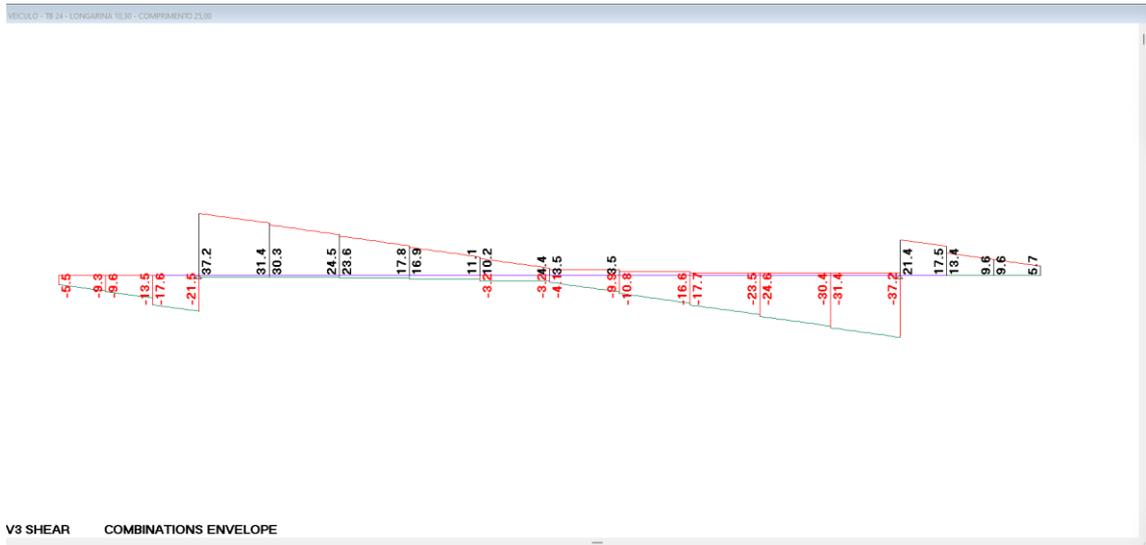
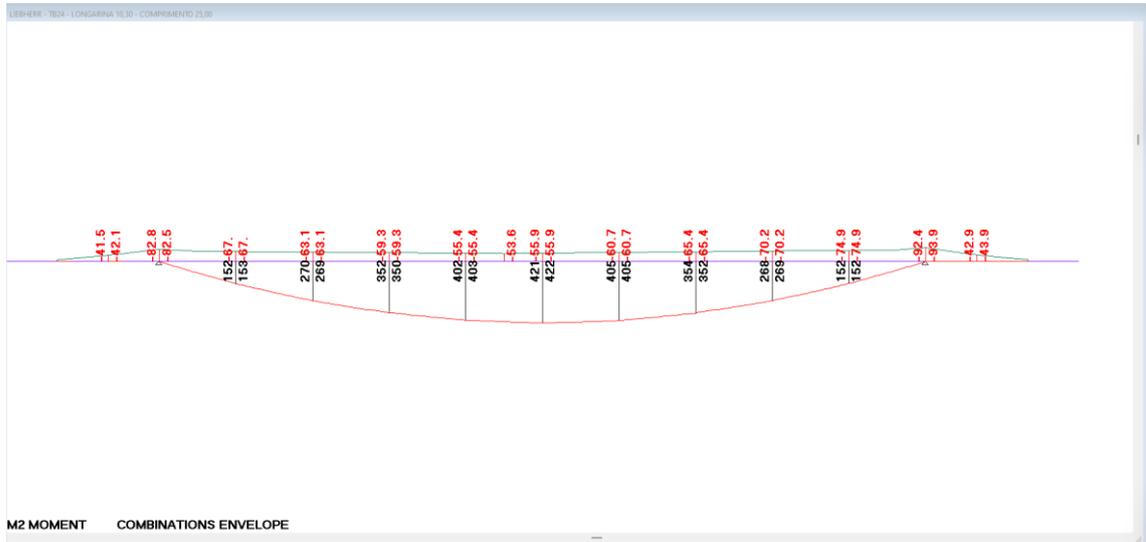


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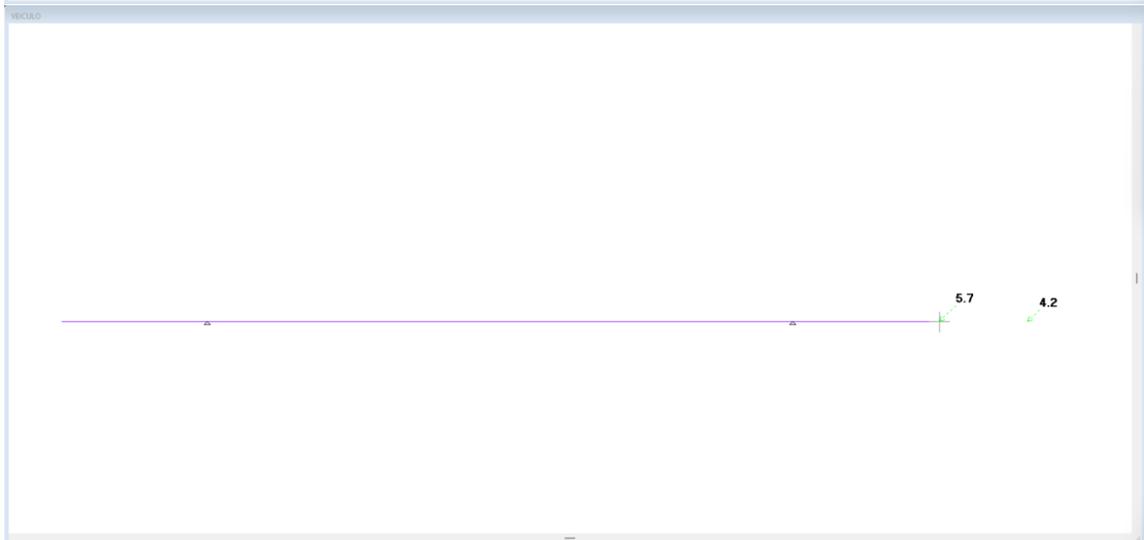
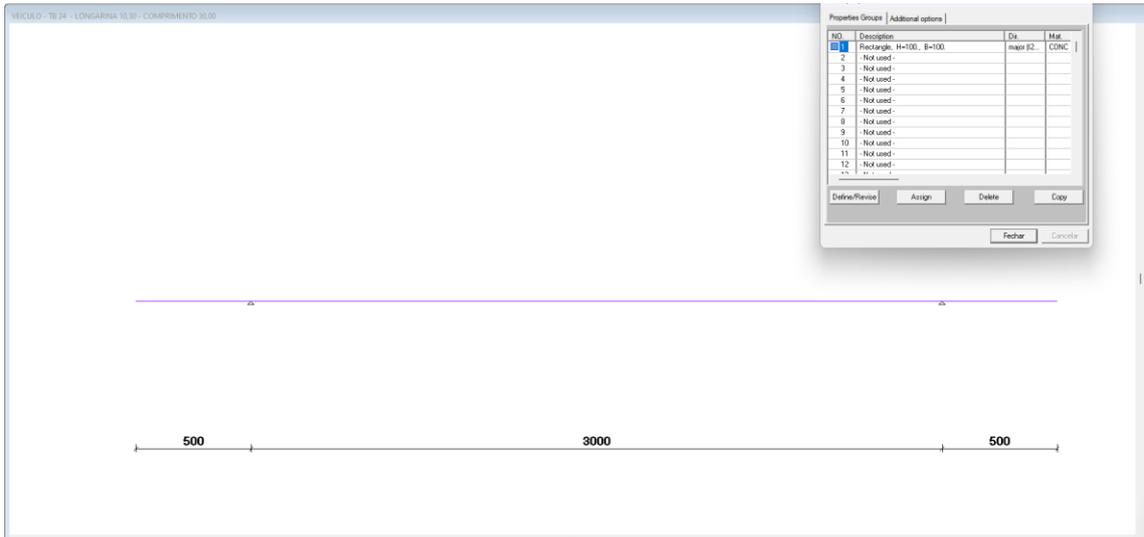


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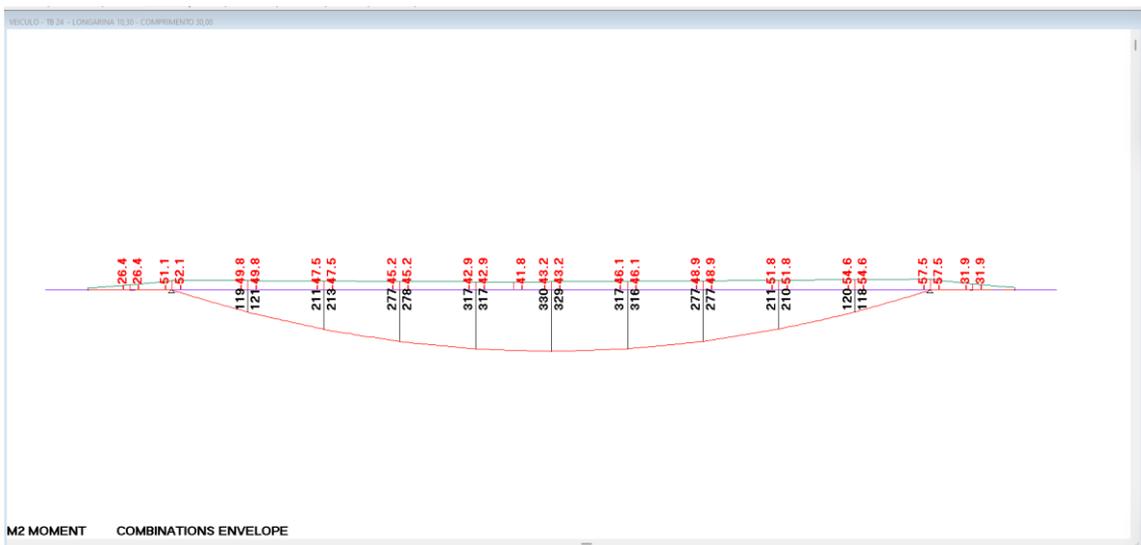
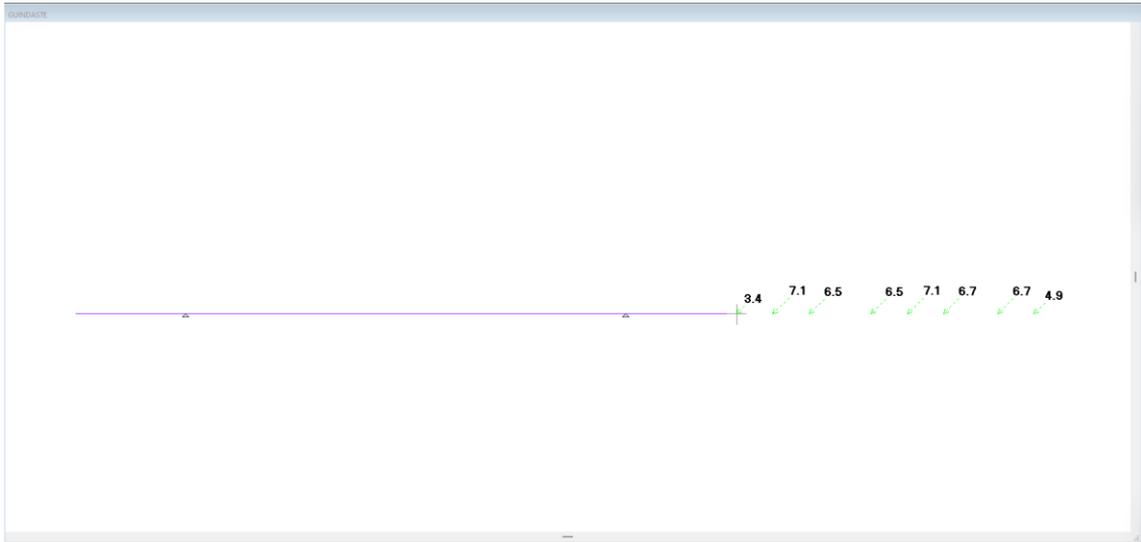
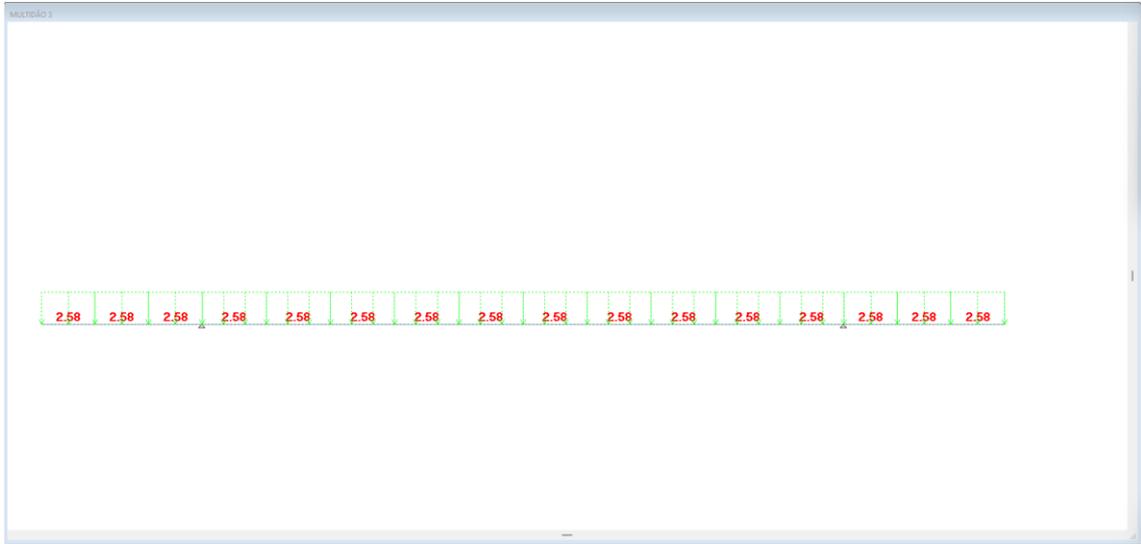


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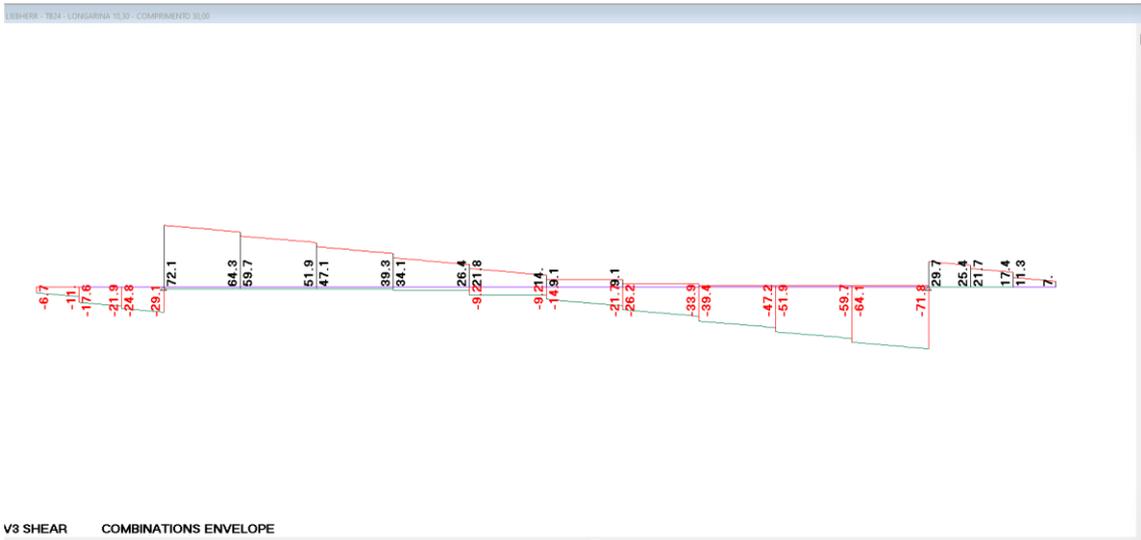
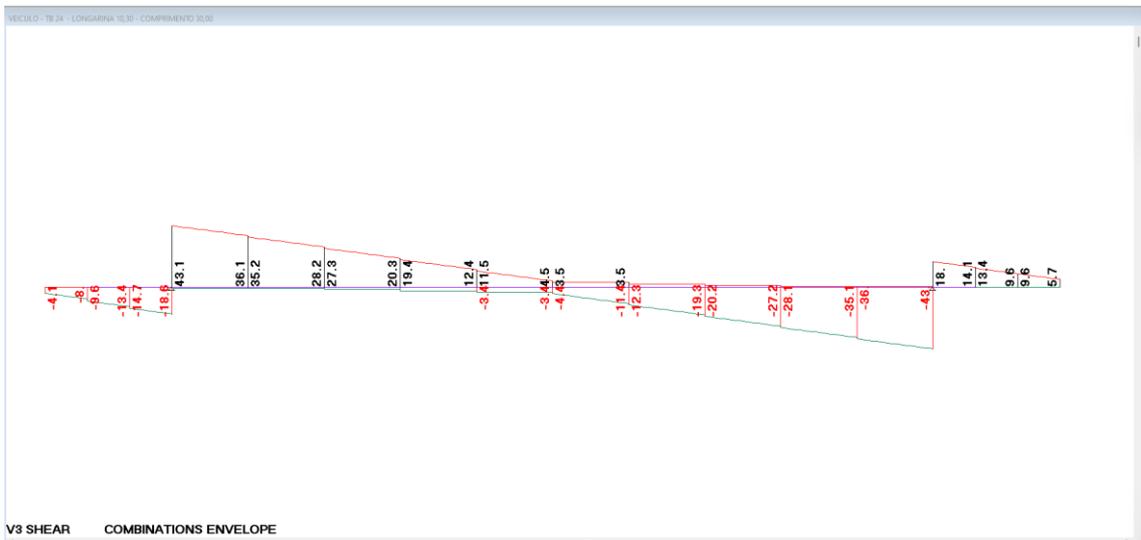
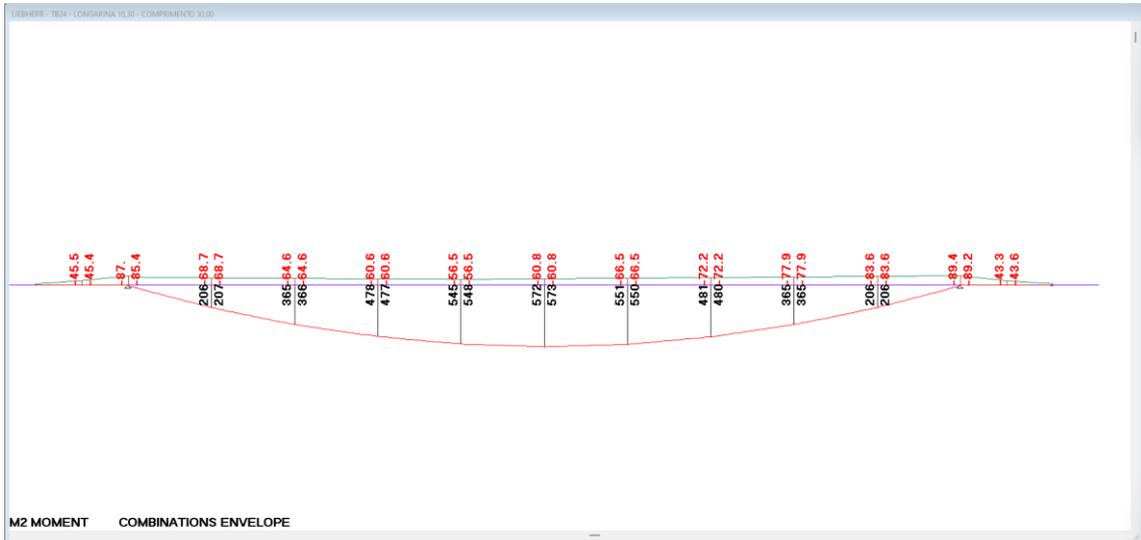


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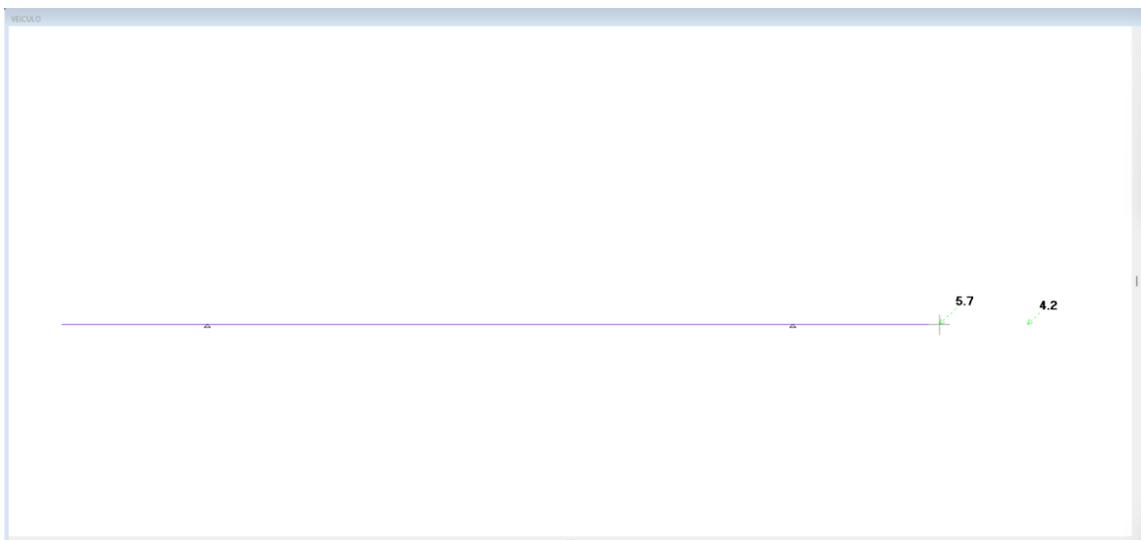
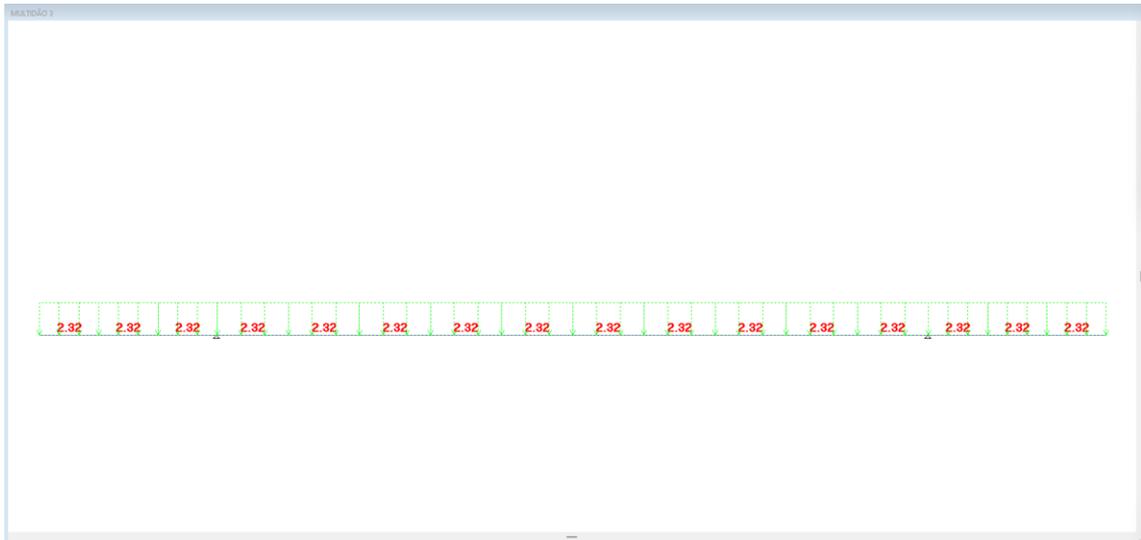
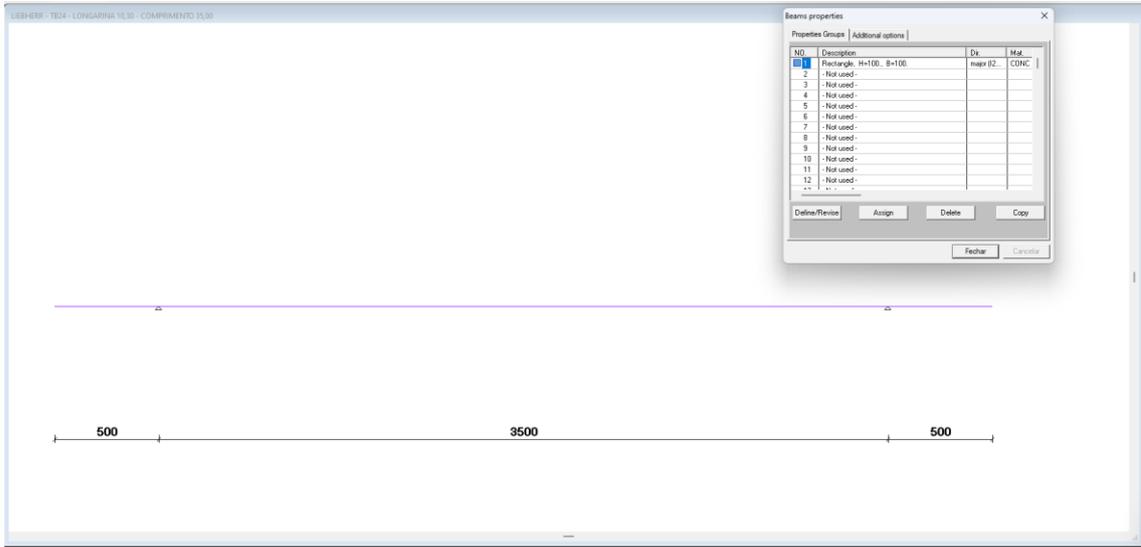


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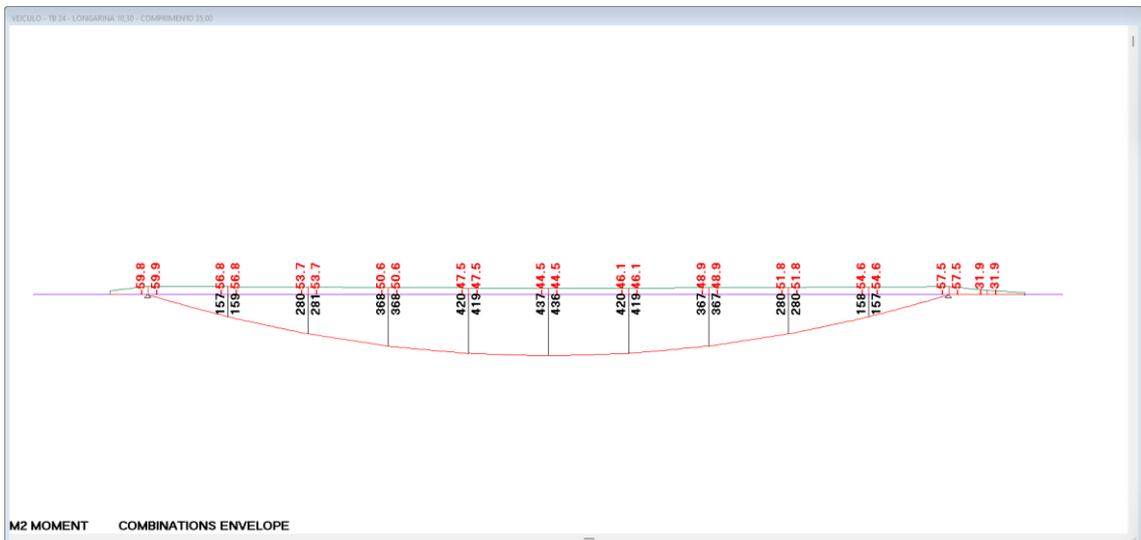
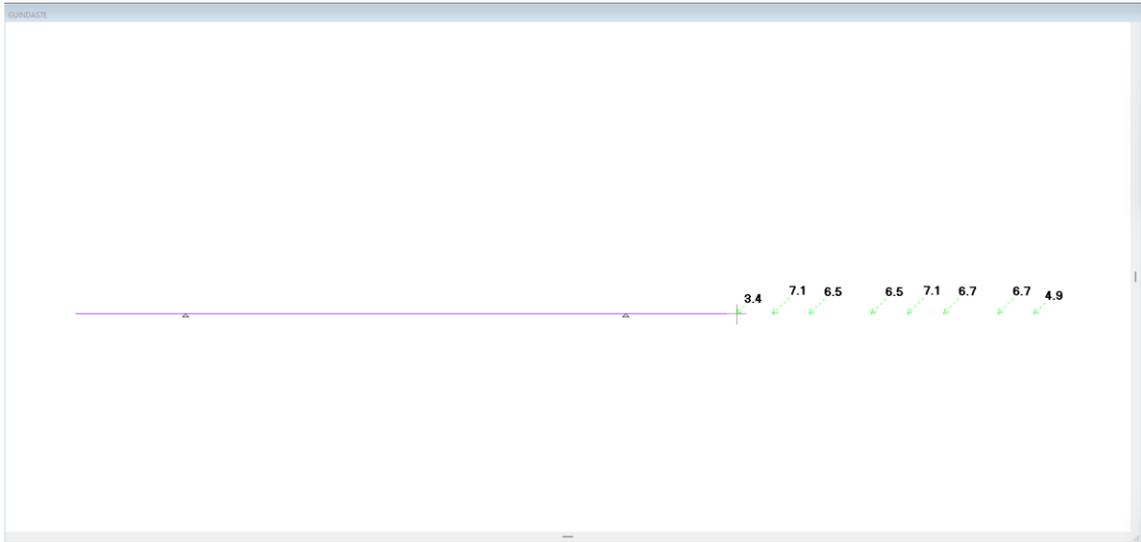
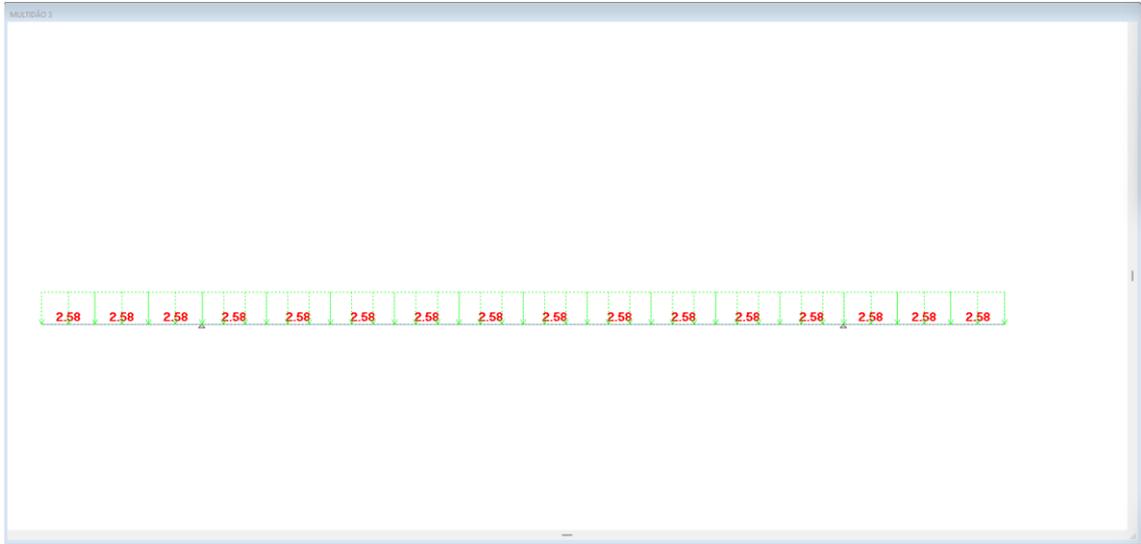


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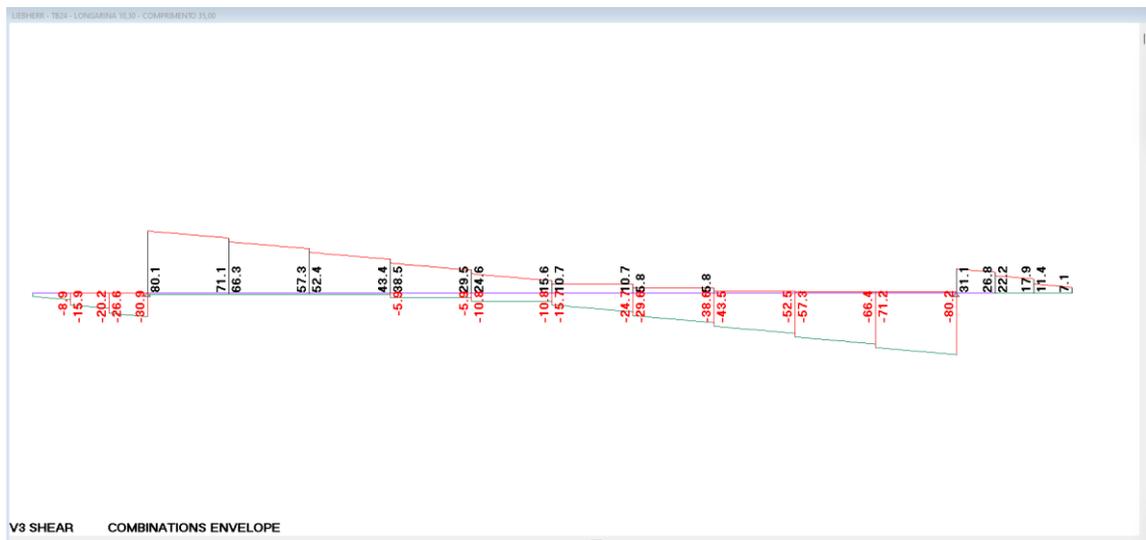
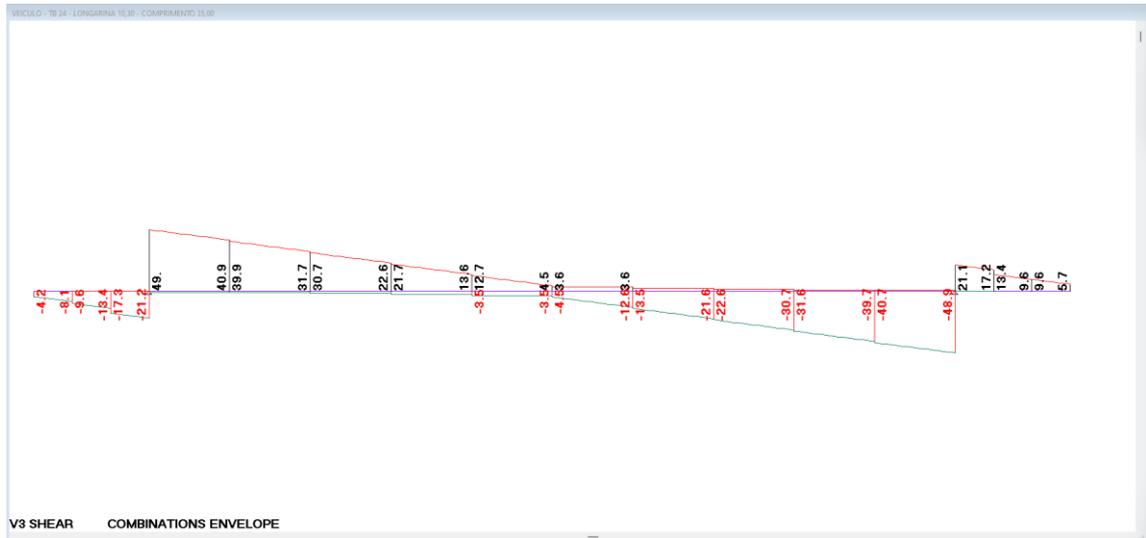
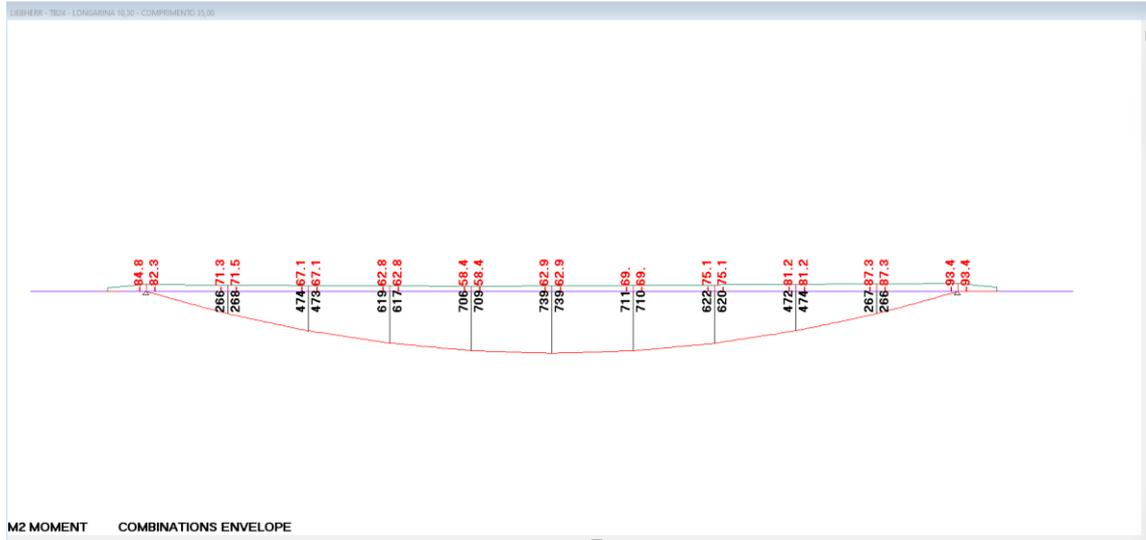


### NOTA TÉCNICA





### NOTA TÉCNICA





NOTA TÉCNICA

## 5.5. Resultados

### 5.5.1. Cálculo do CS (Coeficiente de Segurança)

CIV DO LIEBHERR	COMPRIMENTO			
	20	25	30	35
P/ VÃO -> $\varphi = 1,00 + 1,06 \times \left(\frac{20}{L + 50}\right)$	1,30	1,28	1,27	1,25
P/ BAL -> $\varphi = 1,00 + 1,06 \times \left(\frac{20}{5 + 50}\right)$	1,39	1,39	1,39	1,39

TB-24

LARGURA	COMPRIMENTO			
	20	25	30	35
8,30 x				
M(+) (tonxm)	147	216	297	391
M(-) (tonxm)	63,6	63,6	63,6	63,6
Ve (tonxm)	20,9	20,9	20,9	20,9
Vd (tonxm)	28,8	33,7	38,6	43,6

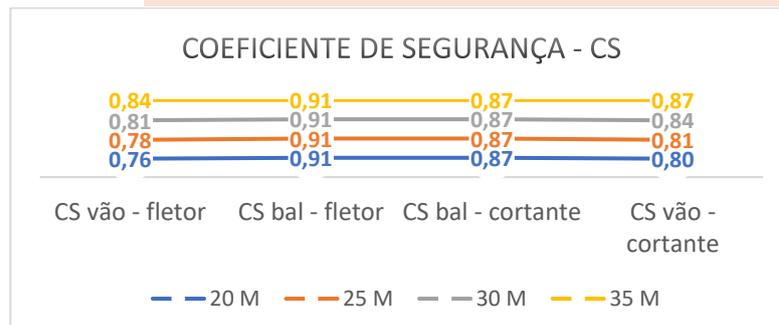
LIEBHERR

LARGURA	COMPRIMENTO			
	20	25	30	35
8,30 x				
M(+) (tonxm)	295	430	578	740
M(-) (tonxm)	100	100	100	100
Ve (tonxm)	34,4	34,4	34,4	34,4
Vd (tonxm)	55,1	64,3	72,3	79,5

$$CS = \frac{1,20 \times 1,40 \times 1,30 \times M_{qTB-24}}{1,10 \times CIV_{vão/bal} \times M_{qLiebherr}}$$

COEFICIENTE DE SEGURANÇA

LARGURA	COMPRIMENTO			
	20	25	30	35
8,30 x				
CS vão - fletor	0,76	0,78	0,81	0,84
CS bal - fletor	0,91	0,91	0,91	0,91
CS bal - cortante	0,87	0,87	0,87	0,87
CS vão - cortante	0,80	0,81	0,84	0,87





### NOTA TÉCNICA

#### TB-24

LARGURA	COMPRIMENTO			
	10,00 x	20	25	30
M(+) (tonxm)	167	248	344	453
M(-) (tonxm)	69,6	69,6	69,6	69,6
Ve (tonxm)	23	23	23	23
Vd (tonxm)	33	38,7	45	50,8

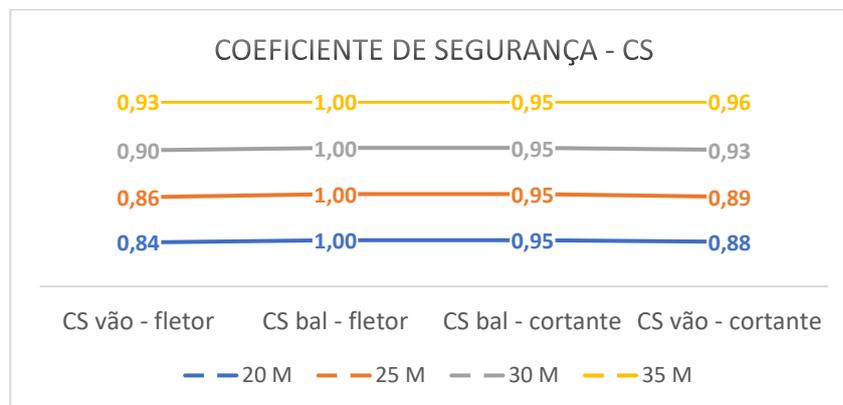
#### LIEBHERR

LARGURA	COMPRIMENTO			
	10,00 x	20	25	30
M(+) (tonxm)	304	445	603	776
M(-) (tonxm)	100	100	100	100
Ve (tonxm)	34,8	34,8	34,8	34,8
Vd (tonxm)	57	67,1	76	84,5

$$CS = \frac{1,20 \times 1,40 \times 1,30 \times M_{qTB-24}}{1,10 \times CIV_{vão/bal} \times M_{qLiebherr}}$$

#### COEFICIENTE DE SEGURANÇA

LARGURA	COMPRIMENTO			
	10,00 x	20	25	30
CS vão - fletor	0,84	0,86	0,90	0,93
CS bal - fletor	1,00	1,00	1,00	1,00
CS bal - cortante	0,95	0,95	0,95	0,95
CS vão - cortante	0,88	0,89	0,93	0,96





### NOTA TÉCNICA

#### TB-24

LARGURA	COMPRIMENTO			
	10,30 x	20	25	30
M(+) (tonxm)	160	237	330	437
M(-) (tonxm)	63,9	63,9	63,9	63,9
Ve (tonxm)	21,5	21,5	21,5	21,5
Vd (tonxm)	31,5	37,1	43,1	49,1

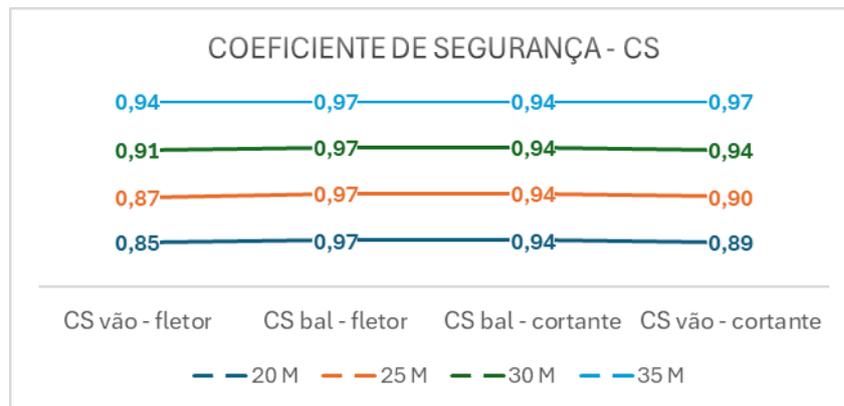
#### LIEBHERR

LARGURA	COMPRIMENTO			
	10,30 x	20	25	30
M(+) (tonxm)	287	421	572	740
M(-) (tonxm)	94,2	94,2	94,2	94,2
Ve (tonxm)	32,7	32,7	32,7	32,7
Vd (tonxm)	54	63,6	72,3	80,4

$$CS = \frac{1,20 \times 1,40 \times 1,30 \times M_{qTB-24}}{1,10 \times CIV_{vão/bal} \times M_{qLiebherr}}$$

#### COEFICIENTE DE SEGURANÇA

LARGURA	COMPRIMENTO			
	10,30 x	20	25	30
CS vão - fletor	0,85	0,87	0,91	0,94
CS bal - fletor	0,97	0,97	0,97	0,97
CS bal - cortante	0,94	0,94	0,94	0,94
CS vão - cortante	0,89	0,90	0,94	0,97





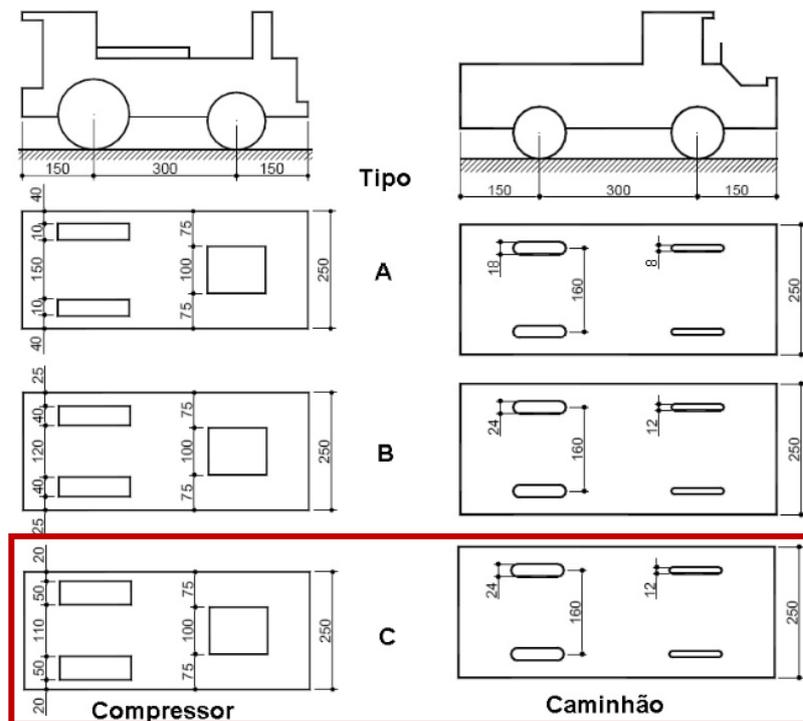
## NOTA TÉCNICA

### 5.5.2. Considerações para o TB-24 (1943 a 1950)

Os coeficientes de segurança ficaram com valores  $< 1$ , então a passagem do guindaste de 96 toneladas e 8 eixos não está liberada para o TB-24 no período de (1943 a 1950). Será necessário realizar o mesmo processo de cálculo para o segundo período (1950 a 1960).

## 6. DESENVOLVIMENTO: TB-24 (1950 A 1960)

Figura 2 - Compressor e caminhão utilizado no trem-tipo segundo NB6/50 (ABNT, 1950)



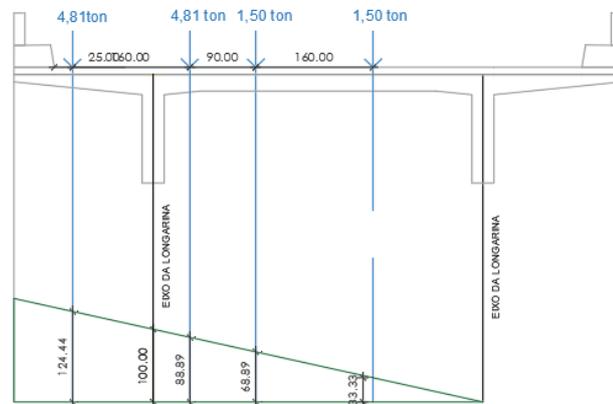
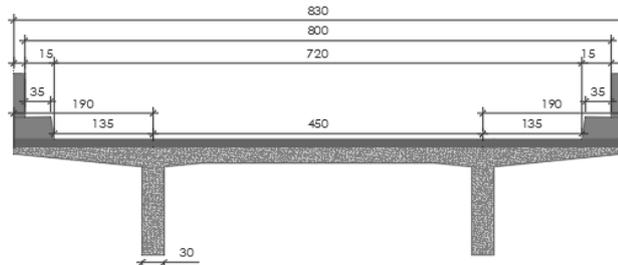
Art. 10 - O trem-tipo para pontes da **Classe I** compõe-se de multidão com  $g_0 = 500 \text{ kgf/m}^2$ , de um compressor **Tipo C** e de tantos caminhões **tipo C** quantas forem as faixas de tráfego, menos uma, e dispostos como no caso do **Art. 8** da norma.



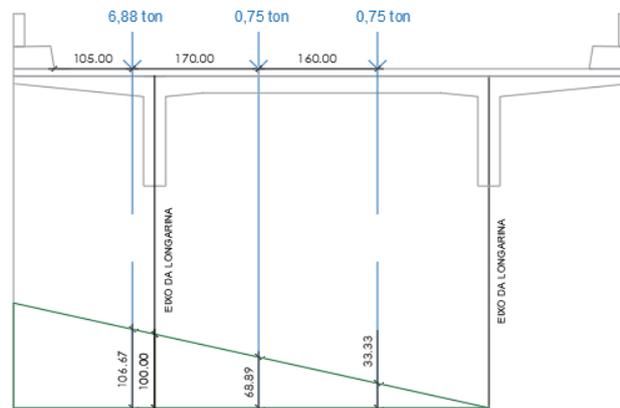
NOTA TÉCNICA

## 6.1. Linhas de influência – Rolo compressor + caminhão

### 6.1.1. Tabuleiro 8,30 m



$$\text{RODAS TRASE IRAS} = 4,81 \times (1,2444 + 0,8889) + 1,50 \times (0,6889 + 0,3333) = 11,80 \text{ ton}$$



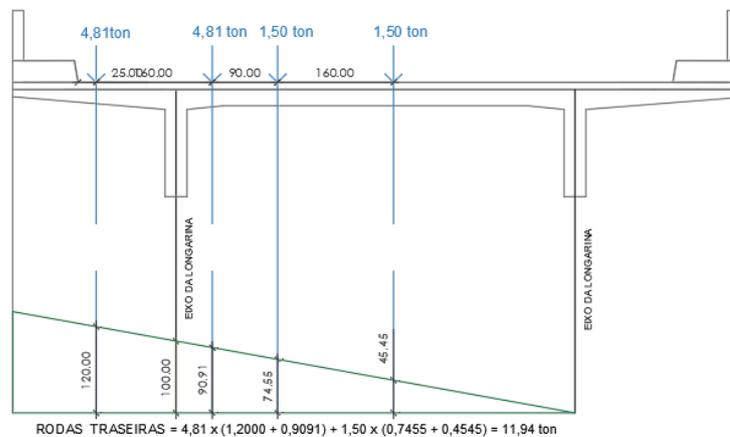
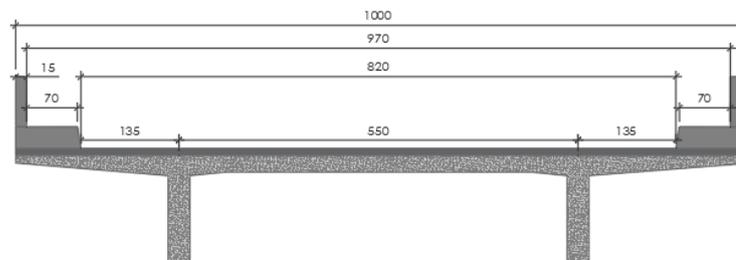
$$\text{RODAS DIANTE IRAS} = (6,88 \times 1,0667) + 0,75 \times (0,6889 + 0,3333) = 8,11 \text{ ton}$$



### NOTA TÉCNICA

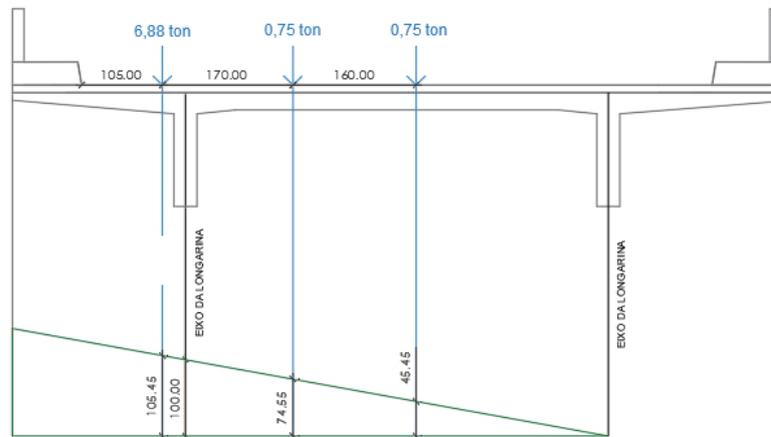


#### 6.1.2. Tabuleiro 10,00 m

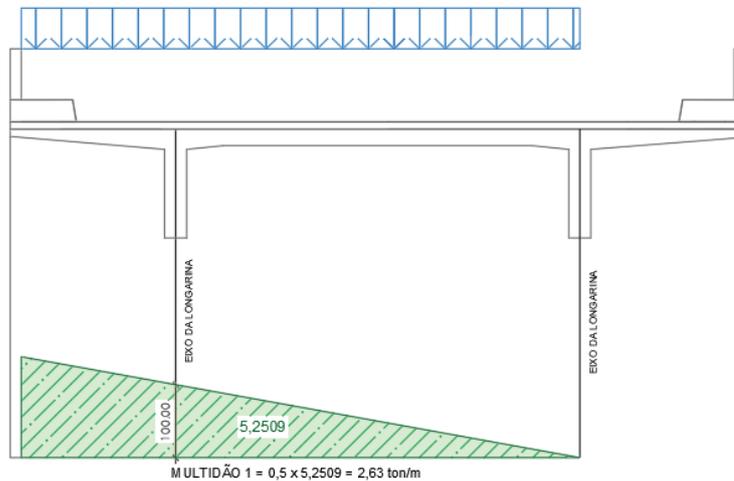




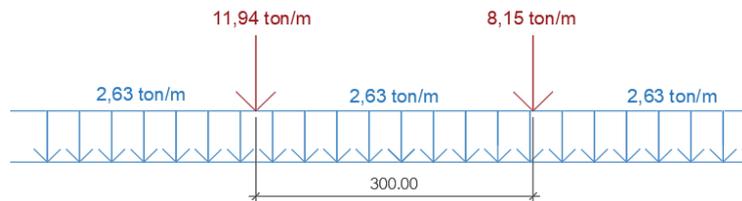
### NOTA TÉCNICA



$$\text{RODAS DIANTEIRAS} = 6,88 \times 1,0545 + 0,75 \times (0,7455 + 0,4545) = 8,15 \text{ ton}$$
$$0,5 \text{ ton/m}$$



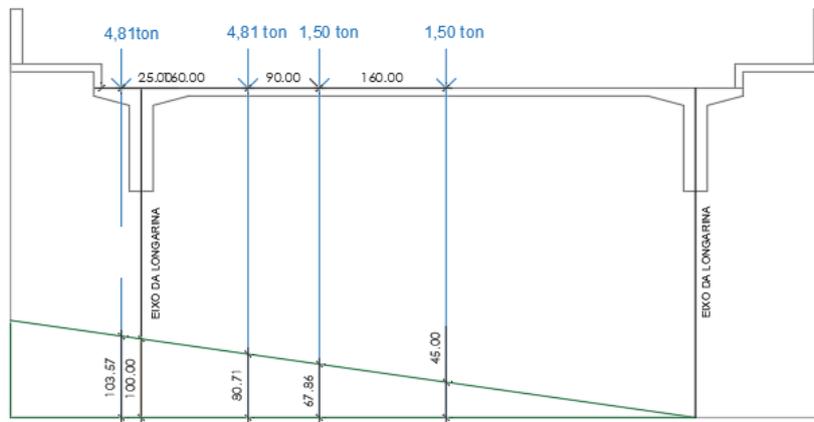
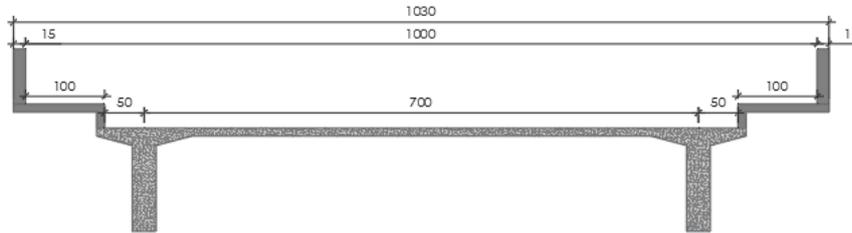
$$\text{MULTIDÃO 1} = 0,5 \times 5,2509 = 2,63 \text{ ton/m}$$



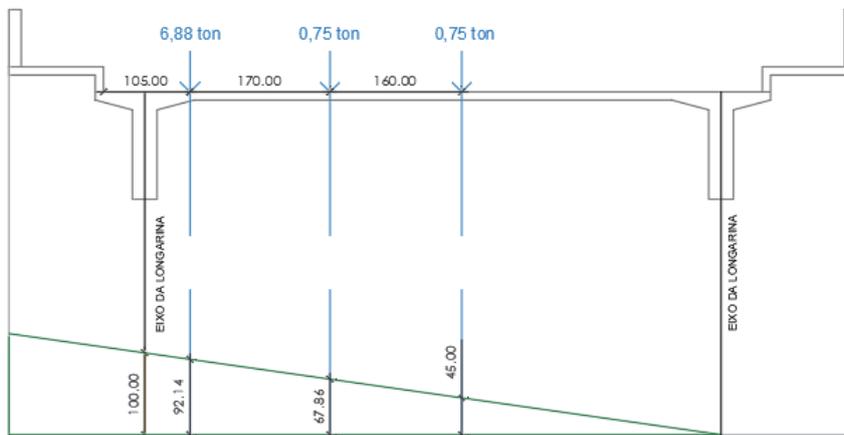


### NOTA TÉCNICA

#### 6.1.3. Tabuleiro 10,30 m



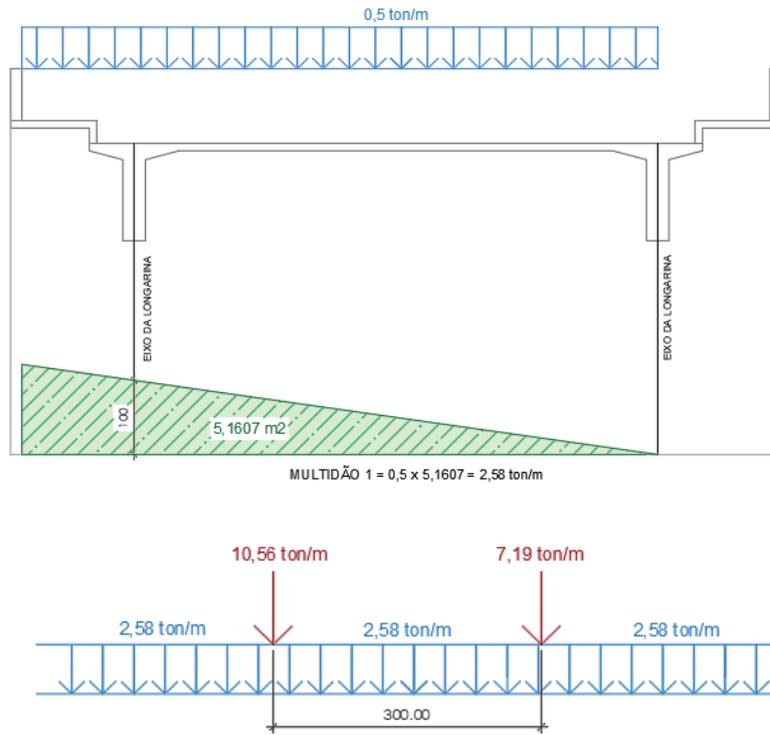
$$\text{RODAS TRASE IRAS} = 4,81 \times (1,0357 + 0,8071) + 1,50 \times (0,6786 + 0,4500) = 10,56 \text{ ton}$$



$$\text{RODAS DIANTE IRAS} = 6,88 \times 0,9214 + 0,75 \times (0,6786 + 0,4500) = 7,19 \text{ ton}$$



### NOTA TÉCNICA





## NOTA TÉCNICA

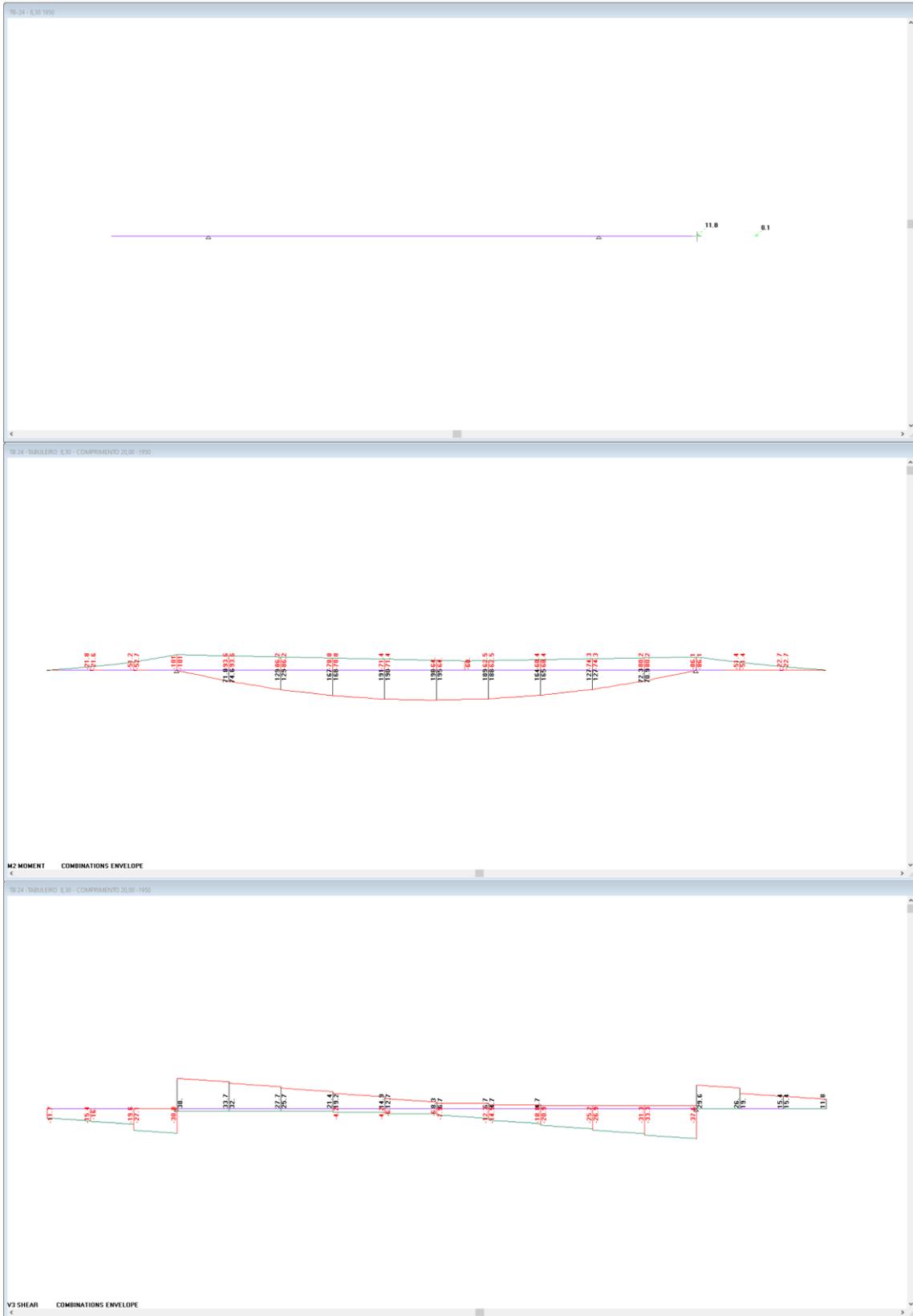
### 6.2. Cargas acidentais – (TB-24 e Guindaste) – Momentos e cortantes

#### 6.2.1. Tabuleiro 8,30 m





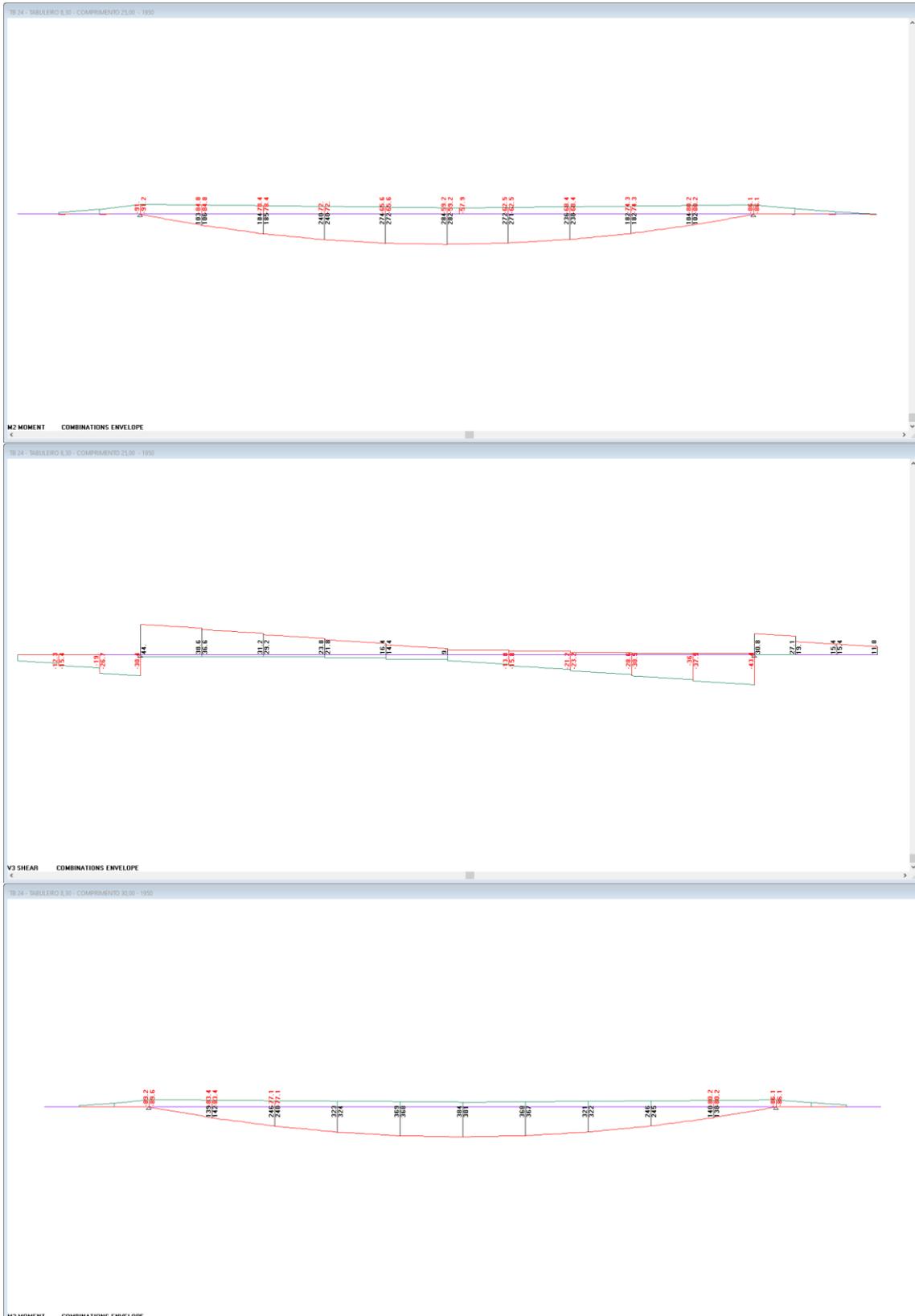
### NOTA TÉCNICA





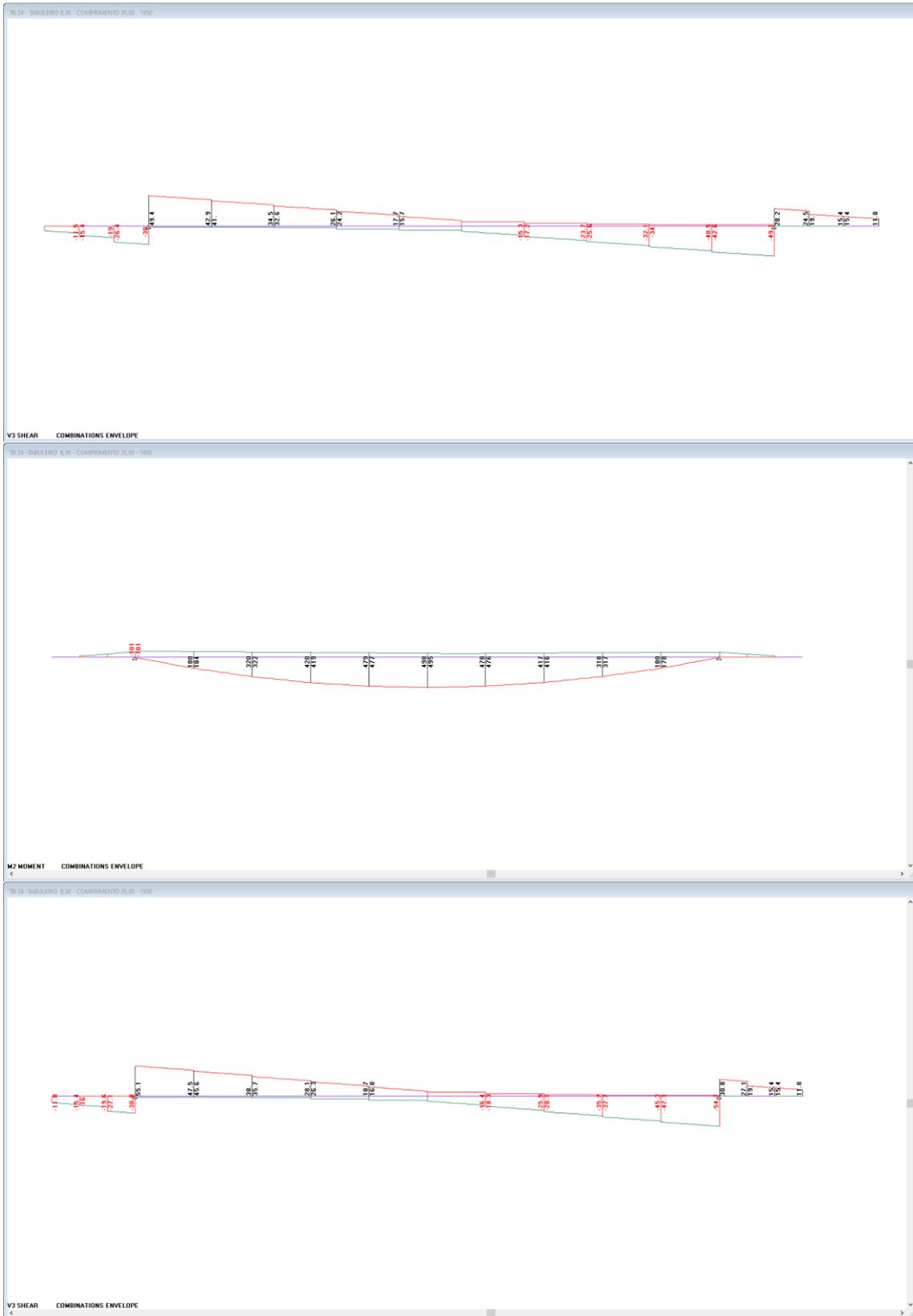
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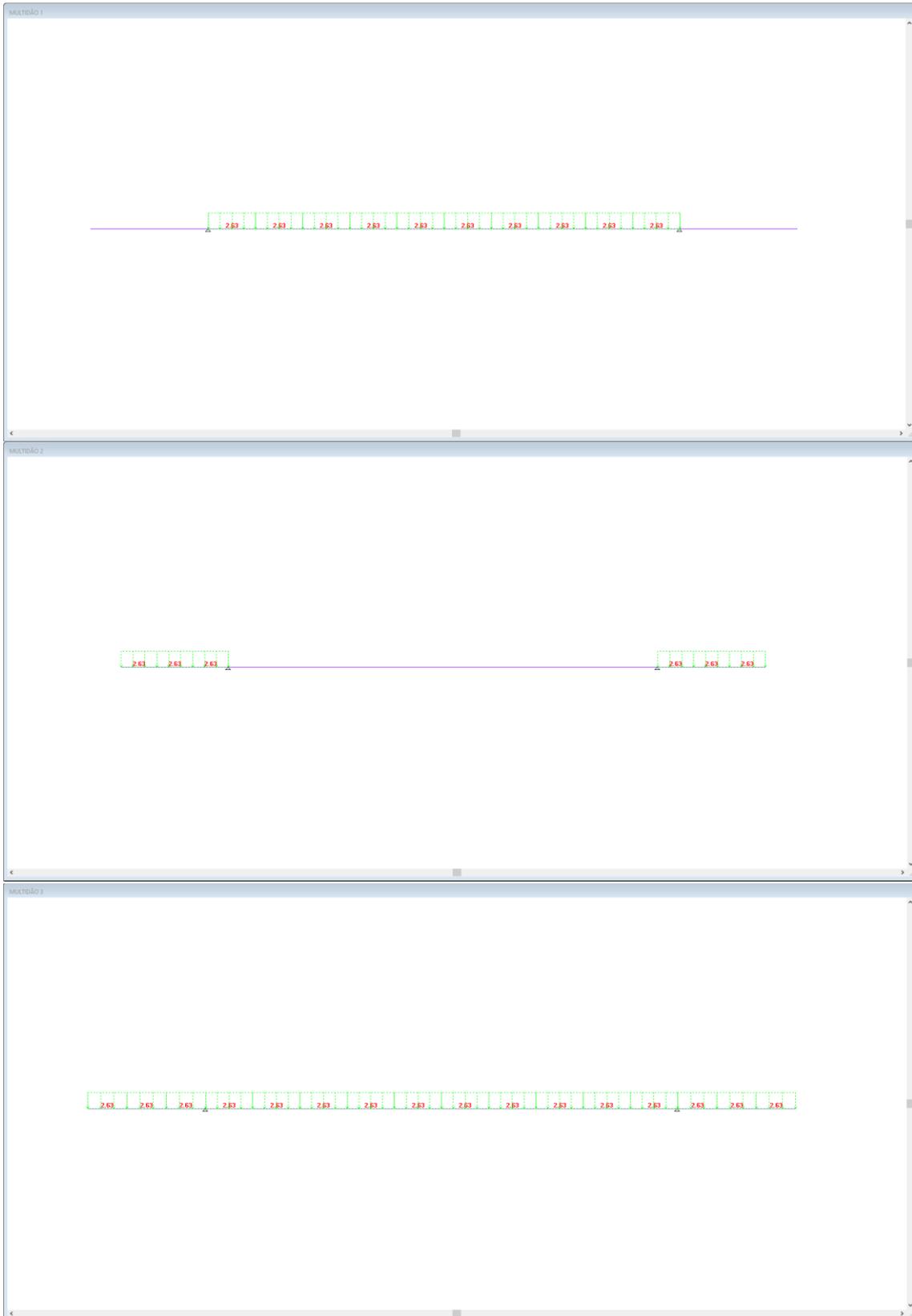
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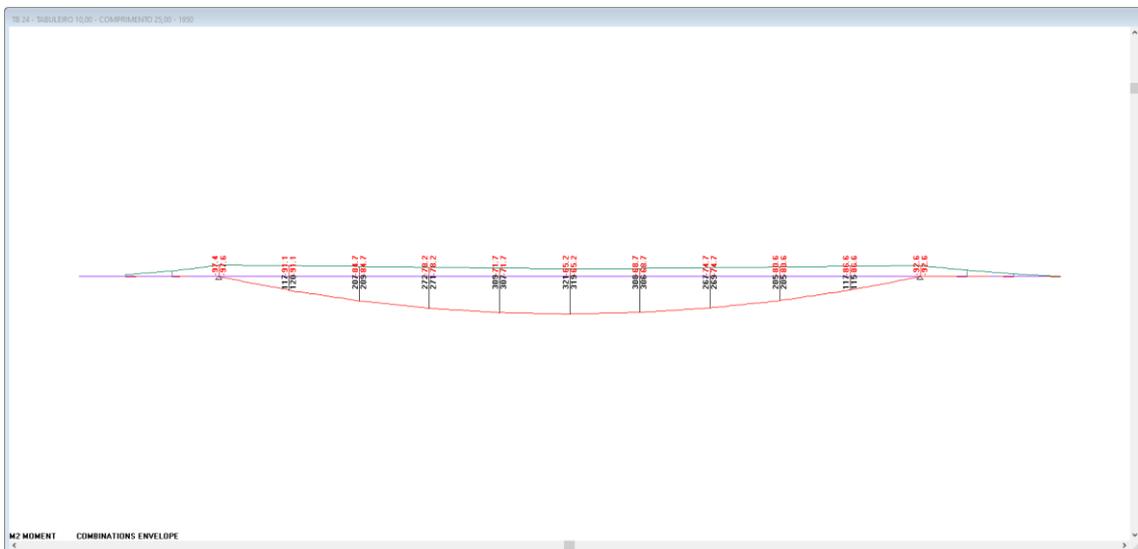
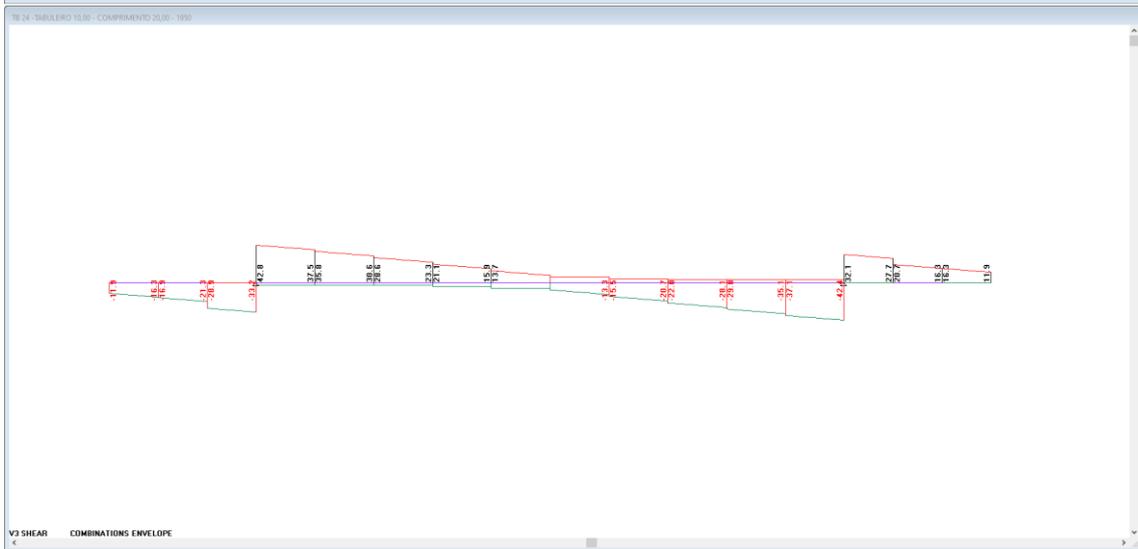
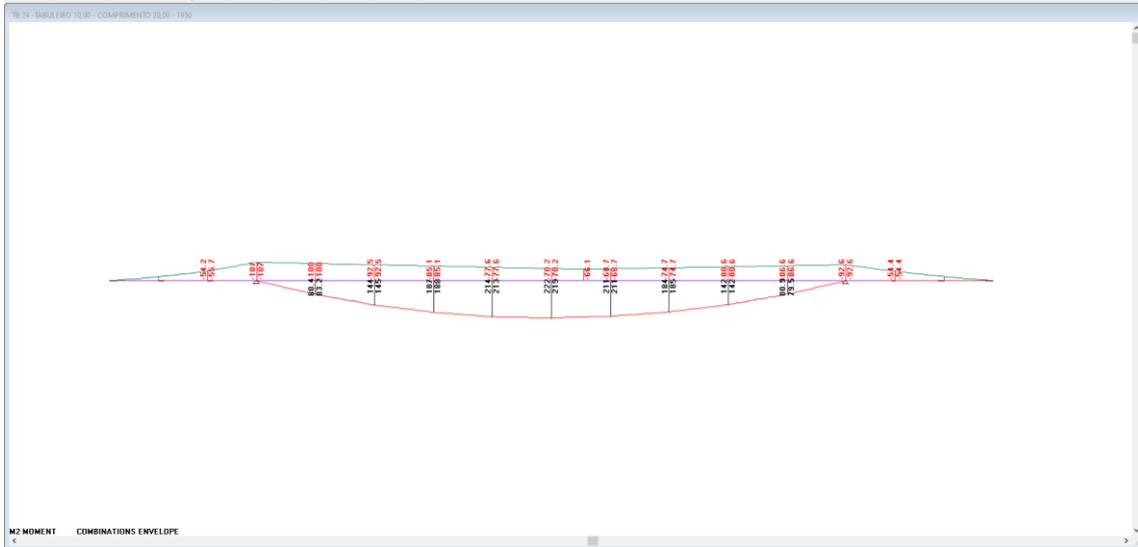
### NOTA TÉCNICA

#### 6.2.2. Tabuleiro 10,00 m



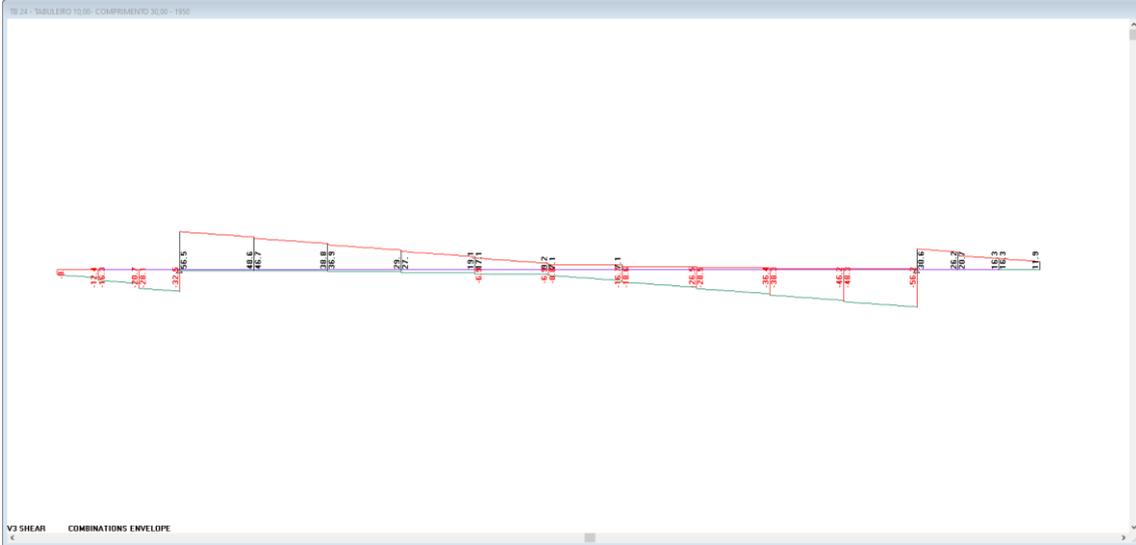
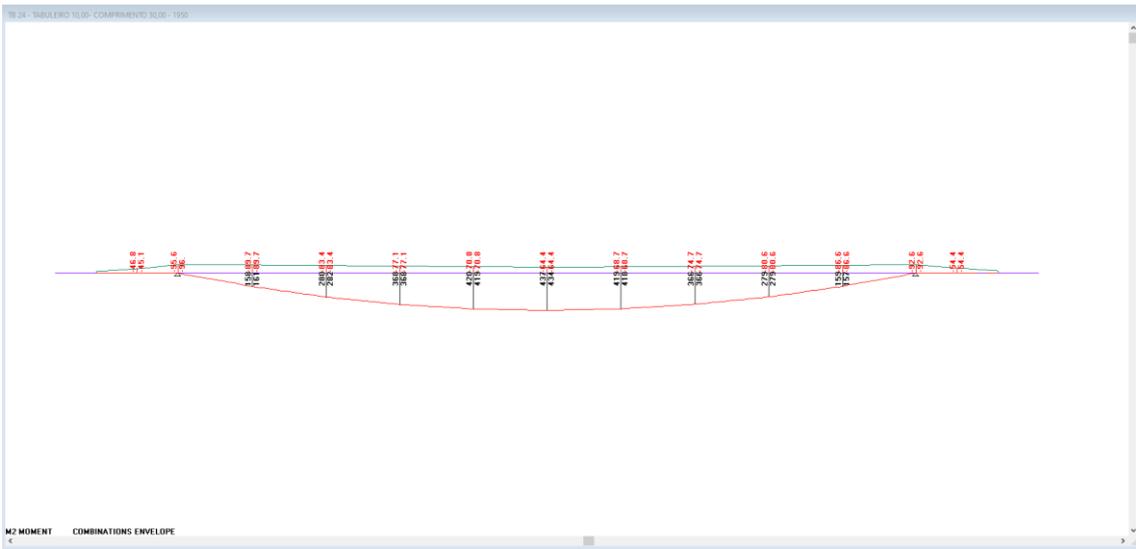
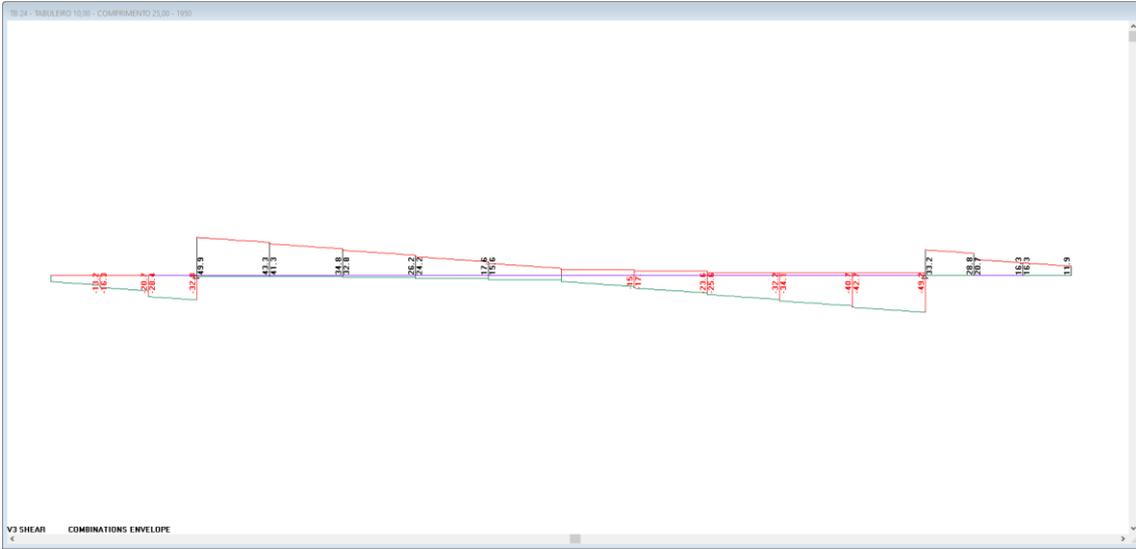


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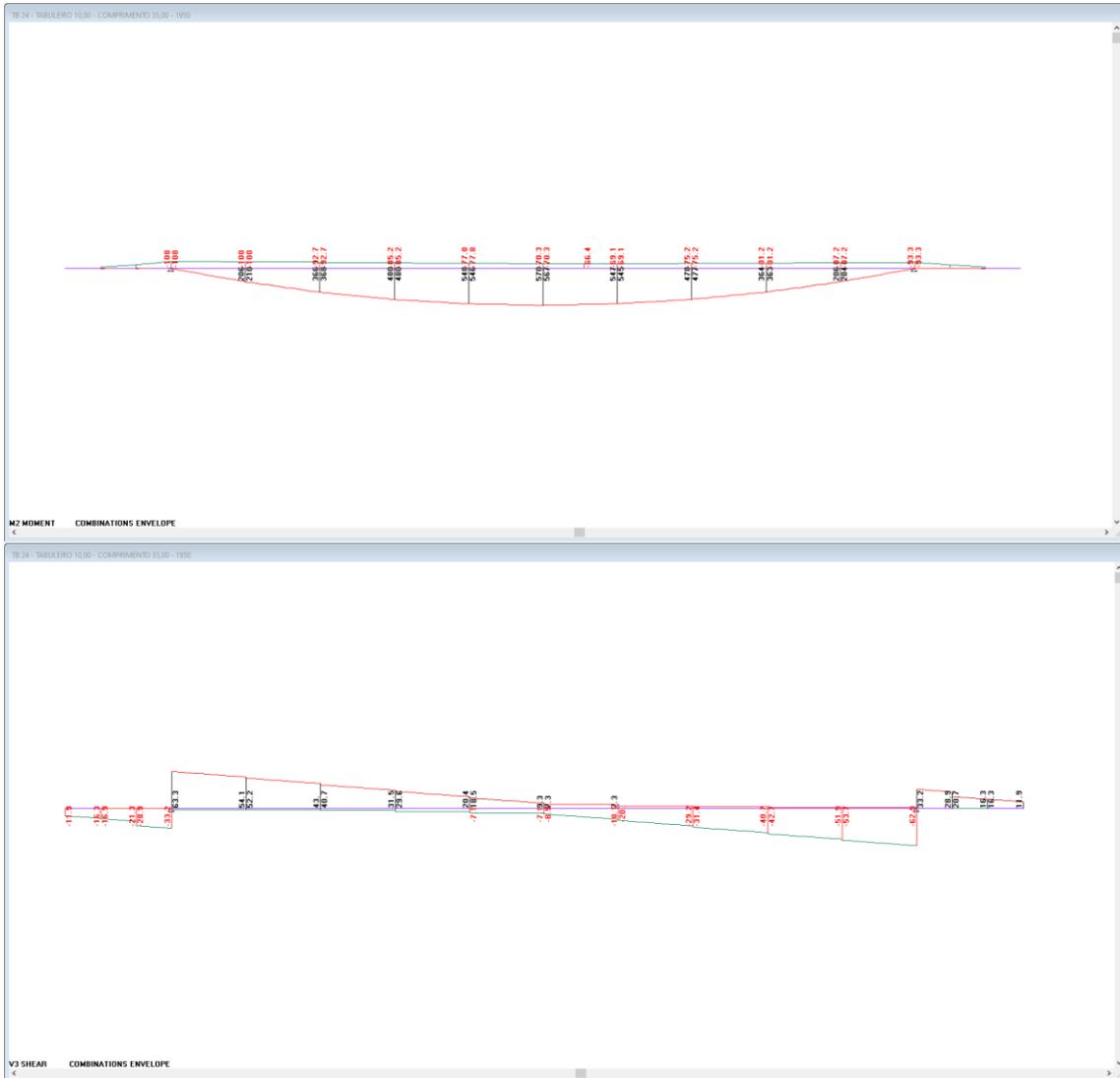


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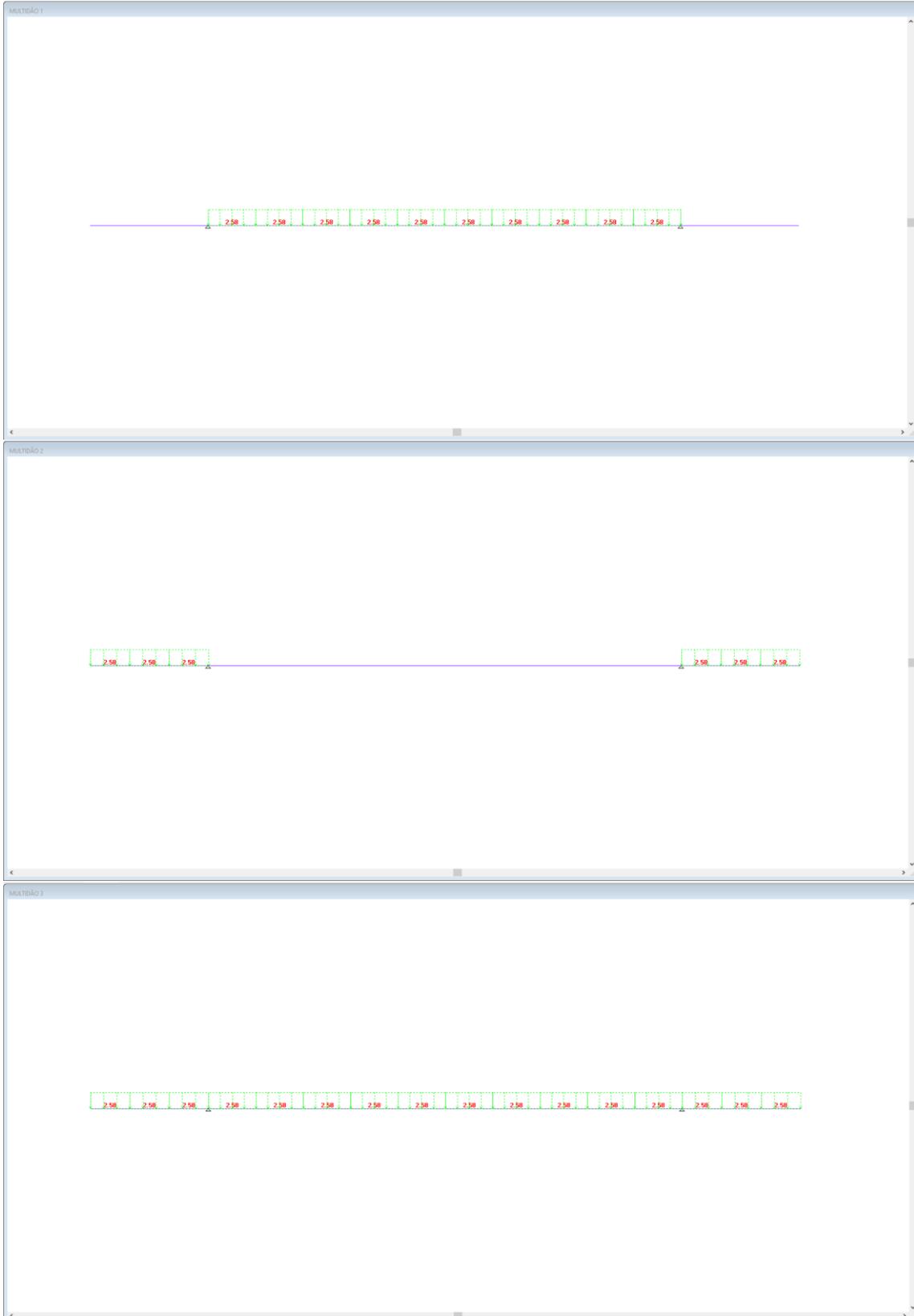
### NOTA TÉCNICA





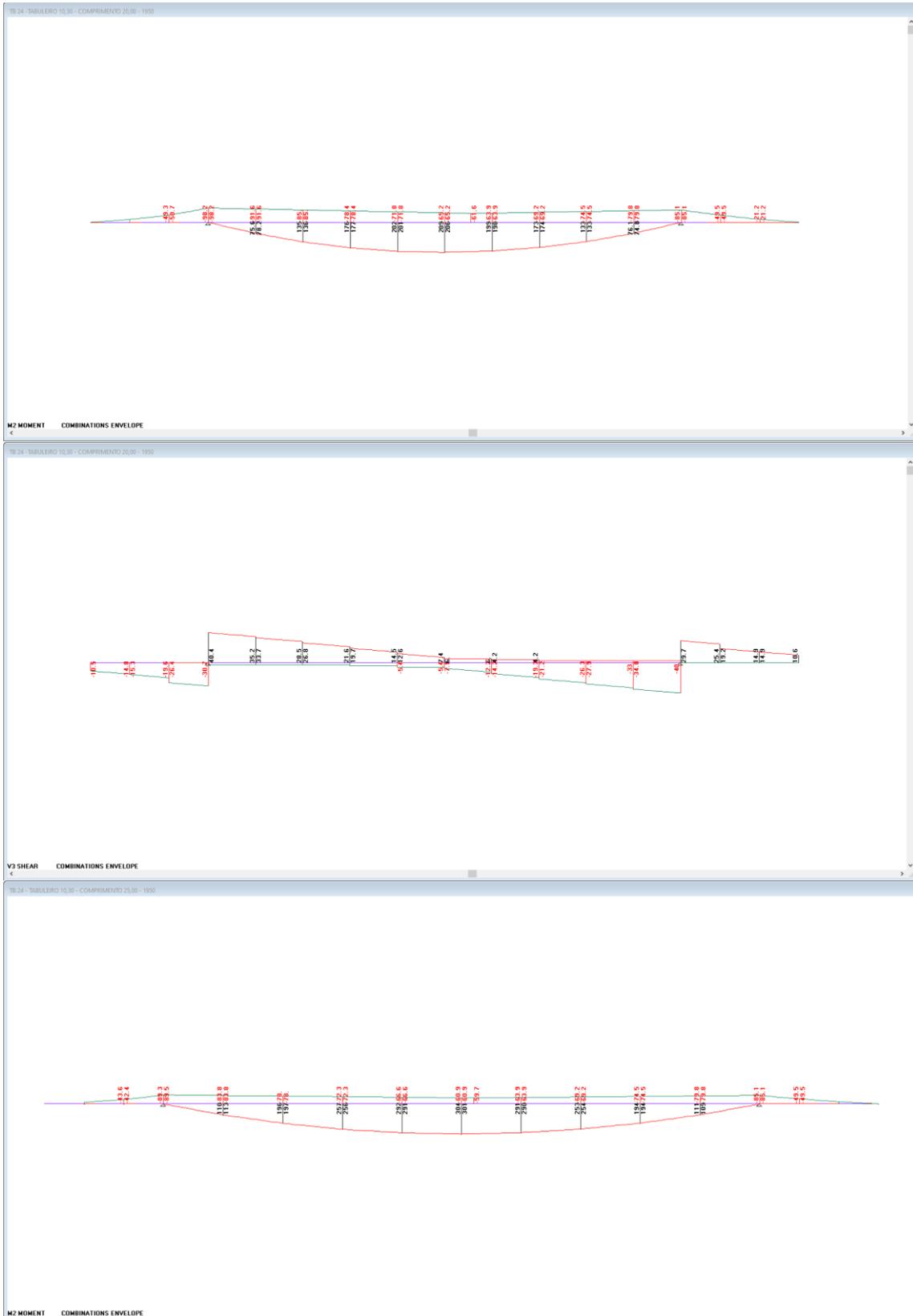
### NOTA TÉCNICA

#### 6.2.3. Tabuleiro 10,30 m



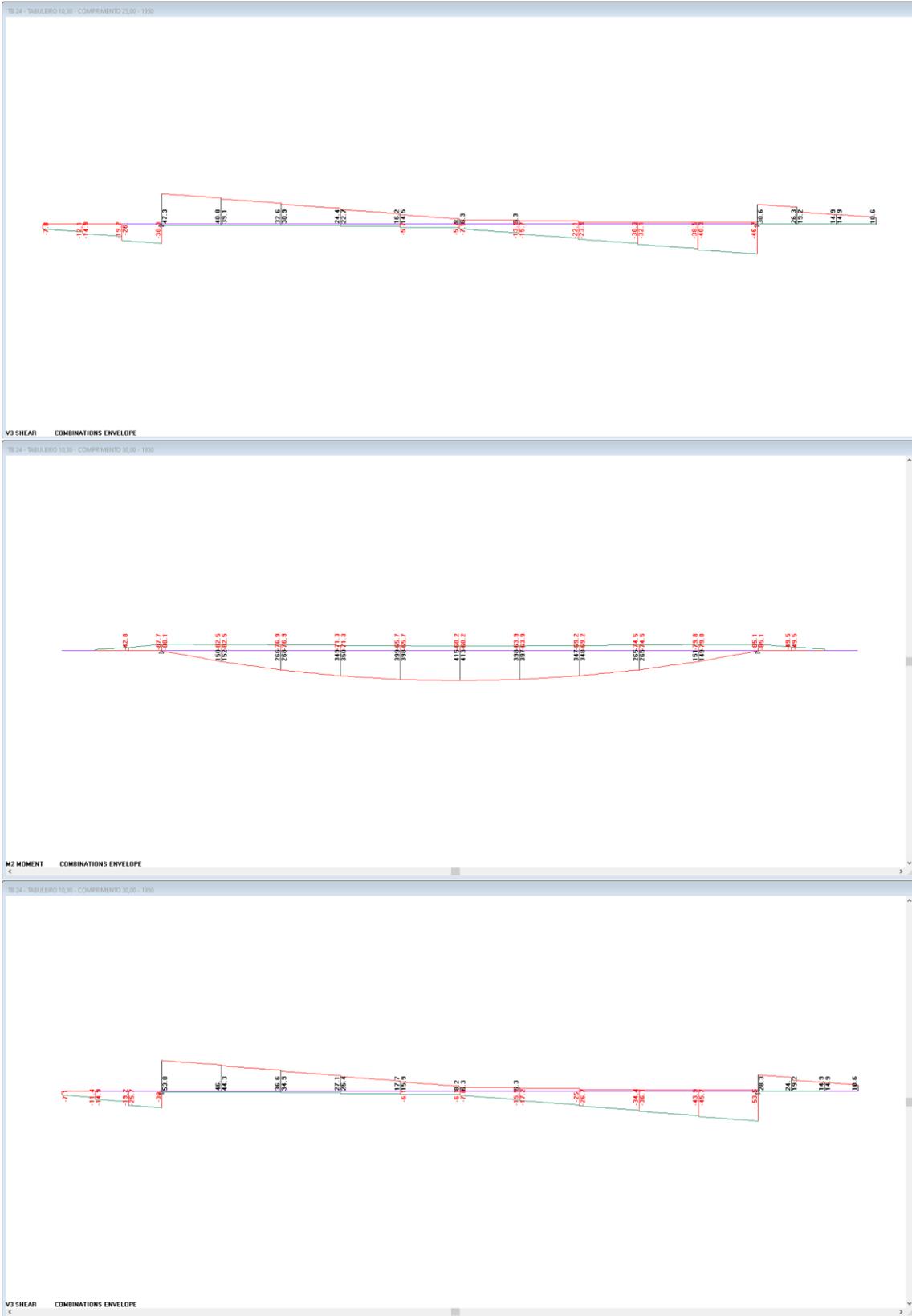


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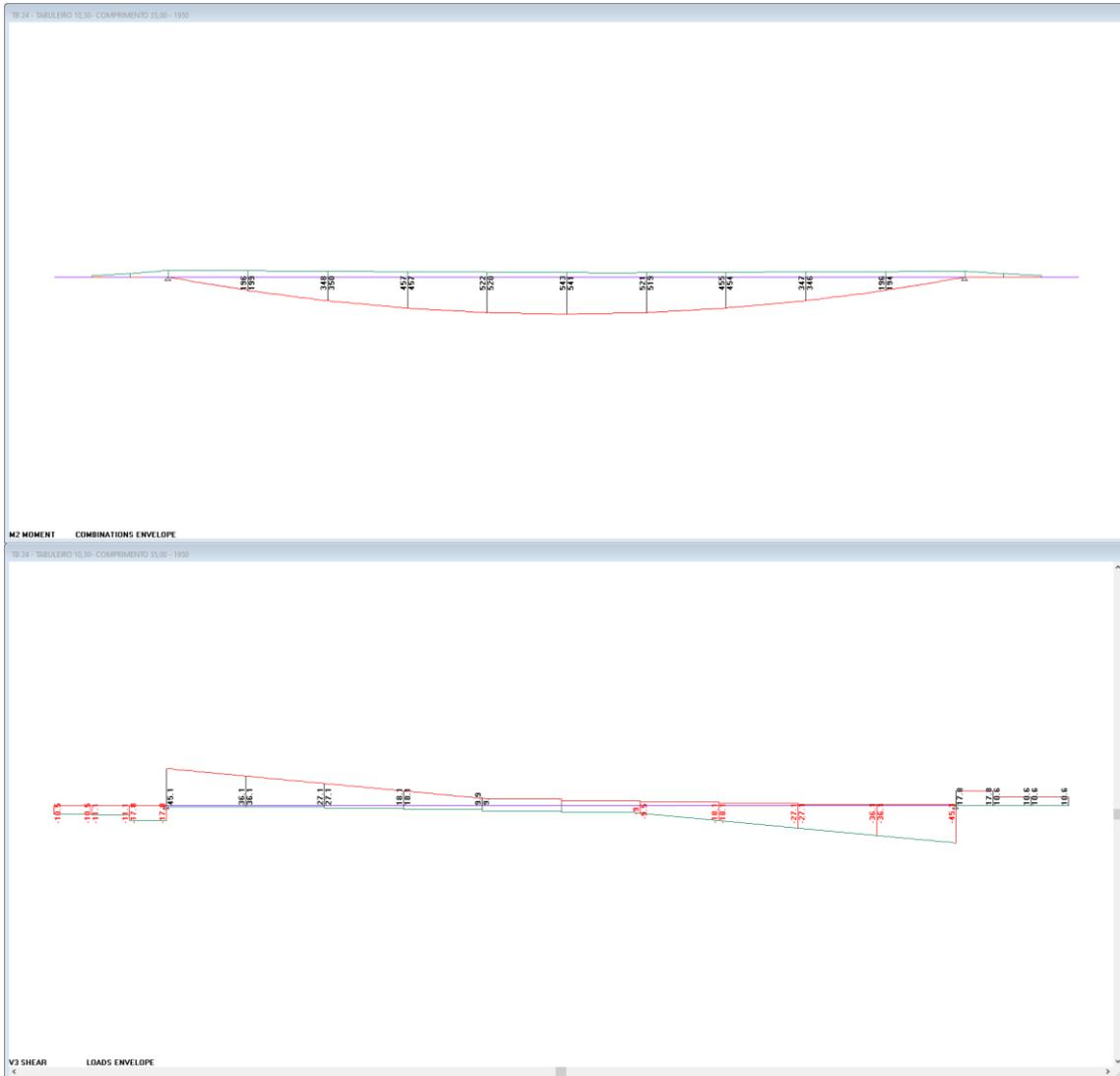
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NOTA TÉCNICA

6.3. Resultados

6.3.1. Cálculo do CS (Coeficiente de Segurança)

CIV DO LIEBHERR	COMPRIMENTO			
	20	25	30	35
P/ VÃO -> $\varphi = 1,00 + 1,06 \times \left(\frac{20}{L + 50}\right)$	1,30	1,28	1,27	1,25
P/ BAL -> $\varphi = 1,00 + 1,06 \times \left(\frac{20}{5 + 50}\right)$	1,39	1,39	1,39	1,39

TB-24

LARGURA	COMPRIMENTO			
	20	25	30	35
8,30 x				
M(+) (tonxm)	195	284	384	499
M(-) (tonxm)	101	101	101	101
Ve (tonxm)	30,8	30,8	30,8	30,8
Vd (tonxm)	38	44	49,4	55,1

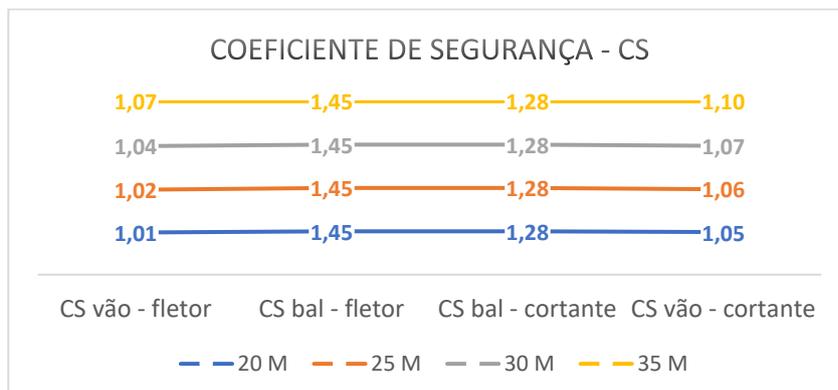
LIEBHERR

LARGURA	COMPRIMENTO			
	20	25	30	35
8,30 x				
M(+) (tonxm)	295	430	578	740
M(-) (tonxm)	100	100	100	100
Ve (tonxm)	34,4	34,4	34,4	34,4
Vd (tonxm)	55,1	64,3	72,3	79,5

$$CS = \frac{1,20 \times 1,40 \times 1,30 \times M_{qTB-24}}{1,10 \times CIV_{vão/bal} \times M_{qLiebherr}}$$

COEFICIENTE DE SEGURANÇA

LARGURA	COMPRIMENTO			
	20	25	30	35
8,30 x				
CS vão - fletor	1,01	1,02	1,04	1,07
CS bal - fletor	1,45	1,45	1,45	1,45
CS bal - cortante	1,28	1,28	1,28	1,28
CS vão - cortante	1,05	1,06	1,07	1,10





### NOTA TÉCNICA

#### TB-24

LARGURA	COMPRIMENTO			
	10,00 x	20	25	30
M(+) (tonxm)	222	319	437	570
M(-) (tonxm)	108	108	108	108
Ve (tonxm)	33,2	33,2	33,2	33,2
Vd (tonxm)	42,8	49,9	56,5	63,3

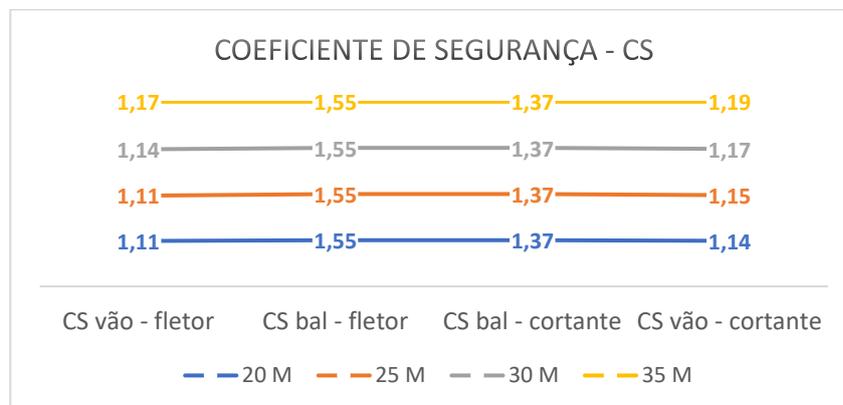
#### LIEBHERR

LARGURA	COMPRIMENTO			
	10,00 x	20	25	30
M(+) (tonxm)	304	445	603	776
M(-) (tonxm)	100	100	100	100
Ve (tonxm)	34,8	34,8	34,8	34,8
Vd (tonxm)	57	67,1	76	84,5

$$CS = \frac{1,68 \times CIV \times M_{qTB-24}}{1,10 \times CIV \times M_{qLiebherr}}$$

#### COEFICIENTE DE SEGURANÇA

LARGURA	COMPRIMENTO			
	10,00 x	20	25	30
CS vão - fletor	1,11	1,11	1,14	1,17
CS bal - fletor	1,55	1,55	1,55	1,55
CS bal - cortante	1,37	1,37	1,37	1,37
CS vão - cortante	1,14	1,15	1,17	1,19





### NOTA TÉCNICA

#### TB-24

LARGURA	COMPRIMENTO			
	10,30 x	20	25	30
M(+) (tonxm)	209	304	415	543
M(-) (tonxm)	98,4	98,4	98,4	98,4
Ve (tonxm)	30,7	30,7	30,7	30,7
Vd (tonxm)	40,4	47,3	53,8	60,4

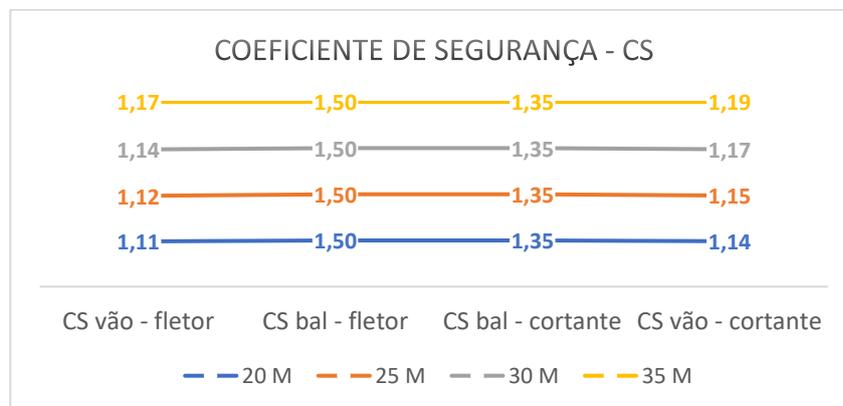
#### LIEBHERR

LARGURA	COMPRIMENTO			
	10,30 x	20	25	30
M(+) (tonxm)	287	421	572	740
M(-) (tonxm)	94,2	94,2	94,2	94,2
Ve (tonxm)	32,7	32,7	32,7	32,7
Vd (tonxm)	54	63,6	72,3	80,4

$$CS = \frac{1,68 \times CIV \times M_{qTB-24}}{1,10 \times CIV \times M_{qLiebherr}}$$

#### COEFICIENTE DE SEGURANÇA

LARGURA	COMPRIMENTO			
	10,30 x	20	25	30
CS vão - fletor	1,11	1,12	1,14	1,17
CS bal - fletor	1,50	1,50	1,50	1,50
CS bal - cortante	1,35	1,35	1,35	1,35
CS vão - cortante	1,14	1,15	1,17	1,19





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### 6.3.2. Considerações para o TB-24 (1950 a 1960)

Os coeficientes de segurança tiveram resultados superiores a 1, portanto a passagem do guindaste de 8 eixos e 96 toneladas está liberada.



## NOTA TÉCNICA

### 7. CONCLUSÃO E CRITÉRIOS

Fica liberada a passagem de guindastes de 7 e 8 eixos para obras verificadas a partir do veículo padrão **TB-24**, desde que pertençam à Classe I (pontes situadas em estradas tronco federais e estaduais ou nas estradas de ligação principais entre esses troncos) e tenham um tabuleiro de no mínimo 8,30 x 20,00 metros. Para essa condição de tabuleiros o tamanho mínimo do guindaste é de 3,00 metros de largura por 19,00 metros de comprimento. Guindastes com dimensões menores podem passar desde que a capacidade não seja maior do que 96 t.

Para obras verificadas a partir do veículo padrão **TB-36**, pode-se adotar o mesmo critério de comprimento e largura da ponte.

Para ambos (**TB-36 e TB-24**) a passagem dos guindastes supra, deve seguir os mesmos critérios, conforme segue abaixo:

- Realizar vistorias anuais em todas as obras do roteiro com relatório conclusivo da data de construção da obra, largura e comprimento dos tabuleiros e estado geral da OAE, que deve estar classificada com, no mínimo, a nota 3 no requisito durabilidade e estrutural da NBR 9452:2023 – Inspeção de pontes, viadutos e passarelas – Procedimento.

CLASSIFICAÇÃO (NOTA)	CONDIÇÃO	ESTRUTURAL	FUNCIONAL	DURABILIDADE
5	Excelente	A estrutura se encontra em condições satisfatórias, apresentando defeitos irrelevantes e isolados	A OAE apresenta segurança e conforto aos usuários	A OAE se encontra em condições satisfatórias, apresentando defeitos irrelevantes e isolados
4	Boa	A estrutura apresenta danos de baixa gravidade, localizados e em pequenas áreas, sem comprometer a segurança estrutural	A OAE apresenta pequenos danos que não chegam a causar desconforto ou insegurança ao usuário	A OAE apresenta pequenas e poucas anomalias, que não comprometem sua vida útil, em região de baixa agressividade ambiental
3	Regular	Há danos que pode vir a gerar alguma deficiência estrutural, mas não há sinais de comprometimento da estabilidade da obra. Recomenda-se acompanhamento dos problemas	A OAE apresenta desconforto ao usuário, com defeitos que requerem ações	A OAE apresenta anomalias de moderada gravidade, que comprometem sua vida útil, em região de moderada a alta agressividade ambiental A OAE apresenta de moderada a muitas anomalias, que comprometem sua vida útil, em região de baixa agressividade ambiental



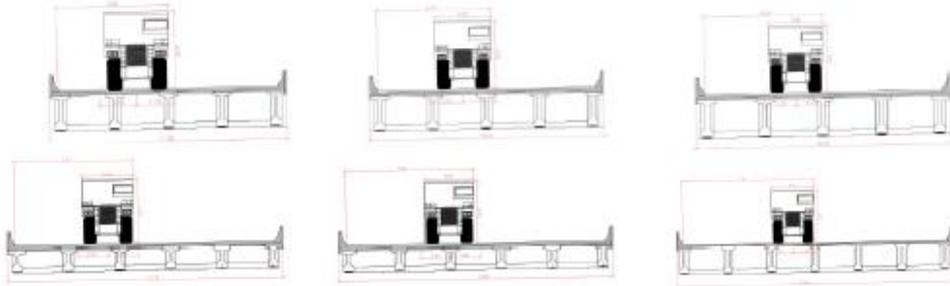
## NOTA TÉCNICA

CLASSIFICAÇÃO (NOTA)	CONDIÇÃO	ESTRUTURAL	FUNCIONAL	DURABILIDADE
2	Ruim	Há danos comprometendo a segurança estrutural da OAE sem aparente risco iminente de colapso. Sua evolução pode levar ao colapso estrutural. A OAE necessita de intervenções significativas	A OAE possui funcionalidade visivelmente comprometida, com riscos de segurança ao usuário	A OAE apresenta de moderadas a muitas anomalias, que comprometem sua vida útil, em região de alta agressividade ambiental A OAE apresenta muitas anomalias, que comprometem sua vida útil, em região de baixa agressividade ambiental
1	Crítica	Há danos gerando grave insuficiência estrutural na OAE. Há elementos estruturais em estado crítico, com risco tangível de colapso estrutural localizado. A OAE necessita de intervenção imediata, podendo ser necessária restrição de carga, interdição parcial, escoramento provisório, instrumentação, associada ou não	A OAE apresenta condições funcionais limitadas de utilização	A OAE se encontra em elevado grau de deterioração, em regiões localizada, apontando problema já de risco estrutural e/ou funcional, requerendo intervenção imediata, podendo ser necessárias restrição de carga e interdição parcial ao tráfego
0	Emergencial	Há elementos estruturais principais colapsados, evoluindo para instabilidade da estrutura. É necessária a interdição total, até que haja avaliação e reclassificação por consultoria especializada ou intervenção	A OAE não apresenta condições funcionais de utilização. A OAE deve ser interdita	A OAE se encontra em elevado grau de deterioração, gerando grave insuficiência estrutural e/ou funcional, requerendo intervenção emergencial e interdição total

- **Velocidade constante do guindaste:** Isto irá evitar forças dinâmicas causadas por acelerações ou frenagens repentinas que maximizam os esforços nas estruturas de suporte do tabuleiro.
- **Evitar comboio com CVC (Combinação de Veículos de Carga):** Isso é importante para evitar a sobrecarga estrutural devido à presença simultânea de múltiplas cargas pesadas. Esperar até que o CVC saia antes de o guindaste entrar na OAE assegura que a carga sobre o tabuleiro seja conforme a viabilização, sem exceder os limites de esforços previstos.
- **Navegação deverá ser na pista adjacente ao eixo do lado carroçável:** Seguir estritamente o caminho para o qual os cálculos foram realizados é fundamental para garantir que a distribuição de carga no tabuleiro corresponda exatamente ao esperado. Desvios do trajeto calculado podem resultar em riscos à estrutura, situações que não foram consideradas nos cálculos.



## NOTA TÉCNICA



- **Respeitar o afastamento necessário:** Manter um espaço claro de 0,40 m nas laterais e 0,50 m na frente e atrás do guindaste, não só ajuda a evitar colisões, mas também garante que o guindaste tenha espaço suficiente para operações seguras e eficazes, permitindo manobras em caso de emergência.
- **Operador de guindaste credenciado e instruído:** A operação de guindastes por motoristas treinados e certificados é vital. A adesão às normas de segurança e às melhores práticas operacionais por parte de operadores qualificados reduz significativamente o risco de acidentes. O operador do guindaste deverá seguir as recomendações de operação, integralmente.

Dessa forma, considera-se segura a passagem dos guindastes, desde que atendidas as condições aqui estabelecidas. Ressalta-se que o estudo foi desenvolvido com base em um guindaste de 8 eixos, com carga total de 96 tf (12 tf por eixo), estendendo-se, por compatibilidade de carregamento, à operação de guindastes de 7 eixos (84 tf), desde que igualmente respeitados os limites de carga por eixo e condições operacionais previstas.



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## NOTA TÉCNICA

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### 8. REFERÊNCIA BIBLIOGRÁFICA

ASSOCIAÇÃO BRASILEIRA DE NORMAS TÉCNICAS. NBR 6118: Projetos de estruturas de concreto: procedimento. Rio de Janeiro: ABNT, 2003.

ASSOCIAÇÃO BRASILEIRA DE NORMAS TÉCNICAS. NBR 9452: Inspeção de pontes, viadutos e passarelas - Procedimento. Rio de Janeiro: ABNT, 2023.

PFEIL, Walter. Manual de inspeção de pontes rodoviárias. Rio de Janeiro, 1980.

SANTOS, Marcelo. Contribuição ao estudo de combinação de veículos de carga sobre pontes rodoviárias de concreto. São Carlos.

STUCCHI, Fernando. FANTI, Fabio. CARANDINA, Juliana. BLANCAS, Francisco. Safety of Existing Bridges. São Paulo. CRC Press, 2016. Digital Library USP. 2003.

TIMERMAN, Júlio. Beier, Martin. Considerações sobre a revisão da ABNT NBR 7188. São Paulo. ABECE. 2012.